## TECHNICAL UNIVERSITY OF DENMARK

41525 Finite Element Methods



# Matlab Codes Assignment 1

TEAM 26 - LION

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## 1 Exercise 1

## 1.1 Input file

This is the file used to load the structure

```
% Created with:
                     FlExtract v1.13
% Element type: truss
% Number of nodes: 19
% Number of elements: 34
clear all;
% Node coordinates: x, y
X = [
0 0
0
    0.5
0.5 0
0.5 0.5
1 0
1
    0.5
1.5 0
1.5 0.5
1.5 1
2
    0
2
    0.5
2.5 0
2.5 0.5
3
    0
3
    0.5
3.5 0
3.5 0.5
    0
4
4
    0.5
];
% Element connectivity: node1_id, node2_id, material_id
2
3
   1
4
    2
         1
    2
3
         1
    3
4
         1
5
    3
         1
6
    4
         1
5
    4
         1
6
    5
         1
7
    5
         1
8
    6
         1
7
    6
    7
8
         1
    7
10
         1
    8
11
         1
10
    8
         1
11
    9
         1
    10
11
         1
12
    10
         1
13
    11
         1
12
    11
         1
13
    12
14
    12
        1
15
    13
14
    13
        1
```

```
15
   14 1
16
   14 1
17
    15
        1
16
    15
        1
17
       1
    16
18
    16
       1
19
    17
        1
        1
18
    17
19
    18
];
% Element properties: Young's modulus, area
mprop = [
7e+010 0.0002
];
% Nodal diplacements: node_id, degree of freedom (1 - x, 2 - y), displacement
bound = [
  1
2
2 2
9 1 0
9 2 0
];
% Nodal loads: node_id, degree of freedom (1 - x, 2 - y), load
loads = [
18 2 -15000
];
% Control parameters
plotdof = 2;
```

## 1.2 File performing the thrust analysis

```
Basis truss program
function fea()
close all
clc
%--- Input file ------%
%example1
                 % Input file
TrussExercise1
ne = size(IX,1);
                          % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
   ' Number of elements ' sprintf('%d',ne)]);
%--- Initialize arrays ------%
Kmatr=sparse(neqn,neqn);
                      % Stiffness matrix
P=zeros(neqn,1);
                            % Force vector
D=zeros(negn,1);
                             % Displacement vector
R=zeros(neqn,1);
                             % Residual vector
strain=zeros(ne,1);
                            % Element strain vector
stress=zeros(ne,1);
                             % Element stress vector
%--- Calculate displacements -----%
[P]=buildload(X,IX,ne,P,loads,mprop); % Build global load vector
[Kmatr] = buildstiff(X,IX,ne,mprop,Kmatr);
                               % Build global stiffness matrix
D = Kmatr \ Pmatr;
                                % Solve system of equations
[strain, stress] = recover(mprop, X, IX, D, ne, strain, stress); % Calculate element
                                         % stress and strain
% Calculate element axial forces and the support reactions
[strain, stress, N, R] = recover2(mprop, X, IX, D, ne, strain, stress, P);
%--- Print the results on the command window ------%
% External matrix
disp('External forces applied (N)')
p,
% Stress
disp('Stress on the bars (MPa)')
stress'
% Displacement
disp('Displacement (m)')
% Strain
disp('Strain of the bars')
strain'
% Forces on the bars
```

```
disp('Internal forces on the bar (N)')
% Support reaction
disp('Support reactions forces (N)')
%--- Plot results ------%
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K] = buildstiff(X,IX,ne,mprop,K);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 % element stiffness matrix
 k_e = E * A * L0 * B0 * B0'; % 4x4 matrix
 % vector of index used for building K
 [edof] = build_edof(IX, e);
 % build K by summing k_e
 for ii = 1:4
  for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
```

```
end
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
function [strain,stress] = recover(mprop, X, IX, D, ne, strain, stress);
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
% allocate memory for stress and strain vectors
strain = zeros(ne, 1);
stress = zeros(ne, 1);
for e=1:ne
 d = zeros(4, 1); % allocate memory for element stiffness matrix
[edof] = build_edof(IX, e); % index for buildg K
 % build the matrix d from D
 for i = 1:4
  d(i) = D(edof(i));
 end
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 strain(e) = B0' * d;
 stress(e) = strain(e) * E;
```

end

```
return
```

```
function [strain, stress, N, R] = recover2(mprop, X, IX, D, ne, strain, stress, P);
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
strain = zeros(ne, 1);
stress = zeros(ne, 1);
B0_sum = zeros(2*size(X,1), 1);
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 for i = 1:4
   d(i) = D(edof(i));
 end
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 strain(e) = B0' * d;
 stress(e) = strain(e) * E;
 N(e) = stress(e) * A;
 % sum BO after having transformed it in order to be compliant for the sum
 % with P
 for jj = 1:4
    B0_sum(edof(jj)) = B0_sum(edof(jj)) + B0(jj)*N(e)*L0;
 end
end
% compute the support reactions (N)
R = B0_sum - P; % 2nnx1 (nn is node number)
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
% This subroutine plots the undeformed and deformed structure
```

```
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
figure_truss_structure= figure('Position', get(0, 'Screensize'));
clf
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
fake_zero = max(abs(stress)) / 1e5; % fake zero for tension sign decision
for e = 1:ne
    xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
    yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
    h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
    [edof] = build_edof(IX, e);
   xx = xx + D(edof(1:2:4));
    yy = yy + D(edof(2:2:4));
    % choice of thhe color according to the state
    if stress(e) > fake_zero % tension
      col = colors(1);
    elseif stress(e) < - fake_zero % compression</pre>
      col = colors(2);
    else col = colors(3); % un-loaded
    end
    if e == 34 % unloaded
      xx1=xx;
      yy1 = yy;
      col1=col;
    elseif e == 4 % compression
      xx4=xx;
      yy4 = yy;
      col4=col;
    elseif e == 5 % tensile
      xx3=xx:
      yy3 = yy;
      col3=col;
    end
    if e \sim 34
     h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
      h2=plot(xx,yy, 'k','LineWidth',3.5); % Deformed structure
    end
end
plotsupports
plotloads
h_u=plot(xx1,yy1,col1,'LineWidth',3.5);
h_c=plot(xx4,yy4,col4,'LineWidth',3.5);
h_t=plot(xx3,yy3,col3,'LineWidth',3.5);
legend([h1 h2 h_u h_c h_t],{'Undeformed state','Deformed ...
state','Unloaded','Compressed','Tensioned'})
axis equal;
hold off
text_size = 20;
```

```
title('Truss structure in deformed and undeformed state')
xlabel('x [m]')
ylabel('y [m]')
text(0,0.6,'A','FontSize', text_size)
text(0.5,0.6,'B','FontSize', text_size)
text(0.5,-0.1,'E','FontSize', text_size)
text(1,-0.1,'F','FontSize', text_size)
text(2.05,0.6,'C','FontSize', text_size)
text(1.6,1,'D','FontSize', text_size)
text(3.85,-0.15,'G','FontSize', text_size)
text(0,-0.1,'H','FontSize', text_size)
text(4.05,0.5,'I','FontSize', text_size)
text(1,0.6,'J','FontSize', text_size)
set(gca,'FontAngle','oblique','FontSize', text_size)
saveas(figure_truss_structure, 'C:\Users\Niccolo\Documents\UNIVERSITA\ ...
5ANNO\FEM\assignment1\truss.png','png');
return
%% Function to compute the length of a bar
function [LO, delta_x, delta_y] = length(IX, X, e);
  i = IX(e, 1);
  j = IX(e, 2);
  xi = X(i, 1);
 xj = X(j, 1);
  yi = X(i, 2);
  yj = X(j, 2);
  delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e);
  edof = zeros(4, 1);
  edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
```

## 2 Exercise 2

## 2.1 Input file

```
% Created with: FlExtract v1.12
% Element type: truss
% Number of nodes: 55
% Number of elements: 124
clear all
close all
clc
%nincr=100;
incr_vector = [100];
%incr_vector = [5:5:100];
eSTOP=10^(-8);
i_max=100;
Pfinal=80;
% Node coordinates: x, y
X = [
0 0
0 4
5.55556
         0
5.55556
          4
5.55556
11.1111
          4
11.1111
11.1111
         12
16.6667
16.6667
         12
16.6667
         16
22.2222
         12
22.2222
         16
22.2222
         20
27.7778
         16
27.7778
          20
27.7778
          24
33.3333
          20
33.3333
          24
33.3333
          28
38.8889
          24
38.8889
          28
38.8889
          32
44.4444
          28
44.4444
          32
44.4444
          36
50 32
50
     36
50
     40
55.5556
          28
55.5556
55.5556
61.1111
         24
61.1111
         28
61.1111
          32
66.6667
          20
66.6667
          24
66.6667
          28
```

```
72.2222
        16
72.2222 20
72.2222
         24
77.7778
         12
         16
77.7778
77.7778
         20
83.3333
         8
83.3333
         12
83.3333
         16
88.8889
         4
88.889
         8
88.889
         12
94.4444
         0
94.4444
         4
94.4444
         8
100 0
100 4
];
% Element connectivity: node1_id, node2_id, material_id
IX = [
2
3
    1
         1
5
  2
         1
    2
4
         1
    2
3
         1
4
    3
         1
6
    3
         1
    4
5
         1
6
    4
          1
8
    5
         1
7
    5
          1
6
    5
          1
7
    6
          1
9
    6
          1
8
    7
          1
    7
9
          1
    8
11
          1
10
    8
         1
9
     8
         1
10
    9
         1
12
     9
         1
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17
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18
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20
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19
     17
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18
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19
     18
         1
```

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21
      18
            1
20
      19
            1
21
      19
            1
23
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22
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            1
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22
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24
      21
            1
23
      22
            1
24
      22
            1
26
      23
            1
25
      23
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24
      23
            1
25
      24
            1
27
      24
            1
26
      25
            1
27
      25
            1
29
      26
            1
28
      26
            1
27
      26
            1
28
      27
            1
32
      27
            1
31
      27
            1
30
      27
            1
29
      28
            1
32
      28
            1
32
      29
            1
31
      30
            1
35
      30
            1
34
      30
            1
33
      30
            1
32
      31
            1
35
      31
            1
35
      32
            1
34
      33
            1
38
      33
            1
37
      33
            1
36
      33
            1
35
      34
            1
38
      34
            1
38
      35
            1
37
      36
            1
41
      36
            1
40
      36
            1
39
      36
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38
      37
            1
41
      37
            1
41
      38
            1
40
      39
            1
44
      39
            1
43
      39
            1
42
      39
            1
41
      40
            1
44
      40
            1
44
      41
            1
43
      42
            1
47
      42
            1
46
      42
            1
45
      42
            1
44
      43
            1
47
      43
            1
```

```
47
     44
        1
46
     45
50
     45
         1
     45
49
         1
48
     45
         1
47
     46
         1
50
     46
          1
50
     47
          1
49
     48
          1
53
     48
          1
52
     48
          1
51
     48
          1
50
     49
          1
53
     49
          1
     50
53
          1
52
     51
         1
55
     51
         1
54
     51
         1
53
     52
         1
55
     52
        1
55
     53
     54
55
         1];
% Element properties: [ E A c1 c2 c3 c4],
mprop = [ 1.0 1.0 1.2 5 0.2 50 ]; % parameters for ex1 to 3
%mprop = [ 1.0 1.0 0 1 0.2 200 ]; % parameters for ex 4
% Nodal diplacements: node_id, degree of freedom (1 - x, 2 - y), displacement
bound = [
1
   1
3
    1
          0
1
    2
          0
     2
3
          0
51
    2
          0
54
    2
          0];
% Nodal loads: node_id, degree of freedom (1 - x, 2 - y), load
loads = [ 24
             2 Pfinal
          30
               2 -Pfinal ];
% Control parameters
plotdof = 48;
```

#### 2.2 Euler method

```
Basic Euler method
function fea()
close all
clc
%--- Input file ------%
TrussExercise2_2022
                        % Input file
ne = size(IX,1);
                         % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
  ' Number of elements ' sprintf('%d',ne)]);
P_final=zeros(neqn,1);  % Stiffness matrix

R=zeros(neqn,1);
%--- Initialize arrays ------%
                            % Residual vector
strain=zeros(ne,1);
                            % Element strain vector
stress=zeros(ne,1);
                            % Element stress vector
P_plot=zeros(max(incr_vector), size(incr_vector, 2));
D_plot=zeros(max(incr_vector), size(incr_vector, 2));
%--- Calculate displacements -----%
[P_final] = buildload(X,IX,ne,P_final,loads,mprop); % vector of the external loads
rubber_param = [mprop(3) mprop(4) mprop(5) mprop(6)]; % coefficients for the nonlinear material
residual_norm = zeros(1, size(incr_vector, 2));
for j = 1:size(incr_vector, 2) % cycle over the different # of load incr
 % number of increments
 nincr = incr_vector(j);
 % load increment
 delta_P = P_final / nincr;
 % Initialize arrays
 P=zeros(negn,1);
                             % Force vector
 D=zeros(negn,1);
                             % Displacement vector
 K = zeros(neqn, neqn);
 for n = 1:nincr
  P = P + delta_P; % increment the load
  K = zeros(neqn, neqn);
   delta_D = K \ delta_P;
                                    % Solve system of equations
   D = D + delta D;
   P_plot(n, j) = P(48);
   D_plot(n, j) = D(48);
```

```
[~, stress]=recover(mprop,X,IX,D,ne,rubber_param);
 end
  [R] = residual(stress,ne,IX, X, P, D, mprop);
  [~, R] = enforce(K,R,bound);
                              % Enforce boundary conditions
 residual_norm(j) = norm(R);
 disp(residual_norm(end))
 % [strain, stress, ~, ~]=recover(mprop, X, IX, D, ne, strain, stress, P, rubber_param);
end
%--- Plot results ------%
save('euler_method.mat', 'P_plot', 'D_plot', 'residual_norm');
%save('euler_method_mi_r2.mat', 'P_plot', 'D_plot', 'residual_norm');
PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
                                                 % Plot structure
figure(2)
legend_name = strings(1, size(incr_vector,2));
for j=1:size(incr_vector,2)
 plot(D_plot(:,j), P_plot(:,j), 'o', 'LineWidth', 2.5)
  % build a vector with the name
 legend_name(j) = strcat("Number of increment n = ", num2str(incr_vector(j)));
 hold on
end
xlabel("Displacement (m)")
ylabel("Force (N)")
legend(legend_name, 'Location', 'southeast')
hold off
figure(3)
plot(incr_vector, residual_norm, 'o');
xlabel('Number of increments')
ylabel('Norm of the final residual')
title('Norm of the final residual')
% plot of the final displacement
figure (4)
for j=1:size(incr_vector,2)
 plot(incr_vector(j), D_plot(incr_vector(j),j), 'o');
 hold on
end
hold off
xlabel('Number of load increments')
ylabel('Final displacement')
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
```

```
pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K, epsilon]=buildstiff(X,IX,ne,mprop,K, D,rubber_param);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 % vector of index used for building K
 [edof] = build_edof(IX, e);
 % build d vector
 [d] = build_d(D, edof);
 % compute the displacement
 epsilon = B0' * d';
 Et = Etfunction(epsilon, rubber_param);
 % element stiffness matrix
 k_e = Et * A * L0 * B0 * B0'; % 4x4 matrix
 % build K by summing k_e
 for ii = 1:4
   for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
   end
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
```

```
K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
function [strain, stress]=recover(mprop,X,IX,D,ne,rubber_param)
% This subroutine recovers the element stress, element strain, force on each element
% and nodal reaction forces
stress = zeros(ne, 1);
strain = zeros(ne,1);
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 strain(e) = B0' * d';
 stress(e) = stress_function(strain(e), rubber_param);
end
return
% function [strain, stress, N, R]=recover(mprop, X, IX, D, ne, strain, stress, P, rubber_param);
% This subroutine recovers the element stress, element strain,
% % and nodal reaction forces
% strain = zeros(ne, 1);
% stress = zeros(ne, 1);
% B0_sum = zeros(2*size(X,1), 1);
% for e=1:ne
  d = zeros(4, 1);
   [edof] = build_edof(IX, e);
응
응
  % build the matrix d from D
응
  for i = 1:4
응
   d(i) = D(edof(i));
응
응
  end
```

```
응
  % compute the bar length
응
   [LO, delta_x, delta_y] = length(IX, X, e);
응
    % displacement vector
응
   B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
용
00
응
   % materials properties
응
   propno = IX(e, 3);
응
   E = mprop(propno, 1);
응
   A = mprop(propno, 2);
응
   strain(e) = B0' * d;
응
   stress(e) = strain(e) * E;
응
   N(e) = stress(e) * A;
응
   % sum BO after having transformed it in order to be compliant for the sum
응
  % with P
응
  for jj = 1:4
응
응
       B0\_sum(edof(jj)) = B0\_sum(edof(jj)) + B0(jj)*N(e)*L0;
응
응
% end
응
% % compute the support reactions (N)
% R = B0_sum - P; % 2nnx1 (nn is node number)
% return
%%%%% Residuals %%%%
function [R] = residual(stress, ne,IX, X, P, D, mprop)
R_{int} = zeros(2*size(X,1), 1);
  for e=1:ne
  d = zeros(4, 1);
  [edof] = build_edof(IX, e);
  % build the matrix d from D
  d = build_d(D, edof);
  % compute the bar length
  [L0, delta_x, delta_y] = length(IX, X, e);
  % displacement vector
  B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
  % materials properties
  propno = IX(e, 3);
  A = mprop(propno, 2);
  N(e) = A*stress(e,1);
  % sum BO after having transformed it in order to be compliant for the sum
  % with P
  for jj = 1:4
      R_{int}(edof(jj)) = R_{int}(edof(jj)) + BO(jj) * N(e) * LO;
  end
  end
R = R_{int} - P;
return
```

```
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
\mbox{\ensuremath{\it \%}} This subroutine plots the undeformed and deformed structure
h1=0;h2=0;
% Plotting Un-Deformed and Deformed Structure
figure(1)
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
fake_zero = 1e-8; % fake zero for tension sign decision
for e = 1:ne
   xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
   yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
   h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
   [edof] = build_edof(IX, e);
   xx = xx + D(edof(1:2:4));
   yy = yy + D(edof(2:2:4));
   % choice of thhe color according to the state
   if stress(e) > fake_zero % tension
     col = colors(1);
   elseif stress(e) < - fake_zero % compression</pre>
     col = colors(2);
   else col = colors(3); % un-loaded
   end
   h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
               'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [L0, delta_x, delta_y] = length(IX, X, e)
 i = IX(e, 1);
 j = IX(e, 2);
 xi = X(i, 1);
 xj = X(j, 1);
yi = X(i, 2);
 yj = X(j, 2);
 delta_x = xj - xi;
 delta_y = yj - yi;
 L0 = sqrt(delta_x^2 + delta_y^2);
return
```

```
%% Function to provide the edof vector
function [edof] = build_edof(IX, e)
      edof = zeros(4, 1);
      edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
%% Function to build d from D
function [d] = build_d(D, edof)
      for i = 1:4
            d(i) = D(edof(i));
      end
return
%% Function to Et
function [Et] = Etfunction(epsilon, rubber_param)
      c1 = rubber_param(1);
     c2 = rubber_param(2);
     c3 = rubber_param(3);
      c4 = rubber_param(4);
      Et = c4*(c1*(1 + 2*(1 + c4*epsilon)^(-3)) + 3*c2*(1 + c4*epsilon)^(-4) + ...
            3*c3*(-1 + (1 + c4*epsilon)^2 - 2*(1 + c4*epsilon)^(-3) + 2*(1 + c4*epsilon)^(-4)));
return
%% Stress function
function [stress] = stress_function(epsilon, rubber_param)
      c1 = rubber_param(1);
      c2 = rubber_param(2);
      c3 = rubber_param(3);
      c4 = rubber_param(4);
      stress = c1*((1+c4*epsilon) - (1+c4*epsilon)^(-2)) + c2*(1 - (1+c4*epsilon)^(-3)) + c3 * (1 - (1+
return
```

#### 2.3 Newton Raphson

```
Newton Raphson method based on week 3
function fea()
close all
clc
%--- Input file ------%
TrussExercise2_2022
                          % Input file
ne = size(IX,1);
                           % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
   ' Number of elements ' sprintf('%d',ne)]);
%--- Initialize arrays ------%
                              % Residual vector
strain=zeros(ne, size(incr_vector, 2));
                                            % Element strain vector
stress=zeros(ne,size(incr_vector, 2));
                                            % Element stress vector
P_plot=zeros(max(incr_vector), size(incr_vector, 2));
D_plot=zeros(max(incr_vector), size(incr_vector, 2));
VM_plot = zeros(1, 100); % vector for plotting the von mises curve
%--- Calculate displacements -----%
[P_final] = buildload(X,IX,ne,P_final,loads,mprop); % vector of the external loads
rubber_param = [mprop(3) mprop(4) mprop(5) mprop(6)]; % coefficients for the ...
nonlinear material behaviour
residual_norm = zeros(1, size(incr_vector,2)); % vector for the norm of final residual
total_iteration = 0;
for j = 1:size(incr_vector,2) % cycle over the different # of load incr
 % number of increments
 nincr = incr_vector(j);
 % load increment
 delta_P = P_final / nincr;
 clear P D0 D
 % Initialize arrays
 P=zeros(neqn,1);
                               % Force vector
 D0=zeros(neqn,1);
                                % Displacement vector
                                % Displacement vector
 D=zeros(neqn,1);
 for n = 1:nincr % cycle to the number of increments
   P = P + delta_P; % increment the load
   DO = D:
   stress = zeros(ne,1);
   for i = 1:i_max
```

```
K=zeros(neqn,neqn);
     [R] = residual(stress, ne,IX, X, P, D0, mprop);
                                % Enforce boundary conditions on R
     [~,R]=enforce(K,R,bound);
     residual_norm(j) = norm(R);
      if norm(R) <= eSTOP * Pfinal % break when we respect the eSTOP</pre>
        total_iteration = total_iteration + i;
      end
     tangent stiffness matrix
     [K, ~] = enforce(K,R,bound);
       [LM, UM] = lu(K);
응
      delta\_DO = - UM \setminus (LM \setminus R);
     delta_DO = - K \ R;
     DO = DO + delta_DO;
     [~, stress] = recover(mprop, X, IX, D0, ne, rubber_param);
   end
   D = D0;
   % save data of the point of interest
   P_plot(n, j) = P(48);
   D_plot(n, j) = D(48);
 end
  residual_norm(j) = norm(R); % norm of the final residual
end
display(total_iteration)
% % External matrix
% disp('External forces applied (N)')
% P'
% % Stress
% disp('Stress on the bars (MPa)')
% stress'
% % Strain
% disp('Strain of the bars')
% strain'
% % Forces on the bars
% disp('Internal forces on the bar (N)')
\approx N
% % Support reaction
% disp('Support reactions forces (N)')
% R'
%--- Plot results ------%
```

```
PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
                                             % Plot structure
save('NR.mat', 'P_plot', 'D_plot', 'residual_norm');
%save('NR_200.mat', 'P_plot', 'D_plot', 'residual_norm');
figure(2)
legend_name = strings(1, size(incr_vector,2));
for j=1:size(incr_vector,2)
 plot(D_plot(:,j), P_plot(:,j), 'o', 'LineWidth', 2.5)
 % build a vector with the name
 legend_name(j) = strcat("Number of increment n = ", num2str(incr_vector(j)));
 hold on
end
xlabel("Displacement (m)")
ylabel("Force (N)")
legend(legend_name, 'Location', 'southeast')
hold off
figure(3)
plot(incr_vector, residual_norm, 'o');
xlabel('Number of increments')
ylabel('Norm of the final residual')
title('Norm of the final residual')
% plot of the final displacement
figure (4)
for j=1:size(incr_vector,2)
 plot(incr_vector(j), D_plot(incr_vector(j),j), 'o');
 hold on
end
hold off
xlabel('Number of load increments')
ylabel('Final displacement')
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K, epsilon] = buildstiff(X,IX,ne,mprop,K,D,rubber_param)
```

```
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
  % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
  % linear strain displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
  % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
  % vector of index used for building K
 [edof] = build_edof(IX, e);
  % build d vector
 [d] = build_d(D, edof); % d ia row vector
 % compute the displacement
 epsilon = B0' * d';
 Et = Etfunction(epsilon, rubber_param);
 % element stiffness matrix
 k_e = Et * A * L0 * B0 * B0'; % 4x4 matrix
 % build K by summing k_sum
 for ii = 1:4
   for jj = 1:4
     K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
   end
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
```

```
function [strain, stress]=recover(mprop,X,IX,D,ne,rubber_param)
% This subroutine recovers the element stress, element strain, force on each element
% and nodal reaction forces
stress = zeros(ne, 1);
strain = zeros(ne,1);
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 strain(e) = B0' * d';
 stress(e) = stress_function(strain(e), rubber_param);
end
return
%%% Residuals
function [R] = residual(stress, ne,IX, X, P, D, mprop)
R_{int} = zeros(2*size(X,1), 1);
 for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
  % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 N(e) = A*stress(e,1);
  % sum BO after having transformed it in order to be compliant for the sum
  % with P
 for jj = 1:4
     R_{int}(edof(jj)) = R_{int}(edof(jj)) + BO(jj) * N(e) * LO;
```

```
end
 R = R_{int} - P;
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
% This subroutine plots the undeformed and deformed structure
h1=0;h2=0;
% Plotting Un-Deformed and Deformed Structure
figure(1)
c1f
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
eSTOP = 1e-8; % fake zero for tension sign decision
for e = 1:ne
   xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
   yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
   h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
   [edof] = build_edof(IX, e);
   xx = xx + D(edof(1:2:4));
   yy = yy + D(edof(2:2:4));
   % choice of thhe color according to the state
   if stress(e) > eSTOP % tension
     col = colors(1);
   elseif stress(e) < - eSTOP % compression</pre>
     col = colors(2);
   else col = colors(3); % un-loaded
   end
   h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
              'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [L0, delta_x, delta_y] = length(IX, X, e)
 i = IX(e, 1);
 j = IX(e, 2);
 xi = X(i, 1);
 xj = X(j, 1);
 yi = X(i, 2);
 yj = X(j, 2);
```

```
delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e)
  edof = zeros(4, 1);
  edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
%% Function to build d from D
function [d] = build_d(D, edof)
  for i = 1:4
   d(i) = D(edof(i));
  end
return
%% Stress
function [stress] = stress_function(epsilon, rubber_param)
  c1 = rubber_param(1);
  c2 = rubber_param(2);
  c3 = rubber_param(3);
  c4 = rubber_param(4);
  stress = c1*((1+c4*epsilon) - (1+c4*epsilon)^(-2)) + c2*(1 - (1+c4*epsilon)^(-3))...
  + c3 * (1 - 3*(1+c4*epsilon) + (1+c4*epsilon)^3 - 2*(1+c4*epsilon)^(-3) + ...
  3*(1+c4*epsilon)^(-2));
return
%% Function to Et
function [Et] = Etfunction(epsilon, rubber_param)
  c1 = rubber_param(1);
  c2 = rubber_param(2);
  c3 = rubber_param(3);
  c4 = rubber_param(4);
  Et = c4*(c1*(1 + 2*(1 + c4*epsilon)^(-3)) + 3*c2*(1 + c4*epsilon)^(-4) + ...
  3*c3*(-1 + (1 + c4*epsilon)^2 - 2*(1 + c4*epsilon)^(-3) + ...
  2*(1 + c4*epsilon)^(-4));
return
```

#### 2.4 Modified Newton Raphson

```
Newton Raphson modified method (based on result of week 3
function fea()
close all
clc
%--- Input file ------%
TrussExercise2_2022
                         % Input file
ne = size(IX,1);
                          % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
  'Number of elements' sprintf('%d',ne)]);
%--- Initialize arrays -----%
                             % Residual vector
strain=zeros(ne, size(incr_vector, 2));
                                           % Element strain vector
stress=zeros(ne,size(incr_vector, 2));
                                           % Element stress vector
P_plot=zeros(max(incr_vector), size(incr_vector, 2));
D_plot=zeros(max(incr_vector), size(incr_vector, 2));
VM_plot = zeros(1, 100); % vector for plotting the von mises curve
%--- Calculate displacements ------%
[P_final] = buildload(X,IX,ne,P_final,loads,mprop); % vector of the external loads
rubber_param = [mprop(3) mprop(4) mprop(5) mprop(6)]; % coefficients for the ...
nonlinear material behaviour
residual_norm = zeros(1, size(incr_vector, 2));
total_iteration = 0;
for j = 1:size(incr_vector,2) % cycle over the different # of load incr
 % number of increments
 nincr = incr_vector(j);
 % load increment
 delta_P = P_final / nincr;
 clear P D0 D
 % Initialize arrays
 P=zeros(negn,1);
                              % Force vector
 D0=zeros(neqn,1);
                               % Displacement vector
                               % Displacement vector
 D=zeros(neqn,1);
 for n = 1:nincr % cycle to the number of increments
   stress = zeros(ne,1);
   P = P + delta_P; % increment the load
   DO = D;
   stiffness matrix
   [K, ~] = enforce(K,R,bound); % enforce boundary on K
   [LM, UM] = lu(K);
```

```
for i = 1:i_max
      [R] = residual(stress, ne,IX, X, P, D0, mprop); % compute residuals
      [~,R]=enforce(K,R,bound); % Enforce boundary conditions on R
       if norm(R) \leftarrow eSTOP * Pfinal % break when we respect the eSTOP
        total_iteration = total_iteration + i;
     delta_D0 = -UM \setminus (LM \setminus R);
     DO = DO + delta_DO;
      [~, stress] = recover(mprop, X, IX, D0, ne, rubber_param);
    end
   D = D0;
    % save data of the point of interest
    P_plot(n, j) = P(48);
    D_plot(n, j) = D(48);
  end
 residual_norm(j) = norm(R); % norm of the final residual
display(total_iteration);
%--- Print the results on the command window ------%
% % External matrix
% disp('External forces applied (N)')
8 P'
% % Stress
% disp('Stress on the bars (MPa)')
% stress'
% % Strain
% disp('Strain of the bars')
% strain'
% % Forces on the bars
% disp('Internal forces on the bar (N)')
% N
% % Support reaction
% disp('Support reactions forces (N)')
8 R'
%--- Plot results ------%
PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
                                                     % Plot structure
save('NR_modified_results.mat', 'P_plot', 'D_plot', 'residual_norm');
%save('NR_modified_200.mat', 'P_plot', 'D_plot', 'residual_norm');
figure(2)
legend_name = strings(1, size(incr_vector,2));
for j=1:size(incr_vector,2)
```

```
plot(D_plot(:,j), P_plot(:,j), 'o', 'LineWidth', 2.5)
  % build a vector with the name
 legend_name(j) = strcat("Number of increment n = ", num2str(incr_vector(j)));
 hold on
end
xlabel("Displacement (m)")
ylabel("Force (N)")
legend(legend_name, 'Location', 'southeast')
hold off
% plot the norm of the final residual
figure (3)
plot(incr_vector, residual_norm, 'o');
xlabel('Number of increments')
ylabel('Norm of the final residual')
title('Norm of the final residual')
% plot of the final displacement
figure (4)
for j=1:size(incr_vector,2)
 plot(incr_vector(j), D_plot(incr_vector(j),j), 'o');
end
hold off
xlabel('Number of load increments')
ylabel('Final displacement')
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K, epsilon]=buildstiff(X,IX,ne,mprop,K,D,rubber_param)
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
  % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
```

```
% linear strain displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 % vector of index used for building K
 [edof] = build_edof(IX, e);
 % build d vector
 [d] = build_d(D, edof); % d ia row vector
 % compute the displacement
 epsilon = BO' * d';
 Et = Etfunction(epsilon, rubber_param);
 % element stiffness matrix
 k_e = Et * A * L0 * B0 * B0'; % 4x4 matrix
 % build K by summing k_sum
 for ii = 1:4
   for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
   end
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
function [strain, stress]=recover(mprop,X,IX,D,ne,rubber_param)
% This subroutine recovers the element stress, element strain, force on each element
% and nodal reaction forces
stress = zeros(ne, 1);
strain = zeros(ne,1);
```

```
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
  % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 strain(e) = B0' * d';
 stress(e) = stress_function(strain(e), rubber_param);
end
return
%%%% Residuals
function [R] = residual(stress, ne,IX, X, P, D, mprop)
R_{int} = zeros(2*size(X,1), 1);
 for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 N(e) = A*stress(e,1);
 \$ sum BO after having transformed it in order to be compliant for the sum
  % with P
 for jj = 1:4
     R_{int}(edof(jj)) = R_{int}(edof(jj)) + BO(jj) * N(e) * LO;
 end
 end
 R = R_{int} - P;
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
```

```
% This subroutine plots the undeformed and deformed structure
h1=0;h2=0;
% Plotting Un-Deformed and Deformed Structure
figure(1)
clf
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
eSTOP = 1e-8; % fake zero for tension sign decision
for e = 1:ne
    xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
    yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
    h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
    [edof] = build_edof(IX, e);
    xx = xx + D(edof(1:2:4));
    yy = yy + D(edof(2:2:4));
    % choice of thhe color according to the state
    if stress(e) > eSTOP % tension
      col = colors(1);
    elseif stress(e) < - eSTOP % compression</pre>
     col = colors(2);
    else col = colors(3); % un-loaded
    end
    h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
                'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [L0, delta_x, delta_y] = length(IX, X, e)
 i = IX(e, 1);
  j = IX(e, 2);
  xi = X(i, 1);
  xj = X(j, 1);
  yi = X(i, 2);
  yj = X(j, 2);
  delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e)
  edof = zeros(4, 1);
  edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
```

#### return

```
%% Function to build d from D
function [d] = build_d(D, edof)
  for i = 1:4
    d(i) = D(edof(i));
  end
return
%% Stress
function [stress] = stress_function(epsilon, rubber_param)
  c1 = rubber_param(1);
  c2 = rubber_param(2);
  c3 = rubber_param(3);
  c4 = rubber_param(4);
  stress = c1*((1+c4*epsilon)^{-}(-2)) + c2*(1 - (1+c4*epsilon)^{-}(-3)) + ...
  c3 * (1 - 3*(1+c4*epsilon) + (1+c4*epsilon)^3 - 2*(1+c4*epsilon)^(-3) + ...
  3*(1+c4*epsilon)^(-2));
return
%% Function to Et
function [Et] = Etfunction(epsilon, rubber_param)
  c1 = rubber_param(1);
  c2 = rubber_param(2);
  c3 = rubber_param(3);
  c4 = rubber_param(4);
  Et = c4*(c1*(1 + 2*(1 + c4*epsilon)^(-3)) + 3*c2*(1 + c4*epsilon)^(-4) + ...
  3*c3*(-1 + (1 + c4*epsilon)^2 - 2*(1 + c4*epsilon)^(-3) +...
  2*(1 + c4*epsilon)^(-4));
return
```

#### 2.5 Code used for plotting all the methods in the same graph

```
clear
close all
clc
NR_modified;
NR_method;
euler_method;
text_size = 20;
close all
clear load
nincr = 100;
% euler = load('euler_method.mat', 'D_plot');
% NR = load('NR.mat');
% NR_modified = load('NR_modified.mat', 'D_plot');
% load_v = load('NR.mat', 'P_plot');
% close all
% figure()
% plot(NR.D_plot, load_v.P_plot, 'o')
% hold on
% plot(NR_modified.D_plot, load_v.P_plot,'x')
% plot(euler.D_plot, load_v.P_plot)
% plot(euler_correction.D_plot, load_v.P_plot)
% legend('NR', 'NR modified', 'euler', 'euler corrected', 'Location', 'southeast')
% xlabel('Displacement [m]')
% ylabel('Load P [N]')
euler = load('euler_method.mat');
NR = load('NR.mat');
NR_modified = load('NR_modified_results.mat');
%% Plot of the multiple method for 1 increment size (with zoom)
close all
figure_method_comparison = figure('Position', get(0, 'Screensize'));
plot(NR.D_plot, NR.P_plot, '-', 'LineWidth', 1.5, 'MarkerSize',6)
hold on
plot(NR_modified.D_plot, NR_modified.P_plot,'x', 'LineWidth', 1.5, 'MarkerSize',6)
plot(euler.D_plot, euler.P_plot, '--k', 'LineWidth', 1.5, 'MarkerSize',6)
legend('Newton-Raphson', 'Newton-Raphson modified', 'Euler','Location','southeast')
xlabel('Displacement [m]')
ylabel('Load P [N]')
grid on
title ('Load-vertical displacement curve for point A', 'FontSize', 16)
set(gca,'FontAngle','oblique','FontSize', text_size)
hold all
axes('position',[0.18 .58 .30 .30])
%a2.Position = [0 0 5 5]; % xlocation, ylocation, xsize, ysize
plot(NR.D_plot(51:63), NR.P_plot(51:63), 'LineWidth', 1.5, 'MarkerSize',6); %axis tight
hold on
plot(NR_modified.D_plot(51:63),NR_modified.P_plot(51:63), 'x', 'LineWidth', 1.5, ...
'MarkerSize',6); %axis tight
plot(euler.D_plot(51:63), euler.P_plot(51:63), '--k', 'LineWidth', 1.5, ...
'MarkerSize',6); axis tight
grid on
set(gca, 'FontAngle', 'oblique', 'FontSize', text_size)
```

```
saveas(figure_method_comparison, 'C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\...
assignment1\method_comparison.png','png');

%% Plot multiple increments

figure()
iteration_n = [1:1:nincr];
plot(iteration_n, NR.residual_norm);
hold on
plot(iteration_n, euler.residual_norm);
plot(iteration_n, NR_modified.residual_norm);
hold off
xlabel('Increment number')
ylabel('Norm of he residual')
title('Norm of the residuals')
```

# 3 Exercise 3

# 3.1 Input file used to determine EI

```
% Created with:
                    FlExtract v1.13
% Element type:
                     truss
% Number of nodes: 34
% Number of elements: 81
clear all;
A = 2; % cross section
incr_vector = [50]; % number of increment
i_max = 1000; % maximum number of iterations
n_incr = 10;
eSTOP = 1e-8;
Pfinal = 0.00005;
a = 0.4;
k = 0.02; % spring stiffness
% Node coordinates: x, y
X = [
0
0
    5
5
    0
5
    5
10
    0
10
    5
    0
15
15
    5
20
    0
20
    5
25
   0
25
    5
30
    0
30
    5
35
   0
35
    5
40
    0
40
    5
45
    0
45
    5
50
    0
50
    5
55
    0
55
    5
60
    0
60
    5
65
    0
65
    5
70
    0
70
    5
75
    0
75
    5
80
80
% Element connectivity: node1_id, node2_id, material_id
IX = [
2 1 1
4 1
         1
```

```
3
     1
            1
4
      2
            1
3
      2
            1
      3
4
            1
6
      3
            1
5
      3
            1
6
      4
            1
5
      4
            1
6
      5
            1
8
      5
            1
7
      5
            1
8
      6
            1
7
      6
            1
8
      7
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10
      7
            1
9
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26
      24
            1
25
      24
            1
26
      25
            1
28
      25
            1
27
      25
            1
```

```
28
    26
        1
27
    26
28
    27
        1
30
    27
        1
29
    27
         1
30
    28
         1
29
    28
        1
30
    29
         1
32
    29
         1
31
    29
         1
32
    30
31
    30
         1
       1
32
    31
        1
34
    31
        1
33
    31
       1
34
    32
33
   32
        1
34
   33 1
];
% Element properties: Young's modulus, area
mprop = [
0.8 0.2
];
% Nodal diplacements: node_id, degree of freedom (1 - x, 2 - y), displacement
bound = [
%1 1 O
1 2 0
33 2 0
];
% Nodal loads: node_id, degree of freedom (1 - x, 2 - y), load
loads = [
18 2 -Pfinal
];
% Control parameters
plotdof = 2;
```

#### 3.2 File used to evaluate EI

```
Basis truss program
function fea()
close all
clc
%--- Input file ------%
vertical_disp_struct
disp(['Number of DOF ' sprintf('%d',neqn) ...
  'Number of elements' sprintf('%d',ne)]);
%--- Initialize arrays -----%
                           % Stiffness matrix
Kmatr=sparse(neqn, neqn);
                           % Force vector
P=zeros(neqn,1);
                            % Displacement vector
D=zeros(neqn,1);
R=zeros(neqn,1);
                            % Residual vector
strain=zeros(ne,1);
                            % Element strain vector
stress=zeros(ne,1);
                            % Element stress vector
%--- Calculate displacements ------%
[P]=buildload(X,IX,ne,P,loads,mprop); % Build global load vector
D = Kmatr \ Pmatr;
                               % Solve system of equations
[strain, stress] = recover(mprop, X, IX, D, ne, strain, stress); % Calculate element
                                        % stress and strain
% Calculate element axial forces and the support reactions
[strain, stress, N, R] = recover2(mprop, X, IX, D, ne, strain, stress, P);
%--- Print the results on the command window -----%
vertical_load = P(36);
vertical_D = D(36);
EI = vertical_load * 80^3/(48 * vertical_D);
P_{critic} = pi^2*EI/80^2;
disp(strcat('External load P = ', num2str(vertical_load)))
disp(strcat('Vertical displacement D = ', num2str(vertical_D)))
disp(strcat('EIx = ', num2str(EI)))
disp(strcat('Critical load P = ', num2str(P_critic)))
% % External matrix
% disp('External forces applied (N)')
% P'
% % Stress
% disp('Stress on the bars (MPa)')
% stress'
```

```
% % Strain
% disp('Strain of the bars')
% strain'
% % Forces on the bars
% disp('Internal forces on the bar (N)')
용 N
% % Support reaction
% disp('Support reactions forces (N)')
% R'
%--- Plot results -----%
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% \ P \ contains \ the \ external \ forces \ applied \ by \ the \ load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K] = buildstiff(X,IX,ne,mprop,K);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 % element stiffness matrix
 k_e = E * A * L0 * B0 * B0'; % 4x4 matrix
 % vector of index used for building K
 [edof] = build_edof(IX, e);
```

```
% build K by summing k_e
 for ii = 1:4
   for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
 end
end
return
function [K,P] = enforce(K,P,bound);
\mbox{\it \%} This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
function [strain,stress] = recover(mprop, X, IX, D, ne, strain, stress);
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
% allocate memory for stress and strain vectors
strain = zeros(ne, 1);
stress = zeros(ne, 1);
for e=1:ne
 d = zeros(4, 1); % allocate memory for element stiffness matrix
[edof] = build_edof(IX, e); % index for buildg K
 % build the matrix d from D
 for i = 1:4
   d(i) = D(edof(i));
 end
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
```

```
E = mprop(propno, 1);
 A = mprop(propno, 2);
 strain(e) = B0' * d;
 stress(e) = strain(e) * E;
end
return
function [strain, stress, N, R] = recover2(mprop, X, IX, D, ne, strain, stress, P);
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
strain = zeros(ne, 1);
stress = zeros(ne, 1);
B0_sum = zeros(2*size(X,1), 1);
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 for i = 1:4
   d(i) = D(edof(i));
 end
  % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 strain(e) = B0' * d;
 stress(e) = strain(e) * E;
 N(e) = stress(e) * A;
 % sum BO after having transformed it in order to be compliant for the sum
 % with P
 for jj = 1:4
     B0_{sum}(edof(jj)) = B0_{sum}(edof(jj)) + B0(jj)*N(e)*L0;
 end
end
% compute the support reactions (N)
R = B0_sum - P; % 2nnx1 (nn is node number)
return
```

```
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
% This subroutine plots the undeformed and deformed structure
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
fake_zero = 1e-8; % fake zero for tension sign decision
for e = 1:ne
    xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
    yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
    h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
    [edof] = build_edof(IX, e);
    xx = xx + D(edof(1:2:4));
    yy = yy + D(edof(2:2:4));
    % choice of thhe color according to the state
    if stress(e) > fake_zero % tension
     col = colors(1);
    elseif stress(e) < - fake_zero % compression</pre>
     col = colors(2);
    else col = colors(3); % un-loaded
    h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
               'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [LO, delta_x, delta_y] = length(IX, X, e);
  i = IX(e, 1);
  j = IX(e, 2);
  xi = X(i, 1);
  xj = X(j, 1);

yi = X(i, 2);
  yj = X(j, 2);
  delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e);
```

```
edof = zeros(4, 1);
edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
```

### 3.3 Input file used to compute buckling of column alone

```
% Created with:
                    FlExtract v1.13
% Element type:
                    truss
% Number of nodes: 34
% Number of elements: 81
clear all;
A = 2; % cross section
%incr_vector = [100]; % number of increment
i_max = 1000; % maximum number of iterations
nincr = 100;
eSTOP = 1e-8;
Pfinal = 0.004;
% Node coordinates: x, y
X = [
0
    0
0
    5
    0
5
5
    5
10
   0
   5
10
15
   0
15
   5
20
   0
20
   5
25
   0
25
   5
30
   0
30
    5
35
    0
35
    5
40
    0
40
    5
45
    0
45
    5
    0
50
50
    5
55
    0
55
    5
60
    0
60
    5
65
    0
65
    5
70
    0
70
    5
75
    0
75
    5
80
    0
80
];
% Element connectivity: node1_id, node2_id, material_id
IX = \Gamma
    1
         1
4
    1
         1
3
4
    2
         1
   2
        1
3
4
    3
         1
```

```
6
      3
            1
5
      3
            1
6
      4
            1
5
      4
            1
6
      5
            1
8
      5
            1
7
      5
            1
8
      6
            1
7
      6
            1
8
      7
            1
10
      7
            1
9
     7
            1
10
      8
            1
9
      8
            1
10
      9
            1
12
      9
            1
11
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            1
12
      10
            1
11
      10
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12
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14
      11
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13
      11
            1
      12
14
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13
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14
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16
      13
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15
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16
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15
      14
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16
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18
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22
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22
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21
      20
            1
22
      21
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24
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23
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24
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23
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24
      23
            1
26
      23
            1
25
      23
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26
      24
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25
      24
            1
26
      25
            1
28
      25
            1
27
      25
            1
28
      26
            1
27
      26
            1
28
      27
            1
```

```
29
    27
        1
30
    28
29
    28
        1
30
    29
        1
32
    29
         1
31
    29
         1
32
    30
        1
31
    30
         1
32
    31
         1
34
    31
         1
33
    31
        1
    32
34
        1
33
    32
        1
34
    33
];
% Element properties: Young's modulus, area
mprop = [
0.8 0.2
];
% Nodal diplacements: node_id, degree of freedom (1 - x, 2 - y), displacement
bound = [
1 2
2 2 0
33 2
       0
34 2 0
1 1 0
];
% Nodal loads: node_id, degree of freedom (1 - x, 2 - y), load
loads = [
1 1 Pfinal*(0.5+1e-3)
33 1 -Pf
2 1 Pfinal/2
         -Pfinal*(0.5+1e-3)
34 1 -Pfinal/2
];
% Control parameters
plotdof = 5;
```

### 3.4 File used to evaluate the buckling of the colum alone

```
Newton Raphson method
function fea()
close all
clc
%--- Input file ------%
buckling_struct
%week3_ex_3_struct
ne = size(IX,1);
                                                                         % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
         ' Number of elements ' sprintf('%d',ne)]);
%--- Initialize arrays ------%
                                                                      % Stiffness matrix
K=sparse(neqn,neqn);
P_final=zeros(neqn,1);
                                                                                % Force vector
R=zeros(neqn,1);
                                                                                % Residual vector
strain=zeros(ne,1);
stress=zeros(ne,1);
                                                                                % Element strain vector
                                                                                % Element stress vector
P_plot=zeros(nincr, 1);
D_plot=zeros(nincr, 1);
%--- Calculate displacements ------%
[P_final] = buildload(X,IX,ne,P_final,loads,mprop); % vector of the external loads
% load increment
delta_P = P_final / nincr;
clear P D0 D
% Initialize arrays
P=zeros(neqn,1);
                                                                                  % Force vector
                                                                                   % Displacement vector
D0=zeros(neqn,1);
D=zeros(neqn,1);
                                                                                   % Displacement vector
for n = 1:nincr % cycle to the number of increments
    P = P + delta_P; % increment the load
    DO = D;
    for i = 1:i_max
        K=zeros(neqn, neqn);
         [R] = residual(stress, ne,IX, X, P, D0, mprop);
          \begin{tabular}{ll} \be
          if norm(R) <= eSTOP * norm(Pfinal) % break when we respect the eSTOP</pre>
              %CONV=i
              %pause
            break
           end
         [K, ~]=buildstiff(X,IX,ne,mprop,K,D0); % Build global tangent stiffness matrix
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```
[K, ~] = enforce(K,R,bound);
       [LM, UM] = lu(K);
응
       delta\_DO = - UM \setminus (LM \setminus R);
응
   delta_D0 = - K \setminus R;
   DO = DO + delta_DO;
   [~, stress] = recover(mprop,X,IX,D0,ne);
 end
 D = D0;
 % save data of the point of interest
 P_{plot(n)} = 2*P(1);
 D_{plot(n)} = D(1) - D(65);
end
%--- Print the results on the command window -----%
disp(strcat('The maximum vertical displacement is d = ', num2str(v_disp)))
% % External matrix
% disp('External forces applied (N)')
% % Stress
% disp('Stress on the bars (MPa)')
% stress'
% % Strain
% disp('Strain of the bars')
% strain'
% % Forces on the bars
% disp('Internal forces on the bar (N)')
응 N
% % Support reaction
% disp('Support reactions forces (N)')
% R'
%save('NR.mat', 'P_plot', 'D_plot');
[LO, ~, ~] = length(IX, X, 1);
lin_space = linspace(0, 0.9);
figure(2)
plot(D_plot, P_plot, '-', 'LineWidth', 2.5)
% build a vector with the name
xlabel("Displacement (m)")
ylabel("Force (N)")
yline(0.00299, '--r', 'Theoretical bouckling load', 'LineWidth',1.5)
```

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return
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function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K, epsilon_G]=buildstiff(X,IX,ne,mprop,K,D);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % linear strain displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 % vector of index used for building K
 [edof] = build_edof(IX, e);
 % build d vector
 [d] = build_d(D, edof); % d ia row vector
  % displacement dependent vector Bd
 Bd = 1/L0^2 * [10 -10;
              0 1 0 -1;
              -1 0 1 0;
              0 -1 0 1] * d';
 % compute the displacement
 epsilon_G = B0' * d' + 1/2*Bd'*d';
 % bar non-physical force
 N_G = A*E*epsilon_G;
 % element stiffness matrix
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k_0 = E * A * L0 * B0 * B0'; % 4x4 matrix
 k_d = E * A * L0 * B0 * Bd' + E * A * L0 * Bd * B0' + E * A * L0 * Bd * Bd';
 k_sigma = 1/L0^2 * [1 0 -1 0; 0 1 0 -1; -1 0 1 0; 0 -1 0 1]*N_G*L0;
 k_sum = k_0 + k_d + k_sigma;
 % build K by summing k_sum
 for ii = 1:4
   for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_sum(ii, jj);
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
function [epsilon_G, stress_G]=recover(mprop,X,IX,D,ne)
% This subroutine recovers the element stress, element strain, force on each element
% and nodal reaction forces
stress_G = zeros(ne, 1);
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % displacement dependent vector Bd
```

```
Bd = 1/L0^2 * [10 -10;
                 0 1 0 -1;
                 -1 0 1 0;
                 0 -1 0 1] * d';
  % compute the displacement
  epsilon_G = B0' * d' + 1/2 * Bd' * d';
  % materials properties
 propno = IX(e, 3);
  A = mprop(propno, 2);
 E = mprop(propno, 1);
 stress_G(e) = E*epsilon_G;
end
return
%%%% Residuals
function [R] = residual(stress, ne,IX, X, P, D, mprop)
R_{int} = zeros(2*size(X,1), 1);
 for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
  % build the matrix d from D
 d = build_d(D, edof);
  % compute the bar length
  [LO, delta_x, delta_y] = length(IX, X, e);
  % displacement vector
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
  % displacement dependent vector Bd
  Bd = 1/L0^2 * [10 -10;
                 0 1 0 -1;
                 -1 0 1 0;
                 0 -1 0 1] * d';
  B_bar = B0 + Bd;
  % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 N_G = A*stress(e,1);
  % sum BO after having transformed it in order to be compliant for the sum
  % with P
  for jj = 1:4
     R_{int}(edof(jj)) = R_{int}(edof(jj)) + B_{bar}(jj) * N_G * L0;
  end
  end
 R = R_int - P;
return
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```
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
% This subroutine plots the undeformed and deformed structure
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
figure(1)
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
eSTOP = 1e-8; % fake zero for tension sign decision
for e = 1:ne
   xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
   yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
   h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
   [edof] = build_edof(IX, e);
   xx = xx + D(edof(1:2:4));
   yy = yy + D(edof(2:2:4));
   % choice of thhe color according to the state
   if stress(e) > eSTOP % tension
     col = colors(1);
    elseif stress(e) < - eSTOP % compression</pre>
     col = colors(2);
   else col = colors(3); % un-loaded
   h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
               'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [LO, delta_x, delta_y] = length(IX, X, e)
 i = IX(e, 1);
  j = IX(e, 2);
  xi = X(i, 1);
  xj = X(j, 1);
  yi = X(i, 2);
 yj = X(j, 2);
  delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
```

```
function [edof] = build_edof(IX, e)
  edof = zeros(4, 1);
  edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return

%% Function to build d from D
function [d] = build_d(D, edof)
  for i = 1:4
    d(i) = D(edof(i));
  end
return
```

# 3.5 Input file for question 3

```
% Created with: FlExtract v1.13
% Element type: truss
% Number of nodes: 156
% Number of elements: 443
close all
clear all
clc
%SCALE = 1; % Ec = 0.8
%SCALE = 0.5; % Ec = 0.4
SCALE = 2; % EC = 1.6
nincr = 200;
i_max = 1000;
eSTOP = 10^(-9);
Pfinal = -0.004*SCALE;
% Node coordinates: x, y
X = [
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% Element connectivity: node1_id, node2_id, material_id
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153
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```

```
153 147 1
152 147 1
149 148 1
155 148 1
    148 1
154
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    149
        1
156
    149
         1
155
    149
         1
154
    149
         1
156
    150
         1
155
    150
         1
152
    151
         1
153 152 1
155 154 1
156 155 1
];
% Element properties: Young's modulus, area
mprop = [0.2 0.1 % beam
       0.8*SCALE
                    0.2]; % column
% Nodal diplacements: node_id, degree of freedom (1 - x, 2 - y), displacement
bound = [
151 1
151 2
         0
         0
152 1
         0
152 2
153 1
         0
153 2
         0
154 1
154 2
         0
         0
155 1
155 2
         0
156 1
         0
156 2
];
% Nodal loads: node_id, degree of freedom (1 - x, 2 - y), load
loads = [
21 2
         Pfinal
    2
         -Pfinal
1
];
% Control parameters
plotdof = 21;
```

#### 3.6 File for question 3

```
Newton Raphson method
function fea()
close all
clc
%--- Input file ------%
TrussExercise3_2022
disp(['Number of DOF ' sprintf('%d',neqn) ...
  ' Number of elements ' sprintf('%d',ne)]);
%--- Initialize arrays -----%
                 % Stiffness matrix
K=sparse(neqn,neqn);
                           % Force vector
P_final=zeros(neqn,1);
                            % Residual vector
R=zeros(neqn,1);
strain=zeros(ne,1);
stress=zeros(ne,1);
                            % Element strain vector
                            % Element stress vector
P_plot=zeros(nincr, 1);
D_plot=zeros(nincr, 1);
%--- Calculate displacements -----%
[P_final] = buildload(X,IX,ne,P_final,loads,mprop); % vector of the external loads
% load increment
delta_P = P_final / nincr;
clear P D0 D
% Initialize arrays
P=zeros(neqn,1);
                             % Force vector
D0=zeros(neqn,1);
                             % Displacement vector
D=zeros(neqn,1);
                             % Displacement vector
for n = 1:nincr % cycle to the number of increments
 P = P + delta_P; % increment the load
 DO = D:
 for i = 1:i_max
  K=zeros(neqn,neqn);
   [R] = residual(stress, ne,IX, X, P, D0, mprop);
                         % Enforce boundary conditions on R
   [~,R]=enforce(K,R,bound);
   if norm(R) <= eSTOP * norm(Pfinal) % break when we respect the eSTOP</pre>
    break
   [K, ~] = enforce(K,R,bound);
   [LM, UM] = lu(K);
```

```
delta_D0 = - UM \setminus (LM \setminus R);
   %delta_D0 = - K \setminus R;
   DO = DO + delta_DO;
   [~, stress] = recover(mprop,X,IX,D0,ne);
 end
 D = D0;
  % save data of the point of interest
 P_{plot}(n) = 2*P(2);
 D_{plot}(n) = -D(42) + D(2);
end
%save('E3_case2.mat', 'P_plot', 'D_plot'); % Ec = 0.4
save('E3_case3.mat', 'P_plot', 'D_plot'); % Ec = 1.6
%--- Print the results on the command window ------%
% disp(strcat('The maximum vertical displacement is d = ', num2str(v_disp)))
% % External matrix
% disp('External forces applied (N)')
% % Stress
% disp('Stress on the bars (MPa)')
% stress'
% % Strain
% disp('Strain of the bars')
% strain'
% % Forces on the bars
% disp('Internal forces on the bar (N)')
응 N
% % Support reaction
% disp('Support reactions forces (N)')
% R'
%--- Plot results ------%
[LO, ~, ~] = length(IX, X, 1);
lin_space = linspace(0, 0.9);
force_vs_disp_ex3_3 = figure('Position', get(0, 'Screensize'));
plot(D_plot, P_plot, '-', 'LineWidth', 2.5)
xlabel("Displacement (m)")
ylabel("Force (N)")
legend('disp','Location','southeast')
set(gca, 'FontAngle', 'oblique', 'FontSize', 20)
saveas(force_vs_disp_ex3_3 , 'C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\...
assignment1\force_vs_disp_ex3_3.png','png');
return
```

```
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
return
function [K, epsilon_G]=buildstiff(X,IX,ne,mprop,K,D);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % linear strain displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 % vector of index used for building K
 [edof] = build_edof(IX, e);
 % build d vector
 [d] = build_d(D, edof); % d ia row vector
  % displacement dependent vector Bd
 Bd = 1/L0^2 * [10 -10;
              0 1 0 -1;
              -1 0 1 0;
              0 -1 0 1] * d';
 % compute the displacement
 epsilon_G = B0' * d' + 1/2*Bd'*d';
 % bar non-physical force
 N_G = A*E*epsilon_G;
 % element stiffness matrix
 k_0 = E * A * L0 * B0 * B0'; % 4x4 matrix
```

```
k_d = E * A * L0 * B0 * Bd' + E * A * L0 * Bd * B0' + E * A * L0 * Bd * Bd';
 k_{sigma} = 1/L0^2 * [10-10;010-1;-1010;0-101]*N_G*L0;
 k_sum = k_0 + k_d + k_sigma;
 % build K by summing k_sum 
 for ii = 1:4
   for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_sum(ii, jj);
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
function [epsilon_G, stress_G] = recover(mprop, X, IX, D, ne)
% This subroutine recovers the element stress, element strain, force on each element
% and nodal reaction forces
stress_G = zeros(ne, 1);
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % displacement dependent vector Bd
 Bd = 1/L0^2 * [10 -10;
```

```
0 1 0 -1;
                -1 0 1 0;
                0 -1 0 1] * d';
 % compute the displacement
 epsilon_G = B0' * d' + 1/2 * Bd' * d';
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 E = mprop(propno, 1);
 stress_G(e) = E*epsilon_G;
end
return
%%%% Residuals
function [R] = residual(stress, ne,IX, X, P, D, mprop)
R_{int} = zeros(2*size(X,1), 1);
 for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 d = build_d(D, edof);
 % compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
 % displacement vector
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % displacement dependent vector Bd
 Bd = 1/L0^2 * [10 -10;
                0 1 0 -1;
                -1 0 1 0;
                0 -1 0 1] * d';
 B_bar = B0 + Bd;
 % materials properties
 propno = IX(e, 3);
 A = mprop(propno, 2);
 N_G = A*stress(e,1);
 % sum BO after having transformed it in order to be compliant for the sum
  % with P
 for jj = 1:4
     R_{int}(edof(jj)) = R_{int}(edof(jj)) + B_{bar}(jj) * N_G * L0;
 end
 R = R_{int} - P;
return
```

```
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress)
% This subroutine plots the undeformed and deformed structure
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
figure(1)
clf
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
eSTOP = 1e-8; % fake zero for tension sign decision
for e = 1:ne
    xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
    yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
    h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
    [edof] = build_edof(IX, e);
    xx = xx + D(edof(1:2:4));
    yy = yy + D(edof(2:2:4));
    % choice of thhe color according to the state
    if stress(e) > eSTOP % tension
      col = colors(1);
    elseif stress(e) < - eSTOP % compression</pre>
     col = colors(2);
    else col = colors(3); % un-loaded
    h2=plot(xx,yy, col,'LineWidth',3.5); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
                'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [L0, delta_x, delta_y] = length(IX, X, e)
  i = IX(e, 1);
  j = IX(e, 2);
  xi = X(i, 1);
  xj = X(j, 1);
yi = X(i, 2);
  yj = X(j, 2);
  delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e)
```

```
edof = zeros(4, 1);
edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
%% Function to build d from D
function [d] = build_d(D, edof)
  for i = 1:4
    d(i) = D(edof(i));
end
return
```

## 3.7 File used to plot all the case in the same graph

```
case1 = load('E3_case1.mat', 'D_plot', 'P_plot');
case2 = load('E3_case2.mat', 'D_plot', 'P_plot');
case3 = load('E3_case3.mat', 'D_plot', 'P_plot');
E3_comparison = figure('Position', get(0, 'Screensize'));
plot(case2.D_plot, case2.P_plot, 'LineWidth', 1.5)
hold on
plot(case1.D_plot, case1.P_plot, 'LineWidth', 1.5)
plot(case3.D_plot, case3.P_plot, 'LineWidth', 1.5)
hold off
xlabel('\Delta_Y [m]')
ylabel('Force [N]')
 \textbf{legend('E_{c}=0.4, P_{f}=0.002', 'E_{c}=0.8, P_{f}=0.004', 'E_{c}=1.6, P_{f}=0.008', \dots } 
'Location','northwest')
title('Influence of materila properties')
set(gca, 'FontAngle', 'oblique', 'FontSize', 20)
saveas(E3_comparison, 'C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\...
E3_comparison.png','png');
```

# 4 Exercise 4

end

### 4.1 Bisect function

```
function [rho] = bisect(rho_old, V_star, f_grad, g_grad, rho_min, eta, epsilon)
% Function to compute rho with the bisection algorithm
lambda_1 = 1e-10; % guess value for low extreme value
lambda_2 = 1e10; % guess value for high extreme value
while( (lambda_2 - lambda_1)/( lambda_1 + lambda_2) > epsilon)
  lambda_mid = (lambda_2 + lambda_1) / 2;
  ne = size(f_grad, 1); % number of elements in the structure
  rho = zeros(ne, 1);
  for e = 1:ne
   Be = - f_grad(e) / (lambda_mid * g_grad(e));
    if rho_old(e) * Be^eta <= rho_min</pre>
     rho(e) = rho_min;
    elseif rho_min < rho_old(e) * Be^eta && rho_old(e) * Be^eta < 1</pre>
      rho(e) = rho_old(e) * Be^eta;
    elseif rho_old(e) * Be^eta >= 1
     rho(e) = 1;
    end
  end
  if rho' * g_grad - V_star > 0
   lambda_1 = lambda_mid;
  else
    lambda_2 = lambda_mid;
  end
end
```

### 4.2 Code for $\eta$ optimization

```
Structure 3 with 40% connectivity has been used for the optimization, for \eta \in [0.65, 0.69].
```

```
응
                 Basic truss program
    Exercise 4.2 - Assignment 1: eta optimization before varying p
function fea()
close all
clc
%--- Input file -----%
mesh3 40
ne = size(IX,1);
                         % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
   ' Number of elements ' sprintf('%d',ne)]);
iterations = zeros(size(eta_vector,2),1);
for j = 1:size(eta_vector,2)
   eta = eta_vector(j);
  clear f_vector
Kmatr=sparse(neqn,neqn);
                   % Stiffness matrix
P=zeros(neqn,1);
                           % Force vector
D=zeros(neqn,1);
                            % Displacement vector
R=zeros(neqn,1);
                            % Residual vector
strain=zeros(ne,1);
                            % Element strain vector
stress=zeros(ne,1);
                            % Element stress vector
rho = zeros(ne,1);
[~,~,~,~,,~,g_grad]=recover(mprop,X,IX,D,ne,strain,stress,P,p,rho);
v = g_grad; % vector of element volumes and q_grad are the same
% Initialize the vector of relative element densities:
% We need the pseudo inverse matrix in order to initialize rho satisfying
% g=0:
v_sum = sum(v);
rho(:) = V_star/v_sum; % initially think rho as constant
[P]=buildload(X,IX,ne,P,loads,mprop); % Build global load vector
for iopt = 1:iopt_max
   rho_old = rho;
   %--- Calculate displacements -----%
   [Kmatr,P]=enforce(Kmatr,P,bound);
                                 % Enforce boundary conditions
  D = Kmatr \ P;
                                      % Solve system of equations
```

```
[~,~,~,~,f_grad,~,~]=recover(mprop,X,IX,D,ne,strain,stress,P,p,rho_old);
   rho = bisect(rho_old, V_star, f_grad, g_grad, rho_min, eta);
    [~,~,~,~,~,f]=recover(mprop,X,IX,D,ne,strain,stress,P,p,rho);
   f_vector(iopt) = f; % vector for convergence plot, cell j and entrance i
    if norm(rho_old - rho) < norm(rho)*epsilon</pre>
       break
end
f_cell{j} = f_vector;
iterations(j) = iopt;
% Save f_vector for convergence plot for different eta values:
[strain, stress, ~, ~, ~, ~, ~] = recover(mprop, X, IX, D, ne, strain, stress, P, p, rho);
% Check on the strain energy density = constant for active members:
energy_density = zeros(ne,1);
for e = 1:ne
    energy_density(e) = (strain(e)*stress(e))/rho(e);
end
end
iterations % stamp number of iterations for the current eta value
figure('color','white')
for s = 1:size(eta_vector,2)
    x_step = [1:1:iterations(s)];
    plot(x_step,f_cell{s},'.-','MarkerSize', 8)
   legend_name(s) = strcat("\eta = ",num2str(eta_vector(s)));
   hold on
end
grid on
set(gca,'FontAngle','oblique','FontSize',14)
legend(legend_name, 'location', 'northeast')
title('Convergence plot for different eta values', 'FontSize', 16)
xlabel('Topology Optimization iteration')
ylabel('Compliance f(\rho)')
% % Convergence plot:
% figure(1)
% x_step = [1:1:(iopt)];
% plot(x_step,f_vector,'-rx')
% grid on
% set(gca,'FontAngle','oblique','FontSize',14)
% title('Convergence plot', 'FontSize', 16)
% xlabel('Topology Optimization iteration')
% ylabel('Compliance f')
%--- Plot results ------%
% figure(2)
```

```
return
function [P]=buildload(X,IX,ne,P,loads,mprop)
P=zeros(size(X,1)*size(X,2),1);
rowX = size(X,1);
columnX = size(X,2);
for i=1:size(loads,1)
   pos = loads(i,1)*columnX - (columnX - loads(i,2));
   P(pos, 1) = loads(i,3);
end
return
function [K] = buildstiff(X,IX,ne,mprop,K,p,rho)
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
   K = zeros(2*size(X,1)); % global stiffness matrix def., 6x6, memory allocation
for e=1:ne
   i = IX(e,1);
   j = IX(e,2);
   xi = X(i,1);
   yi = X(i,2);
   xj = X(j,1);
   yj = X(j,2);
   delta_x = (xj-xi);
   delta_y = (yj-yi);
   L0 = sqrt(delta_x^2 + delta_y^2);
   B0 = (1/(L0^2))*[-delta_x, -delta_y, delta_x, delta_y]';
   % material properties of the current beam
   propno = IX(e,3);
   E0 = mprop(propno,1);
   A = mprop(propno,2);
   k_0e = E0*A*L0*(B0)*(B0'); % 4x4 matrix, local
   k_e = (rho(e))^p * k_0e;
   edof = [IX(e,1)*2 - 1, IX(e,1)*2 - 0, IX(e,2)*2 - 1, IX(e,2)*2 - 0];
   for ii = 1:4
      for jj = 1:4
         K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
      end
```

end

#### end

```
return
function [K,P] = enforce(K,P,bound)
% This subroutine enforces the support boundary conditions
% 0 and 1 Method:
for i=1:size(bound,1)
   node = bound(i,1); % from example1.m data
   ldof = bound(i,2);
   K(:,2*node - (2-ldof)) = 0; % zeros in the column
   K(2*node - (2-ldof),:) = 0; % zeros in the row
   K(2*node - (2-ldof), 2*node - (2-ldof)) = 1; % put a 1 in the diagonal
   P(2*node - (2-ldof)) = 0; % updating P vector
end
return
function [strain, stress, N, R, f_grad, g_grad, f] = recover(mprop, X, IX, D, ne, strain, stress, P, p, rho)
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
d = zeros(4,1);
strain = zeros(ne,1); % allocation strain vector
stress = zeros(ne,1); % allocation stress vector
N = zeros(ne,1); % allocation element forces vector
B0sum = zeros(2*size(X,1),1);
f_grad = zeros(ne,1);
g_grad = zeros(ne,1);
f = 0; % initialize outside of the loop
for e=1:ne
   edof = [IX(e,1)*2 - 1, IX(e,1)*2 - 0, IX(e,2)*2 - 1, IX(e,2)*2 - 0];
   % define small d
   for i=1:4
      d(i) = D(edof(i));
   end
   i = IX(e,1);
   j = IX(e,2);
   xi = X(i,1);
   yi = X(i,2);
   xj = X(j,1);
   yj = X(j,2);
   delta_x = (xj-xi);
   delta_y = (yj-yi);
   L0 = sqrt(delta_x^2 + delta_y^2);
   B0 = (1/(L0^2))*[-delta_x, -delta_y, delta_x, delta_y]';
```

propno = IX(e,3); E0 = mprop(propno,1);

```
A = mprop(propno,2);
   % local k matrix for gradient calculation
   k_0e = E0*A*L0*(B0)*(B0'); % 4x4 matrix, local
   strain(e) = (B0') * d;
   stress(e) = rho(e)^p*E0*strain(e);
   N(e) = stress(e)*A;
   % Element volume inside the respective vector:
   g_grad(e) = A*L0;
   % Calculation of the gradients of f and g:
   f_grad(e) = -p*((rho(e))^(p-1)) * (d') * k_0e * d;
   f = f + (d')*(rho(e)^p)*k_0e*d; % objective function
   % Calculation of reaction forces R:
   for jj=1:4
       BOsum(edof(jj)) = BOsum(edof(jj)) + BO(jj)*N(e)*LO;
end
% Reaction forces vector:
R = B0sum - P;
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress,rho)
% This subroutine plots the undeformed and deformed structure
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
clf
hold on
box on
color_vector = ['r', 'b', 'g']; % vector for colors of the trusses
fake_zero = 1e-10; % fake zero to enter the if cycle below
for e = 1:ne
   xx = X(IX(e,1:2),1); % x-coord. of the nodes of the selected element (bar, truss)
   yy = X(IX(e,1:2),2);
    % plot of undeformed structure!
   h1=plot(xx,yy,'k:','LineWidth',1);
   edof = [2*IX(e,1)-1 2*IX(e,1) 2*IX(e,2)-1 2*IX(e,2)];
   xx = xx + D(edof(1:2:4));
   yy = yy + D(edof(2:2:4));
   if stress(e) > fake_zero
       col = color_vector(2); % element in tension
   elseif stress(e) < - fake_zero</pre>
       col = color_vector(1); % element in compression
       col = color_vector(3); % unloaded element
```

## 4.3 Code for testing different p values

Structure 3 with 40% connectivity has been used for  $\eta \in [0.65, 0.69]$  and  $p \in [1.5:0.2:1.9]$ .

```
용
                 Basic truss program
        Exercise 4.2 - Assignment 1: different p value
function fea()
close all
clc
mesh3 40
neqn = size(X,1)*size(X,2);
                         % Number of equations
ne = size(IX,1);
                         % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
   ' Number of elements ' sprintf('%d',ne)]);
iterations = zeros(size(p_vector,2),1);
f_vector_plot = zeros(size(p_vector,2),iopt_max);
for j = 1:size(p_vector,2)
  p = p_vector(j);
  clear f_vector
%--- Initialize arrays ------%
Kmatr=sparse(neqn,neqn);
                   % Stiffness matrix
P=zeros(neqn,1);
                           % Force vector
D=zeros(neqn,1);
                            % Displacement vector
                            % Residual vector
R=zeros(neqn,1);
strain=zeros(ne,1);
                            % Element strain vector
stress=zeros(ne,1);
                            % Element stress vector
rho = zeros(ne,1);
[~,~,~,~,,~,g_grad]=recover(mprop,X,IX,D,ne,strain,stress,P,p,rho);
v = g_grad; % vector of element volumes and g_grad are the same
% Initialize the vector of relative element densities:
% We need the pseudo inverse matrix in order to initialize rho satisfying
% q=0:
v_sum = sum(v);
rho(:) = V_star/v_sum; % initially think rho as constant
for iopt = 1:iopt_max
   rho_old = rho;
   %--- Calculate displacements -----%
   [Kmatr,P]=enforce(Kmatr,P,bound);
                                 % Enforce boundary conditions
```

```
D = Kmatr \setminus P;
                                                        % Solve system of equations
    [-,-,-,-,-,-] = recover (mprop, X, IX, D, ne, strain, stress, P, p, rho_old);
    rho = bisect(rho_old, V_star, f_grad, g_grad, rho_min, eta);
    [~,~,~,~,~,f]=recover(mprop,X,IX,D,ne,strain,stress,P,p,rho);
    f_vector(iopt) = f; % vector for convergence plot, cell j and entrance i
    f_vector_plot(j,iopt) = f;
    if norm(rho_old - rho) < norm(rho)*epsilon</pre>
        break
    end
end
f_cell{j} = f_vector;
iterations(j) = iopt;
% Save f_vector for convergence plot for different eta values:
[strain, stress, ~, ~, ~, ~, ~] = recover(mprop, X, IX, D, ne, strain, stress, P, p, rho);
% Check on the strain energy density = constant for active members:
energy_density = zeros(ne,1);
for e = 1:ne
    energy_density(e) = (strain(e)*stress(e))/rho(e);
end
iterations % stamp number of iterations for the current eta value
figure('color','white')
for s = 1:size(p_vector,2)
    x_step = [1:1:iterations(s)];
    plot(x_step,f_cell{s},'.-','MarkerSize', 8)
    legend_name(s) = strcat("p = ",num2str(p_vector(s)));
    hold on
end
hold off
grid on
set(gca,'FontAngle','oblique','FontSize',14)
legend(legend_name, 'location', 'northeast')
title('Convergence plot for different p values', 'FontSize', 16)
xlabel('Topology Optimization iteration')
ylabel('Compliance f(\rho)')
figure('color','white')
for s = 1:size(p_vector,2)
    x_step = [1:1:iterations(s)];
    semilogy(x_step,f_cell{s},'.-','MarkerSize', 8)
    legend_name(s) = strcat("p = ",num2str(p_vector(s)));
    hold on
end
hold off
```

```
axis([0 100 0 10^(-4)])
grid on
set(gca, 'FontAngle', 'oblique', 'FontSize', 14)
legend(legend_name, 'location', 'northeast')
title('Convergence plot for different p values in log scale', 'FontSize', 16)
xlabel('Topology Optimization iteration')
ylabel('Compliance f(\rho)')
% % Convergence plot:
% figure(1)
% x_step = [1:1:(iopt)];
% plot(x_step,f_vector,'-rx')
% grid on
% set(gca,'FontAngle','oblique','FontSize',14)
% title('Convergence plot', 'FontSize', 16)
% xlabel('Topology Optimization iteration')
% ylabel('Compliance f')
%--- Plot results ------%
%x_step = [1:1:100];
%save('E4_case_3.mat','f_vector_plot','x_step');
return
function [P]=buildload(X,IX,ne,P,loads,mprop)
P=zeros(size(X,1)*size(X,2),1);
rowX = size(X,1);
columnX = size(X,2);
for i=1:size(loads,1)
   pos = loads(i,1)*columnX - (columnX - loads(i,2));
  P(pos, 1) = loads(i,3);
end
return
function [K] = buildstiff(X,IX,ne,mprop,K,p,rho)
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
   K = zeros(2*size(X,1)); % global stiffness matrix def., 6x6, memory allocation
for e=1:ne
   i = IX(e,1);
   j = IX(e, 2);
   xi = X(i,1);
   yi = X(i,2);
  xj = X(j,1);
   yj = X(j,2);
```

```
delta_x = (xj-xi);
   delta_y = (yj-yi);
   L0 = sqrt(delta_x^2 + delta_y^2);
   B0 = (1/(L0^2))*[-delta_x, -delta_y, delta_x, delta_y]';
   % material properties of the current beam
   propno = IX(e,3);
   E0 = mprop(propno,1);
   A = mprop(propno,2);
   k_0e = E0*A*L0*(B0)*(B0'); % 4x4 matrix, local
   k_e = (rho(e))^p * k_0e; % now the stiffness is a function of the design variable density
   edof = [IX(e,1)*2 - 1, IX(e,1)*2 - 0, IX(e,2)*2 - 1, IX(e,2)*2 - 0];
   for ii = 1:4
       for jj = 1:4
          K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + k_e(ii, jj);
       end
   end
end
return
function [K,P] = enforce(K,P,bound)
% This subroutine enforces the support boundary conditions
% 0 and 1 Method:
for i=1:size(bound,1)
   node = bound(i,1); % from example1.m data
   ldof = bound(i,2);
   K(:,2*node - (2-ldof)) = 0; % zeros in the column
   K(2*node - (2-ldof),:) = 0; % zeros in the row
   K(2*node - (2-ldof), 2*node - (2-ldof)) = 1; % put a 1 in the diagonal
   P(2*node - (2-ldof)) = 0; % updating P vector
end
return
function [strain, stress, N, R, f_grad, g_grad, f] = recover(mprop, X, IX, D, ne, strain, stress, P, p, rho)
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
d = zeros(4,1);
strain = zeros(ne,1); % allocation strain vector
stress = zeros(ne,1); % allocation stress vector
N = zeros(ne,1); % allocation element forces vector
B0sum = zeros(2*size(X,1),1);
f_grad = zeros(ne,1);
g_grad = zeros(ne,1);
```

```
f = 0; % initialize outside of the loop
for e=1:ne
   edof = [IX(e,1)*2 - 1, IX(e,1)*2 - 0, IX(e,2)*2 - 1, IX(e,2)*2 - 0];
   % define small d
   for i=1:4
       d(i) = D(edof(i));
   end
   i = IX(e,1);
   j = IX(e,2);
   xi = X(i,1);
   yi = X(i,2);
   xj = X(j,1);
   yj = X(j,2);
   delta_x = (xj-xi);
   delta_y = (yj-yi);
   L0 = sqrt(delta_x^2 + delta_y^2);
   B0 = (1/(L0^2))*[-delta_x, -delta_y, delta_x, delta_y]';
   propno = IX(e,3);
   E0 = mprop(propno,1);
   A = mprop(propno,2);
   % local k matrix for gradient calculation \\
   k_0e = E0*A*L0*(B0)*(B0'); % 4x4 matrix, local
   strain(e) = (B0') * d;
   stress(e) = rho(e)^p*E0*strain(e);
   N(e) = stress(e)*A;
   % Element volume inside the respective vector:
   g_grad(e) = A*L0;
   % Calculation of the gradients of f and g:
   f_grad(e) = -p*((rho(e))^(p-1)) * (d') * k_0e * d;
   f = f + (d')*(rho(e)^p)*k_0e*d; % objective function
   % Calculation of reaction forces R:
   for jj=1:4
       BOsum(edof(jj)) = BOsum(edof(jj)) + BO(jj)*N(e)*LO;
   end
end
% Reaction forces vector:
R = B0sum - P;
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress,rho)
% This subroutine plots the undeformed and deformed structure
```

```
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
clf
hold on
box on
color_vector = ['r', 'b', 'g']; % vector for colors of the trusses
fake_zero = 1e-10; % fake zero to enter the if cycle below
for e = 1:ne
    xx = X(IX(e,1:2),1); % x-coord. of the nodes of the selected element (bar, truss)
    yy = X(IX(e,1:2),2);
    % plot of undeformed structure!
    h1=plot(xx,yy,'k:','LineWidth',1);
    edof = [2*IX(e,1)-1 2*IX(e,1) 2*IX(e,2)-1 2*IX(e,2)];
    xx = xx + D(edof(1:2:4));
    yy = yy + D(edof(2:2:4));
    if stress(e) > fake_zero
        col = color_vector(2); % element in tension
    elseif stress(e) < - fake_zero</pre>
        col = color_vector(1); % element in compression
        col = color_vector(3); % unloaded element
    end
    h2=plot(xx,yy,col,'LineWidth',7.5*rho(e));
end
plotsupports
plotloads
title('Non-Active elements are plotted in white color', 'FontSize', 16)
legend([h1 h2],{'Undeformed state',...
                'Deformed state'})
axis equal;
hold off
return
```

# 4.4 Input file for one node configuration

```
% Created with:
                    FlExtract v1.13
% Element type:
                    truss
% Number of nodes: 24
% Number of elements: 157
%clear all
eta = 0.67;
p = 1.5;
V_star = 6;
iopt_max = 100;
rho_min = 1e-6;
epsilon = 1e-5;
% Node coordinates: x, y
X = [
0
    0
0 0.5
0
    1
0.25 0
0.25 0.5
0.25 1
0.5 0
0.5 0.5
0.5 1
0.75 0.5
0.75 1
1 0.5
1 1
1.25 0.5
1.25 1
1.5 0
1.5 0.5
1.5 1
1.75 0
1.75 0.5
1.75 1
2
    0
2
    0.5
2
    1
];
% Element connectivity: node1_id, node2_id, material_id
IX = \Gamma
2
    1
3
4
5
   1
6
    1
         1
7
    1
         1
8
    1
         1
9
    1
         1
3
    2
         1
4
    2
         1
5
    2
         1
6
    2
         1
7
    2
         1
8
    2
         1
    2
         1
9
10
    2
         1
```

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11
     2
           1
12
     2
           1
13
      2
           1
4
      3
           1
5
     3
           1
6
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           1
7
     3
           1
8
     3
           1
9
     3
           1
10
     3
           1
11
     3
           1
12
      3
           1
13
     3
           1
5
     4
           1
6
     4
           1
7
     4
           1
8
      4
           1
9
      4
           1
11
      4
           1
6
      5
           1
7
      5
8
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           1
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      5
           1
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           1
14
      10
           1
```

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17
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12
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            1
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            1
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24
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19
      18
            1
20
      18
            1
```

```
21
   18 1
22
   18 1
23
    18
       1
24
    18
       1
20
    19
        1
21
    19
        1
22
    19
        1
23
    19
        1
24
    19
        1
21
    20
        1
22
    20
        1
23
    20
       1
    20
24
22
    21 1
       1
23
    21
       1
24
   21
       1
23
   22
24 22 1
24
];
% Element properties: Young's modulus, area
mprop = [
1
   1
2
    2
];
% Nodal diplacements: node_id, degree of freedom (1 - x, 2 - y), displacement
bound = [
  1
1
1
    2
         0
4
4
    2
7
         0
7
    2
        0
16
    1
        0
16
    2
        0
19
    1
        0
19
    2
        0
22
    1
        0
22
];
% Nodal loads: node_id, degree of freedom (1 - x, 2 - y), load
loads = [
10 2 -0.01
% Control parameters
plotdof = 2;
```

# 4.5 Code for running the method on the same node configuration with different connectivities

```
% RUN OVER DIFFERENT NUMBER OF NODES WITH ONLY NEIGHBOR CONNECTIONS %
function fea()
close all
c1 c
file vector = [ ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh1.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2.m" ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5 ANNO\FEM\assignment1\ex4\mesh\mesh3.m" \dots
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh4.m" ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh5.m"
file_number = size(file_vector, 2);
node_number_vector = [10 29 90 223 406]; % number of the node where the force is applied
disp_vector = zeros(1, file_number); % vector of final displacements
comple_vector = zeros(1, file_number); % vector of final compliance
total_nodes = zeros(1, file_number); % number of nodes of the structure
for j=1:file_number
%loadfile(file_vector(j));
run(file_vector(j));
node_number = node_number_vector(j);
%ex4_1
ne = size(IX,1);
                            % Number of elements
disp(['Number of DOF ' sprintf('%d',neqn) ...
   ' Number of elements ' sprintf('%d',ne)]);
$--- Initialize arrays ------
Kmatr=sparse(neqn,neqn);
                               % Stiffness matrix
                               % Force vector
P=zeros(neqn,1);
D=zeros(neqn,1);
                               % Displacement vector
R=zeros(neqn,1);
                                % Residual vector
strain=zeros(ne,1);
                                % Element strain vector
stress=zeros(ne,1);
                               % Element stress vector
rho = zeros(ne,1);
rho_old = zeros(ne,1);
[~,~,~,~,g_grad,~] =recover(mprop,X,IX,D,ne,strain,stress,P, p, rho); % volume vector
 % initialize the density vector, supposing each element equal
 rho(:) = V_star / sum(g_grad); % v and g_grad are the same
 [P]=buildload(X,IX,ne,P,loads,mprop); % Build global load vector
 for i=1:iopt_max
   rho_old = rho;
   [Kmatr, Pmatr] = enforce (Kmatr, P, bound); % Enforce boundary conditions
```

```
D = Kmatr \ Pmatr;
                                         % Solve system of equations
   [~,~,~,f_grad,~,~] =recover(mprop,X,IX,D,ne,strain,stress,P, p, rho_old); ...
   % compute f_grad
   rho = bisect(rho_old, V_star, f_grad, g_grad, rho_min, eta, epsilon); ...
   % compute the better guess for rho
   [~,~,~,~,,,,f(i)] =recover(mprop,X,IX,D,ne,strain,stress,P, p, rho); ...
   % compute the compliance f
    if norm(rho_old - rho) < norm(rho) * epsilon % check the convergence
     break
    end
 end
 disp\_vector(j) = D(node\_number * 2); % y displacement of the node of interest
 compl_vector(j) = f(end); % final compliance of the method
 total_nodes(j) = size(X, 1); % number of nodes
end
응응
%--- Plot results ------%
compliance_vs_node_neighbor = figure('Position', get(0, 'Screensize'));
plot(total_nodes, compl_vector, 'o', 'LineWidth', 3.5);
xlabel('Nodes')
ylabel('Compliance [J]')
title('Compliance for only neighbor connections')
set(gca, 'FontAngle', 'oblique', 'FontSize', 20)
saveas(compliance_vs_node_neighbor, 'C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment
compliance_vs_node_neighbor.png','png');
displacement_vs_node_neighbor = figure('Position', get(0, 'Screensize'));
plot(total_nodes, disp_vector, 'o', 'LineWidth', 3.5)
xlabel('Nodes')
ylabel('Displacement [m]')
title('Displacement for only neighbor connection')
set(gca, 'FontAngle', 'oblique', 'FontSize', 20)
compliance_vs_node_neighbor.png','png');
응응
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% P contains the external forces applied by the load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
 pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
 P(pos, 1) = loads(i, 3);
end
```

return

```
function [K] = buildstiff(X,IX,ne,mprop,K,p,rho);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector (4x1)
 B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E = mprop(propno, 1);
 A = mprop(propno, 2);
 % element stiffness matrix
 k_0e = E * A * L0 * B0 * B0'; % 4x4 matrix
 % vector of index used for building K
 [edof] = build_edof(IX, e);
 % build K by summing k_e
 for ii = 1:4
   for jj = 1:4
    K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + rho(e)^p*k_0e(ii, jj);
 end
end
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
  node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
  P(pos) = 0; % putting 0 in P
end
return
% function [strain, stress]=recover(mprop, X, IX, D, ne, strain, stress);
```

```
% % This subroutine recovers the element stress, element strain,
% % and nodal reaction forces
% % allocate memory for stress and strain vectors
% strain = zeros(ne, 1);
% stress = zeros(ne, 1);
% for e=1:ne
   d = zeros(4, 1); % allocate memory for element stiffness matrix
  [edof] = build_edof(IX, e); % index for buildg K
응
응
  % build the matrix d from D
응
  for i = 1:4
응
    d(i) = D(edof(i));
응
응
  end
응
응
   % compute the bar length
응
  [L0, delta_x, delta_y] = length(IX, X, e);
응
응
  % displacement vector
응
  B0 = 1/L0^2 * [-delta_x - delta_y delta_x delta_y]';
00
응
  % materials properties
용
  propno = IX(e, 3);
용
  E = mprop(propno, 1);
응
   A = mprop(propno, 2);
   strain(e) = B0' * d;
응
응
   stress(e) = strain(e) * E;
응
% end
2
0
% return
function [strain, stress, N, R, f_grad, g_grad, f] = recover(mprop, X, IX, D, ne, ...
strain, stress, P, p, rho)
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
strain = zeros(ne, 1);
stress = zeros(ne, 1);
B0_sum = zeros(2*size(X,1), 1);
g_grad = zeros(ne, 1); % vector of volumes IT IS THE SAME AS v
f_grad = zeros(ne,1); % gradient of f
f = 0; % compliance
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
  % build the matrix d from D
 for i = 1:4
   d(i) = D(edof(i));
 end
```

```
% compute the bar length
 [LO, delta_x, delta_y] = length(IX, X, e);
  % displacement vector (4x1)
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E0 = mprop(propno, 1);
 A = mprop(propno, 2);
  % element stiffness matrix
 k_0e = E0 * A * L0 * B0 * B0'; % 4x4 matrix
 % compute the volume
 g_grad(e) = L0 * A;
 strain(e) = B0' * d;
 stress(e) = rho(e)^p*strain(e) * E0;
 N(e) = stress(e) * A;
 % sum BO after having transformed it in order to be compliant for the sum
  % with P
 for jj = 1:4
     B0_sum(edof(jj)) = B0_sum(edof(jj)) + B0(jj)*N(e)*L0;
 end
 f_grad(e) = -p*rho(e)^(p - 1)*d'*k_0e*d; % ATTENTION TO DIMENSION OF d
 f = f + d' * rho(e)^p * k_0e * d; % compute the compliance
end
% compute the support reactions (N)
R = B0\_sum - P; % 2nnx1 (nn is node number)
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress,rho)
% This subroutine plots the undeformed and deformed structure
h1=0; h2=0;
% Plotting Un-Deformed and Deformed Structure
clf
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
fake_zero = 1e-8; % fake zero for tension sign decision
for e = 1:ne
   xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
   yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
   h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
   [edof] = build_edof(IX, e);
   xx = xx + D(edof(1:2:4));
   yy = yy + D(edof(2:2:4));
```

```
% choice of thhe color according to the state
    if stress(e) > fake_zero % tension
      col = colors(1);
    elseif stress(e) < - fake_zero % compression</pre>
     col = colors(2);
    else col = colors(3); % un-loaded
    end
    thick = 3.5*rho(e);
    h2=plot(xx,yy, col,'LineWidth',thick); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
                'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [LO, delta_x, delta_y] = length(IX, X, e)
  i = IX(e, 1);
  j = IX(e, 2);
 xi = X(i, 1);
 xj = X(j, 1);
yi = X(i, 2);
  yj = X(j, 2);
  delta_x = xj - xi;
  delta_y = yj - yi;
  L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e)
  edof = zeros(4, 1);
  edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
```

### 4.6 Code for computing different connectivities and different configurations

```
% RUN OVER DIFFERENT NUMBER OF NODES AND DIFFERENT CONNECTIVITY FACTORS
function fea()
close all
clc
%--- Input file ------%
file_vector = [
  ["C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh1_30.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh1_30.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh1_40.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh1_50.m" ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5\ANNO\FEM\assignment1\ex4\mesh\mesh1\_70.m" \dots
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh1_90.m"] ...
  ["C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2\_30.m", \dots
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2_40.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2_50.m" ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2_70.m" ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh2_90.m"]
  ["C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh3.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh3_30.m", ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh3\_40.m", \dots
 "C:\Users\Niccolo\Documents\UNIVERSITA\5\ANNO\FEM\assignment1\ex4\mesh\mesh3\_50.m" \dots
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh3_70.m" ...
 "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh3_90.m"]
   ["C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh4\_30.m", ...
   "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh4_40.m", ...
   "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh4_50.m" ...
   "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh4_70.m" ...
   "C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM\assignment1\ex4\mesh\mesh4_90.m"|
 ];
node_item = size(file_vector, 1);
conn_item = size(file_vector, 2);
percentage_rate = [0 30 40 50 70 90];
file_number = size(file_vector, 2);
node_number_vector = [10 29 58 223]; % number of the node where the force is applied
disp_mat = zeros(node_item, conn_item); % vector of final displacements
compl_mat = zeros(node_item, conn_item); % vector of final compliance
total_nodes = zeros(node_item, conn_item); % number of nodes of the structure
f = zeros(node_item,4);
for n = 1:node_item % run over number of nodes
 for j = 1:conn_item % run over different connectivitues
   run(file_vector(n, j)); % load the file
   neqn = size(X,1)*size(X,2);
                                     % Number of equations
   ne = size(IX,1);
                                     % Number of elements
   node_number = node_number_vector(n); % node number
   Kmatr=sparse(neqn, neqn);
                                         % Stiffness matrix
```

```
P=zeros(neqn,1);
                                          % Force vector
   D=zeros(neqn,1);
                                           % Displacement vector
   R=zeros(neqn,1);
                                           % Residual vector
    strain=zeros(ne,1);
                                           % Element strain vector
                                           % Element stress vector
    stress=zeros(ne,1);
   rho = zeros(ne,1);
   rho_old = zeros(ne,1);
    [~,~,~,~,g_grad,~] =recover(mprop,X,IX,D,ne,strain,stress,P, p, rho); % volume vector
    % initialize the density vector, supposing each element equal
    rho(:) = V_star / sum(g_grad); % v and g_grad are the same
    [P]=buildload(X,IX,ne,P,loads,mprop);
                                           % Build global load vector
    for i=1:iopt_max
     rho_old = rho;
      [Kmatr] = buildstiff(X,IX,ne,mprop,Kmatr,p,rho_old);
                                                          % Build global stiffness matrix
      [Kmatr, Pmatr] = enforce (Kmatr, P, bound);
                                                % Enforce boundary conditions
      D = Kmatr \ Pmatr;
                                                 % Solve system of equations
      [~,~,~,~,f_grad,~,~] = recover(mprop,X,IX,D,ne,strain,stress,P, p, rho_old); ...
      % compute f_grad
      rho = bisect(rho_old, V_star, f_grad, g_grad, rho_min, eta, epsilon); ...
      % compute the better guess for rho
      [~,~,~,~,,~,f] = recover(mprop,X,IX,D,ne,strain,stress,P, p, rho);...
      % compute the compliance f
      if norm(rho_old - rho) < norm(rho) * epsilon % check the convergence</pre>
       break
      disp_mat(n, j) = D(node_number * 2); % y displacement of the node of interest
      compl_mat(n, j) = f; % final compliance of the method
    end
  end
  total_nodes(n) = size(X, 1); % number of nodes
end
% manually add results for mesh 4
mesh4_results_disp = [0.00923402 0.00683920, 0.00633002, 0.00691394, 0.00725176, 0.00636457]; .
% displacement of mesh 4
mesh4_results_complinace = [0.00009234 6.8392e-5, 6.3300e-5, 6.9139e-5, 7.2517e-5, 6.3646e-5];
% complinace of mesh 4
응응
%--- Plot results ------%
save("results", "compl_mat", "disp_mat", "total_nodes");
res = load("results.mat")
node_item = 3;
percentage_rate = [0 30 40 50 70 90];
% manually add results for mesh 4
mesh4_results_disp = [0.00923402 0.00683920, 0.00633002, 0.00691394, 0.00725176, 0.00636457]; %
mesh4_results_complinace = [0.00009234 6.8392e-5, 6.3300e-5, 6.9139e-5, 7.2517e-5, 6.3646e-5];
compl_mat = res.compl_mat;
```

```
%disp_mat = res.disp_mat;
total_nodes = res.total_nodes;
%compliance_vs_percentage_vs_node = figure('Position', get(0, 'Screensize'));
compliance_vs_percentage_vs_node = figure('Color','White');
legend_vector = strings(1, node_item);
for i =1:node_item
 plot(percentage_rate, compl_mat(i,:), '-', 'LineWidth',1,...
  'Marker', '.', 'MarkerSize',35);
 legend_vector(i) = strcat("Structure ", num2str(i), ": ", num2str(total_nodes(i)), " nodes");
 hold on
end
plot(percentage_rate, mesh4_results_complinace, '-', 'LineWidth',1, 'Marker', '.', 'MarkerSize
hold off
xlabel('Connectivity [%]')
ylabel('Compliance [J]')
legend_vector(end + 1) = "Structure 4: 537 nodes";
legend(legend_vector)
legend(legend_vector)
title ('Compliance for different nodes and connectivity radius', 'FontSize', 16)
set(gca, 'FontAngle', 'oblique', 'FontSize', 14)
saveas(compliance_vs_percentage_vs_node , 'C:\Users\Niccolo\Documents\UNIVERSITA\5ANNO\FEM ...
\assignment1\compliance_vs_percentage_vs_node.png','png');
% displacement_vs_percentage_vs_node = figure('Position', get(0, 'Screensize'));
% for i=1:node_item
   plot(percentage_rate, disp_mat(i,:), 'o', 'LineWidth', 3.5)
   hold on
% end
% hold off
% xlabel('Nodes')
% ylabel('Displacement [m]')
% legend(legend_vector)
% title('Displacement for 71 nodes - different connection percentage')
% set(gca, 'FontAngle', 'oblique', 'FontSize', 20)
% marker = ['o', '+', '*', 'x']; % markers for different plots
% legend_vector = strings(1, node_item);
% displacement_vs_percentage_vs_node = figure('Position', get(0, 'Screensize'));
% for i=1:node_item
  yyaxis left
  plot(percentage_rate, compl_mat(i,:), marker(i), 'LineWidth', 1.5);
응
% legend_vector(i) = strcat(num2str(total_nodes(i)), " nodes");
% end
% for i = 1:node_item
  yyaxis right
  plot(percentage_rate, abs(disp_mat(i,:)), marker(i), 'LineWidth', 1.5)
응
   hold on
% end
% yyaxis left
% plot(percentage_rate, mesh4_results_complinace, marker(end), 'LineWidth', 1.5);
% vvaxis right
% plot(percentage_rate, mesh4_results_disp, marker(end), 'LineWidth', 1.5);
% hold off
% xlabel('Nodes')
% yyaxis right
% ylabel('Displacement [m]')
% yyaxis left
% ylabel('Compliance [J]')
```

```
% legend_vector(end + 1) = "537 nodes";
% legend(legend_vector)
% title('Compliance and disp. for different nodes and connectivities')
% set(gca, 'FontAngle', 'oblique', 'FontSize', 20)
\$ \ save as (displacement\_vs\_percentage\_vs\_node, \ 'C: \ \ Vsers \setminus Niccolo \setminus Documents \setminus UNIVERSITA \setminus 5ANNO \setminus FEM \setminus algorithms \setminus SANNO \setminus SAN
return
function [P]=buildload(X,IX,ne,P,loads,mprop);
rowX = size(X, 1);
columnX = size(X, 2);
% \ P \ contains \ the \ external \ forces \ applied \ by \ the \ load
% P is a 2nnx1 matrix (nn is the number of nodes)
P = zeros(columnX * rowX, 1); % assign the memory for P
for i=1:size(loads,1)
     pos = loads(i, 1)*columnX - (columnX - loads(i, 2));
      P(pos, 1) = loads(i, 3);
end
return
function [K] = buildstiff(X,IX,ne,mprop,K,p,rho);
% This subroutine builds the global stiffness matrix from
% the local element stiffness matrices
K = zeros(2*size(X, 1)); % allocate memory
for e = 1:ne % cycle on the different bar
       % compute the bar length
      [LO, delta_x, delta_y] = length(IX, X, e);
      % displacement vector (4x1)
      B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
      % materials properties
      propno = IX(e, 3);
      E = mprop(propno, 1);
      A = mprop(propno, 2);
      % element stiffness matrix
      k_0e = E * A * L0 * B0 * B0'; % 4x4 matrix
       % vector of index used for building K
      [edof] = build_edof(IX, e);
       % build K by summing k_e
      for ii = 1:4
            for jj = 1:4
                  K(edof(ii), edof(jj)) = K(edof(ii), edof(jj)) + rho(e)^p*k_0e(ii, jj);
             end
      end
```

#### end

```
return
function [K,P] = enforce(K,P,bound);
% This subroutine enforces the support boundary conditions
% 0-1 METHOD
for i=1:size(bound,1)
   node = bound(i, 1); % number of node
   ldof = bound(i, 2); % direction
   pos = 2*node - (2 - 1dof);
   K(:, pos) = 0; % putting 0 on the columns
   K(pos, :) = 0; % putting 0 on the rows
   K(pos, pos) = 1; % putting 1 in the dyagonal
   P(pos) = 0; % putting 0 in P
end
return
% function [strain, stress]=recover(mprop, X, IX, D, ne, strain, stress);
% % This subroutine recovers the element stress, element strain,
% % and nodal reaction forces
% % allocate memory for stress and strain vectors
% strain = zeros(ne, 1);
% stress = zeros(ne, 1);
% for e=1:ne
  d = zeros(4, 1); % allocate memory for element stiffness matrix
응
응
% [edof] = build_edof(IX, e); % index for buildg K
응
 % build the matrix d from D
 for i = 1:4
응
응
   d(i) = D(edof(i));
응
   end
00
  % compute the bar length
응
   [LO, delta_x, delta_y] = length(IX, X, e);
용
00
응
   % displacement vector
응
   B0 = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
응
   % materials properties
  propno = IX(e, 3);
응
응
  E = mprop(propno, 1);
  A = mprop(propno, 2);
응
응
  strain(e) = B0' * d;
응
  stress(e) = strain(e) * E;
용
응
% end
```

```
% return
strain,stress,P,p,rho)
% This subroutine recovers the element stress, element strain,
% and nodal reaction forces
strain = zeros(ne, 1);
stress = zeros(ne, 1);
B0_sum = zeros(2*size(X,1), 1);
g_grad = zeros(ne, 1); % vector of volumes IT IS THE SAME AS v
f_grad = zeros(ne,1); % gradient of f
f = 0; % compliance
for e=1:ne
 d = zeros(4, 1);
 [edof] = build_edof(IX, e);
 % build the matrix d from D
 for i = 1:4
   d(i) = D(edof(i));
 end
 % compute the bar length
 [L0, delta_x, delta_y] = length(IX, X, e);
 % displacement vector (4x1)
 BO = 1/L0^2 * [-delta_x -delta_y delta_x delta_y]';
 % materials properties
 propno = IX(e, 3);
 E0 = mprop(propno, 1);
 A = mprop(propno, 2);
 % element stiffness matrix
 k_0e = E0 * A * L0 * B0 * B0'; % 4x4 matrix
 % compute the volume
 g_grad(e) = L0 * A;
 strain(e) = B0' * d;
 stress(e) = rho(e)^p*strain(e) * E0;
 N(e) = stress(e) * A;
 % sum BO after having transformed it in order to be compliant for the sum
 % with P
 for jj = 1:4
     B0_{sum}(edof(jj)) = B0_{sum}(edof(jj)) + B0(jj)*N(e)*L0;
 f_grad(e) = -p*rho(e)^(p - 1)*d'*k_0e*d; % ATTENTION TO DIMENSION OF d
 f = f + d' * rho(e)^p * k_0e * d; % compute the compliance
end
% compute the support reactions (N)
R = B0_sum - P; % 2nnx1 (nn is node number)
```

```
return
function PlotStructure(X,IX,ne,neqn,bound,loads,D,stress,rho)
% This subroutine plots the undeformed and deformed structure
h1=0;h2=0;
% Plotting Un-Deformed and Deformed Structure
hold on
box on
colors = ['b', 'r', 'g']; % vector of colors for the structure
fake_zero = 1e-8; % fake zero for tension sign decision
for e = 1:ne
   xx = X(IX(e,1:2),1); % vector of x-coords of the nodes
   yy = X(IX(e,1:2),2); % vector of y-coords of the nodes
   h1=plot(xx,yy,'k:','LineWidth',1.); % Un-deformed structure
   [edof] = build_edof(IX, e);
   xx = xx + D(edof(1:2:4));
   yy = yy + D(edof(2:2:4));
   % choice of thhe color according to the state
   if stress(e) > fake_zero % tension
     col = colors(1);
   elseif stress(e) < - fake_zero % compression</pre>
     col = colors(2);
   else col = colors(3); % un-loaded
   end
   thick = 3.5*rho(e);
   h2=plot(xx,yy, col,'LineWidth',thick); % Deformed structure
end
plotsupports
plotloads
legend([h1 h2],{'Undeformed state',...
              'Deformed state'})
axis equal;
hold off
return
%% Function to compute the length of a bar
function [LO, delta_x, delta_y] = length(IX, X, e)
 i = IX(e, 1);
 j = IX(e, 2);
 xi = X(i, 1);
```

xj = X(j, 1);
yi = X(i, 2);
yj = X(j, 2);
delta\_x = xj - xi;
delta\_y = yj - yi;

```
L0 = sqrt(delta_x^2 + delta_y^2);
return
%% Function to provide the edof vector
function [edof] = build_edof(IX, e)
  edof = zeros(4, 1);
  edof = [IX(e,1)*2-1 IX(e,1)*2 IX(e,2)*2-1 IX(e,2)*2];
return
```