

# Hw 06A

## Problem 7.1

1 Name Nichols Hawse

2 Given

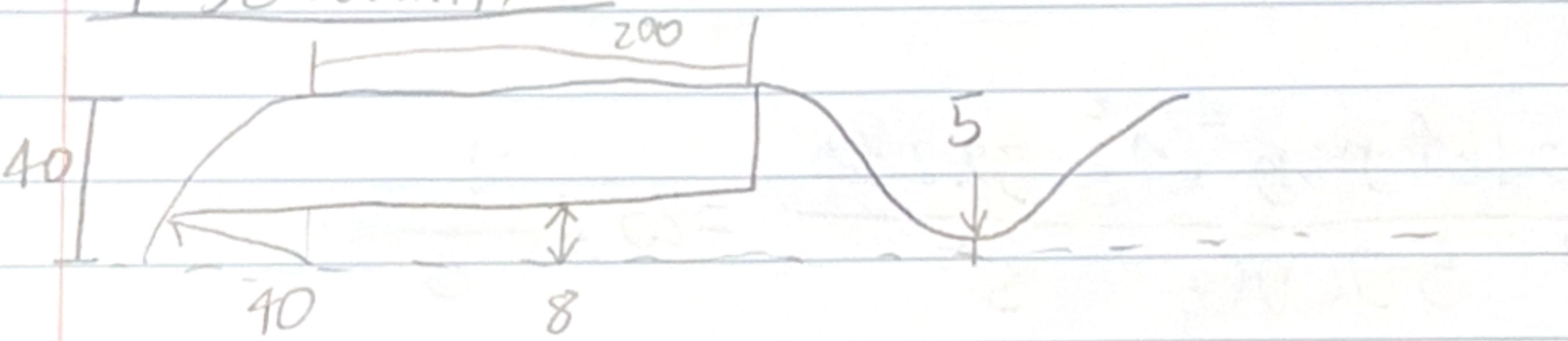
$$C^* = 5000 \frac{ft}{s} \quad P_{c,i} = 500 \text{ Psi}$$

$$r_b = a P_c^{0.4} \frac{\text{in}}{\text{s}} \quad S_p = 0.05 \frac{lbm}{\text{in}^2}$$

3 Find

- the constant  $a$
- $P_c$  @ 10 in
- $t$  @ 10 in

4 Schematic



5 Assumptions

- Steady State
- constant burn rate
- No through erosion
- instant flame spread

## 6 basic equations

$$\dot{m} = \frac{P_c A_{\text{c}}}{C^*} = A_b \cdot h \cdot g_p$$

$$L^2 + 8^2 = 40^2$$

## 7 Analysis

$$A_{bi} = \pi L r_i \left( \sqrt{40^2 - r_i^2} + 200 \right) + 2\pi (40^2 - r_i^2)$$

$$A_{bi} = 16850 \text{ in}^2$$

$$\dot{m} = \frac{500 \text{ lbf} \pi \cdot 0.5 \text{ in}^2 \cdot 32.2 \text{ ft}}{\text{in}^2 \cdot 5000 \text{ ft} \cdot 32 \text{ s}} = 253 \frac{\text{lbf}}{\text{s}}$$

$$n = \frac{\dot{m}}{A_b \cdot g_p} = \frac{253 \text{ lbf}}{3 \cdot 16850 \text{ in}^2 \cdot 0.05 \text{ lbf}} = 0.3 \frac{\text{in}}{\text{s}}$$

$$r = a P_0^{0.4}$$

$$a = \frac{r}{P_0^{0.4}} = \frac{0.3 \text{ in}}{5500^{0.4}} = 0.025$$

$$A_{b,10} = \pi \left( 2(r_i + 10) \left( \sqrt{t_0^2 - (r_i + 10)^2} + 200 \right) + (t_0^2 - (r_i + 10)^2) \right)$$

$$A_b = 30668 \text{ in}^2$$

$$m_{\text{dot}} = 30668 \text{ in}^2 \cdot 0.3 \text{ in} \cdot 0.05 \frac{\text{lb in}}{\text{in}^3} = 460 \frac{\text{lb in}}{\text{s}}$$

$$P_c = \frac{m C^*}{A_t} = \frac{460 \text{ lb in} \cdot 5000 \text{ ft}}{8 \pi \cdot 25 \text{ in}^2} \cdot \frac{8^2}{8 \cdot 32.2 \text{ ft}} = 909 \frac{\text{lb}}{\text{in}^2}$$

$$t = \frac{W}{r} = \frac{10 \text{ in s}}{0.3 \text{ in}} = 33 \text{ s}$$

### 8 Answers

a)  $a = 0.025$

b)  $P_c = 909 \text{ Psi}$

c)  $t = 33.3 \text{ s}$

### 9 Comment

If seems like assuming that  $r$  is constant is not a great assumption. It might be better to use a computer.

7.26

Name Nicholas

Given

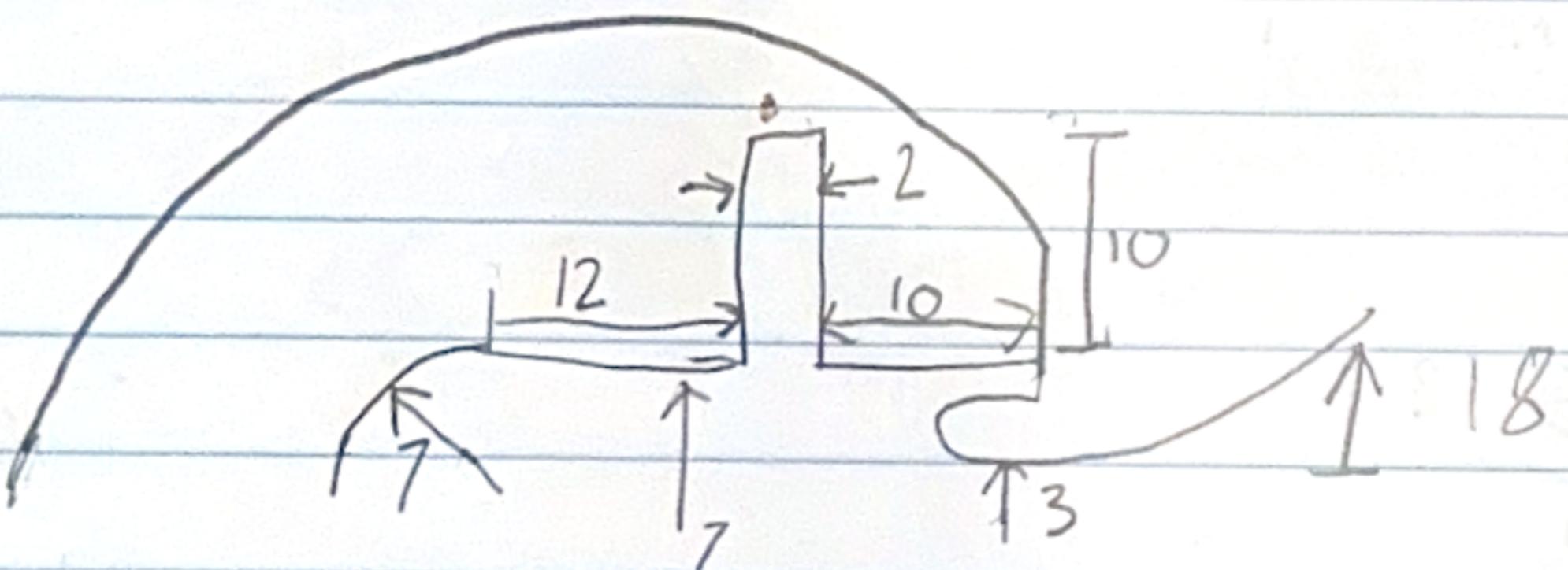
$$S_p = 0.063 \frac{\text{lb}}{\text{in}^3} \quad C^* = 4900 \frac{\text{ft}}{\text{s}} \quad \gamma = 1.2$$

$$r_b = 0.06 P_c^{0.25}$$

3 find

$$P_i \quad F_{t,vac}$$

4 Schematic



5 Assumptions

Steady state

no thought erosion

instant flame transport

## 6 basic equations

$$\dot{m} = \frac{P_c A_t}{C^*} = \rho r A_b$$

$$\frac{P_c}{P} = \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{\gamma}{\gamma-1}}$$

$$F = \dot{m} V_e + (P_e - P_a) A_c = P_c A_t \left[ \frac{2\gamma^2}{\gamma-1} \left( \frac{2}{\gamma+1} \right)^{\frac{\gamma+1}{\gamma-1}} \left( 1 - \left( \frac{P_e}{P_c} \right)^{\frac{\gamma-1}{\gamma}} \right)^{\frac{\gamma+1}{\gamma}} \right] + P_e A_c$$

$$\frac{A_c}{A_t} = \frac{1}{M_e} \left( \frac{2 + (\gamma-1) M_e^2}{\gamma+1} \right)^{\frac{\gamma+1}{2(\gamma-1)}}$$

## 7 Analysis

$$\dot{m} = \frac{P_c A_t}{C^*} = \rho_r r A_b$$

$$\frac{P_c A_t}{C^*} = \rho_p 0.06 P_c^{1/4} A_b$$

$$\frac{P_c}{P_c^{1/4}} = \frac{C^* \rho_p 0.06 A_b}{A_t}$$

$$P_c = \left( \frac{C^* \rho_p 0.06 A_b}{A_t} \right)^{4/3}$$

$$A_b = \frac{1}{2} 4\pi r^2 + 12 \cdot 7 \cdot 2\pi r + 2 \cdot \pi (17^2 - 7^2) + 2 \cdot 5\pi \cdot 2 \cdot 17 + 2 \cdot \pi \cdot 10 \cdot 7$$

$$A_b = 3000 \text{ in}^2$$

$$A_t = \pi \cdot 3^2 = 28.27$$

$$P_c = \left( \frac{4900 \text{ ft} \cdot 0.063 \text{ lb} \cdot 0.06 \cdot 3000 \text{ ft}^3 \cdot 8 \text{ ft}}{8 \text{ in}^3 \cdot 28.27 \text{ in}^2 \cdot 32.2 \text{ ft} \cdot 8} \right)^{\frac{1}{3}}$$

$$P_c = \left( \frac{1493 \text{ m} \cdot 1743 \text{ kg} \cdot 0.0254 \text{ m} \cdot 1.939 \text{ m}^2}{\text{s} \cdot \text{m}^3 \cdot 0.0182 \text{ m}^2} \right)^{\frac{1}{3}}$$

$$P_c = 240 \text{ Psi}$$

$$\dot{m} = \frac{P_c A_t}{C * 32.2} = \frac{240 \text{ lb} \cdot 9.50 \text{ in}^2 \cdot 32.2 \frac{\text{ft}}{\text{s}^2}}{\text{in}^2 \cdot 4900 \text{ ft}} = 44.6 \frac{\text{lb}}{\text{s}}$$

$$\frac{A_e}{A_t} = \frac{18}{3^2} = 36 \quad M_e = 4.17$$

$$\frac{P_e}{P_c} = \left( 1 + \frac{1.2 - 1}{2} (4.17)^2 \right)^{\frac{-1.2}{1.2 - 1}} = 2.3 \times 10^{-4}$$

$$P_e = \frac{P_e}{P_c} \cdot P_c = 0.013$$

$$240(950) \left( \frac{2 \cdot 1.2^2}{0.2} \left( \frac{2}{2.2} \right)^{\frac{2.2}{0.2}} \left( 1 - \left( 2.3 \times 10^{-3} \right)^{\frac{0.2}{1.2}} \right) \right)^{\frac{1}{2}} + 0.013 \cdot 98.87^2$$

$$F_{thc} = 12725 \text{ lb}$$

## 8 Answers

$$P_c = 240 \text{ PSI} \quad F_{t,vac} = 12725/6$$

## 9 Comment

It is impulsive to pay attention to the units in the pressure equation to get the correct number

Sutton 12.1

1 Name Nicholas Nurse

2 Given

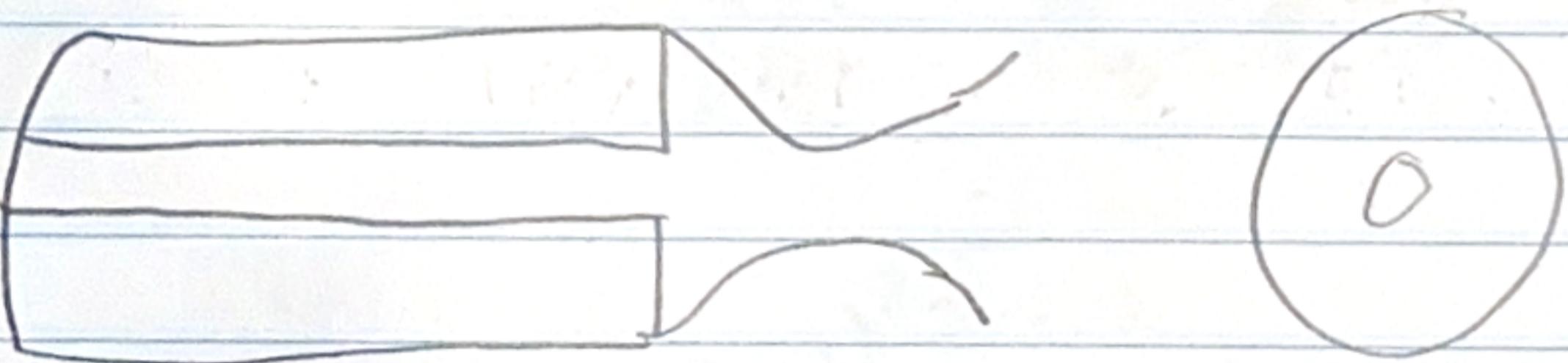
$$P_c = 14 \text{ MPa} \quad T_c = 2220 \text{ K} \quad \gamma = 1.21 \quad Z_D = 23 \frac{\text{kg}}{\text{K mol}}$$

$$r = 38 \frac{\text{mm}}{\text{s}} \quad \rho_p = 1710 \frac{\text{kg}}{\text{m}^3} \quad n = 0.3 \quad \sigma_p = 0.007 \text{ K}^{-1}$$

3 find

$$\frac{A_b}{A_t}, \alpha, \tau c_k$$

4 Schematic



5 Assumptions

Ideal rocket  
Steady state  
no thought calculations

## 6 Basic equations

$$\rho_K = \frac{\sigma_p}{1-n}$$

$$C^* = \frac{\sqrt{8RT_c}}{8\sqrt{\left[\frac{z}{8+1}\right]}}$$

$$a = \frac{r}{P_c^n}$$

$$\frac{A_b}{A_t} = \frac{P_c^{1-n}}{P_p a C^*}$$

## 7 Analysis

$$\rho_K = \frac{0.007}{K^{0.3}} = 0.023 K^{-1}$$

$$C^* = \frac{\sqrt{1.27 \cdot 8314 \text{ kg m}^2 \text{ s}^{-2} \text{ K}^{-1} \text{ mol}^{-1} \text{ kmol}}}{23 \text{ kg}} = 2220 \text{ K}$$

$$1.27 \sqrt{\left(\frac{2}{2.27}\right)^{\frac{2.27}{0.27}}}$$

$$C^* = 35 + \frac{m}{s}$$

$$a = \frac{38 \times 10^{-3} \text{ m}}{s(14 \times 10^6 \text{ Pa})^{0.3}} = 2.7 \times 10^{-4} \frac{\text{m}}{\text{s Pa}^{0.3}}$$

$$\frac{A_b}{A_t} = \frac{(14 \times 10^6)^{1-0.3} \text{ Pa}^{0.3} \cdot m^3}{1710 \text{ Kg} \cdot 2.72 \times 10^{-4} \text{ m} \cdot 1354 \text{ m}} \text{ s Pa}^{0.3}$$

$$\frac{A_b}{A_t} = 159$$

8 Answer

$$\boxed{\frac{A_b}{A_t} = 159, \alpha = 2.72 \times 10^{-4} \frac{m}{s Pa^{0.3}}, \tau_{cr} = 0.023 \frac{1}{K}}$$

9 comment

It seems the units will just work if everything is in base SI units.  
SI units are great.

**Problem SP07-A1**

1. **Name:** Nicholas Hawse
2. **Given:** Solid rocket motor with the following characteristics:

Propellant	Motor
$c^* = 5210 \text{ ft/s}$	$N = 4$ (Number of Grains)
$\gamma = 1.25$	$r_I = 1.00 \text{ in}$ (Initial Grain Radius)
$a_0 = 0.030 \left( \frac{\text{in}}{\text{s}} \right) \left[ \left( \frac{\text{lbf}}{\text{in}^2} \right)^{-n} \right]$	$r_o = 2.375 \text{ in}$ (Final Grain Radius)
$n = 0.35$	$L_0 = 8.00 \text{ in}$ (Initial Grain Length)
$\sigma_p = 0.001 /F$	$A_{t0} = 1.00 \text{ in}^2$ (Initial Throat Area)
$T_{b,0} = 70 \text{ }^\circ\text{F} (\text{ref temp})$	$\varepsilon_0 = 4.0$
$\rho_p = 0.065 \frac{\text{lbm}}{\text{in}^3}$	

**3. Find:**

- a) Equation for Area of Burn Surface,  $A_{b,i}$  as a function of web,  $w_i$
- b) Calculate Area of Burn Surface value by hand at web = 0.50 in
- c) Equation for mass of propellant,  $m_{p,i}$  as a function of web,  $w_i$
- d) Calculate mass of propellant by hand at web = 0.50 in
- e) Equation for steady state chamber pressure,  $p_{c,i}$
- f) Calculate steady state chamber pressure by hand at web = 0.50 in
- g) Calculate Vacuum Thrust Coefficient,  $c_{f,vs}$  at web = 0.50 in
- h) Calculate Vacuum Thrust,  $F_{v,i}$  at web = 0.50 in
- i) Equation for propellant burning rate  $r_{b,i}$ , including temperature sensitivity terms
- j) Calculate propellant burning rate by hand at web = 0.50 in
- k) Equation for time  $t_{i+1} - t_i$  step function of burning rate and web step ( $w_{i+1} - w_i$ )
- l) Calculate the time step by hand at web = 0.50 in
- m) Equation for total impulse as a function of  $F_{i+1}$ ,  $F_i$ ,  $t_{i+1}$ , and  $t_i$
- n) Equation for Specific Impulse,  $I_{sp}$  based on total impulse

**Summary:**

Hand Calculations of ( $w = 0.50 \text{ in.}$ , $T_b = 100 \text{ }^\circ\text{F}$ )						
$A_{b,i}$ ( $\text{in}^2$ )	$m_{p,i}$ ( $\text{lbfm}$ )	$P_{c,i}$ ( $\text{lbf/in}^2$ )	$c_{f,i}$ (-)	$r_i$ ( $\text{in/s}$ )	$F_{vac,i}$ ( $\text{lbf}$ )	$(t_{i+1} - t_i)$ sec
350	19.3	1450	1.6	0.395	2310	0.0253

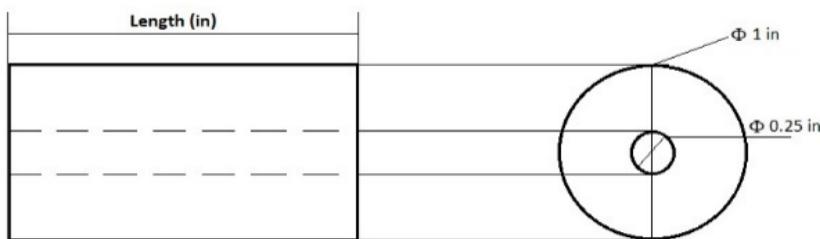
**TYPE** Final equations here in symbolic form, using symbols from the end of this document.

$$\begin{aligned}
 A_{b,i} &= -75.4w_i^2 + 101w_i + 318 \\
 m_{p,i} &= 1.63w_i^3 - 3.27w_i^2 - 20.7w_i + 30.3 \\
 p_{c,i} &= (-24.5w_i^2 + 32.8w_i + 103.4)^{1.538}
 \end{aligned}$$

$$\begin{aligned}
 c_{f,y} &= 1.6 \\
 F_{vac,i} &= 1.6(-24.5w_i^2 + 32.8w_i + 103.4)^{1.538} \\
 r_{b,i} &= 0.031(-24.5w_i^2 + 32.8w_i + 103.4)^{0.538} \\
 t_{i+1} - t_i &= \frac{w_{i+1} - w_i}{r_{b,i}} \\
 I_i &= \left(\frac{F_{i+1} + F_i}{2}\right)(t_{i+1} - t_i) \\
 I &= \sum_{i=0}^k \left(\frac{F_{i+1} + F_i}{2}\right)(t_{i+1} - t_i) \\
 I_{sp} &= \frac{I_{total}}{m_{p,i}(0)g_e}
 \end{aligned}$$

## Problem SP07-A2

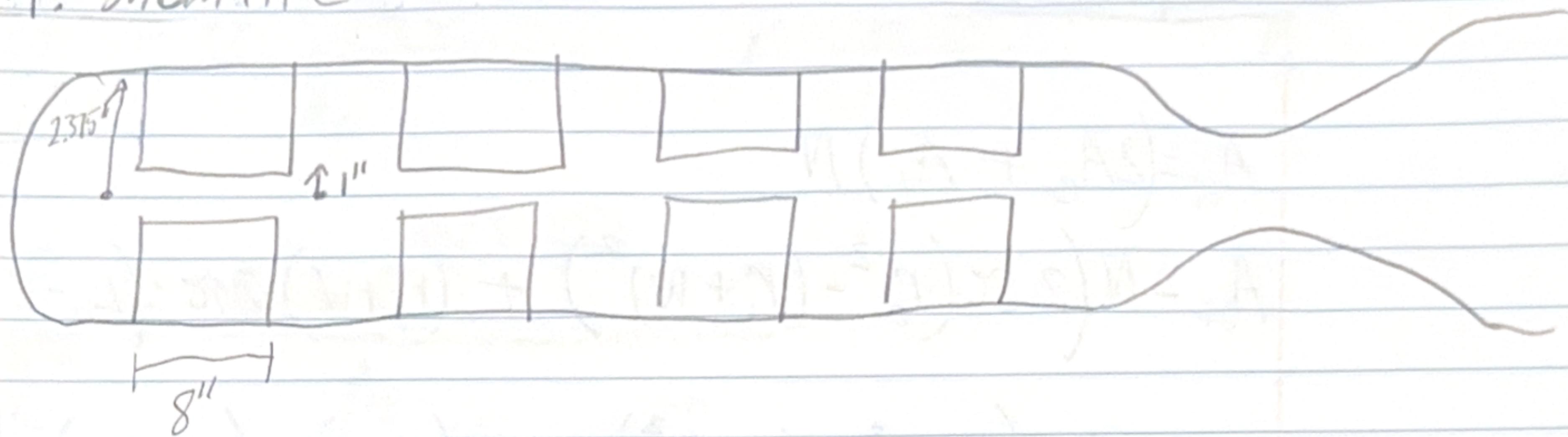
1. Name: Nicholas Hawse
2. Given: Solid propellant center perforated, cylindrical grain, Inner radius  $R_i = 0.25 \text{ in}$ , Outer radius  $R_f = 1.0 \text{ in}$ , length  $L_0 = 3.0 \text{ in}$ ,  $a_0 = 0.03 \text{ (in/s)}(\text{psi}^n)$ ,  $n = 0.35$ ,  $\sigma_p = 0.001/F$ ,  $c^* = 5210 \text{ ft/s}$ ,  $\rho_p = 0.065 \text{ lb}_m/\text{in}^3$ ,  $A_t = 0.05 \text{ in}^2$ ,  $k = 1.3$ ;  $T_{0,b} = 70F$ , area ratio  $\epsilon = 4.0$ ,  $p_a = 14.7 \text{ psia}$
3. Find:
  - a) For a grain length of 3.0 in., plot of total burn surface area as a function of web distance burned if
    1. the ends are not inhibited.
    2. Both ends are inhibited.
  - b) Repeat part (a) for a grain length of 1.0 in.
  - c) Minimum values of  $L_0$  and  $(R_f - R_i)$
4. Schematic:



5. Assumptions:
  - Assume  $T_b = T_{bo} = 70 \text{ }^\circ\text{F}$
  - Steady state
  - Instant flame spread

# SP07-A1

## 4. Schematic



## 5 Assumptions

Ideal rocket

Steady State

No friction/erosion

## 6 Basic equations

$$A_c = \pi r^2 \quad A_d = 2\pi r L$$

$$\dot{m} = \frac{P_0 A_t}{C^*} = \rho_p r A_b \quad r = a_0 e^{(\sigma_p (T_b - T_{b0})) / P_c^n}$$

$$P_c = \frac{\rho_p r_i A_b C^*}{A_t}$$

$$\frac{P_e}{P_c} = \left( 1 + \frac{\gamma-1}{2} M^2 \right)^{\frac{\gamma+1}{\gamma}}$$

$$C_{f,v} = \left[ \frac{2\gamma^2}{\gamma-1} \left( \frac{2}{\gamma+1} \right)^{\frac{\gamma+1}{\gamma-1}} \left( 1 - \left( \frac{P_e}{P_c} \right)^{\frac{\gamma-1}{\gamma}} \right) \right] + \left( \frac{P_e}{P_c} \right) \epsilon$$

$$\epsilon = \frac{1}{M} \left( \frac{2 + (\gamma-1)M^2}{\gamma+1} \right)^{\frac{1}{2(\gamma-1)}}$$

## 7 Analysis

$$A_{bi} = (2A_e + A_L)N$$

$$A_{bi} = N \left( 2\pi(r_o^2 - (r_i + w)^2) + (r_i + w) \cdot 2\pi \cdot (L_o - 2w) \right)$$

$$A_{bi} = 8\pi \left( 2.375^2 - (1+w)^2 \right) + 8\pi(1+w) \cdot (8-2w)$$

$$= 8\pi(5.64) - 8\pi(1+2w+w^2) + 8\pi(8-2w+8w-2w^2)$$

$$= 8\pi(5.64 - 1+2w+w^2 + 8-2w+8w-2w^2)$$

a) 
$$= -75.4w^2 + 101w + 318$$

b)

$$-75.4(0.5)^2 + 101(0.5) + 318 = 350 \text{ in}^2$$

$$m_p = \rho_p V$$

$$V = N \cdot L \cdot A_e = (8-2w) \cdot 4 \cdot \pi(2.375^2 - (1+w)^2)$$

$$m_p = 0.065 \frac{\text{lbm}}{\text{in}^3} \cdot 4 \cdot (8-2w) \cdot \pi \cdot (2.375^2 - 1-2w-w^2)$$

c) 
$$m_p = 1.63w^3 - 3.27w^2 - 20.7w + 30.3$$

$$m_{p,0.5} = 1.63(0.5^3) - 3.27(0.5^2) - 20.7(0.5) + 30.3$$

d) 
$$m_p = 19.3 \text{ lbm}$$

$$P_c = \frac{S_p r_i A_b C^*}{A_t} \quad r_i = a_0 e^{\frac{(S_p(T_b - T_{b0}))}{P_c^n}}$$

$$\frac{P_c}{P_c^n} = \frac{S_p a_0 C}{A_t} e^{\frac{S_p(T_b - T_{b0})}{A_b C^*}}$$

$$P_c^{1-n} = \frac{0.065 \cdot 0.03 e^{\frac{1bf}{in^3 \cdot 0.001(100°F - 70°F)}}}{\frac{(-75.4W^2 + 101W + 318) \cdot 5210ft}{in^2 \cdot 1.00in^2 s \cdot 32.2}}$$

$$\frac{lbm \cdot in \cdot (psi)^{-n} \cdot in^2 \cdot ft \cdot s \cdot 1bf}{in^3 \cdot in^2 \cdot s \cdot 32.2 \cdot ft \cdot lbm}$$

$$P_c = (-24.5W^2 + 32.8W + 103.4) \quad | \text{e)}$$

$$P_{c,0.5} = 1450 \text{ psi} \quad | \text{f)}$$

$$M = f(\varepsilon, \gamma) = 2.7$$

$$\frac{P_c}{P_e} = \left(1 + \frac{0.25}{2} (2.7)^2\right) = 0.0395$$

$$C_{f,V} = \left[ \frac{2 \cdot 1.25^2}{0.25} \left( \frac{2}{2.25} \right)^{\frac{2.25}{0.25}} \left( 1 - \left( \frac{1}{1.13} \right)^{\frac{0.25}{1.25}} \right) \right]^{0.5} + \left( \frac{1}{1.13} \right) (4)$$

g)  $C_{f,V} = 1.6$

$$F_{0.5} = 1.6 \cdot 1450 \cdot 1 =$$

b)  $F_{0.5} = 2310 \text{ lbf}$

$$r_{b_i} = 0.03 e^{\left( \frac{0.03}{(-24.5W^2 + 32.8W + 103.4)} \right)^{1.538} 0.35}$$

i)  $r_{b_i} = 0.03 \left( -24.5W^2 + 32.8W + 103.4 \right)^{0.538}$

j)  $r_{b_i, 0.5} = 0.395$

k)  $\Delta t = \frac{W_{i+1} - W_i}{r_i} \quad t = \frac{d}{V}$

$$\Delta W = 0.01$$

$$\Delta t = 0.01$$

$$0.031(-24.5(0.5)^2 + 32.8(0.5) + 103.4)^{0.538}$$

D)  $\boxed{\Delta t_{0.5} = 0.0253 \text{ s}}$

$$I = F \cdot t =$$

M)  $I = \sum_{i=0}^n \left( \frac{F_{i+1} + F_i}{2} \right) (t_{i+1} - t_i)$

N)  $\boxed{I_{sp} = \frac{I}{m_p(0) g_e}}$

Comment

It seems like this is a process best done only once. It has taken over 3 hours to complete.

## 6 Basic Equations

$$A = \pi r^2 \quad A = 2\pi r L$$

### Analysis

$$1) A = 2\pi \left( R_f^2 - (R_i + w)^2 \right) + 2\pi (R_i + w)(L_o - 2w)$$

$$2) A = 2\pi (R_i + w)(L_o - 2w)$$

$$1) A = 2\pi \left( 1 - (0.25 + w)^2 \right) + 2\pi (0.25 + w)(3 - 2w)$$

$$2) A = 2\pi (0.25 + w)(3 - 2w)$$

$$0.25 + w \leq 1 \quad 0 \leq 3 - 2w$$

$$w \leq 0.75$$

$$-3 \leq -2w \quad w \leq \frac{3}{2} = 1.5$$

$$0 \leq 1 - 2w$$

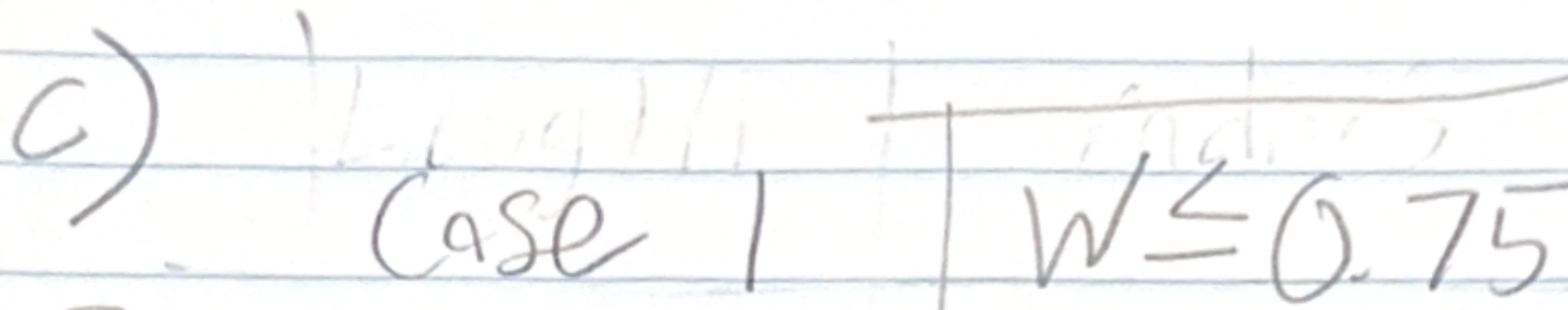
$$-1 \leq -2w$$

$$w \leq \frac{1}{2}$$

## 8 Answers

a) See Plots below

b) See Plots below

c)   
Case 1       $W \leq 0.75$   
Case 2       $W \leq 1.5$

$L_0 = 3$       Case 2       $W \leq 1.5$

$L_0 = 1$       Case 1       $W \leq 0.75$   
Case 2       $W \leq 0.5$

## 9 comment

It seems that it is necessary to check the web distance carefully before using it to find area.

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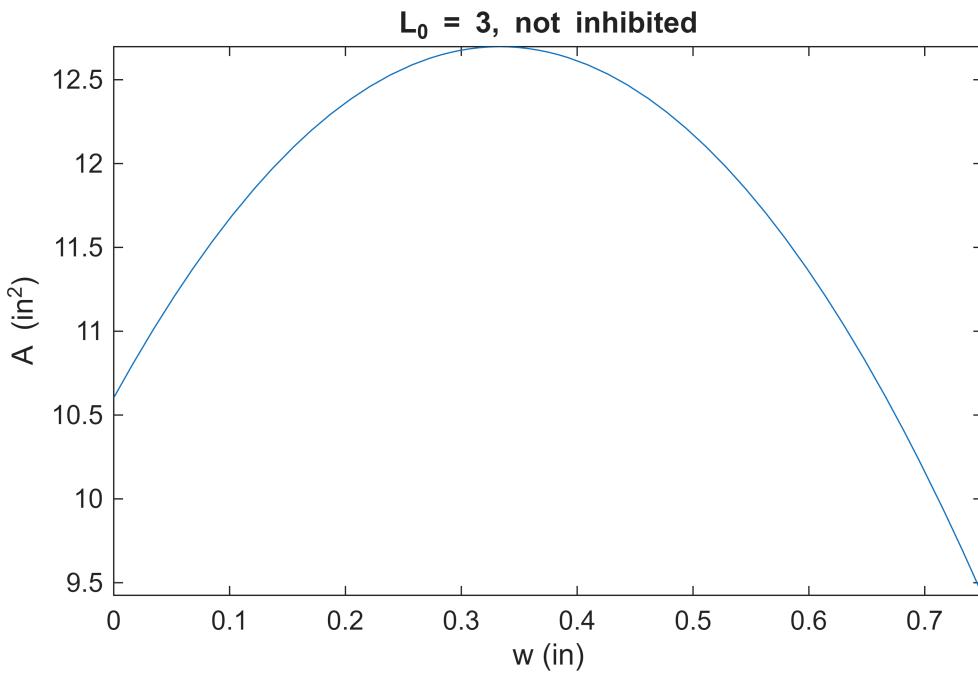
clear; clc; close all; clf;

r_f = 1;
r_i = 0.25;
l_0 = 3;

A_1 = @(w) 2*pi*( r_f^2 - (r_i+w).^2 + (r_i+w).*(l_0 - 2.*w));
A_2 = @(w) 2*pi.*(r_i+w).*(l_0 - 2.*w);

fplot(A_1,[0 0.75])
xlabel('w (in)')
ylabel('A (in^2)')
title('L_0 = 3, not inhibited')

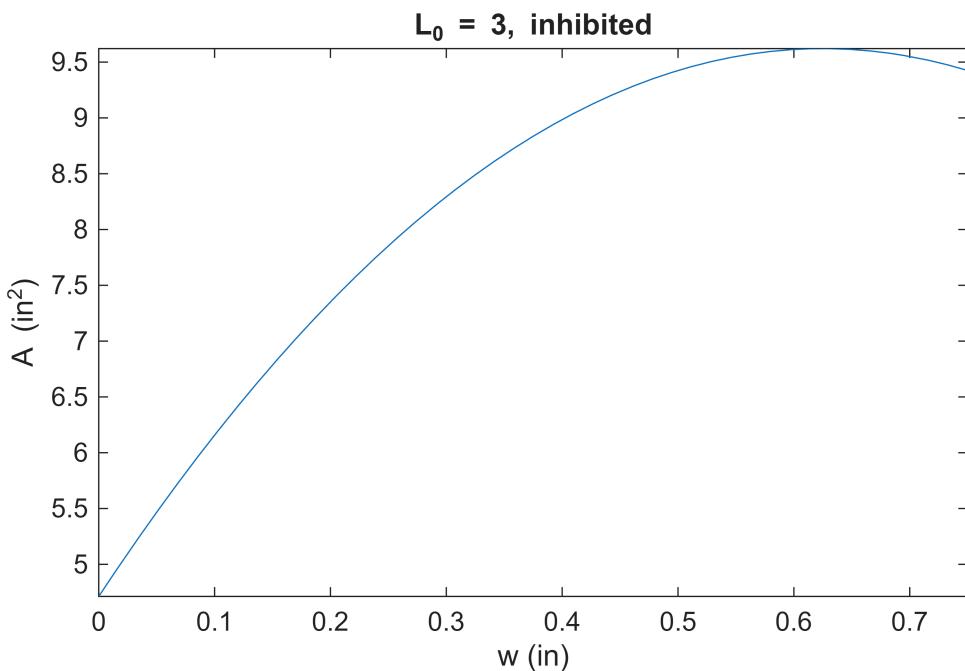
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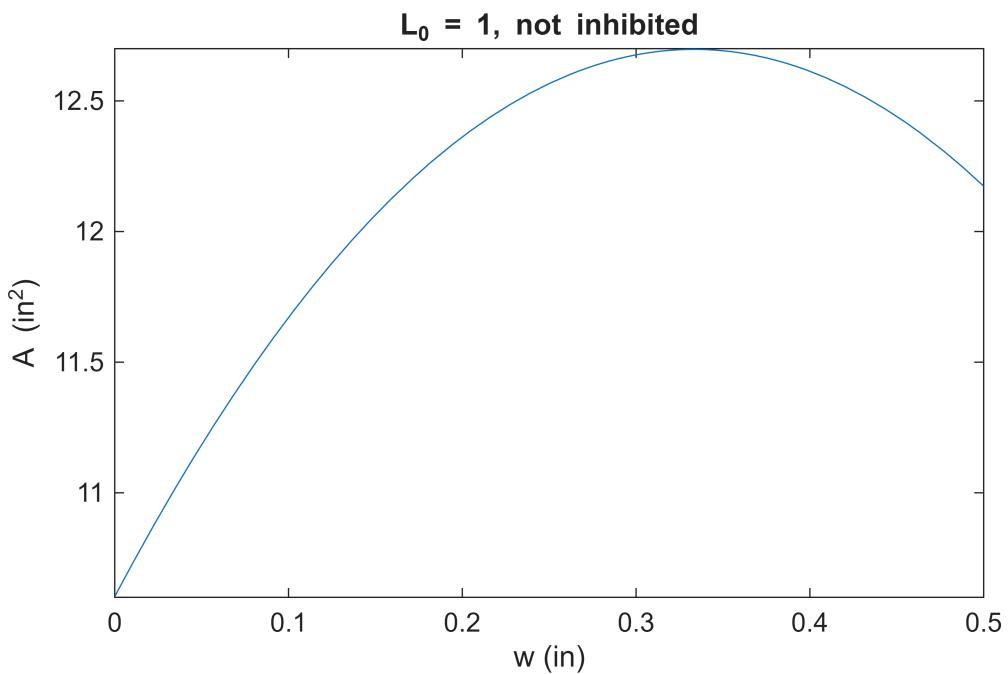
fplot(A_2,[0 0.75])
xlabel('w (in)')
ylabel('A (in^2)')
title('L_0 = 3, inhibited')

```



```
l_θ = 1;
```

```
fplot(A_1,[0 0.5])
xlabel('w (in)')
ylabel('A (in^2)')
title('L_θ = 1, not inhibited')
```



```
fplot(A_2,[0 0.75])
```

```
xlabel('w (in)')
ylabel('A (in^2)')
title('L_0 = 1, inhibited')
```

