

EME 152 Discussion 9

November 24, 2021

Agenda

- Derivation of slider velocity
- Input/output torque example
- Three-position synthesis example

Derivation of Slider Velocity

Input/output Torque Example

- Setting US/SI units is now very important!
 - Set the unit system with `uscUnit(true)` for US units and `false` for SI units.
- In the `CFourbar` class:
 - Use the function `setGravityCenter()` to set the gravity center properties (including r_g and delta) of links 2, 3, and 4.
 - Use the function `setInertia()` to set inertial properties of links 2, 3, and 4.
 - Use the function `setMass()` to set the masses of links 2, 3, and 4.
 - Use the functions `forceTorque()`, `forceTorques()`, and `plotForceTorques()` to calculate or plot forces on joints in the four bar linkage mechanism.
- Visit the Ch Mechanism Toolkit file in *C-STEM Studio > My Workspace > LearnMechanism > chmechanism.pdf* for the parameters and return value of these functions.

01_forceTorque.ch

02_plotForceTorques.ch

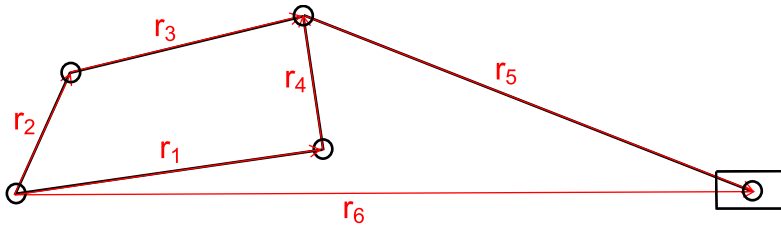
Four Bar Linkage Position Synthesis

- Need to have ϕ_1 , ϕ_2 , ϕ_3 and ψ_1 , ψ_2 , ψ_3 in radians.
- In the `CFourbar` class:
 - The function `synthesis()` requires an empty array for the length of links `r[1:4]`, an array of the input angles `phi[1:3]`, and an array of the output angles `psi[1:3]`. This function synthesizes the four bar linkage and generates the array `r[1:4]` which you can then use in the function `setLinks()`.
 - After using `setLinks()`, you can treat the `CFourbar` class like a normal four bar mechanism and you can call any other function (e.g. calculating forces and torques, animating, etc.)

03_synthesis.ch

Thank you!

Questions? Email!



Fourbar Slider Acceleration Derivation

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March 22, 2010

1 Derivation

$$\vec{r}_6 = \vec{r}_2 + \vec{r}_3 + \vec{r}_5 \quad (1)$$

$$r_6 e^{i\theta_6} = r_2 e^{i\theta_2} + r_3 e^{i\theta_3} + r_5 e^{i\theta_5} \quad (2)$$

$$\dot{r}_6 = r_2 i \omega_2 e^{i\theta_2} + r_3 i \omega_3 e^{i\theta_3} + r_5 i \omega_5 e^{i\theta_5} \quad (3)$$

The unknowns in the previous equation are \dot{r}_6 and ω_5 . We assume that ω_3 has already been found, since it is part of the four-bar mechanism. If we use the equality $i = e^{i\pi/2}$ in the above equation, we may rewrite it as

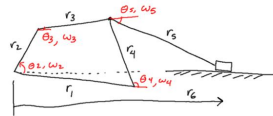
$$\dot{r}_6 = r_2 \omega_2 e^{i(\theta_2 + \pi/2)} + r_3 \omega_3 e^{i(\theta_3 + \pi/2)} + r_5 \omega_5 e^{i(\theta_5 + \pi/2)} \quad (4)$$

The above equation may be readily solved with `complexsolve()`, or using analytical methods discussed in previous discussions.

Taking a derivative one more time, we get

$$\ddot{r}_6 = r_2 i e^{i\theta_2} (\alpha_2 - i \omega_2^2) + r_3 i e^{i\theta_3} (\alpha_3 - i \omega_3^2) + r_5 i e^{i\theta_5} (\alpha_5 - i \omega_5^2) \quad (5)$$

Again, we assume the only unknowns in the above equation are \ddot{r}_6 and α_5 , since we found ω_5 in the last step. We assume all other angular velocities and accelerations have been solved for during the analysis of the fourbar part of the mechanism.



$$r_6 = r_2 + r_3 + r_5 = r_1 + r_4 + r_5$$

$$r_6 e^{i\theta_6} = r_2 e^{i\theta_2} + r_3 e^{i\theta_3} + r_5 e^{i\theta_5}$$

complex solve PR $\rightarrow r_6, \theta_6$

$$\dot{r}_6 = r_2 i \omega_2 e^{i\theta_2} + r_3 i \omega_3 e^{i\theta_3} + r_5 i \omega_5 e^{i\theta_5}$$

$$\dot{r}_6 = \dot{z}_1 + \dot{z}_2 + M e^{i\theta}$$

$$\dot{r}_6 = \dot{z}_3 + \dot{M} e^{i\theta}$$

complex solve PR $\rightarrow r_6, \omega_5$

$$\dot{r}_6 = r_2 i \omega_2 e^{i(\theta_2 + \frac{\pi}{2})} + r_3 i \omega_3 e^{i(\theta_3 + \frac{\pi}{2})} + r_5 i \omega_5 e^{i(\theta_5 + \frac{\pi}{2})}$$

$$\ddot{r}_6 = \ddot{z}_1 + \ddot{z}_2 + \ddot{M} e^{i\theta}$$

$$\ddot{r}_6 = \ddot{z}_3 + \ddot{M} e^{i\theta}$$

com. ... PR $\rightarrow \ddot{r}_6, M$

$$M \rightarrow \alpha_5$$

