

Example Bolt-1  
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CIVE 3205

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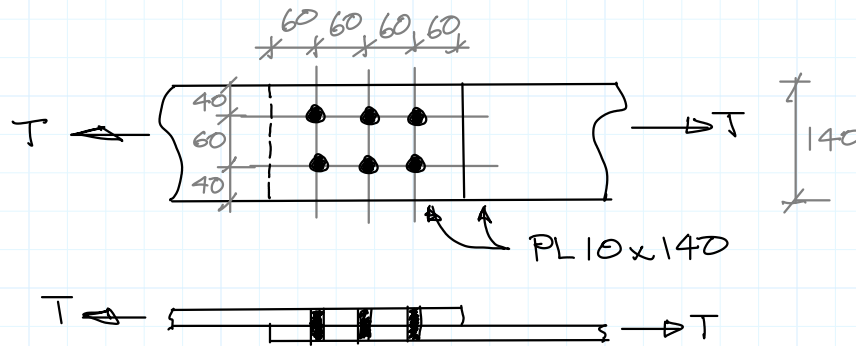
- revisions:

- Apr 26, 2019: corrected length check (new S16) (page 3)
- Feb 6, 2012: clarifying note added to page 1 (max edge distance).

### Example Bolt-1

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Calculate the resistance of the following assembly  
1) as a bearing-type connection, and  
2) as a slip-critical connection



Plates: 350W steel, sheared edges  
Bolts: A325M M20 punched holes

Plates:

$$F_y = 350 \text{ MPa}$$

$$F_u = 450 \text{ MPa}$$

Bolts:

$$F_u = 830 \text{ MPa}$$

(Table 3-3 or §13.12.1.2)

$$d_h = 24 \text{ mm}$$

(§22.3.5.1 + §12.3.2)

(hole allowance)

### Check Bolting Details

Min spacing: (§22.3.1)

$$= 2.7d = 2.7 \times 20 \text{ mm} = 54 \text{ mm}$$

$$60 > 54 \text{ mm}$$

O.K.

Min edge distance: (§22.3.2)

from Table 6 for  $d = 20 \text{ mm}$ , sheared edge

$$e_{\min} = 34 \text{ mm}$$

$$40 > 34 \text{ mm}$$

O.K.

Min end distance: (§22.3.4)

from Table 6

$$e_{\min} = 34 \text{ mm (as above)}$$

$$60 > 34 \text{ mm}$$

O.K.

Max edge distance: (§22.3.3)

$$e_{\max} = 12 \times 10 \text{ mm} = 120 \text{ mm}$$

$$60 < 120 \text{ mm}$$

O.K.

read carefully

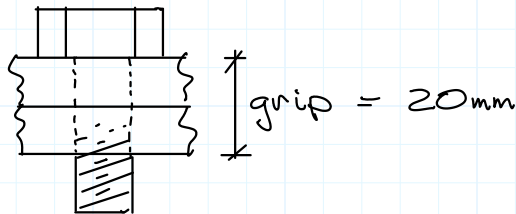
§22.3.3

applies to end distance as well

# Fastener Strength

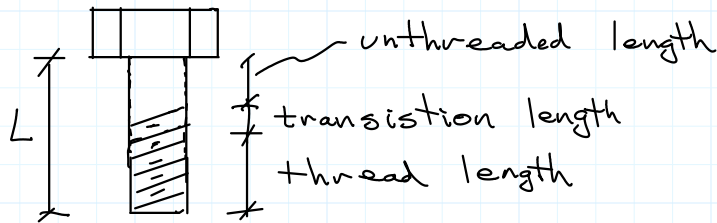
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Check grip & thread length M20 bolts  
grip req'd = 10mm + 10mm = 20mm



from p. 6-161, M20

L	min grip	max grip
45	-	23
50	14	28
55	19	32



only these 3 bolts lengths are possible.

From p 6-159, M20 bolts

L	thread length	transition length	unthreaded length
45	36	7.5	0
50	36	7.5	6.5
55	36	7.5	11.5

Compare unthreaded length to thickness of one plate. If less, then shear plane intercepts threads.

In this case, for 45 & 50mm bolts, threads would be intercepted for L=55mm they would not.

As a practical matter, it is difficult to ensure that the correct bolts are used, so we should take the conservative assumption that threads are intercepted.

# Strength - Bearing-Type Connection

Bolt shear: §13.12.1.2 (c)

$$\begin{aligned}
 V_r &= 0.70 \times 0.60 \phi_b n m A_b F_u \\
 &= 0.70 \times 0.60 \times 0.8 \times 6 \times 1 \times \pi \times \frac{(20 \text{ mm})^2}{4} \times \frac{830 \text{ N}}{\text{mm}^2} \times 10^{-3} \frac{\text{kN}}{\text{N}} \\
 &= \underline{526 \text{ kN}}
 \end{aligned}$$

check length: (§13.12.1.2 d)

$$L = 120 \text{ mm}$$

$$L < 760 \text{ mm}$$

∴ no reduction necessary

Plate bearing: §13.12.1.2 (a)

$$\begin{aligned}
 B_r &= 3 \phi_b n t d F_u \\
 &= 3 \times 0.8 \times 6 \times 10 \text{ mm} \times 20 \text{ mm} \times \frac{450 \text{ N}}{\text{mm}^2} \times 10^{-3} \frac{\text{kN}}{\text{N}} \\
 &= \underline{1296 \text{ kN}}
 \end{aligned}$$

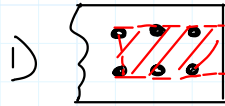
Plate - gross area yielding:

$$\begin{aligned}
 T_r &= \phi A_g F_y \\
 &= 0.9 \times 10 \text{ mm} \times 140 \text{ mm} \times \frac{350 \text{ N}}{\text{mm}^2} \times 10^{-3} \frac{\text{kN}}{\text{N}} \\
 &= \underline{441 \text{ kN}}
 \end{aligned}$$

Plate - net section fracture:

$$\begin{aligned}
 A_n &= (140 \text{ mm} - 2 \times 24 \text{ mm}) \times 10 \text{ mm} \\
 &= 920 \text{ mm}^2
 \end{aligned}$$

$$\begin{aligned}
 T_r &= \phi A_n F_u \\
 &= 0.75 \times 920 \text{ mm}^2 \times \frac{450 \text{ N}}{\text{mm}^2} \times 10^{-3} \frac{\text{kN}}{\text{N}} \\
 &= \underline{310 \text{ kN}} \quad \leftarrow \text{governs}
 \end{aligned}$$



$$A_n = (60 - 24) \times 10 = 360 \text{ mm}^2$$

$$A_{gv} = 3 \times 60 \times 10 \times 2 = 3600 \text{ mm}^2$$

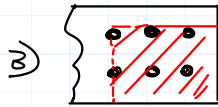
$$U_t = 1.0$$



$$A_n = 2 \times (40 - \frac{24}{2}) \times 10 = 560 \text{ mm}^2$$

$$A_{gv} = 3600 \text{ mm}^2$$

$$U_t = 0.9$$



$$A_n = (60 + 40 - 1.5 \times 24) \times 10$$

$$= 640 \text{ mm}^2$$

$$A_{gv} = 1800 \text{ mm}^2$$

$$U_t = 0.6$$



$$A_n = 0$$

$$A_{gv} = 7200 \text{ mm}^2$$

$$T_r = \phi_u \left[ U_t A_n F_u + 0.6 A_{gv} \left( \frac{F_y + F_u}{2} \right) \right]$$

$$= 0.75 \left[ 450 U_t A_n + 240 A_{gv} \right]$$

case	$A_n$	$U_t$	$A_{gv}$	$T_r$
1)	360	1.0	3600	770 kN
2)	560	0.9	3600	818 kN
3)	640	0.6	1800	454 kN
4)	0	—	7200	1296 kN

$\therefore$  As a bearing-type connection

$$T_r = 310 \text{ kN (plates)} \leftarrow \text{governs}$$

$$T_r = 526 \text{ kN (fasteners)}$$

As a slip-critical connection:

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You must check all of the above (§13.12.2.1) plus the following:

$$V_s = 0.53 C_1 k_s m n A_b F_u \quad (§13.12.2.2)$$

From Table 3, class A, A325M bolts

$$C_1 = 0.82$$

$$k_s = 0.33$$

$$V_s = 0.53 \times 0.82 \times 0.33 \times 1 \times 6 \times \pi \times \frac{20^2}{4} \text{ mm}^2 \times \frac{830 \text{ N}}{\text{mm}^2} \times 10^{-3} \frac{\text{KN}}{\text{N}}$$

$$\underline{V_s = 224 \text{ kN}}$$

As a slip-critical connection:

∴ Limit for service loads

$$T_s = 224 \text{ kN}$$

Limit for factored loads

$$\underline{\underline{T_r = 310 \text{ kN}}}$$

