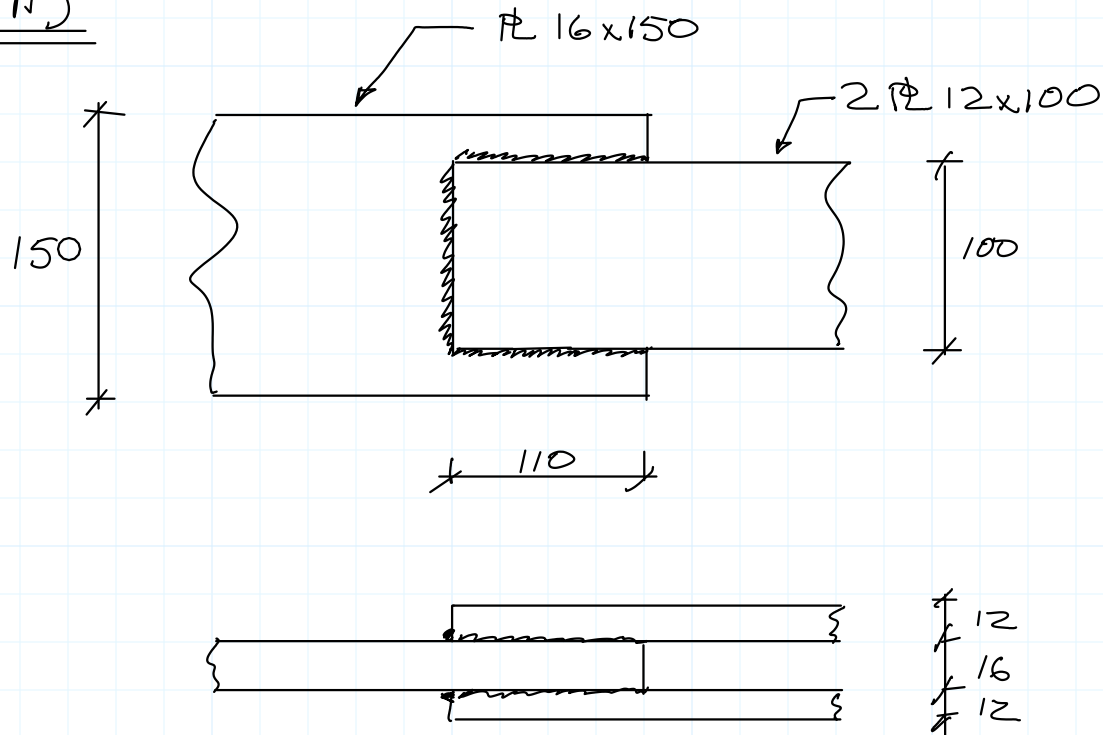


Part A)

Compute factored tension capacity, T_r , of the plates. CSA G40.21 350A steel. Fillet welds around 3 sides of each 12mm plate.

350A Steel: $F_y = 350 \text{ MPa}$ (Table 6-3)
 $F_u = 480 \text{ MPa}$

12mm plates:

$$A_g = 12 \text{ mm} \times 100 \text{ mm} \times 2 = 2400 \text{ mm}^2$$

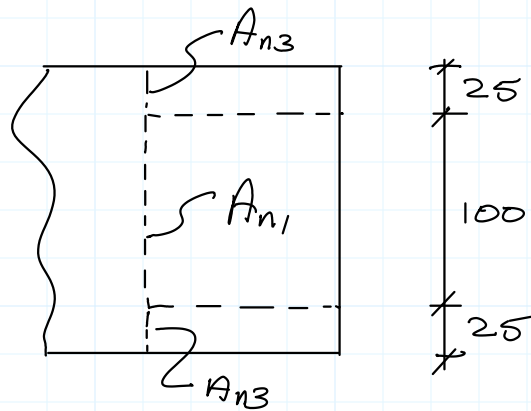
$$A_{n1} = 12 \text{ mm} \times 100 \text{ mm} \times 2 = 2400 \text{ mm}^2$$

$$A_{ne} = A_{n1} = 2400 \text{ mm}^2$$

yield: $T_r = \phi A_g F_y$
 $= 0.9 \times 2400 \text{ mm}^2 \times 0.350 \frac{\text{kN}}{\text{mm}^2} = 756 \text{ kN}$

fract: $T_r = \phi_u A_{ne} F_u$
 $= 0.75 \times 2400 \text{ mm}^2 \times 0.480 \frac{\text{kN}}{\text{mm}^2} = 864 \text{ kN}$

16 mm plate:



$$A_g = 16 \text{ mm} \times 150 \text{ mm} = 2400 \text{ mm}^2$$

$$A_{n1} = 16 \text{ mm} \times 100 \text{ mm} = 1600 \text{ mm}^2$$

$$A_{n3}: \quad L = 110 \text{ mm} \quad w = 25 \text{ mm} \quad \bar{x} = 12.5 \text{ mm}$$

$$L > w$$

$$\therefore A_{n3} = \left(1 - \frac{12.5}{110}\right) \times 25 \times 16 \times 2$$

$$A_{n3} = 709 \text{ mm}^2$$

$$A_{ne} = 1600 + 709 = 2309 \text{ mm}^2$$

yield: $T_r = \phi A_g F_y$

$$= 0.9 \times 2400 \text{ mm}^2 \times 0.350 \frac{\text{kN}}{\text{mm}^2}$$

$$= 756 \text{ kN} \quad \leftarrow \text{governs}$$

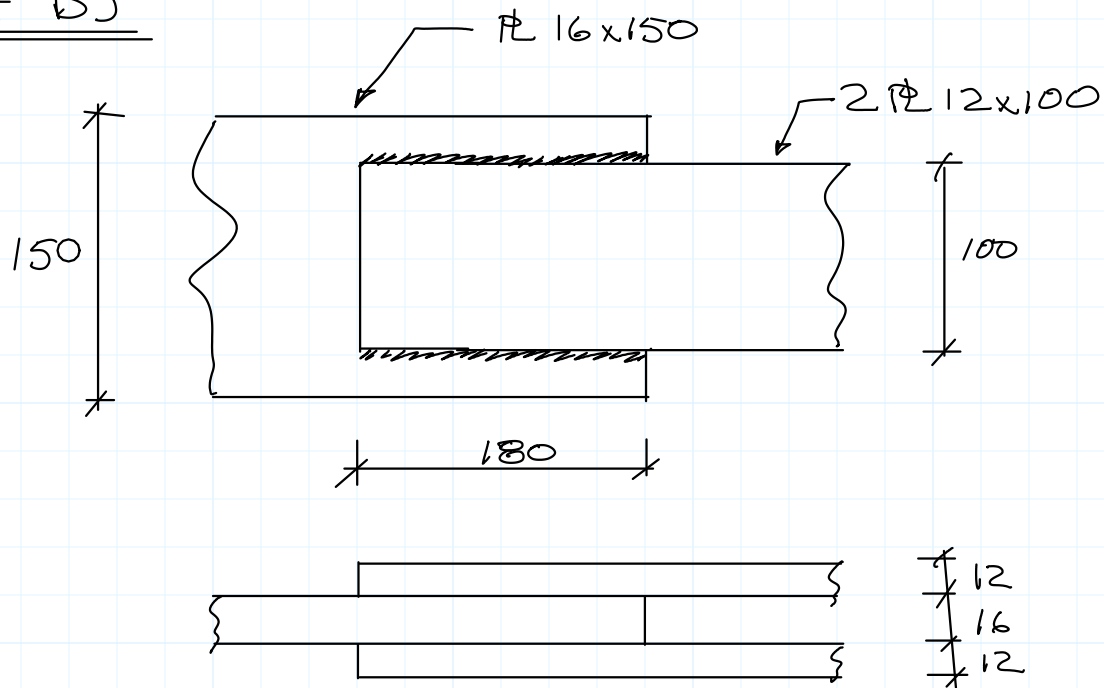
fracture: $T_r = \phi_u A_{ne} F_u$

$$= 0.75 \times 2309 \text{ mm}^2 \times 0.480 \frac{\text{kN}}{\text{mm}^2}$$

$$= 831 \text{ kN}$$

Capacity of plates

$$T_r = \underline{\underline{756 \text{ kN}}} \quad \leftarrow$$

Part B)

Compute the factored tension capacity, T_r of the plates. CSA G40.21 350A steel. Fillet welds on 2 sides of each 12 mm plate.

350A Steel: $F_y = 350 \text{ MPa}$ (Table 6-3)
 $F_u = 480 \text{ MPa}$

12 mm plates:

$$A_g = 12 \text{ mm} \times 100 \text{ mm} \times 2 = 2400 \text{ mm}^2$$

$$A_{n2}: \quad L = 180 \text{ mm}$$

$$w = 100 \text{ mm}$$

$$2w > L > w$$

$$\therefore A_{n2} = (0.5 \times 100 \times 12 + 0.25 \times 180 \times 12) \times 2$$

$$= 2280 \text{ mm}^2$$

$$A_{ne} = 2280 \text{ mm}^2$$

yield: $T_r = 0.9 \times 2400 \times 0.35 = 756 \text{ kN} \leftarrow \text{gov.}$

fracture: $T_r = 0.75 \times 2280 \times 0.48 = 821 \text{ kN}$

16 mm plate:

$$A_g = 2400 \text{ mm}^2$$

$$A_{n2}: \quad L = 180 \quad w = 100$$

$$\begin{aligned} A_{n2} &= 0.5 \times 100 \times 16 + .25 \times 180 \times 16 \\ &= 1520 \text{ mm}^2 \end{aligned}$$

$$A_{n3}: \quad L = 180 \quad w = 25 \quad \bar{x} = 12.5$$

$$\begin{aligned} A_{n3} &= \left(1 - \frac{12.5}{180}\right) \times 25 \times 16 \times 2 \\ &= 744 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} A_{ne} &= 1520 + 744 \\ &= 2264 \text{ mm}^2 \end{aligned}$$

$$\text{yield:} \quad T_r = 0.9 \times 2400 \times 0.35 = 756 \text{ kN} \quad \leftarrow \text{gov.}$$

$$\text{fract:} \quad T_r = 0.75 \times 2264 \times .48 = 815 \text{ kN}$$

Plate Capacity:

$$T_r = \underline{\underline{756 \text{ kN}}} \quad \leftarrow$$