

3.3

1. Name Nicholas Hawse

2 Given

$$V_{boid} = 10000 \frac{\text{ft}}{\text{s}}$$

$$M_{p1} = 500 \text{ lb}_m$$

$$\text{1st } I_{sp1} = 270 \text{ s } \lambda_1 = 0.9$$

$$\Delta V_1 = \Delta V_2$$

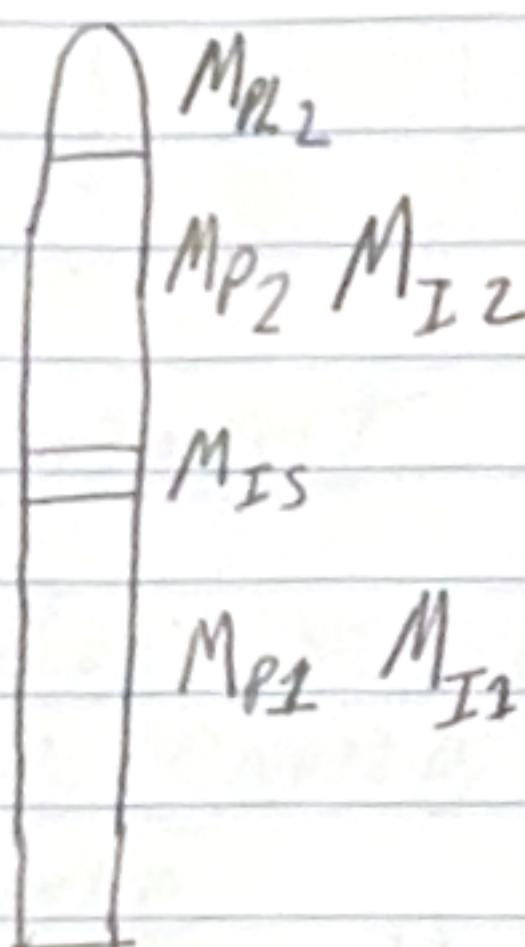
$$M_{IS} = 200 \text{ lb}_m$$

$$\text{2nd } I_{sp2} = 350 \text{ s } \lambda_2 = 0.8$$

3 Find

a) M_{p1} M_{p2} M_{I1} M_{I2} b) GLOW

4 Schematic



5 Assumptions

$$V_{ideal}$$

no gravity

no drag

$$\Delta V_1 = \Delta V_2$$

constant thrust

constant m

6 Basic Equations

$$\Delta V_{id} = g_e I_{sp} \ln \left(\frac{m_0}{m_f} \right) \quad MR = \frac{m_0}{m_f} = \frac{m_{I1} + m_p + m_i}{m_{I1} + m_i} = \frac{x m_{p1} + m_p}{x m_{p1} + m_p (1-x)}$$

$$\lambda = \frac{m_p}{m_p + m_i}$$

$$MR = e^{\frac{\Delta V_{id}}{g_e I_{sp}}} \quad m_p = m_{p1} \frac{MR - 1}{MR - (MR - 1) \lambda^{-1}}$$

7 Analysis

$$MR_2 = e^{\frac{5000 \text{ ft} s^2}{53505.322 \text{ ft}}} = 1.558$$

$$m_{p2} = \frac{500 \text{ lbm}}{\left(1.558 - (1.558 - 1) \left(\frac{1}{0.8}\right)\right)} = 324.5 \text{ lbm}$$

$$(m_{p1} + m_i) MR = m_{p1} + m_p + m_i$$

$$MR m_i + MR m_{p1} = m_{p1} + m_p + m_i$$

$$m_i (MR - 1) = m_{p1} (1 - MR) + m_p$$

$$m_i = \frac{m_{p1} (1 - MR) + m_p}{MR - 1}$$

$$m_{i2} = 81.1 \text{ lbm}$$

$$M_2 = 81.1 + 324.5 + 500 = 906 \text{ lbm}$$

$$m_{p1,1} = m_2 + m_{IS} = 1106 \text{ lbm}$$

$$MR_1 = e^{\frac{5000}{270 \cdot 32.2}} = 1.78$$

$$m_{p1} = 1106 \cdot \frac{1.78 - 1}{1.78 - (1.78 - 1) \cdot 0.9} = 940.7$$

$$m_{i1} = 105 \text{ lbm}$$

$$\begin{aligned} b) GLOW &= m_{p1} + m_p + m_{i1} \\ &= 2150 \text{ lbm} \end{aligned}$$

8 Answers

	1	2 (lbm)
m_p	940.7	324.5
m_{i1}	105	81.1

$$GLOW = 2150 \text{ lbm}$$

9 Comment

A Real rocket would likely not have the same ΔV in the upper and lower stage.

3.13

1) Name Nicholas House

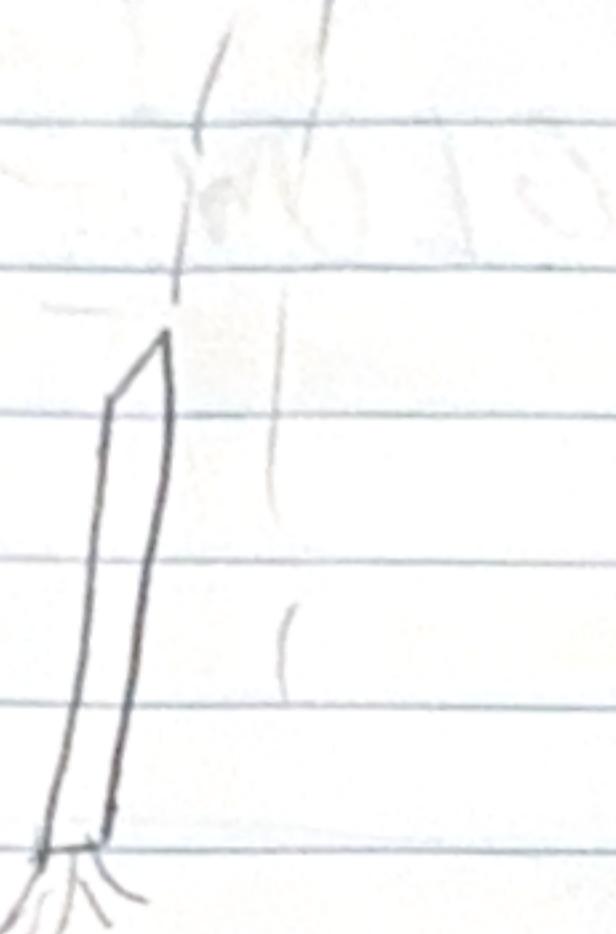
2) Given

$$m_0 = 50 \text{ kg} \quad m_{b0} = 20 \text{ kg}$$

$$I_{sp} = 250 \text{ s}$$

3) $h_{b0 \text{ max}}$ for t_b

4)



5 Assumptions

Point mass

no drag

const gravity

6) Basic equations

$$h_{b0} = g_e I_{sp} t_b \left(\frac{m_f}{m_0 - m_s} \ln \left(\frac{m_f}{m_0} \right) + 1 \right) - \frac{g_e}{2} t_b^2$$

7) analysis

$$\frac{\partial t_b}{\partial} = 0$$

$$0 = g_e I_{sp} \left(\frac{m_f}{m_0 - m_f} \ln \left(\frac{m_f}{m_0} \right) + 1 \right) - g_e t_b$$

$$t_b = I_{sp} \left(\frac{m_f}{m_0 - m_f} \ln \left(\frac{m_f}{m_0} \right) + 1 \right) = 250 \left(\frac{20}{50-20} \ln \left(\frac{2}{5} \right) + 1 \right)$$

$$t_b = 97.285 \text{ s}$$

$$h_{b0} = 9.81 \cdot 250 \cdot 97 \left(\frac{20}{50-20} \ln \left(\frac{2}{5} \right) + 1 \right) - \frac{9.81}{2} (97)^2$$

$$h_{b0} = 46420 \text{ m}$$

8 Answer

$$t_{b0} = 97.3 \text{ s} \quad h_{b0} = 46,420 \text{ m}$$

9 comment

maximizing the burnout height is not a good way to increase the overall apogee.

3.23

1 Name Nicholas House

2 Given

$$\dot{m}_A = 150 - 5t \quad 0 < t < 30$$

$$\dot{m}_B = 12.5 + 10t \quad 0 < t < 20$$

3 find

Greater I_{sp} between A, B

Greater V_{b0} between A, B

4 Schematic



5 Assumptions

no drag
point mass
const I_{sp}

6 Basic equations

$$F = ma$$

$$F_T = I_{sp} g_e m$$

$$F_g = g_e m(t)$$

$$\Delta V = I_{sp} g_e \ln \left(\frac{m_0}{m_f} \right)$$

$$V_{b0} = I_{sp} g_e \ln \left(\frac{m_0}{m_f} \right) - g_e t_b$$

Zanalysis

$$\frac{m_A}{m} = \frac{I_{sp} g_e \dot{m}}{m} - g_e \frac{\dot{m}}{m}$$

$$a = I_{sp} g_e \frac{\dot{m}(t)}{m(t)} - g_e$$

$$\frac{dV}{dt} = I_{sp} g_e \frac{\dot{m}}{m}$$

$$A) dV = I_{sp} g_e \frac{150-5t}{m_0-150+5t} dt$$

$$m(t) = \int_0^t \dot{m}(t) dt \quad \Delta m_A(t) = \int_0^{30} 150-5t dt$$

$$\Delta m_A = \left[150t - \frac{5}{2}t^2 \right]_0^{30} = 2250 \quad \bar{m}_A = 75$$

$$\Delta m_B = \left[12.5t + 5t^2 \right]_0^{20} = 2250 \quad \bar{m}_B = 112.5$$

$$\Delta V_A = I_{sp} g_e \ln \left(\frac{m_0}{m_0 - 2250} \right) \quad \Delta V_B = I_{sp} g_e \ln \left(\frac{m_0}{m_0 - 2250} \right)$$

$$\Delta V_A = \Delta V_B \text{ Identical}$$

b)

$$V_{boA} = I_{sp} g_c \ln\left(\frac{m_0}{m_0 - 2250}\right) - g_c(30)$$

$$V_{boB} = I_{sp} g_c \ln\left(\frac{m_0}{m_0 - 2250}\right) - g_c(20)$$

$$V_{boB} > V_{boA}$$

8 Answer

a) $\Delta V_A = \Delta V_B$

b) $V_{boB} > V_{boA}$

9 Comment

With no gravity the mass flow rate doesn't matter assuming constant I_{sp} , and with gravity you want as large of a m as possible.

SP03-B1

Name Nicholas Hawse

2 Given

$$I_{sp} = 200 \text{ s}$$

$$m_0 = 53.0 \text{ lbm}$$

$$m_p = 10 \text{ lbm}$$

$$V_0 = h_0 = 0$$

$$t_b = 3.2 \text{ s}$$

$$A_f = 0.208981 \text{ ft}^2$$

$$C_D = 0.3$$

$$\rho \left(\frac{\text{lbm}}{\text{ft}^3} \right) = \left(1.255 \times 10^{-11} \right) h^{-2} - \left(1.9453 \times 10^{-6} \right) h + 0.67579$$

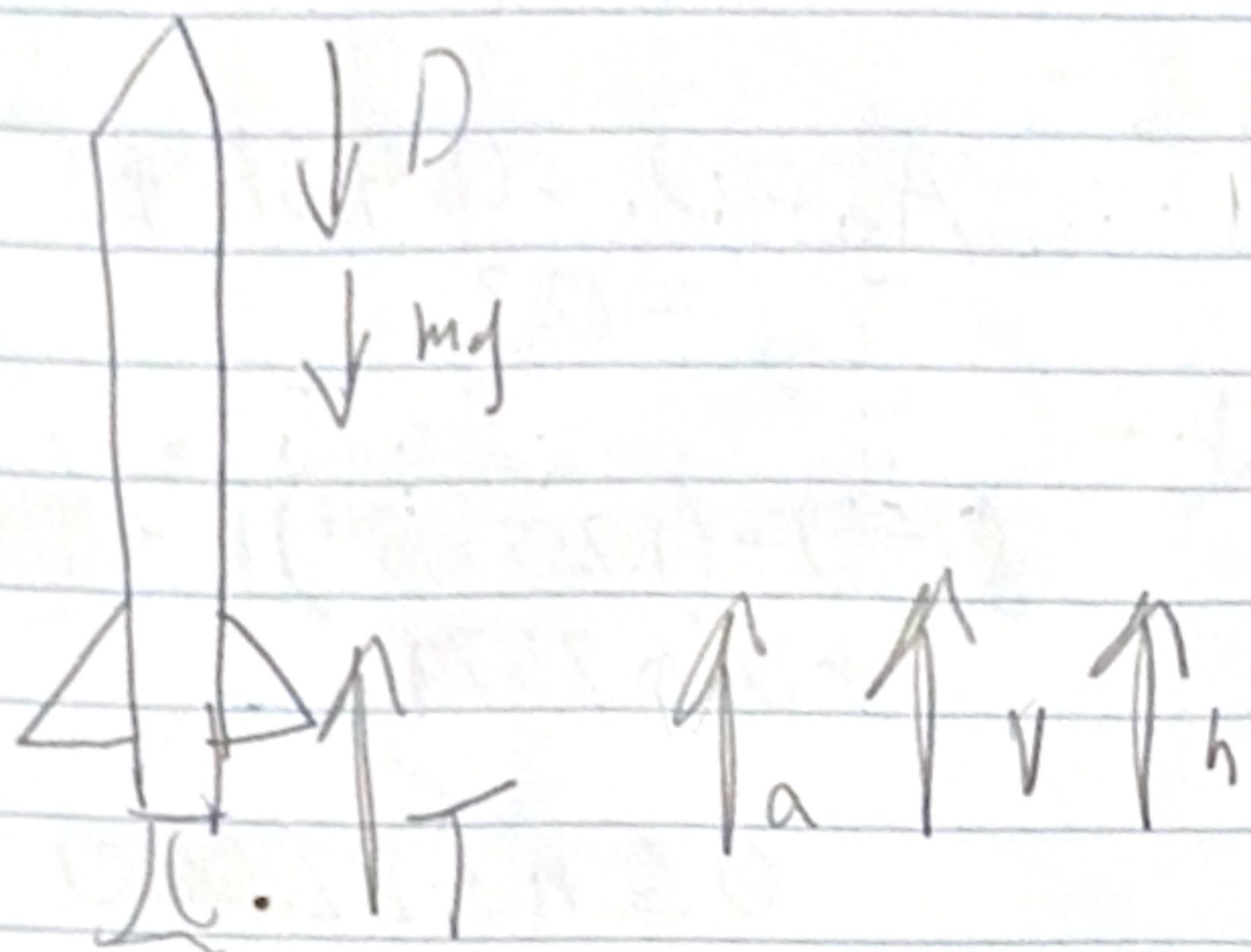
$$0 \leq h \leq 82,000$$

3 Find

Plot of density of air between $h=0, h=100,000 \text{ ft}$
Show equations in symbolic form and
hand calculate the first 3 steps
Plot a vs t from $t=0-10 \text{ s}$ with and without drag
do the same for V, h

$a_0 \frac{\text{ft}}{\text{s}^2}$	NO D	D
$a_b \frac{\text{ft}}{\text{s}^2}$		
$h_b \text{ ft}$		
$V_b \frac{\text{ft}}{\text{s}}$		
$V_{max} \frac{\text{ft}}{\text{s}}$		
$h_{ap} \text{ ft}$		
$t_{ap} \text{ s}$		

4 Schematic



5 Assume

Vertical trajectory

Cost ISP

Cost in

Const $g = 32.2 \frac{\text{ft}}{\text{s}^2}$

$V = h_0 = 0$

$\Delta t = 0.25$

Correct no drag solution

Const $CD = 0.3$

Given air density
Point mass

6 basic equations

$$m_{i+1} = m_i - \dot{m}_i (t_{i+1} - t_i)$$

$$a_i = \frac{I_{sp} g_e m}{m_i} - g_e - \frac{s_h C_D V_i |V_i| A_f}{2 m_i} \quad 0 < t_b$$

$$a_i = -g_e - \frac{s_h C_D V_0 |V_i| A_f}{2 m_i} \quad t_b < t < \infty$$

$$V_{i+1} = V_i + a_i (t_{i+1} - t_i)$$

$$h_{i+1} = h_i + \frac{(V_{i+1} + V_i)}{2} (t_{i+1} - t_i)$$

$$F_t = \dot{m} g_e I_{sp} \quad \dot{m} = \frac{m_p}{t_b}$$

7 analysis

$$t=0 \quad m=53 \text{ lbm} \quad h_0=0 \quad V_0=0 \quad \dot{m} = \frac{10}{32}$$

$$a_0 = \frac{32.2 \cdot 10 \cdot 200}{3.2 \cdot 53} - 32.2 - \frac{0.0758 \cdot 0.3 \cdot 0 \cdot 0 \cdot 0.209}{2 \cdot 53}$$

$$a_0 = 347.5 \frac{\text{ft}}{\text{s}^2}$$

$$t=0.2$$

$$m_r = 53 - \frac{10}{32}(0.4 - 0.2) = 52.375$$

$$V_r = 0 + 347.5(0.2 - 0) = 69.5 \frac{\text{ft}}{\text{s}}$$

$$h_r = 0 + \frac{(69.5 + 0)}{2}(0.2 - 0) = 6.95 \text{ ft}$$

$$a_1 = \frac{32.2 \cdot 10 \cdot 200}{3.2 \cdot 52.375} - 32.2 - \frac{0.0758 \cdot 0.3 \cdot (69.5)(69.5) \cdot 0.209}{2 \cdot 52.375}$$

$$a_1 = 351.8 \frac{\text{ft}}{\text{s}^2}$$

$$t=0.4$$

$$m_2 = 52375 \frac{10}{3.2} (0.6 - 0.4) = 51.75 \text{ lbm}$$

$$V_2 = 69.5 + 351.8 (0.4 - 0.2) = 139.9 \frac{\text{ft}}{\text{s}}$$

$$h_2 = 6.95 + \frac{(139.9 + 69.5)}{2} (0.4 - 0.2) = 27.9 \text{ ft}$$

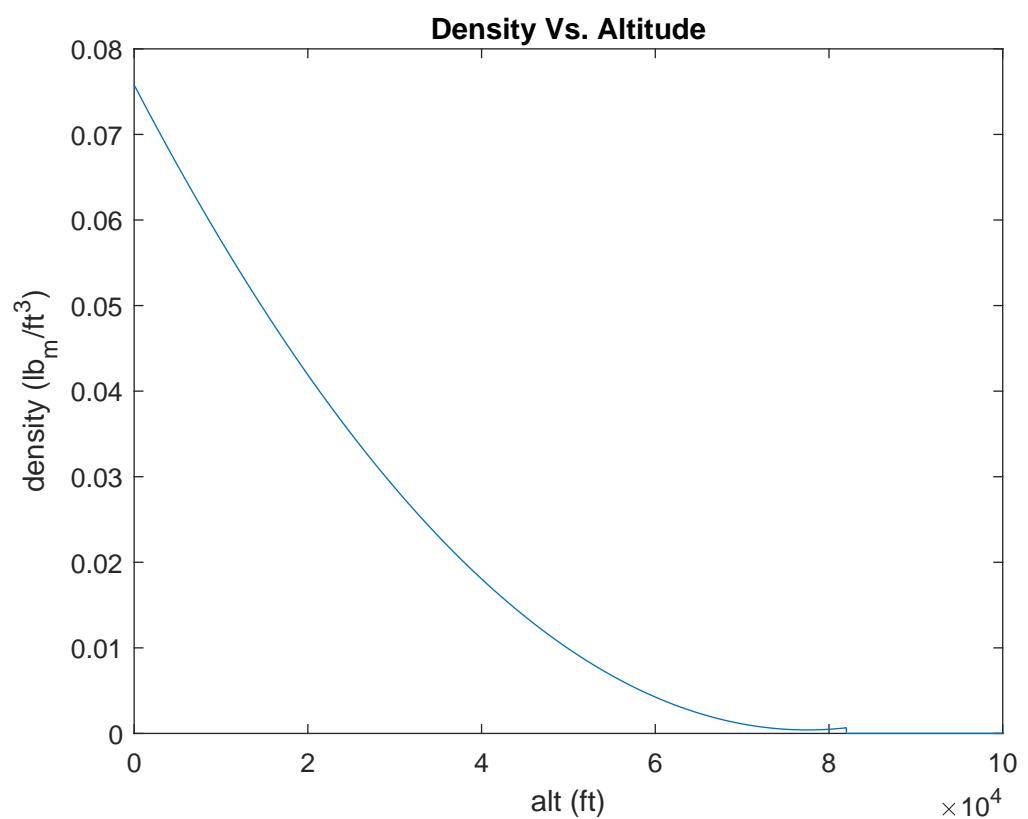
$$a_2 = \frac{32.2 \cdot 10 \cdot 200}{3.2 \cdot 51.75} - 32.2 - \frac{0.0757 \cdot 0.3 \cdot (139.9)^2 \cdot 0.209}{2 \cdot 51.75}$$

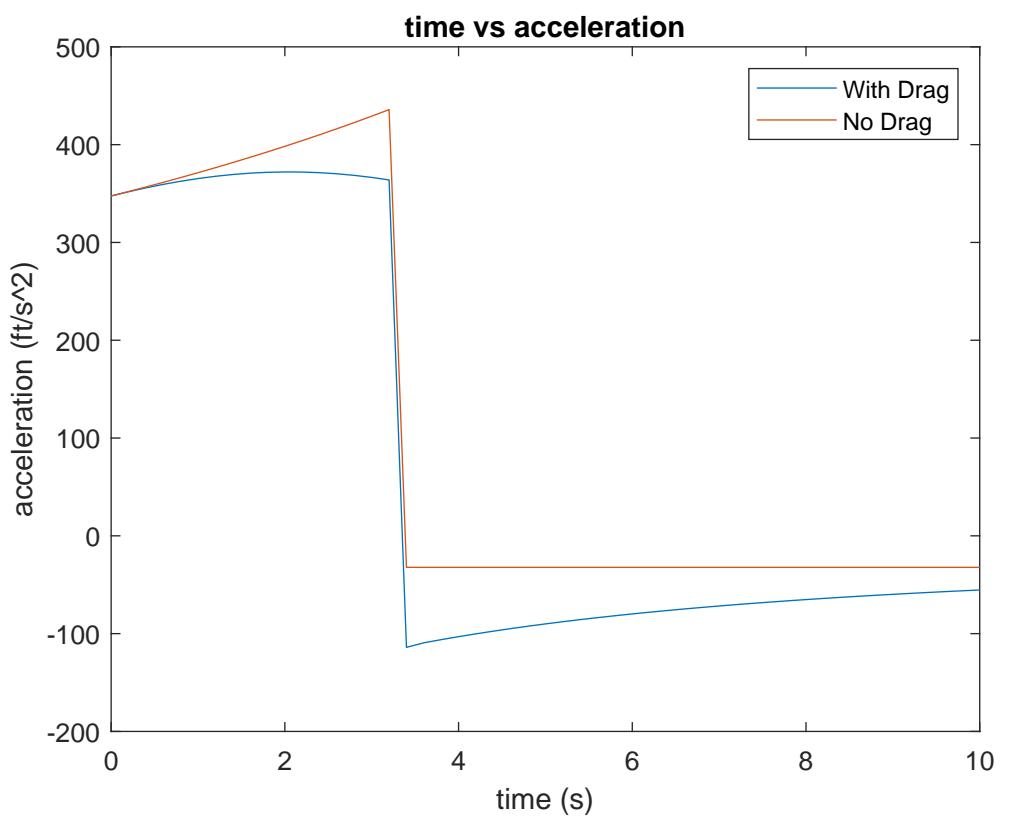
$$a_2 = 355.8$$

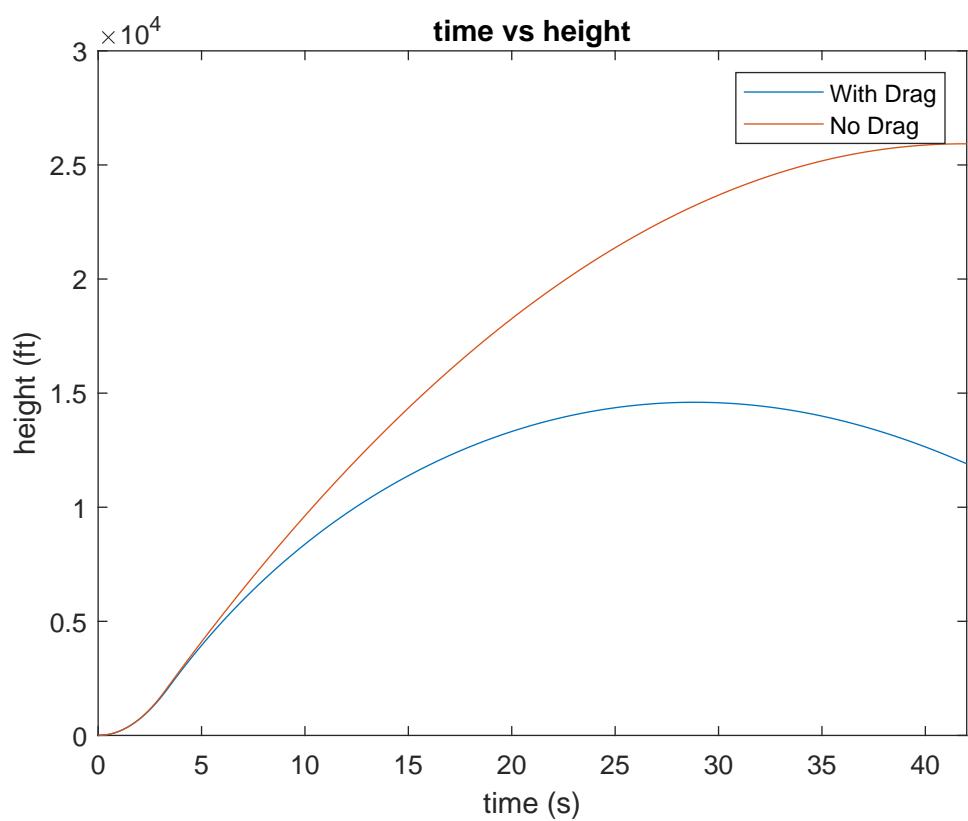
8 Answers

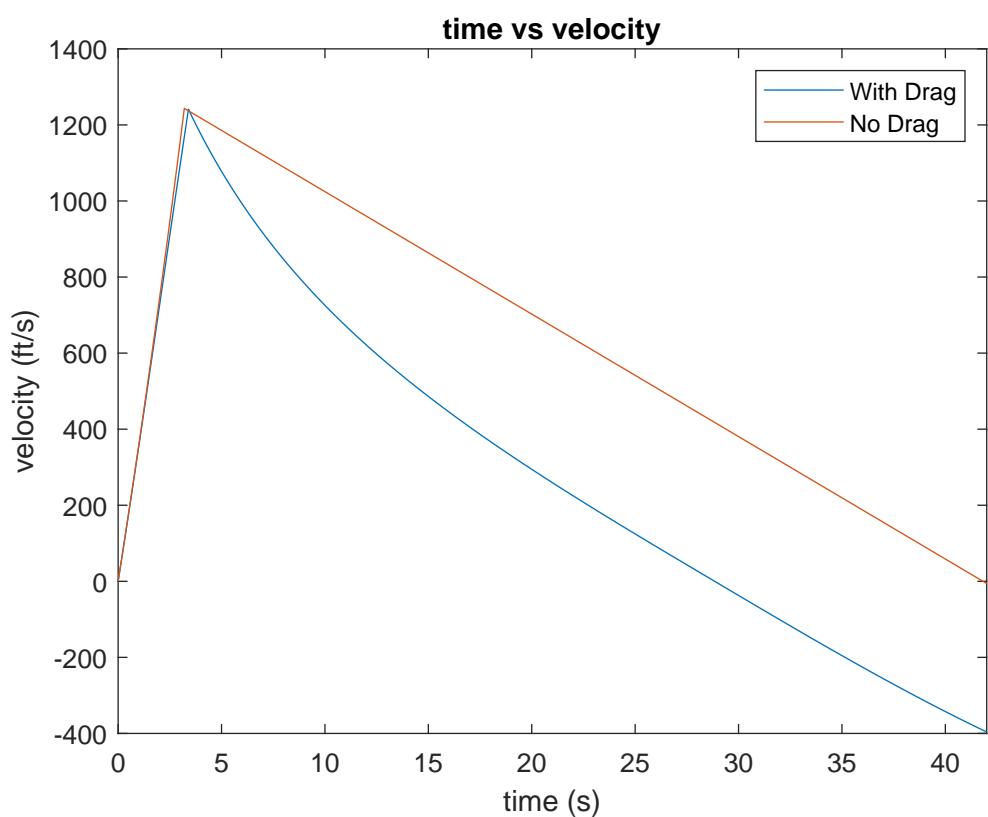
	NOD	D
a _o	347,5	347,5
a _b	435,8	363,9
b _b	1915	1852
V _b	1244	1169
V _{max}	1244	1169
h _{ap}	25925	14600
t _{ap}	42	24

	t	m	a	v	h
0	0	53	348	0	0
0.2	52.375	352	69.5	6.95	
0.4	51.75	356	140	27.9	









9 Comment

The edlers method code was no harder to implement and thus should basically always be used.