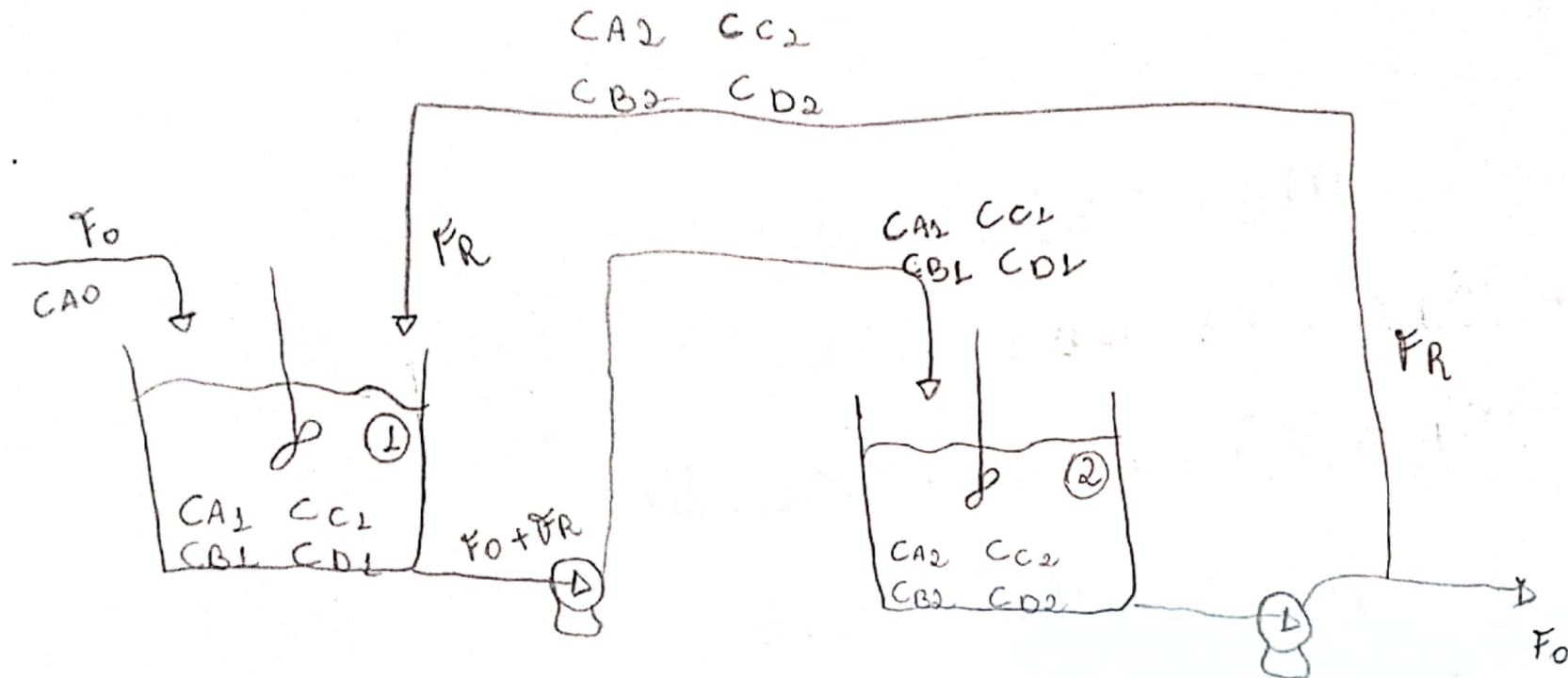


lista 01

2.



→ hipóteses:

H_1 : mistura perfeita

H_2 : isotérmica.

H_3 : Cilindro perfeito

H_4 : propriedades físicas constantes.

H_5 : Volume constante. ($V_S = F_0 + F_R$)

1. $V \cdot D \cdot \rho = \text{massa}$

2. $V \cdot C = \text{Reator 01 e Reator 02}$

3. $V \cdot E :$

→ Para o reator 01:

Componente A:

acúmulo: $m_A = C_{A1} \cdot V \cdot M_{MA}$

entra: $m_{Ae} = F_0 \cdot C_{A0} \cdot M_{MA} \cdot \Delta t + F_R \cdot C_{A2} \cdot M_{MA} \cdot \Delta t$

saí: $m_{As} = F_S \cdot C_{A1} \cdot M_{MA} \cdot \Delta t$

Reage: $m_{AR} = R_A \cdot V \cdot M_{MA} \cdot \Delta t$

Componente B:

acúmulo: $m_B = C_{B1} \cdot V \cdot M_{MB}$

entra: $m_{Be} = F_R \cdot C_{B2} \cdot M_{MB} \cdot \Delta t$

saí: $m_{Bs} = F_S \cdot C_{B1} \cdot M_{MB} \cdot \Delta t$

Reage: $m_{Reage} = R_B \cdot V \cdot M_{MB} \cdot \Delta t$

Componente C:

acúmulo: $m_C = C_{C1} \cdot V \cdot M_{MC}$

entra: $m_{Ce} = F_R \cdot C_{C2} \cdot M_{MC} \cdot \Delta t$

saí: $m_{Cs} = F_S \cdot C_{C1} \cdot M_{MC} \cdot \Delta t$

Reage: $m_{Reage} = R_C \cdot V \cdot M_{MC} \cdot \Delta t$

Componente D :

Acúmulo : $m_D = C_{D1} \cdot V \cdot MM_D$

entra : $m_{De} = F_R \cdot C_{D2} \cdot MM_D \cdot \Delta t$

sai : $m_{Ds} = F_S \cdot C_{D1} \cdot MM_D \cdot \Delta t$

Reage : $M_{reage} = R_D \cdot V \cdot MM_D \cdot \Delta t$

4- Conservação de massa:

$$m_{T+\Delta T} = m_T + m_e(T \rightarrow \Delta T) - m_s(T \rightarrow \Delta T)$$

→ Componente A:

$$\begin{aligned} C_{A1} \cdot V \cdot M_{MA}|_{T+\Delta T} &= C_{A1} \cdot V \cdot M_{MA}|_T + F_0 C_{A0} M_{MA} \cdot \Delta T \\ &+ F_R \cdot C_{A2} M_{MA} \cdot \Delta T - F_S C_{A1} M_{MA} \cdot \Delta T \\ &+ R_A \cdot V \cdot M_{MA} \cdot \Delta T \quad \quad \quad \cdot \Delta T \end{aligned}$$

$$\lim_{\Delta T \rightarrow 0} \left(\frac{C_{A1} \cdot V|_{T+\Delta T} - C_{A1} \cdot V|_T}{\Delta T} \right) = F_0 C_{A0} + F_R \cdot C_{A2} - F_S C_{A1} + R_A V$$

$$\frac{d(C_{A1} \cdot V)}{dT} = F_0 C_{A0} + F_R \cdot C_{A2} - F_S C_{A1} + R_A V$$

$$\cancel{V} \frac{dC_{A1}}{dT} + C_{A1} \left(\frac{dV}{dT} \right)^{\overset{0}{\text{constante}}} = \frac{F_0 C_{A0} + F_R \cdot C_{A2} - F_S C_{A1} + R_A V}{V}$$

$$\frac{dC_{A1}}{dT} = \frac{F_0 C_{A0} + F_R \cdot C_{A2} - F_S C_{A1}}{V} + R_A$$

Componente B:

$$C_{B1} \cdot V \cdot M_B |_{t+\Delta t} - C_{B1} \cdot V \cdot M_B |_t = F_R \cdot C_{B2} \cdot M_B \cdot \Delta t \\ - F_S C_{B1} M_B \cdot \Delta t + R_B \cdot V \cdot M_B \Delta t$$

$$\lim_{\Delta t \rightarrow 0} \left(\frac{C_{B1} \cdot V \cdot |_{t+\Delta t} - C_{B1} \cdot V |_t}{\Delta t} \right) = F_R \cdot C_{B2} - F_S C_{B1} + R_B \cdot V$$

$$\frac{d(C_{B1} \cdot V)}{dt} = F_R \cdot C_{B2} - F_S C_{B1} + R_B \cdot V$$

$$V \cdot \frac{d(C_{B1})}{dt} + C_{B1} \left(\frac{dV}{dt} \right)^0 = F_R C_{B2} - F_S C_{B1} + R_B \cdot V$$

$$\frac{d(C_{B1})}{dt} = \frac{F_R C_{B2} - F_S C_{B1} + R_B \cdot V}{V}$$

Componente C:

$$\lim_{\Delta y \rightarrow 0} \left(\frac{C_{c1} \cdot V \cdot \text{MMC}|_{y+\Delta y} - C_{c1} \cdot V \cdot \text{MMC}|_y}{\Delta y} \right)$$

$$= F_R \cdot C_{c2} \cdot \text{MMC} - F_S C_{c1} \cdot \text{MMC} + R_c \cdot V \cdot \text{MMC}$$

$$\frac{d(C_{c1} \cdot V)}{dy} = F_R \cdot C_{c2} - F_S C_{c1} + R_c \cdot V$$

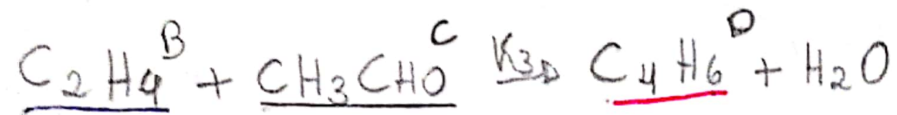
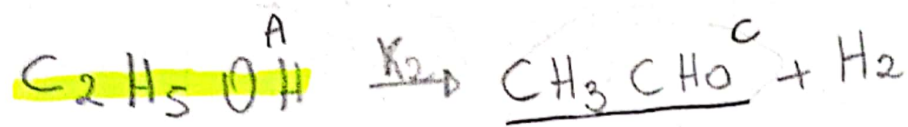
$$C_{c1} \frac{dV}{dy} + V \frac{d(C_{c1})}{dy} = F_R \cdot C_{c2} - F_S C_{c1} + R_c V$$

$$\frac{d(C_{c1})}{dy} = \frac{F_R \cdot C_{c2} - F_S C_{c1}}{V} + R_c$$

Conservação de massa:

$$\frac{d(C_{D1})}{dt} = \frac{F_R \cdot C_{D2} - F_S C_{D1} + R_D}{V}$$

Analyse das Taxes:



$$\left\{ \begin{array}{l} - R_A = K_1 C_A + K_2 C_A \\ - R_B = K_3 C_B C_C - K_1 C_A \\ - R_C = K_3 C_B C_C - K_2 C_A \\ R_D = + K_3 C_B C_C \end{array} \right.$$

→ Resultados das Taxas:

$$\frac{d(C_{A1})}{dt} = \frac{F_0 C_{A0} + F_R \cdot C_{A2} - F_S C_{A1}}{A_1 \cdot h_1} - K_1 C_{A1} - K_2 C_{A1}$$

$$\frac{d(C_{B1})}{dt} = \frac{F_R C_{B2} - F_S C_{B1}}{A_1 \cdot h_1} - K_3 C_{B1} C_C + K_1 C_{A1}$$

$$\frac{d(C_{C1})}{dt} = \frac{F_R C_{C2} - F_S C_{C1}}{A_1 \cdot h_1} - K_3 C_{B1} C_{C1} + K_2 C_{A1}$$

$$\frac{d(C_{D1})}{dt} = \frac{F_R C_{D2} - F_S C_{D1}}{A_1 \cdot h_1} + K_3 C_{B1} C_{C1}$$

Reator 02:

Componente A:

Acúmulo: $m_A = C_{A2} \cdot V \cdot MMA$

entra: $m_{Ae} = F_S \cdot C_{A1} \cdot MMA \cdot \Delta t$

sai: $m_{As} = F_S \cdot C_{A2} \cdot MMA \cdot \Delta t$

Reage: $m_{AR} = R_A \cdot V \cdot MMA \cdot \Delta t$

Componente B:

$$\text{acúmulo: } C_{B2} \cdot V \cdot M_{MB}$$

$$\text{entra: } F_s \cdot C_{B1} \cdot M_{MB} \cdot \Delta T$$

$$\text{saí: } F_s \cdot C_{B2} \cdot M_{MB} \cdot \Delta T$$

$$\text{Reage: } R_B \cdot V \cdot M_{MB} \cdot \Delta T$$

Componente C:

$$\text{acúmulo: } m_C = C_{C2} \cdot V \cdot M_{MC}$$

$$\text{entra: } m_{Ce} = F_s C_{C1} \cdot M_{MC} \cdot \Delta T$$

$$\text{saí: } m_{Cs} = F_s \cdot C_{C2} \cdot M_{MC} \cdot \Delta T$$

$$\text{Reage: } m_{CR} = R_C \cdot V \cdot M_{MC} \cdot \Delta T$$

Componente D:

$$\text{acúmulo: } m_D = C_{D2} \cdot V \cdot M_{MD}$$

$$\text{entra: } m_{De} = F_s \cdot C_{D1} \cdot M_{MD} \cdot \Delta T$$

$$\text{saí: } m_{Ds} = F_s \cdot C_{D2} \cdot M_{MD} \cdot \Delta T$$

$$\text{Reage: } m_{DR} = R_D \cdot V \cdot M_{MD} \cdot \Delta T$$

9- Con conservação de massa:

$$m_{T+\Delta T} = m_T + m_e (T \rightarrow T+\Delta T) - m_s (T \rightarrow T+\Delta T)$$

Componente B:

$$C_{B2} V \cdot \cancel{MM_B} \Big|_{T+\Delta T} - C_{B2} \cdot V \cdot \cancel{MM_B} \Big|_T = F_S C_{B1} \cdot \cancel{MM_B} \Delta T - F_S C_{B2} \cdot \cancel{MM_B} \cdot \Delta T + R_B \cdot V \cdot \cancel{MM_B} \cdot \Delta T \quad \div \Delta T$$

$$\lim_{\Delta T \rightarrow 0} \left(\frac{C_{B2} V \cdot \cancel{MM_B} \Big|_{T+\Delta T} - C_{B2} \cdot V \cdot \cancel{MM_B} \Big|_T}{\Delta T} \right) = F_S (C_{B1} - C_{B2}) + R_B \cdot V$$

$$\frac{d(C_{B2} V)}{dT} = F_S (C_{B1} - C_{B2}) + R_B \cdot V$$

$$C_{B2} \frac{dV}{dT} + \frac{d(C_{B2})}{dT} V = F_S (C_{B1} - C_{B2}) + R_B \cdot V$$

$$\frac{d(C_{B2})}{dT} = \frac{F_S}{V} (C_{B1} - C_{B2}) + R_B$$

H₃:

$$\frac{d(C_{B2})}{dT} = \frac{F_S}{A_2 h_2} (C_{B1} - C_{B2}) - K_3 C_{B1} C_{C2} + K_2 C_{A2}$$

Analogamente, fica:

$$\frac{d(C_{A2})}{d\tau} = \frac{F_S}{A_2 h_2} (C_{A1} - C_{A2}) - K_1 C_{A2} - K_2 C_{A2}$$

$$\frac{d(C_{C2})}{d\tau} = \frac{F_S}{A_2 h_2} (C_{C1} - C_{C2}) - K_3 C_{B2} C_{C2} + K_2 C_{A2}$$

$$\frac{d(C_{D2})}{d\tau} = \frac{F_S}{A_2 h_2} (C_{D1} - C_{D2}) + K_3 C_{B2} C_{C2}$$

→ Análise de graus de liberdade:

n° variáveis: $h_1, h_2, A_1, A_2, F_0, F_R, C_{A1}, C_{A2}, C_{A0},$
 $C_{B1}, C_{B2}, C_{C1}, C_{C2}, C_{D1}, C_{D2}, K_1, K_2,$
 $K_3 = 18$

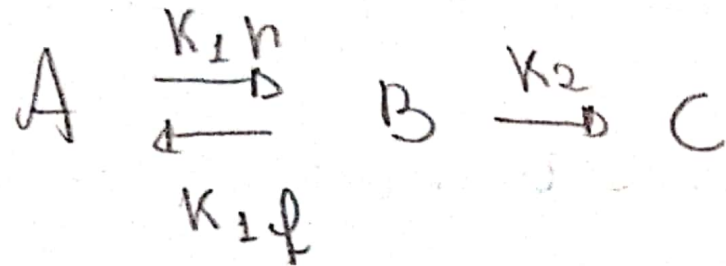
n° variáveis conhecidas: $A_1, A_2, K_1, K_2, K_3 = 5$

n° de equações: 8

$$IF = 18 - 5 - 8 = 5$$

$(F_0, F_R, C_{A0}, C_{A2}, C_{B2})$

Ex 01 -



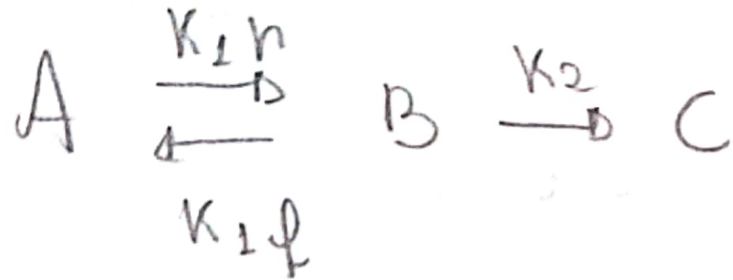
Rates :

$$- R_A = k_{1h} C_A - k_{1f} C_B$$

$$- R_B = R_A + k_2 C_B$$

$$R_C = k_2 C_B$$

Ex 01 -

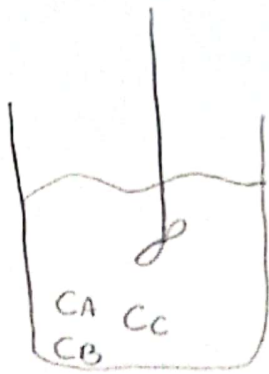


Rates :

$$- R_A = k_{1h} C_A - k_{1f} C_B$$

$$- R_B = R_A + k_2 C_B$$

$$R_C = k_2 C_B$$



H₁: cilindro perfeito

H₂: isotérmica

H₃: não tem fluxo de entrada e de saída.

1 - V.D.F = massa

2 - V.C = Reator

3 - V.E = massa

i) B.M.G

acúmulo: $m = \rho \cdot V$

entra: 0

sai: 0

ii) B.M.C.

Componente A

Acúmulo: $m_A = C_A \cdot V \cdot M_{MA}$

Reage: $m_{A \text{ Reage}} = R_A \cdot V \cdot M_{MA} \cdot \Delta t$

Componente B:

Acúmulo: $m_B = C_B \cdot V \cdot M_{MB}$

Reage: $m_{B \text{ Reage}} = R_B \cdot V \cdot M_{MB} \cdot \Delta t$

Componente C:

$$\text{acúmulo: } m_C = C_C \cdot V \cdot \Delta t$$

$$\text{reage: } m_{CR} = R_C \cdot V \cdot \Delta t$$

4- conservação de massa:

→ comp A:

$$\lim_{\Delta t \rightarrow 0} \left(\frac{C_A V|_{t+\Delta t} - C_A V|_t}{\Delta t} \right) = R_A \cdot V$$

$$\frac{d(C_A V)}{dt} = R_A \cdot V$$

$$\cancel{V} \frac{d(C_A)}{dt} + C_A \cdot \cancel{\frac{dV}{dt}} \overset{\text{vol. constante}}{=} 0 = R_A \cdot \cancel{V}$$

$$\frac{dC_A}{dt} = R_A$$

Assim,

$$\frac{dC_B}{dt} = R_B \quad ; \quad \frac{dC_C}{dt} = R_C$$

Para Taxa A:

$$\frac{dC_A}{dt} = -K_1 n C_A + K_1 f C_B$$

Para a Taxa B:

$$\frac{dC_B}{dt} = K_1 n C_A - K_1 f C_B - K_2 C_B$$

Para a Taxa C:

$$\frac{dC_C}{dt} = K_2 C_B$$