ASEN2003 Review Lectures C1 and C2

Control Systems

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Laplace Transform of 2nd Order ODEs

• The standard 2nd order form is:

$$\ddot{x}(t) + 2\zeta\omega_n\dot{x}(t) + \omega_n^2x(t) = \omega_n^2u(t)$$

• Taking the Laplace Transform of our standard form equation:

$$L\left[\ddot{x}(t) + 2\zeta\omega_n\dot{x}(t) + \omega_n^2x(t)\right] = L\left[\omega_n^2u(t)\right]$$

$$\left[s^2 X(s) - sx(0) - \dot{x}(0) \right] + 2\zeta \omega_n \left[sX(s) - x(0) \right] + \omega_n^2 X(s) = \omega_n^2 U(s)$$

$$\left[s^2 + 2\zeta\omega_n s + \omega_n^2 \right] X(s) = \omega_n^2 U(s) + \left[s + 2\zeta\omega_n \right] x(0) + \dot{x}(0)$$

• If we assume that the initial conditions are zero (system starts at rest):

$$\left[s^2 + 2\zeta \omega_n s + \omega_n^2 \right] X(s) = \omega_n^2 U(s)$$

Laplace Transform of 2nd Order ODEs

• Therefore,

$$X(s) = \frac{\omega_n^2}{\left(s^2 + 2\zeta\omega_n s + \omega_n^2\right)} U(s) = G(s)U(s)$$

• Where G(s) is the *Transfer Function*:

$$G(s) = \frac{X(s)}{U(s)} = \frac{\omega_n^2}{\left(s^2 + 2\zeta\omega_n s + \omega_n^2\right)}$$

• So, knowing the control u(t), we can compute its Laplace Transform U(s), and then convolve that with G(s) to get X(s). Then we simply compute the inverse Laplace Transform:

$$x(t) = L^{-1} \lceil X(s) \rceil = L^{-1} \lceil G(s)U(s) \rceil$$

A General 2nd Order System with PD Control

A general *PD control* can be written as:

$$u = -K_P(x - x_R) - K_D(\dot{x} - \dot{x}_R)$$

where we are driving $x \Rightarrow x_R$ and $\dot{x} \Rightarrow \dot{x}_R$. The Laplace Transform of u is:

$$U(s) = -K_{P}(X - X_{R}) - sK_{D}(X - X_{R})$$

But we still need to decide what this control looks like in the time domain (step, ramp, etc.). For example, for a step function in the time domain, the LT of a step function is 1/s, so we need to multiply U(s) above by 1/s.

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Rigid Arm Dynamics

• The torque or moment produced by the output shaft is what drives the arm, governed by Newton's equations. The angle of the arm (or output shaft) is denoted by, θ_L . The first derivative of θ_L is the speed of the output shaft, ω_L . The second derivative of θ_L is the angular acceleration of the load. The equation of motion is determined by summing the moments about the (fixed) output shaft as follows:

$$J\ddot{\theta}_L + B\dot{\theta}_L + M_L = M_o$$

• Now substituting for the torque exerted by the shaft:

$$J\ddot{\theta}_{L} + B\dot{\theta}_{L} + M_{L} = \frac{K_{g}K_{m}}{R_{m}} \left(V_{in} - K_{g}K_{m}\omega_{L}\right)$$

$$\ddot{\boldsymbol{\theta}}_{L} + \left(\frac{B}{J} + \frac{K_{g}^{2}K_{m}^{2}}{JR_{m}}\right)\dot{\boldsymbol{\theta}}_{L} = \frac{K_{g}K_{m}}{JR_{m}}V_{in} - \frac{M_{L}}{J}$$

Rigid Arm Dynamics

• Ignoring friction and assume no disturbances ($M_L = 0$):

$$\ddot{\boldsymbol{\Theta}}_{L} + \left(\frac{K_{g}^{2}K_{m}^{2}}{JR_{m}}\right)\dot{\boldsymbol{\Theta}}_{L} = \frac{K_{g}K_{m}}{JR_{m}}V_{in}$$

• Taking the Laplace Transform:

$$s^{2}\Theta_{L} + s\left(\frac{K_{g}^{2}K_{m}^{2}}{JR_{m}}\right)\Theta_{L} = \frac{K_{g}K_{m}}{JR_{m}}\mathbf{V}_{in}$$

• Which gives the open loop transfer function, G(s), between $V_{\rm in}$ and position of the arm:

$$G(s) = \frac{\Theta_L}{V_{in}} = \frac{K_g K_m / JR_m}{s(s + K_g^2 K_m^2 / JR_m)}$$

Rigid Arm Control

• Now introduce our PD control:

$$V_{in} = K_p \left(\theta_D - \theta_L \right) + K_d \left(\dot{\theta}_D - \dot{\theta}_L \right)$$

• Its Laplace Transform is (assuming we are driving rate to zero):

$$V_{in} = V_{PD} = K_p \left(\Theta_D - \Theta_L\right) - sK_d\Theta_L$$

• Substituting into our Open Loop transfer function and solving for the closed loop transfer function:

$$\overline{G}(s) = \frac{\Theta_{L}}{\Theta_{D}} = \frac{K_{p}K_{g}K_{m}/JR_{m}}{s^{2} + \left(K_{g}^{2}K_{m}^{2}/JR_{m} + K_{d}K_{g}K_{m}/JR_{m}\right)s + K_{p}K_{g}K_{m}/JR_{m}}$$

$$\omega_{n}^{2} = \frac{K_{p}K_{g}K_{m}}{JR_{m}} \qquad \zeta = \frac{K_{g}^{2}K_{m}^{2} + K_{d}K_{g}K_{m}}{2\sqrt{K_{p}K_{g}K_{m}}JR_{m}}$$

Rigid Arm Control

- We still need to implement this transfer function to control the arm: $\Theta_{I}(s) = \overline{G}(s)\Theta_{D}(s)$
- We need to specify what $\Theta_R(s)$ looks like (ramp, step, etc.). For example, if it is a step function, then:

$$\Theta_D(s) = \Theta_D \frac{1}{s}$$

• And then we can get x(t) through the inverse LT:

$$x(t) = L^{-1} \left| \overline{G}(s) \frac{\Theta_D}{s} \right|$$

• The step function gets implemented through Matlab using the **tf** and **step** functions – see the lab document for sample code.