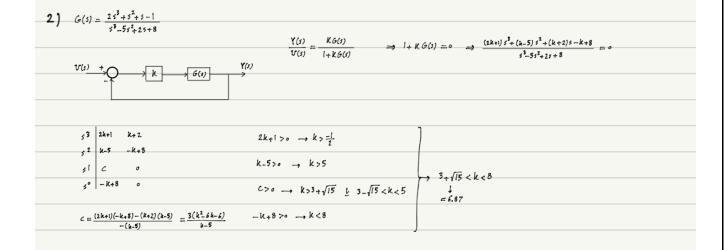
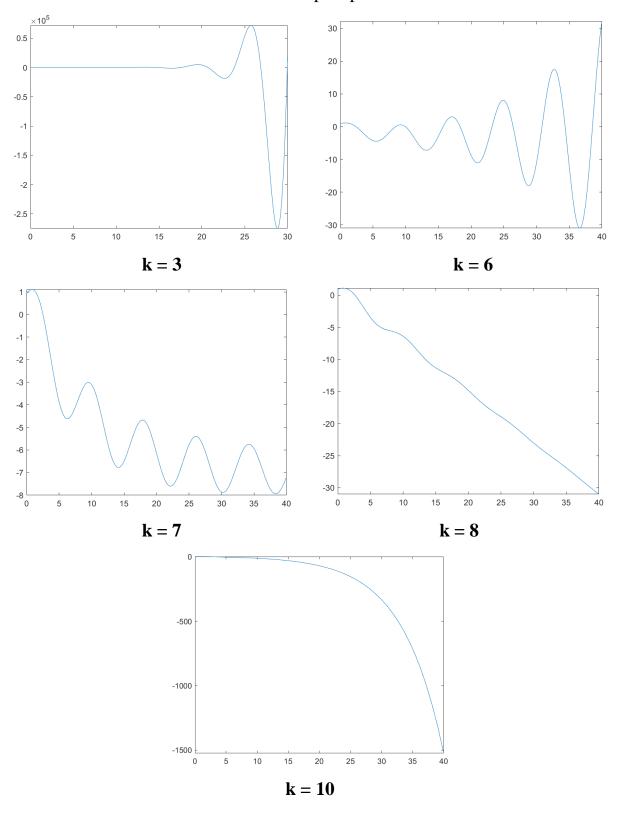
$\frac{2 \cdot G_2(s)}{s^{4+3}s^{3}+3s^{2}+9s+1}$	$3. G_3(s) = \frac{4}{s^{4} + 4s^3 + 3s^2 - 4s - 4}$
.4 3	54 1 3 -4
3 3 9 0 C= 96-3	c3 4 -4 a
52 € 1 °	52 4 -4 0
31 C 0 0 E + 0 +	52 4 -4 ° 51 \$1 \$1 \$1 \$1 \$1 \$1 \$1 \$1 \$1 \$1 \$1 \$1 \$1
50 1 0 0	5° -4 ° ° JA(t) = 85
unstable (two unstable poles)	unstable (one unstable pole)
777420	
s ⁶ 1 20 25 2	
5 ⁵ 7 30 [l o	
52 15.3 2 0 0	
5° 2 0 0	
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$



2 Range of a Gain for Closed-Loop Stability

For different values of k we have these step responces:



3- a) $y(t) = \int_{-\infty}^{t} u(t-\tau) h(\tau) d\tau$

 $\frac{t = \tau_{5} \Rightarrow}{\|y\|_{\infty}} = y(\tau_{5}) = \int_{0}^{\tau_{5}} u(\tau_{5} - \tau) h(\tau) d\tau \leq \int_{0}^{\tau_{5}} |u(\tau_{5} - \tau)| |h(\tau)| d\tau \leq \int_{0}^{\infty} |u(\tau_{5} - \tau)| |h(\tau)| d\tau \leq \int_{0}^{\infty} ||u||_{\infty} |h(\tau)| d\tau \leq ||u||_{\infty} \int_{0}^{\infty} |h(\tau)| d\tau$

b) u = a sgn(h(t)) u(t) (a>0)

 $\Rightarrow ||y||_{\infty} = ||x||_{\infty} \int_{0}^{\infty} |h(\tau)| d\tau \qquad \Rightarrow ||S|| = \int_{0}^{\infty} |h(\tau)| d\tau$

c) 1) $S_1: G_1(s) = \frac{1}{s+1}$ $\stackrel{f^{-1}}{\longrightarrow}$, e^{-t} $\stackrel{f}{\longrightarrow}$ $||s|| = \int_0^\infty |e^{-t}| d\tau = \int_0^\infty e^{-t} d\tau = -e^{-t} \Big|_0^\infty = 1$ $\stackrel{f}{\longrightarrow}$ stable

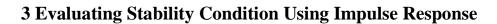
2) $\leq_2 : G_2(s) = \frac{1}{s-1}$ $\xrightarrow{\phi^{-1}} e^t$ $\xrightarrow{\phi} \|s\| = \int_0^\infty |e^\tau| d\tau = \int_0^\infty e^\tau d\tau = e^\tau \Big|_0^\infty = \infty$ $\xrightarrow{}$ unstable

 $3) \leq_{5}: G_{3}(5) = \frac{1}{5^{2}+1} \xrightarrow{f^{-1}} 5in(t) \xrightarrow{} \left\| 5 \right\| = \int_{0}^{\infty} \left| 5in(\tau) \right| d\tau = \frac{5in(\tau)}{\left| 5in(\tau) \right|} \int_{0}^{\infty} 5in(\tau) d\tau = \frac{-6s(\tau)}{\left| 5in(\tau) \right|} \int_{0}^{\infty} = \frac{\rho}{1} \xrightarrow{} unstable$

4) $S_4: G_4(s) = \frac{1}{(s+1)^2}$ te^{-t} te^{-t} t

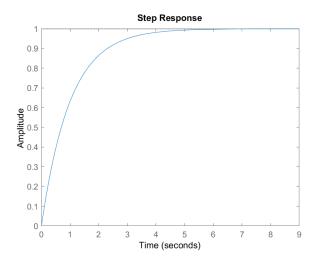
 $= -e^{-\tau}|\tau| \int_{0}^{\infty} -\frac{\tau e^{-\tau}}{|\tau|} \Big|_{0}^{\infty} = \frac{-(\tau^{2} + \tau)e^{-\tau}}{|\tau|} \Big|_{0}^{\infty} = 1 \longrightarrow stable$

6) $S_6: h_6(t) = \frac{1}{t^2+1}$ $\longrightarrow ||S|| = \int_0^\infty \left|\frac{1}{\tau^2+1}\right| d\tau = \int_0^\infty \frac{1}{\tau^2+1} d\tau = \arctan(\tau) \Big|_0^\infty = \frac{\pi \tau}{2}$ $\longrightarrow Stable$

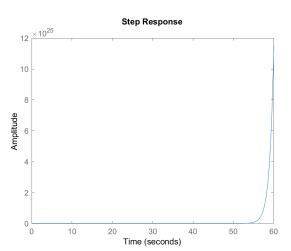




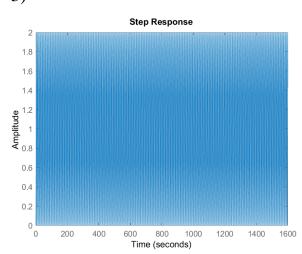
1)



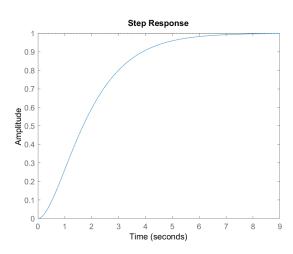
2)



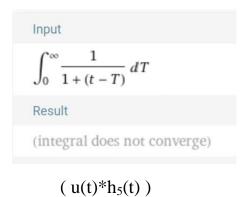
3)



4)



5)



6)

Definite integral

$$\int_0^\infty \frac{1}{1 + (t - T)^2} \ dT = \tan^{-1}(t) + \frac{\pi}{2}$$

$$(u(t)*h_6(t))$$

(4) a)
$$\frac{1}{\sqrt{1-z^2}} e^{-\overline{L} \omega_n t} < 0.02 \implies T_s = \frac{\ln(0.02\sqrt{1-z^2})}{-\overline{L} \omega_n} \Rightarrow T_s = \frac{4}{L\omega_n}$$

$$\mathcal{Z} = 1 \implies \Upsilon(s) = \frac{\omega_n^2}{s(s^2 + 2\omega_n s + \omega_n^2)} = \frac{\omega_n^2}{s(s + \omega_n)^2} = \frac{1}{s} - \frac{1}{s + \omega_n} - \frac{\omega_n}{(s + \omega_n)^2} \longrightarrow \Re(s) = 1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t}$$

$$\Rightarrow e^{-w_n t} + w_n t e^{-w_n t} < 0.02 \Rightarrow [w(1 + w_n T_s) - w_n T_s = 4 \Rightarrow w_n T_s = 6 \Rightarrow T_s = \frac{6}{w_n}$$

b)
$$M_p = \max(y(t)) - 1 = e^{\frac{-2\pi}{\sqrt{t-2}}}$$

$$Y(s) = \frac{w_{N}^{2}}{s(s^{2} + 2w_{N}s + w_{n}^{2})} \implies sY(s) = \frac{w_{N}^{2}}{s^{2} + 2w_{N}s + w_{n}^{2}}$$

$$\Rightarrow \dot{j}(t) = \int_{-t}^{t} \left\{ s \gamma(t) \right\} = \frac{\omega_n}{\sqrt{t - t^2}} e^{\frac{t}{2} \omega_n t} \sin \left(\omega_n \sqrt{t - t^2} \right) = 0 \Rightarrow t = \frac{n\pi}{\omega_n \sqrt{t - t^2}} \Rightarrow T_p = \frac{\pi}{\omega_n \sqrt{t - t^2}}$$

$$\frac{1}{\sqrt{1-\xi^2}} = e^{\frac{-\xi \pi}{\sqrt{1-\xi^2}}} \sin(\pi + \xi_1^{-1}\xi) \qquad \Rightarrow \max_{x \in \mathbb{R}} (g(x)) = 1 + e^{\frac{-\xi \pi}{\sqrt{1-\xi^2}}} \implies M_y \in e^{\frac{-\xi \pi}{\sqrt{1-\xi^2}}}$$

$$\frac{1}{\sqrt{1-\xi^2}} \xrightarrow{f} \lim_{x \to \infty} (\pi + \xi_1^{-1}\xi) \longrightarrow -1$$

for not having overshoot the poles must be real-valued

For Fastest response we should make dominant pole as fast as possible

so we want two real-valued poles at the same location \Rightarrow Z=1 \rightarrow S_{1,2} = -W_N

$$Z = I$$
 \rightarrow $G(s) = \frac{w_{n}^{2}}{(s + w_{n}^{2})}$

MATLAB Assignments

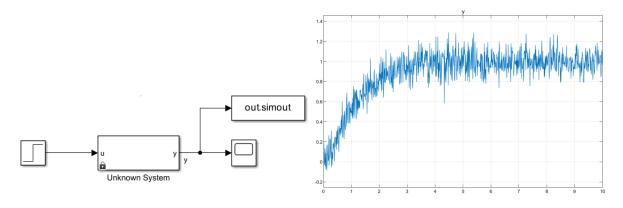
5 Curve Fitting Toolbox

a)

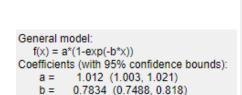
$$G(s) = \frac{K}{\tau s + 1}$$

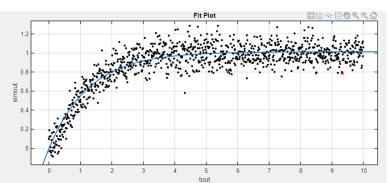
$$U(s) = \frac{1}{s}$$

b)



c)





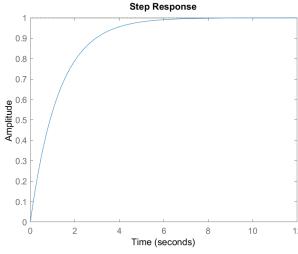
From data we have:

$$f(x) = a (1-e^{-bx}) = 1.012 (1-e^{-0.7834x}) \approx 1 (1-e^{-0.78x})$$

compare to result in part a:

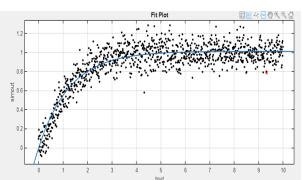
$$K = 1$$
 , $\tau = \frac{1}{0.78} = 1.28$

d)



```
%% 5_d

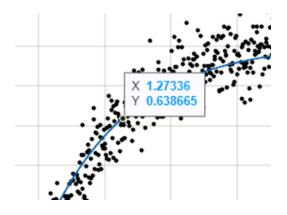
K2 = 1;
T2 = 1.28;
step( tf([K2],[T2,1]) )
```



As we see the result of step response for our system is similar to the output from the unknown system.

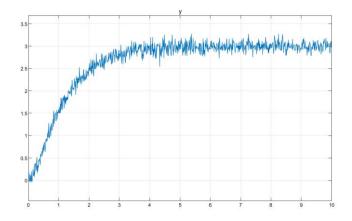
e) For the DC gain we should consider the value of response as the time goes to infinity. We can say that DC gain could be a little more than one (because of a). so 1 is a proper estimation for K (DC gain)

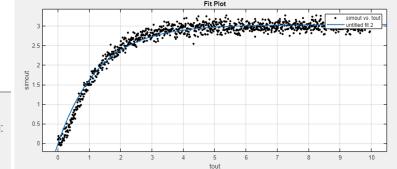
We know: $1-e^{-1} = 0.632$, so the time constant could be estimated to be the time when the curve reaches to 63.2% of its maximum value.



As we see the value of time constant that we've estimated (1.28) could be a proper value for it.

f) We set the input amplitude on 3.



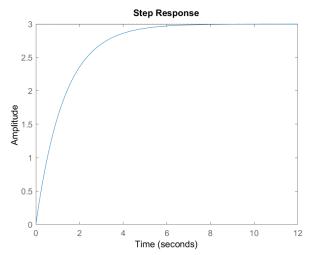


General model: f(x) = a*(1-exp(-b*x))Coefficients (with 95% confidence bounds): a = 3.034 (3.023, 3.044)b = 0.769 (0.7552, 0.7827)

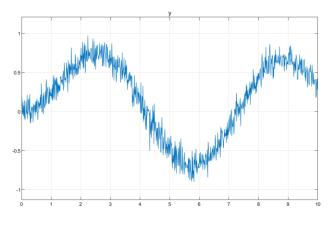
$$f(x) = a \; (1 \text{--} e^{bx} \;) = 3.034 \; (1 \text{--} e^{-0.769x} \;) \approx 3 \; (1 \text{--} e^{-0.77x})$$

compare to results in part a:

$$K = 3$$
 , $\tau = \frac{1}{0.77} = 1.3$

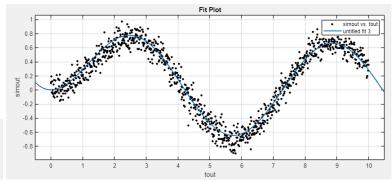


As we see the result of step response for our system is similar to the output from the unknown system. g) input : sin(t)



val =

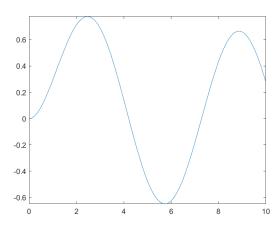
L{ $\sin(t)$ } = $\frac{1}{s^2+1}$ => response:



General model: f(x) = (K*sin(x)-K*T*cos(x)+K*T*exp(-x/T))/(T^2+1) Coefficients (with 95% confidence bounds):

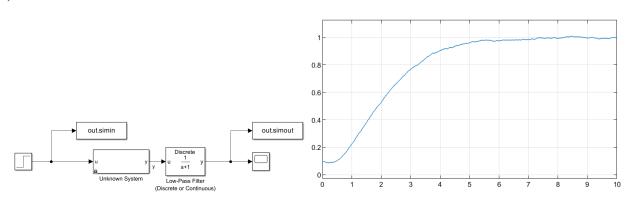
K = 1.238 (1.21, 1.266) T = 1.582 (1.535, 1.63)

 $f(x) = \frac{1}{T^2 + 1} (K \sin(t) - KT \cos(t) + KT e^{-\frac{t}{T}})$ $= \frac{1}{(1.582)^2 + 1} (1.238 \sin(t) - 1.238 \times 1.582 \cos(t) + 1.238 \times 1.582 e^{-\frac{t}{1.582}})$ $\approx 0.35 \sin(t) - 0.56 \cos(x) + 0.56 e^{-0.63x} \qquad (K = 1.24, T = 1.58)$



As we see the result of step response for our system is similar to the output from the unknown system. h) Increasing data length means to have more data to calculate the proper equation for the output curve. This also helps us to understand the steady state behavior of the response better. So we can say that increasing data length will increase the accuracy of estimating output equation and coefficients.

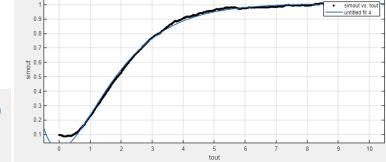
i)



Time constant:
$$a = 1 \implies f_C = \frac{1}{2\pi a} = 0.16 \ Hz$$

$$G(s)F(s) = \frac{k}{\tau s + 1} \frac{1}{as + 1}$$

=> step response:



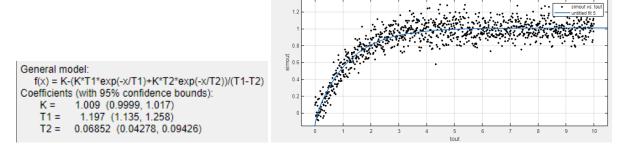
General model: f(x) = K+(-K*T*exp(-x/T)+K*exp(-x))/(T-1)Coefficients (with 95% confidence bounds): K = 1.006 (1.004, 1.008)T = 1.186 (1.174, 1.198)

$$K \approx 1$$
 , $\tau \approx 1.18$ => $G(s) = \frac{1}{1.18s+1}$

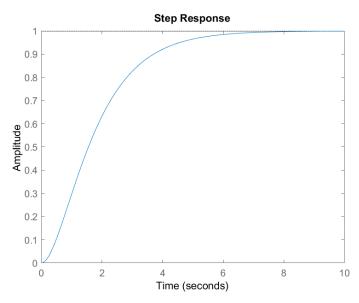
j)

Answers from different inputs have near values for K and τ . Although the values we got from sinusoidal input were a little different from the others.

```
k)
```

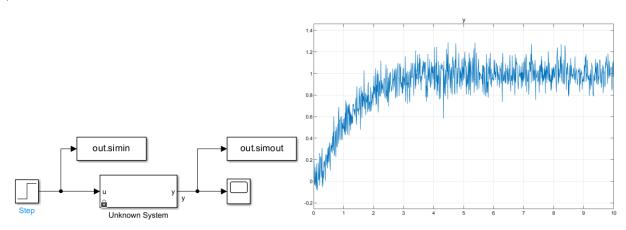


 $K\approx 1$, $\tau_1\approx 1.2$, $\tau_2\approx 0.68$



6 System Identification Toolbox

a)



b)

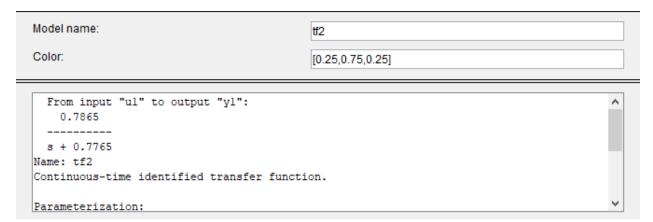
Result from System Identification toolbox :

Model name: Color:	tf1 [0.25,0.75,0.25]	
From input "ul" to output "yl 0.8007	";	^
s + 0.7898 Name: tfl		
Continuous-time identified tran Parameterization:	sfer function.	

u(t)

K = 0.8007 a = 0.7898

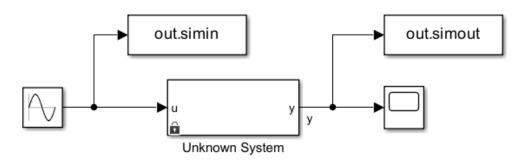
c)



3u(t)

$$K = 0.7865$$
 $a = 0.7765$

d)

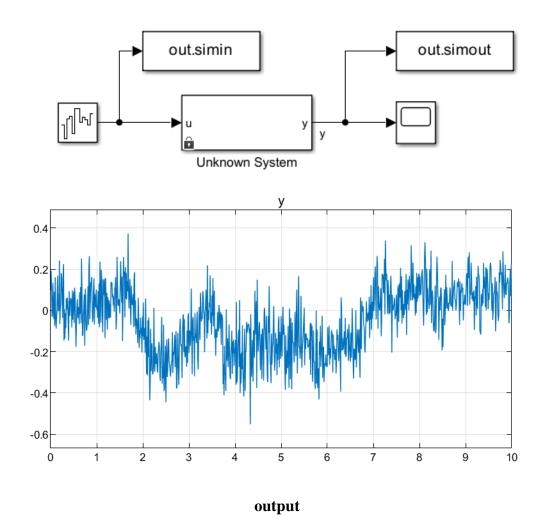


Model name: Color:	tf3 [0.25,0.75,0.25]
From input "ul" to output "yl": 0.7859	^
s + 0.6404 Name: tf3 Continuous-time identified transfer fu Parameterization:	nction.

Sin(t)

$$K = 0.7859$$
 $a = 0.6404$

e)

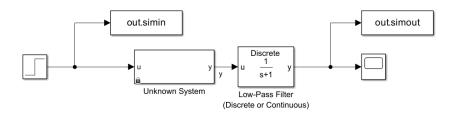


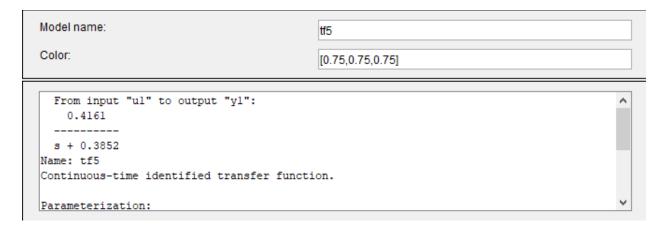
Model name:	tf4	
Color:	[0.75,0.75,0.2]	
From input "ul" to output "yl": 0.7051		^
s + 0.8805		
Name: tf4 Continuous-time identified transfer	r function.	
Parameterization:		~

White noise

$$K = 0.7051$$
 $a = 0.8805$







u(t) with low-pass filter

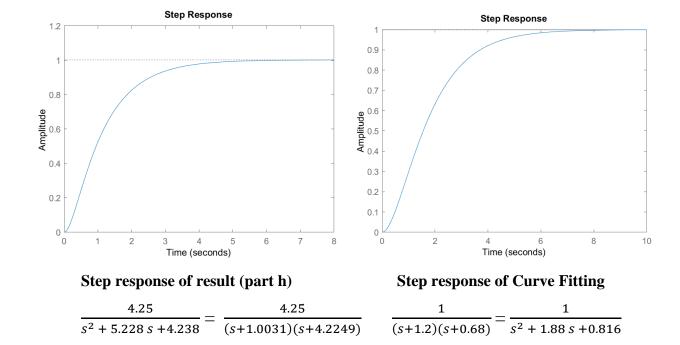
$$K = 0.4161$$
 $a = 0.3852$

g)

Answers from different inputs have near values for K and a. Although the values we got from white noise and sinusoidal input and filtered system were a little different from the others.

h) Result from System Identification toolbox:

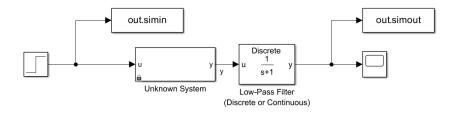
Model name: Color:	[0,0,1]	
From input "ul" to output "y	1":	^
s^2 + 5.228 s + 4.238 Name: tf6 Continuous-time identified transfer function.		
Parameterization:		v



Result from Curve Fitting toolbox is similar to our system and had better

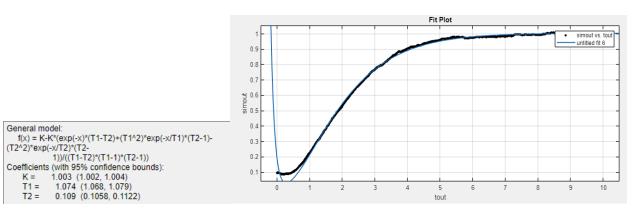
performance compare to System Identification toolbox.

*) suggested method:



Step response:

```
val =
K - (K*a^2*exp(-t/a))/((T1 - a)*(T2 - a)) - (K*T1^2*exp(-t/T1))/((T1 - T2)*(T1 - a)) + (K*T2^2*exp(-t/T2))/((T1 - T2)*(T2 - a))
=
K - (K*exp(-t))/((T1 - 1)*(T2 - 1)) - (K*T1^2*exp(-t/T1))/((T1 - T2)*(T1 - 1)) + (K*T2^2*exp(-t/T2))/((T1 - T2)*(T2 - 1))
```



 $K\approx 1$, $\tau_1\approx 1.07$, $\tau_2\approx 0.11$