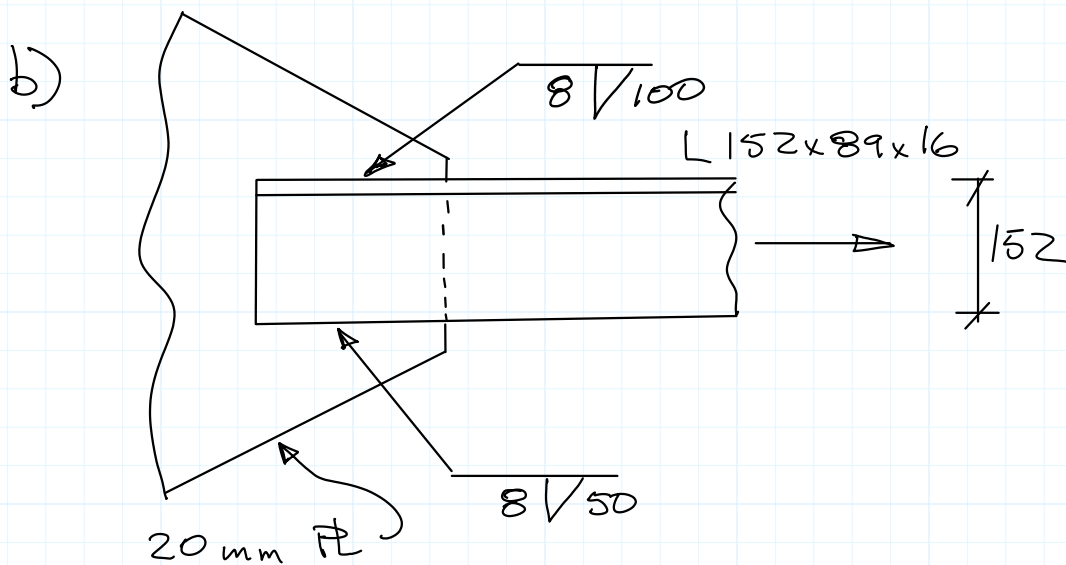
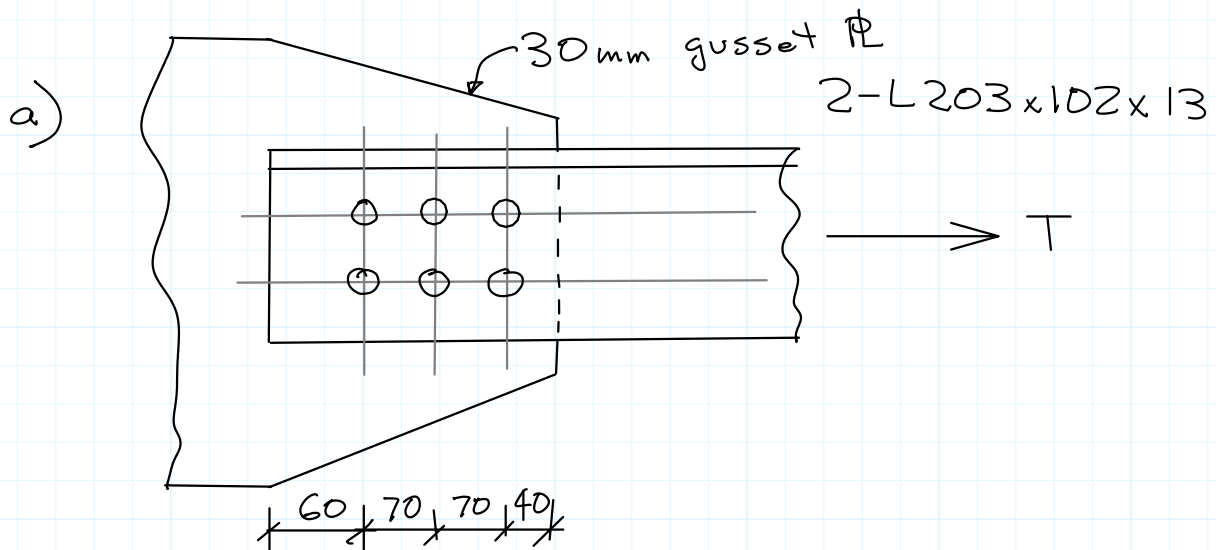


- 2) Tension members - compute the factored tensile resistance,  $T_r$ , of each of the following assemblies. Unless otherwise noted, assume:  
Grade 300W steel  
M20 bolts in punched holes  
Do not compute strength of fasteners.

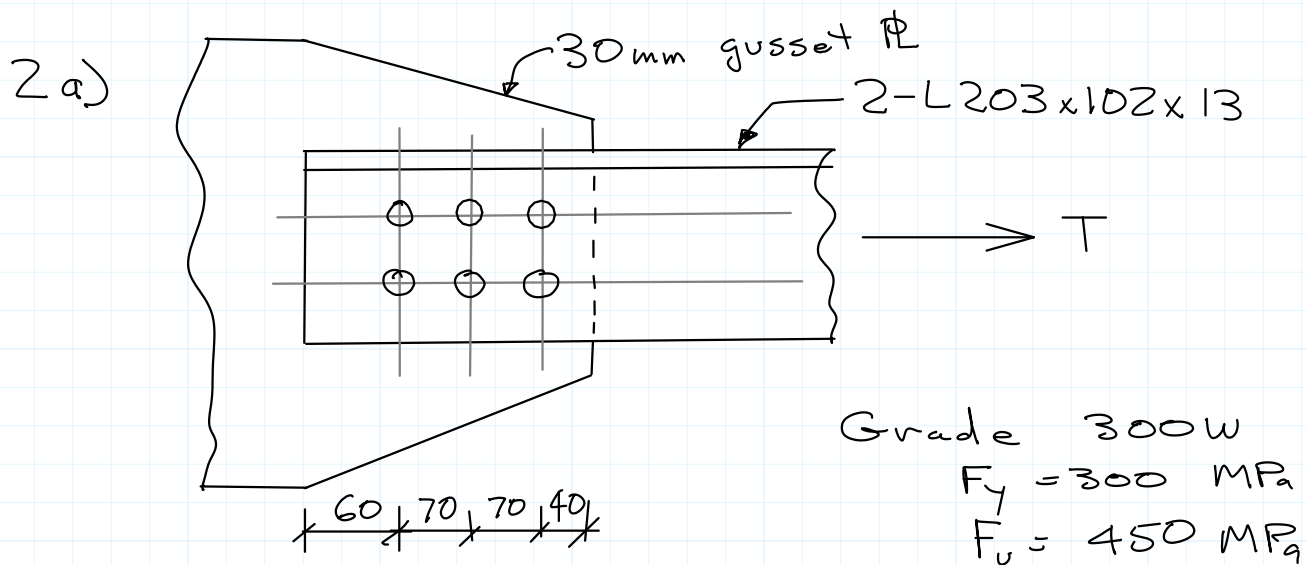


Note: symbol:

leg size of  
fillet weld  
(ignore for now)

8V50

length of  
fillet weld



1-L203x102x13:

$$A = 3710 \text{ mm}^2$$

$$t = 12.7 \text{ mm}$$

i) angle - gross section yielding

$$\begin{aligned} T_r &= \phi A_g F_y \\ &= 0.9 \times 3710 \times 300 \times 10^{-3} \times 2 \\ &= \underline{2003 \text{ kN}} \end{aligned}$$

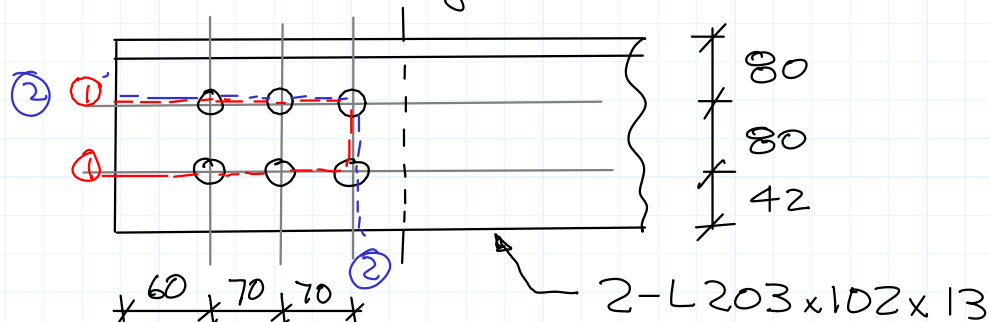
ii) angle - net section fracture

$$\begin{aligned} A_n &= (3710 - 2 \times (20 + 4) \times 12.7) \times 2 \\ &= 6201 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} A_{ne} &= 0.6 A_n \\ &= 0.6 \times 6201 \\ &= 3720 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} T_r &= 0.75 \times 3720 \times 450 \times 10^{-3} \\ &= \underline{1256 \text{ kN}} \leftarrow \text{governs} \end{aligned}$$

iii) Block tearout: angle



### Path 1-1:

$$A_n = (80 - 24) \times 12.7 \times 2 = 1422 \text{ mm}^2$$

$$A_{gv} = (60 + 70 + 70) \times 12.7 \times 2 \times 2 = 10160 \text{ mm}^2$$

$$U_t = 0.6 \quad (\text{conservative})$$

$$\begin{aligned} T_r &= \phi_u \left( U_t A_n F_u + 0.6 A_{gv} \frac{F_y + F_u}{2} \right) \\ &= 0.75 \left( 0.6 \times 1422 \times 450 + 0.6 \times 10160 \times \frac{30 + 45}{2} \right) \end{aligned}$$

$$T_r = 2002 \text{ kN}$$

### Path 2-2:

$$A_n = (80 + 42 - 1.5 \times 24) \times 12.7 \times 2 = 2184 \text{ mm}^2$$

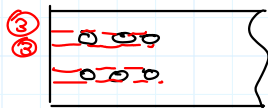
$$A_{gv} = (60 + 70 + 70) \times 12.7 \times 2 = 5080 \text{ mm}^2$$

$$U_t = 0.6$$

$$T_r = 0.75 \left( 0.6 \times 2184 \times 45 + 0.6 \times 5080 \times \frac{30 + 45}{2} \right)$$

$$T_r = 1299 \text{ kN}$$

### Path 3-3: (Bolt tearout)



$$\begin{aligned} A_{gv} &= 2 \times 10160 \text{ mm}^2 \\ &= 20320 \text{ mm}^2 \end{aligned}$$

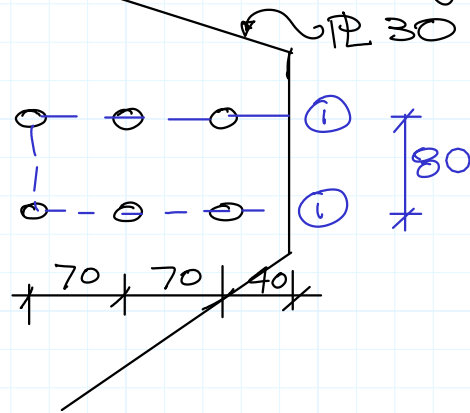
$$A_n = 0$$

$$T_r = 0.75 \left( 0.6 \times 20320 \times \frac{30 + 45}{2} \right)$$

$$= 3429 \text{ kN}$$

iv) Check block tearout in gusset

4/5



By inspection,  
only 1 path

$$A_n = (80 - 24) \times 30 = 1680 \text{ mm}^2$$

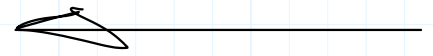
$$U_t = 1.0$$

$$A_{gv} = (70 + 70 + 40) \times 30 \times 2 = 10800 \text{ mm}^2$$

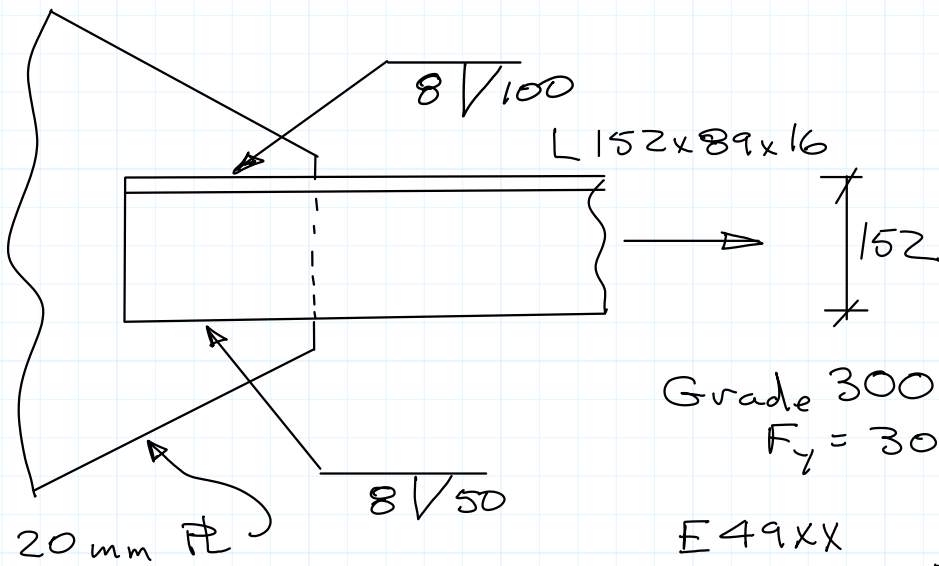
$$\begin{aligned} T_r &= \phi_u \left( U_t A_n F_u + 0.6 A_{gv} \frac{F_y + F_u}{2} \right) \\ &= 0.75 \left( 1.0 \times 1680 \times 45 + 0.6 \times 10800 \times \frac{3 + 45}{2} \right) \\ &= \underline{2390 \text{ kN}} \end{aligned}$$

Net Section fracture ii) governs

$$\underline{\underline{T_r = 1260 \text{ kN}}}$$



2b)



Grade 300 W

$$F_y = 300 \quad F_u = 450$$

E49XX

$$X_v = 490$$

L 152 x 89 x 16:

$$A_g = 3580 \text{ mm}^2$$

$$t = 15.9 \text{ mm}$$

Calculate  $A_{ne}$  for angle

$$A_{n2}: \quad w = 152 \quad L_1 = 100 \quad L_2 = 50 \quad L = 75$$

$$w > L \therefore 12.3.3.3 \text{ (b) (iii)}$$

$$\begin{aligned} A_{n2} &= 0.75 L t \\ &= 0.75 \times 75 \times 15.9 \\ &= 894.4 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} A_{n3}: \quad L &= 100 \quad w = 89 - 15.9 = 73.1 \\ \bar{x} &= w/2 = 36.55 \end{aligned}$$

 $w < L$ , thus from 12.3.3.3 (c)(i)

$$\begin{aligned} A_{n3} &= \left(1 - \frac{36.55}{100}\right) \times 73.1 \times 15.9 \\ &= 737.5 \text{ mm}^2 \end{aligned}$$

$$A_{ne} = 894.4 + 737.5 = 1632 \text{ mm}^2$$

Angle capacity:

$$\begin{aligned} \text{yield: } T_r &= \phi A_g F_y \\ &= 0.9 \times 3580 \times 300 \times 10^{-3} \\ &= 966.6 \text{ kN} \end{aligned}$$

$$\begin{aligned} \text{fracture: } T_r &= 0.75 \times 1632 \times 450 \times 10^{-3} \\ &= \underline{551 \text{ kN}} \quad \leftarrow \text{governs, angle} \end{aligned}$$