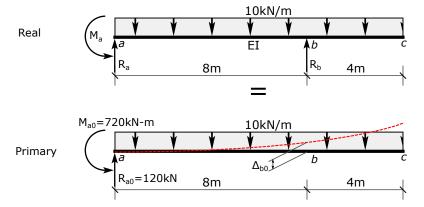
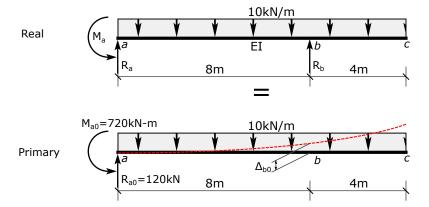


Because the displacement at b in the real structure is 0, it is not quite so tricky to get the signs right. $\Delta_b = 0$ is on one side of the compatibility equation, and it doesn't matter if it is +0 or -0. If support b settled or was elastic, more care would be required.



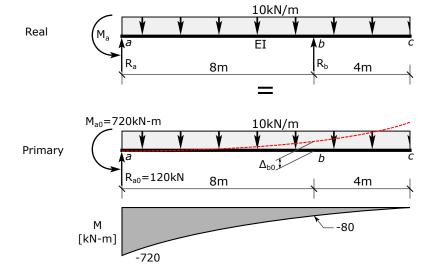
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This sketch does not establish a sign convention for displacements. The direction of the unit virtual load does that.

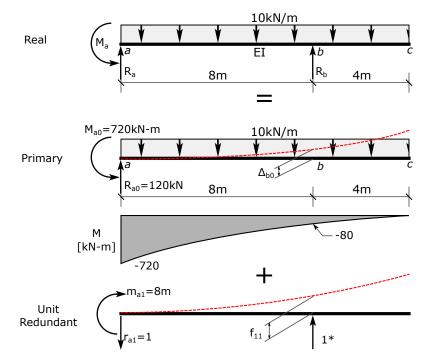
We have sketched the displacement to be consistent with the sign we establish below, even though we suspect displacement will be downward. Δ_{b0} will come out with the proper sign.



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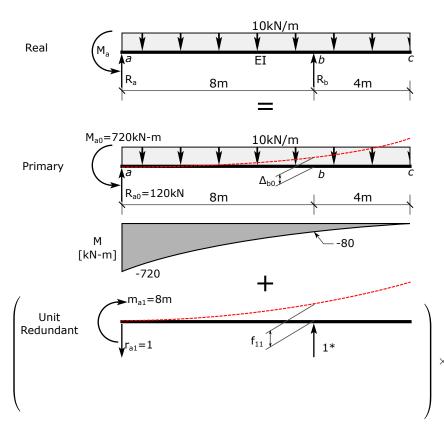


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For convenience, the unit load is chosen in the same direction we assumed for R_b . This establishes **upward** displacements as being positive.



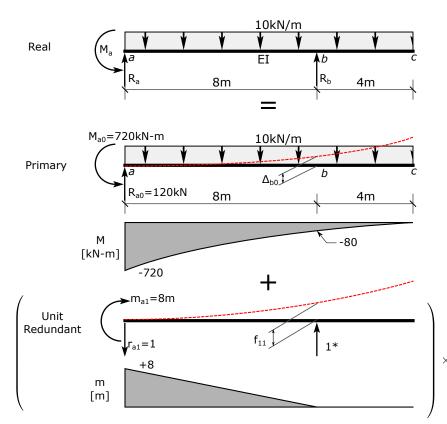
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 $\times R_b$



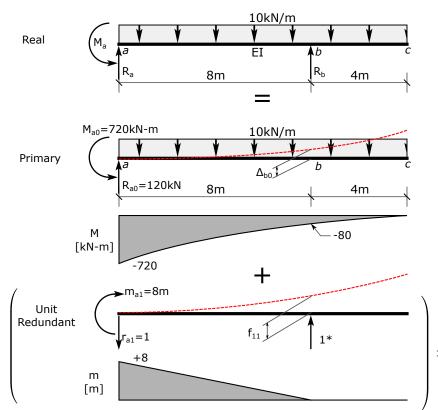
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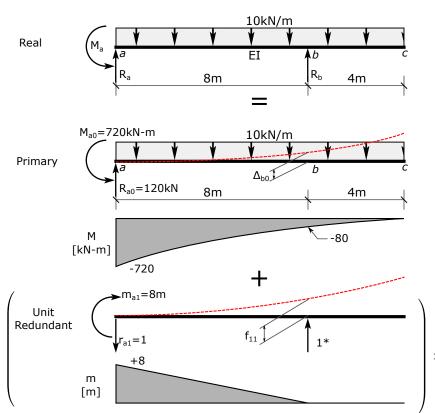
Displacements in the primary structure:

$$\Delta_{b0} = \int \frac{mM}{EI} = \frac{1}{EI} \int_{-720 \text{kN-m}}^{8\text{m}} \frac{}_{-720 \text{kN-m}}$$

$$= \frac{1}{EI} \left[\frac{8}{24} \left[8 \times (10 \times 8^2 + 8 \times -720 + 4 \times -80) \right] \text{kN m}^3 \right]$$

$$= \frac{-14507 \text{kN m}^3}{EI} \quad (:.\downarrow)$$

This integral is not in the main part of the table, so we must use the most general case with $m_0 = 8$, $m_1 = 0$, $M_0 = -720$, $M_1 = -80$ and w = 10.



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Displacements in the primary structure:

$$\Delta_{b0} = \int \frac{mM}{EI} = \frac{1}{EI} \int_{-720 \text{kN-m}}^{8\text{m}} \frac{\text{-80kN-m}}{\text{-720kN-m}}$$

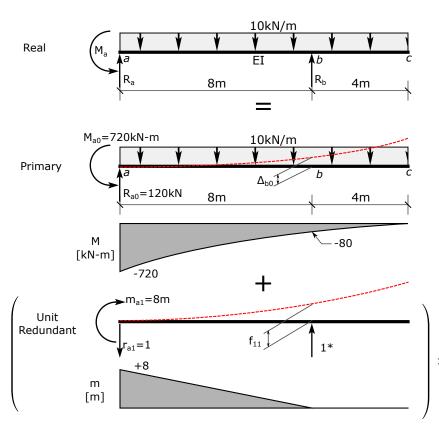
$$= \frac{1}{EI} \left[\frac{8}{24} \left[8 \times (10 \times 8^2 + 8 \times -720 + 4 \times -80) \right] \text{kN m}^3 \right]$$

$$= \frac{-14507 \text{kN m}^3}{EI} \quad (:.\downarrow)$$

Flexibility coefficients (displacements due to unit redundants):

$$f_{11} = \int \frac{mm}{EI} = \frac{1}{EI} \int_{8m}^{8m} \frac{8m}{8m}$$
$$= \frac{1}{EI} \frac{8 \text{ m}}{3} \times 8 \text{ m} \times 8 \text{ m}$$
$$= \frac{512 \text{ m}^3}{3EI} \quad (::\uparrow)$$

This integral is not in the main part of the table, so we must use the most general case with $m_0 = 8$, $m_1 = 0$, $M_0 = -720$, $M_1 = -80$ and w = 10.



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 $\times R_b$

Displacements in the primary structure:

$$\Delta_{b0} = \int \frac{mM}{EI} = \frac{1}{EI} \int_{-720 \text{kN-m}}^{8 \text{m}} \frac{1}{-720 \text{kN-m}} = \frac{1}{EI} \left[\frac{8}{24} \left[8 \times (10 \times 8^2 + 8 \times -720 + 4 \times -80) \right] \text{kN m}^3 \right] = \frac{-14507 \text{kN m}^3}{EI} \quad (:\downarrow)$$

Flexibility coefficients (displacements due to unit redundants):

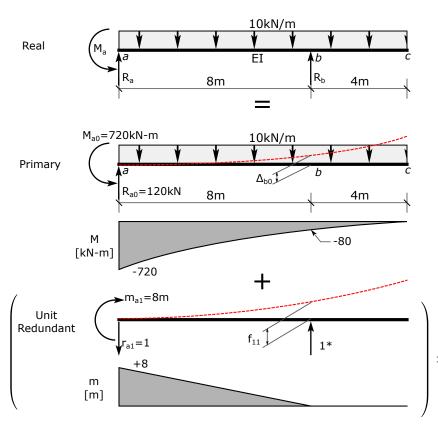
$$f_{11} = \int \frac{mm}{EI} = \frac{1}{EI} \int_{8m}^{8m} \frac{8m}{8m}$$
$$= \frac{1}{EI} \frac{8m}{3} \times 8m \times 8m$$
$$= \frac{512m^3}{3EI} \quad (::\uparrow)$$

Compatibility Equation (wrt displacement at b):

$$\Delta_b = \Delta_{b0} + R_b f_{11} = 0$$
$$\frac{-14507 \,\text{kN m}^3}{EI} + R_b \times \frac{512 \,m^3}{3EI} = 0$$

This integral is not in the main part of the table, so we must use the most general case with $m_0 = 8$, $m_1 = 0$, $M_0 = -720$, $M_1 = -80$ and w = 10.

The sign convention for displacements is +ive upwards.



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For convenience, the unit load is chosen in the same direction we assumed for R_b . This establishes **upward** displacements as being positive.

 $\times R_b$

Displacements in the primary structure:

$$\begin{split} \Delta_{b0} &= \int \frac{mM}{EI} = \frac{1}{EI} \int^{8\text{m}}_{8\text{m}} -80\text{kN-m} \\ &= \frac{1}{EI} \left[\frac{8}{24} \left[8 \times (10 \times 8^2 + 8 \times -720 + 4 \times -80) \right] \text{kN m}^3 \right] \\ &= \frac{-14507 \text{kN m}^3}{EI} \quad (:.\downarrow) \end{split}$$

Flexibility coefficients (displacements due to unit redundants):

$$f_{11} = \int \frac{mm}{EI} = \frac{1}{EI} \int_{8m}^{8m} \frac{8m}{8m}$$

$$= \frac{1}{EI} \frac{8 \,\mathrm{m}}{3} \times 8 \,\mathrm{m} \times 8 \,\mathrm{m}$$

$$= \frac{512 \,\mathrm{m}^3}{3EI} \quad (::\uparrow)$$

Compatibility Equation (wrt displacement at b):

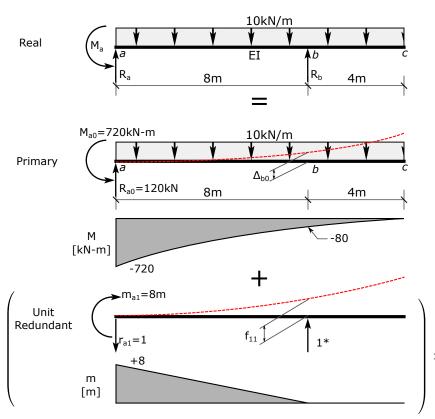
$$\Delta_b = \Delta_{b0} + R_b f_{11} = 0$$
$$\frac{-14507 \,\text{kN m}^3}{EI} + R_b \times \frac{512 \,m^3}{3EI} = 0$$

Solving:

$$R_b = 85.0 \text{ kN}$$

This integral is not in the main part of the table, so we must use the most general case with $m_0 = 8$, $m_1 = 0$, $M_0 = -720$, $M_1 = -80$ and w = 10.

The sign convention for displacements is +ive **upwards**.



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For convenience, the unit load is chosen in the same direction we assumed for R_b . This establishes **upward** displacements as being positive.

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must use the most general case with $m_0 = 8$, $m_1 = 0$,

 $\times R_b$

Displacements in the primary structure:

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 $M_0 = -720$, $M_1 = -80$ and w = 10.

Flexibility coefficients (displacements due to unit redundants):

$$f_{11} = \int \frac{mm}{EI} = \frac{1}{EI} \int_{8m}^{8m} \frac{8m}{8m}$$

$$= \frac{1}{EI} \frac{8m}{3} \times 8m \times 8m$$

$$= \frac{512 \,\mathrm{m}^3}{3EI} \quad (:\uparrow)$$

Compatibility Equation (wrt displacement at b):

$$\Delta_b = \Delta_{b0} + R_b f_{11} = 0$$
$$\frac{-14507 \text{ kN m}^3}{EI} + R_b \times \frac{512 m^3}{3EI} = 0$$

Solving:

$$R_b = 85.0 \text{ kN}$$

Superposition to determine other reactions:

$$M_a = M_{a0} - m_{a1}R_b = 720 - 8 \times 85 = 40 \text{ kN m}$$

 $R_a = R_{a1} - r_{a1}R_b = 120 - 1 \times 85 = 25 \text{ kN}$

The sign convention for displacements is +ive upwards.