

previous weeks: Ex. 1 a – forward kinematics

$$\{\vec{r}_{IE}, C_{\mathcal{I}\mathcal{E}}\} = \mathrm{FK}(\vec{q})$$

unique mapping



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Ex. 1 b – differential forward kinematics

$$\{\vec{v}_{IE}, \vec{\omega}_{\mathcal{I}\mathcal{E}}\} = \mathrm{DFK}(\vec{q}, \dot{\vec{q}}) = J(\vec{q}) \dot{\vec{q}}$$

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today:

Ex. 1 c – inverse kinematics

$$\vec{q} = \operatorname{IK}(\vec{r}_{IE}, C_{\mathcal{I}\mathcal{E}})$$

non-unique mapping



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#### 1) IK & DIK

Let  $\vec{q} \in \mathbb{R}^n$  be the joint variables, e.g.,  $q_1, q_2, \ldots$ 

Let  $\vec{\chi} \in \mathbb{R}^m$  be the task variables, e.g.,  $\vec{r}_{IE}, C_{IE}, \dots$ 



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DIK problem: find  $\dot{\vec{q}}$  s.t.  $\dot{\vec{\chi}}_d = J(\vec{q}) \dot{\vec{q}} \longrightarrow \dot{\vec{q}} = J^+(\vec{q}) \dot{\vec{\chi}}_d$ 





Assuming no kinematic singularities, we define the following three cases:



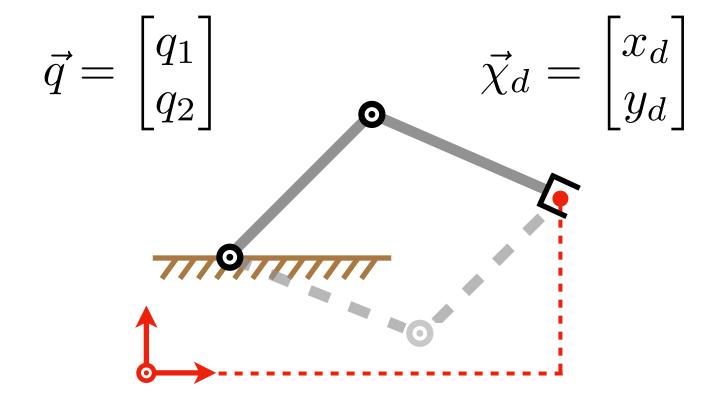
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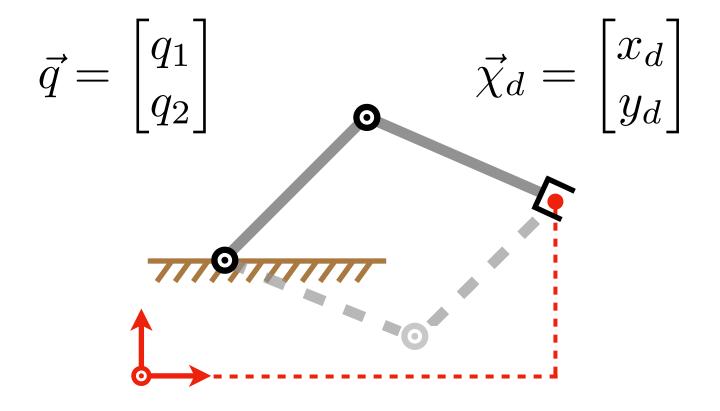
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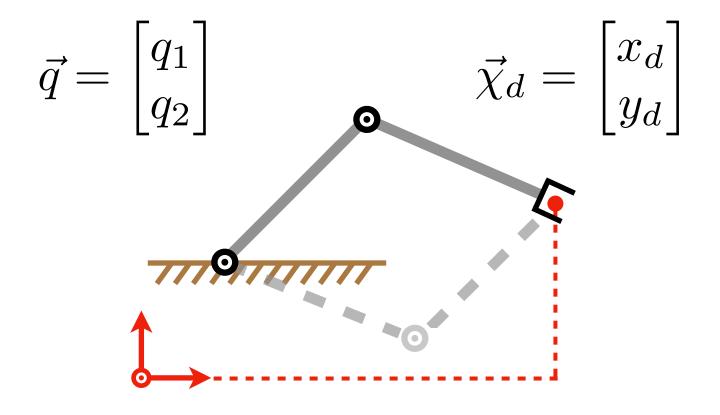


non unique but finitely many solutions for IK



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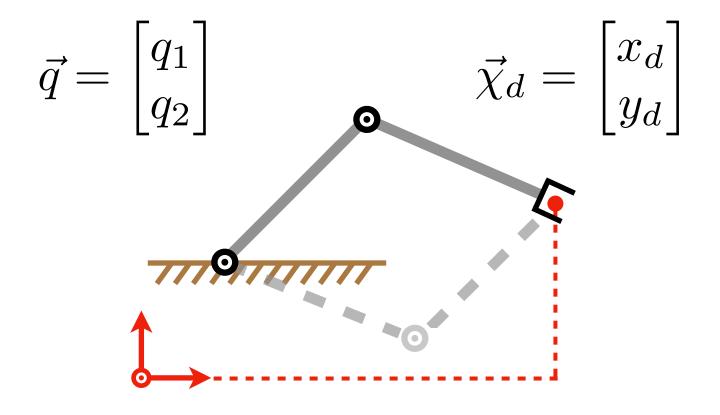
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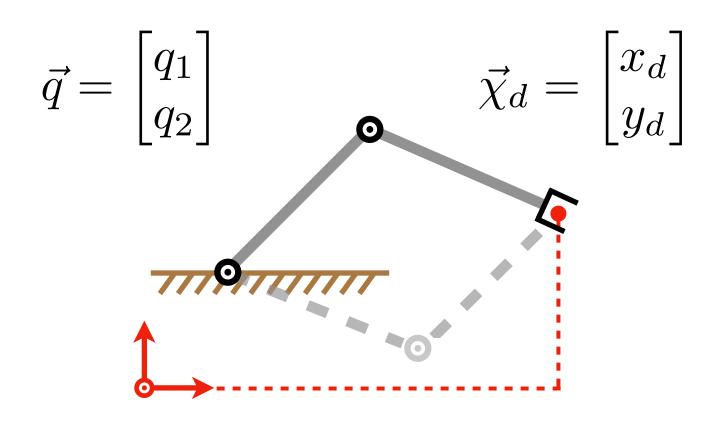
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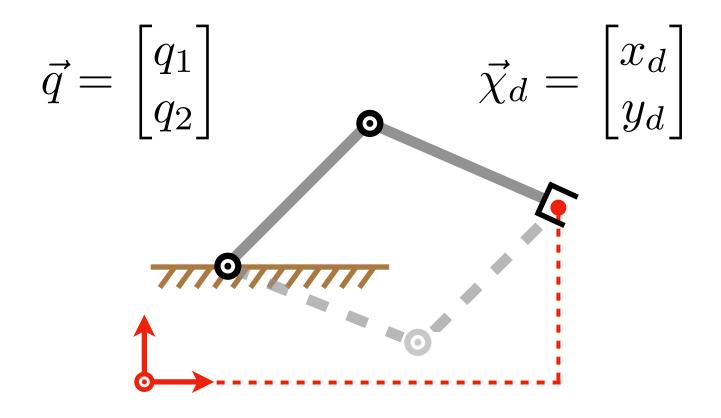
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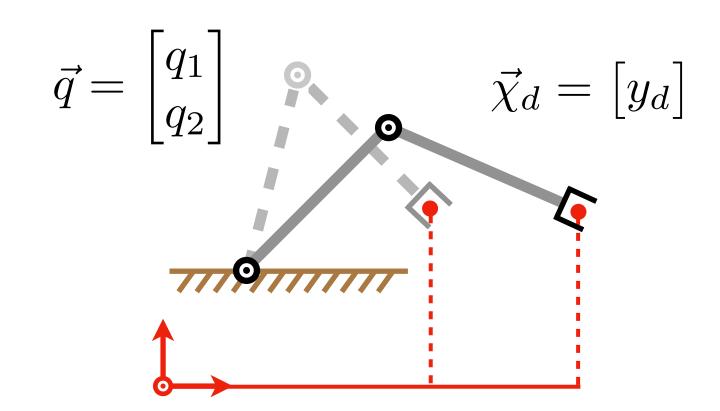


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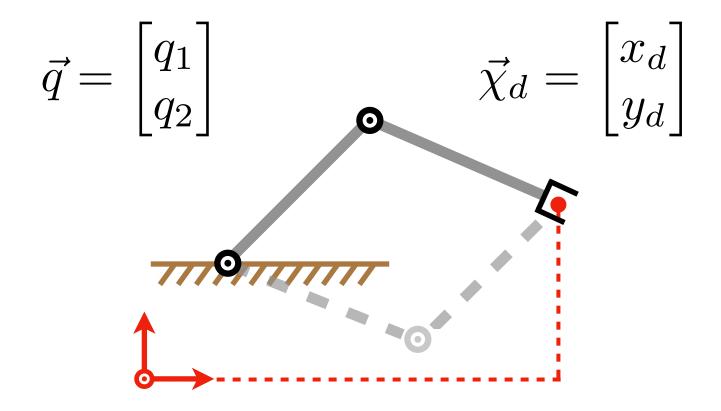
Case 2: m < n (redundant)





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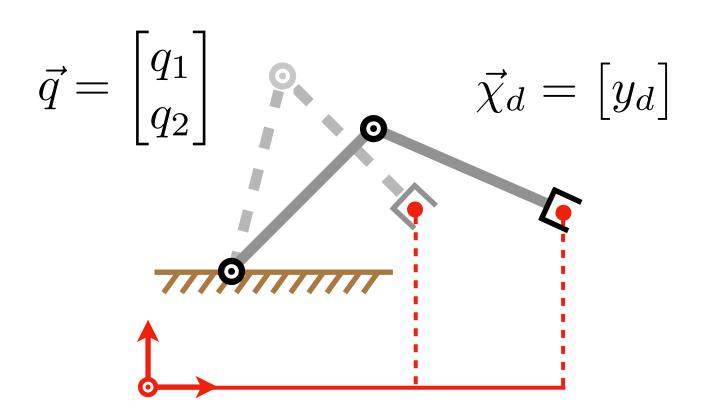


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$$J^+(\vec{q}) = J^{-1}(\vec{q})$$

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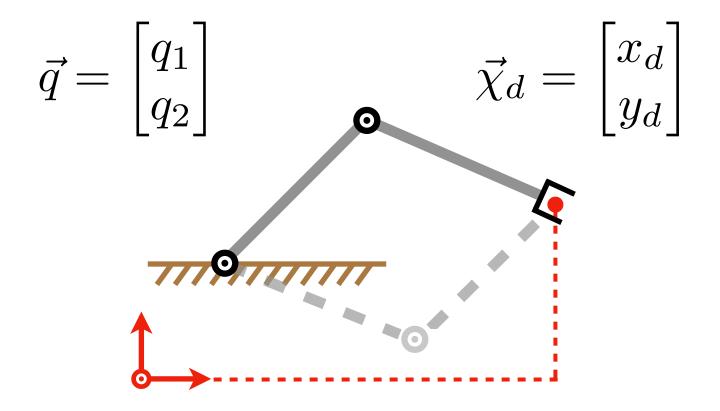


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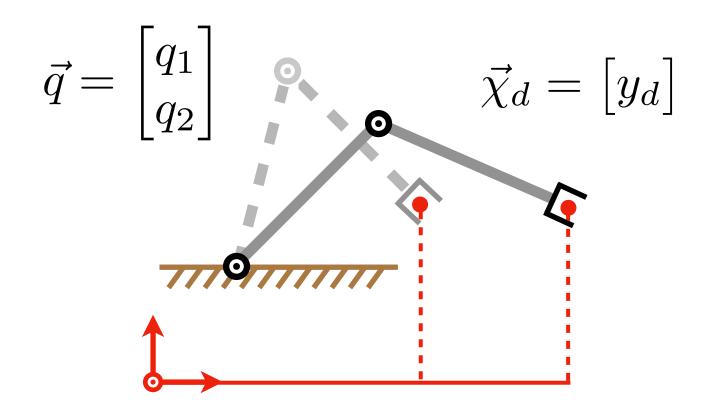


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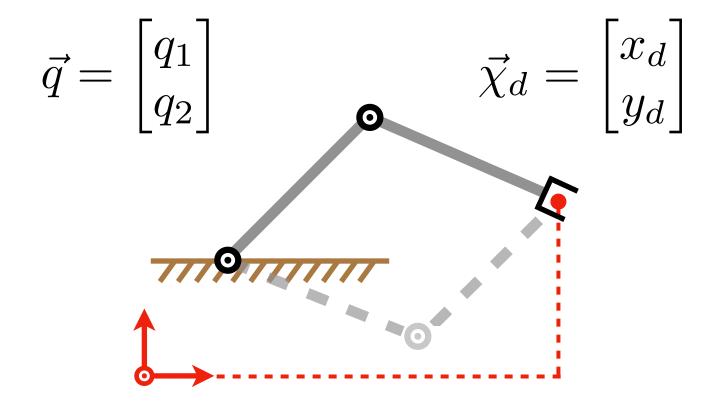
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$$J^{+}=J^{\top}\left(JJ^{\top}\right)^{-1}$$
 right pseudo-inverse



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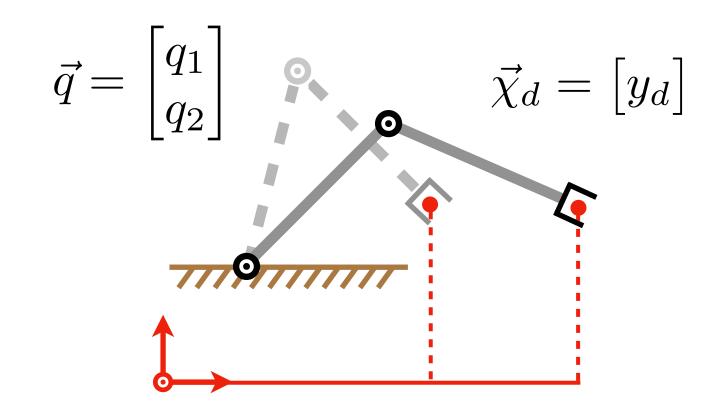


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$$J^{+} = J^{\top} \left( J J^{\top} \right)^{-1} \quad \mbox{right pseudo-inverse} \label{eq:J}$$

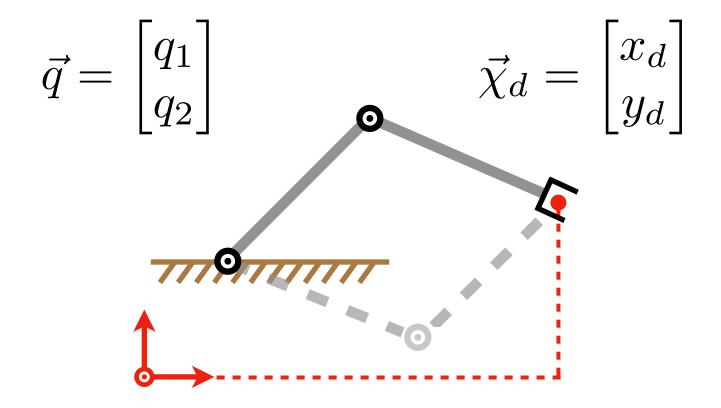
is constructed s.t.

$$\dot{ec{q}}^* = egin{cases} \mathrm{argmin} \ \dot{ec{q}} \ \dot{ec{q}} \ \mathrm{s.t.} \ \dot{\chi_d} = J(ec{q}) \ \dot{ec{q}} \ \end{cases}$$



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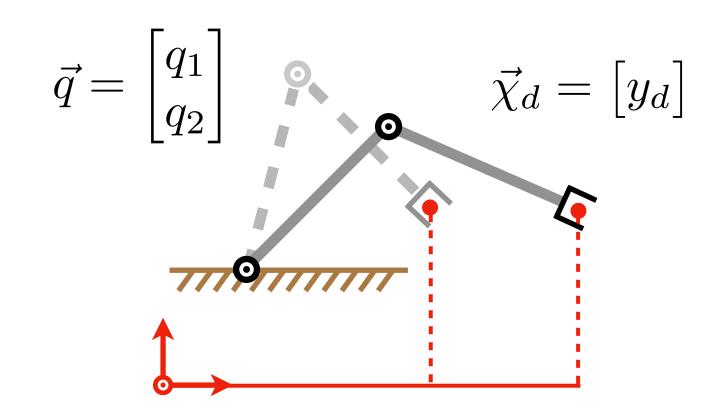


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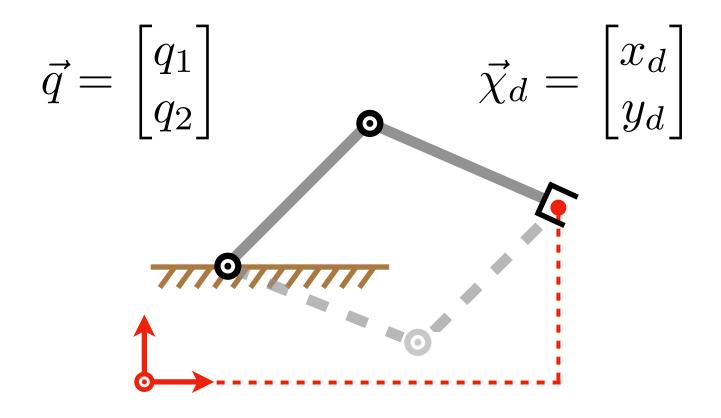
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Case 3: m > n



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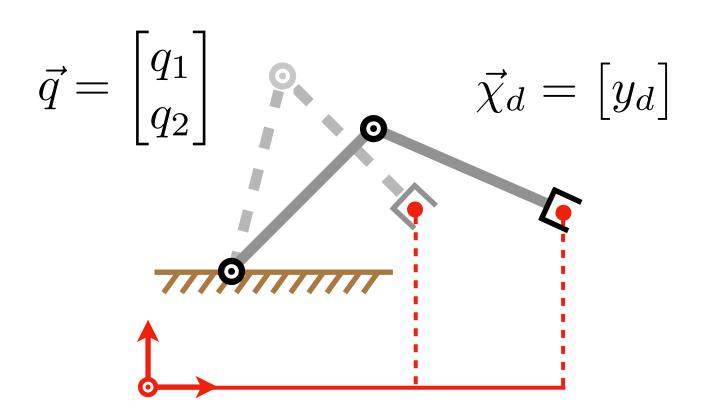


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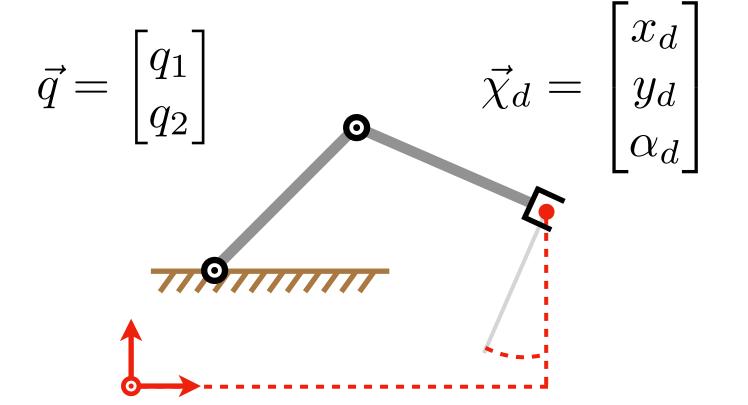
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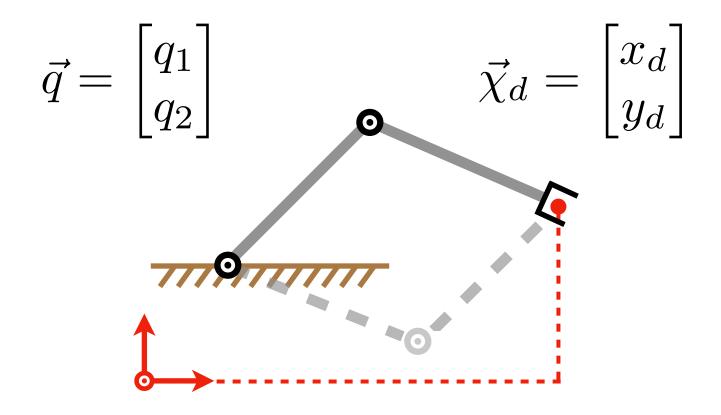
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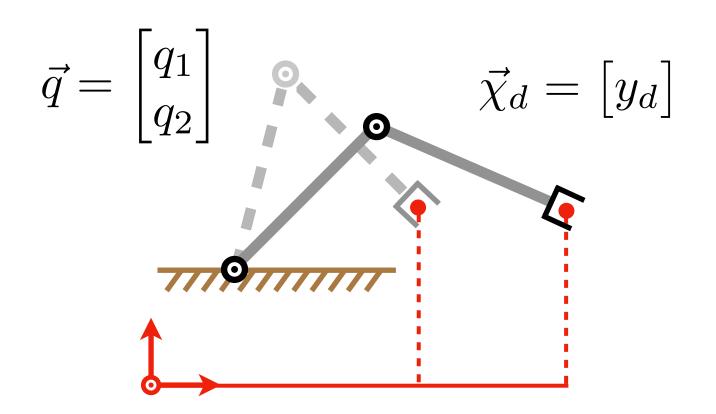


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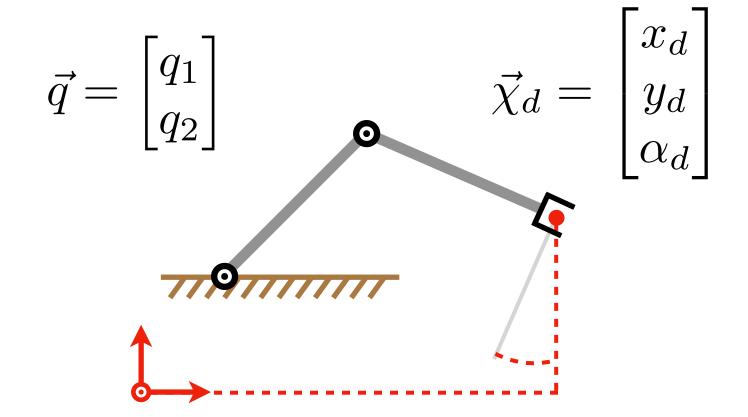
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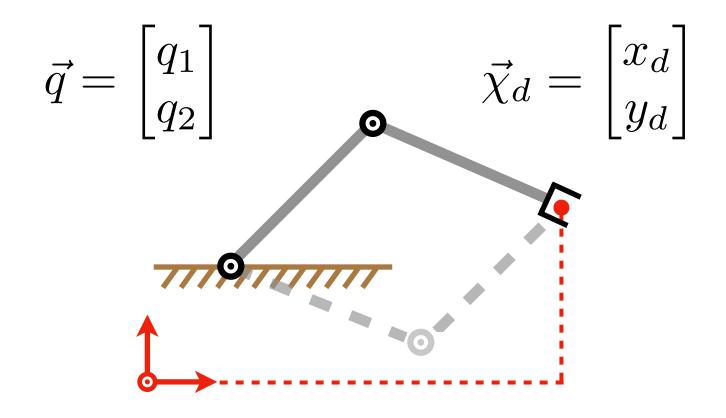


no exact solution for IK



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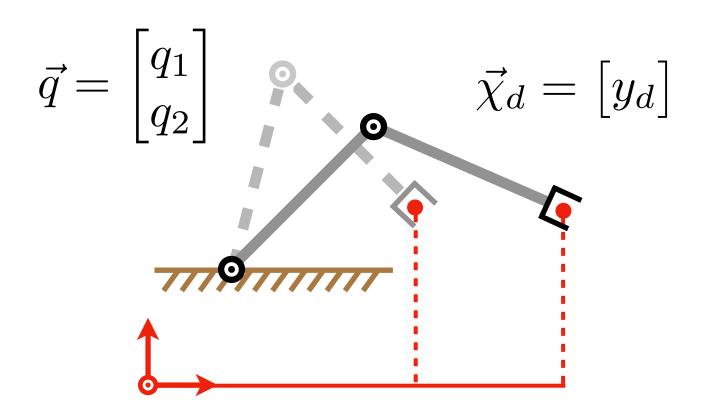


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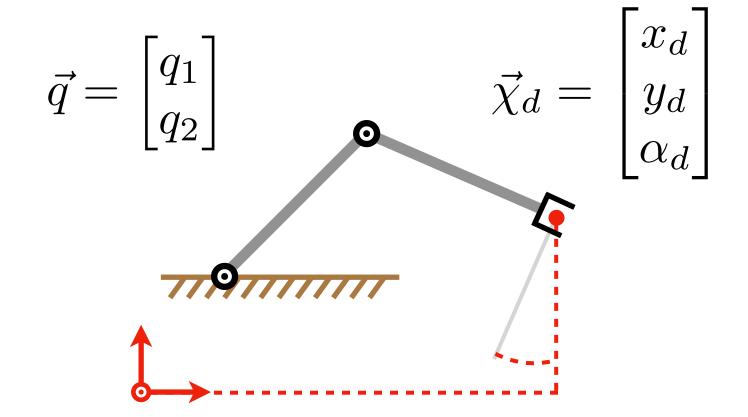
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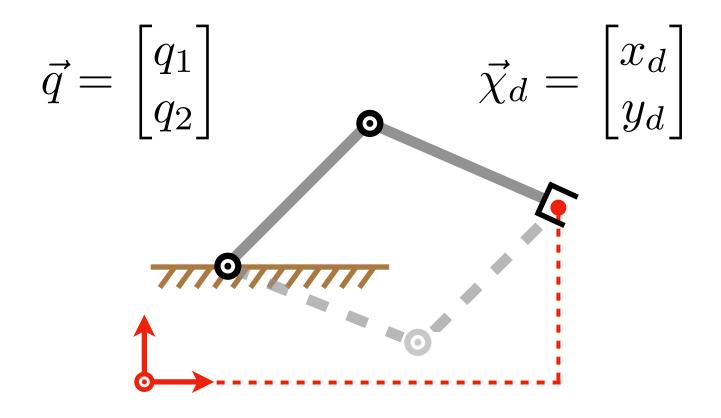
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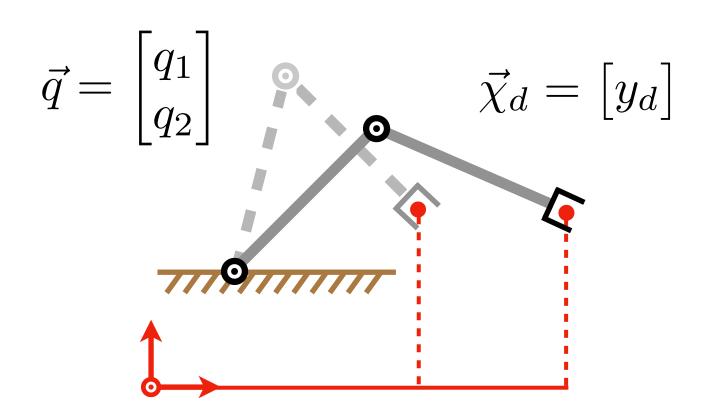


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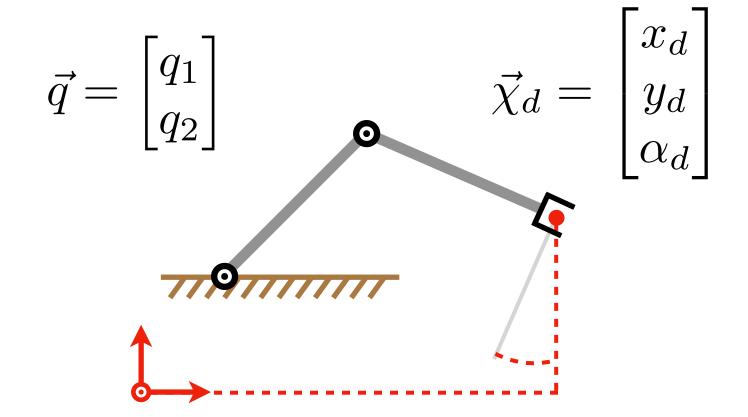
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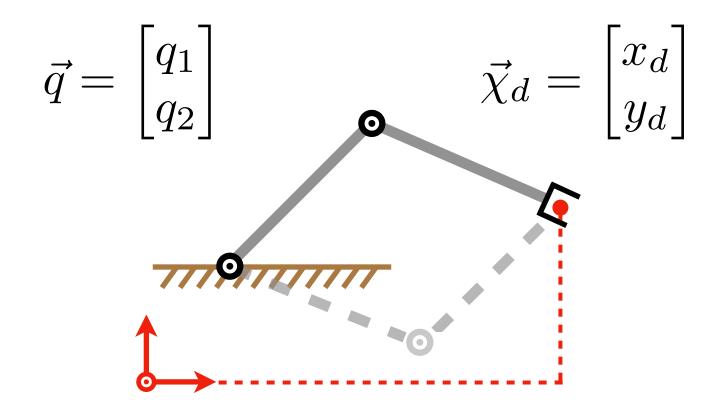
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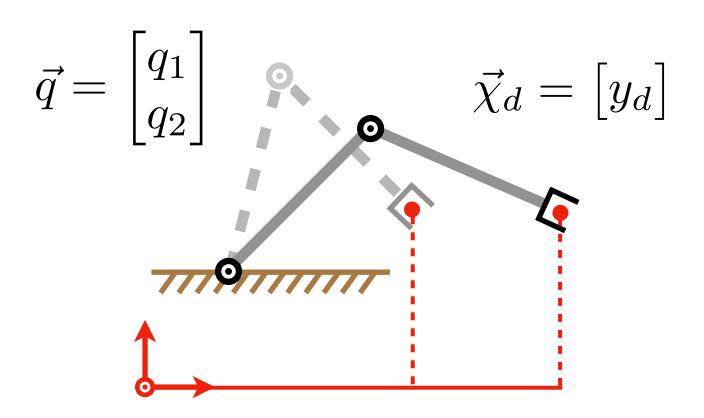


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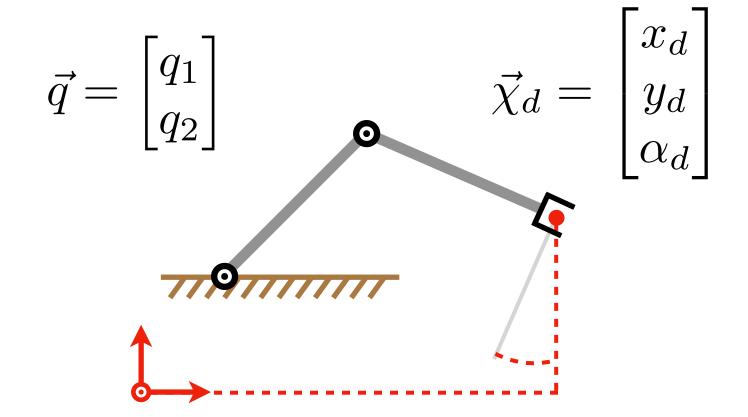
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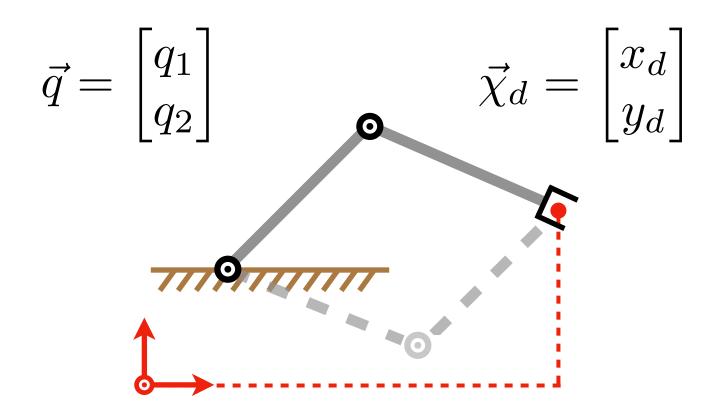
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For kinematics singularities: Add  $\lambda^2 \mathbb{I}$  before taking the inverse (i.e. damping)

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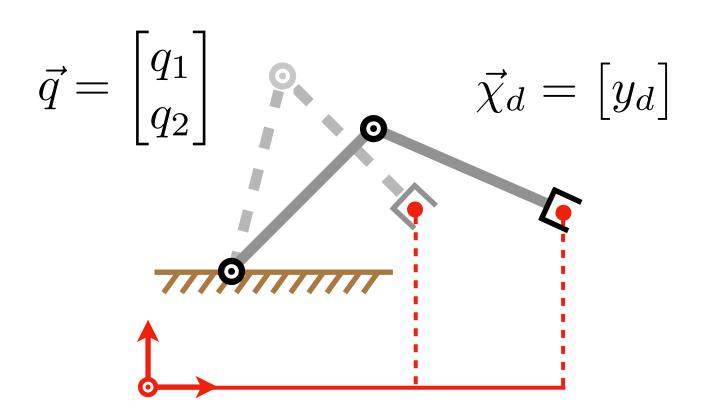


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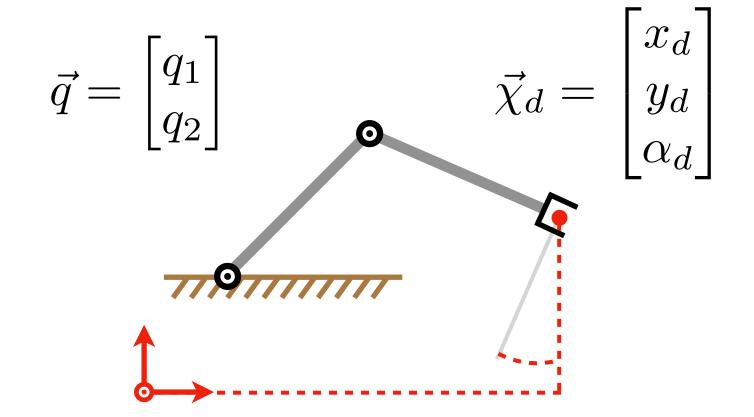
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For kinematics singularities: Add  $\lambda^2 \mathbb{I}$  before taking the inverse (i.e. damping)

→ (Jacobian will have linearly dependent columns in case of singularity)



2) Iterative Inverse Kinematics



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$$\vec{q}_{k+1} = \vec{q}_k + J_A^+(\vec{q}_k) \underbrace{\left(\vec{\chi}_d - \vec{f}(\vec{q}_k)\right)}_{\Delta \vec{\chi}_{\mathcal{I}\mathcal{E}}}$$



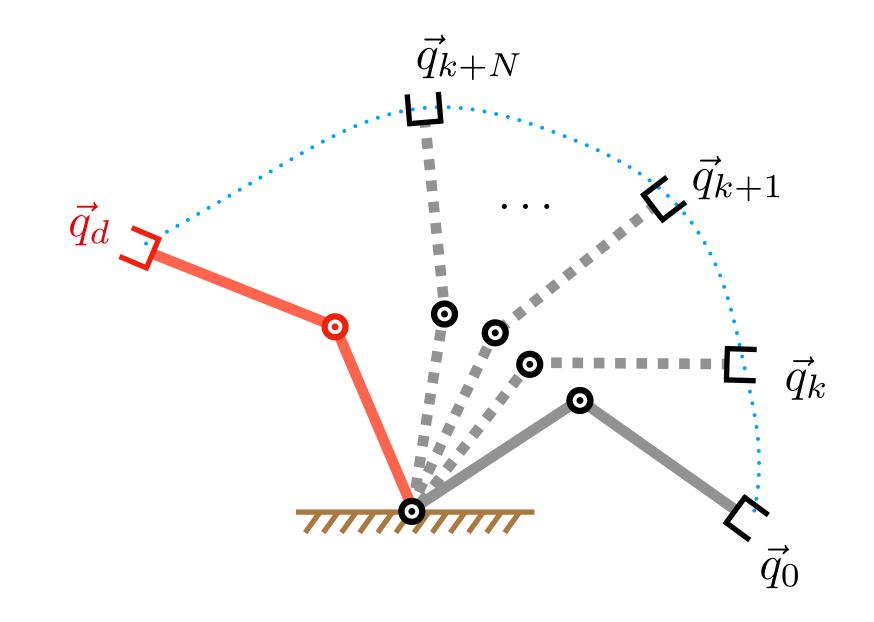
#### 2) Iterative Inverse Kinematics

Solving IK is equivalent to finding the roots of  $\vec{g}(\vec{q}) = \vec{\chi}_d - \vec{f}(\vec{q}) = \vec{0}$ Use of numerical technique analogous to Newton's method:

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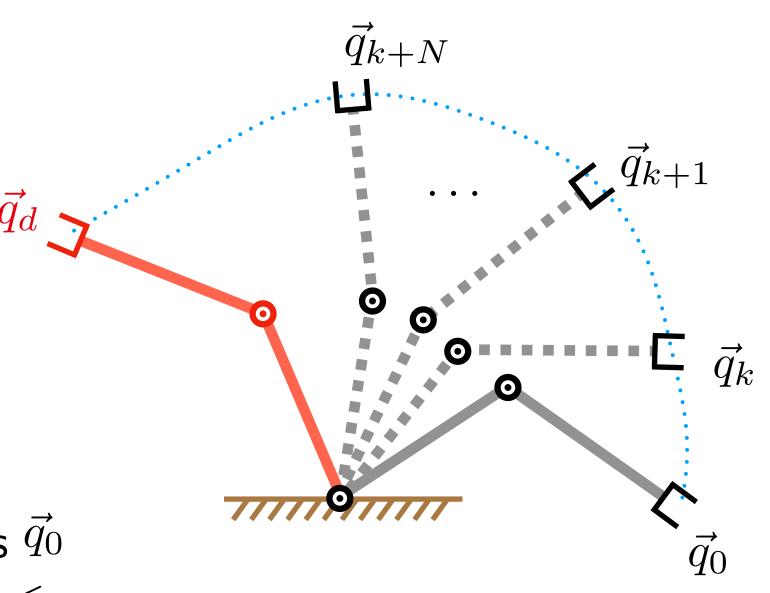
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for which we need an initial guess  $\vec{q}_0$  and a stopping criterion  $\|\vec{g}(\vec{q}_d)\|_2 \leq \varepsilon$ 





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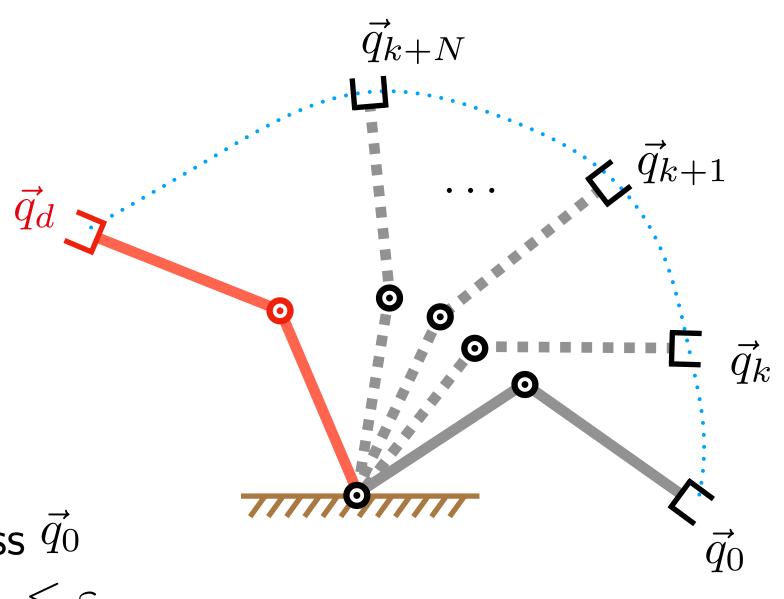
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 pose error  $\underline{\wedge}$ !





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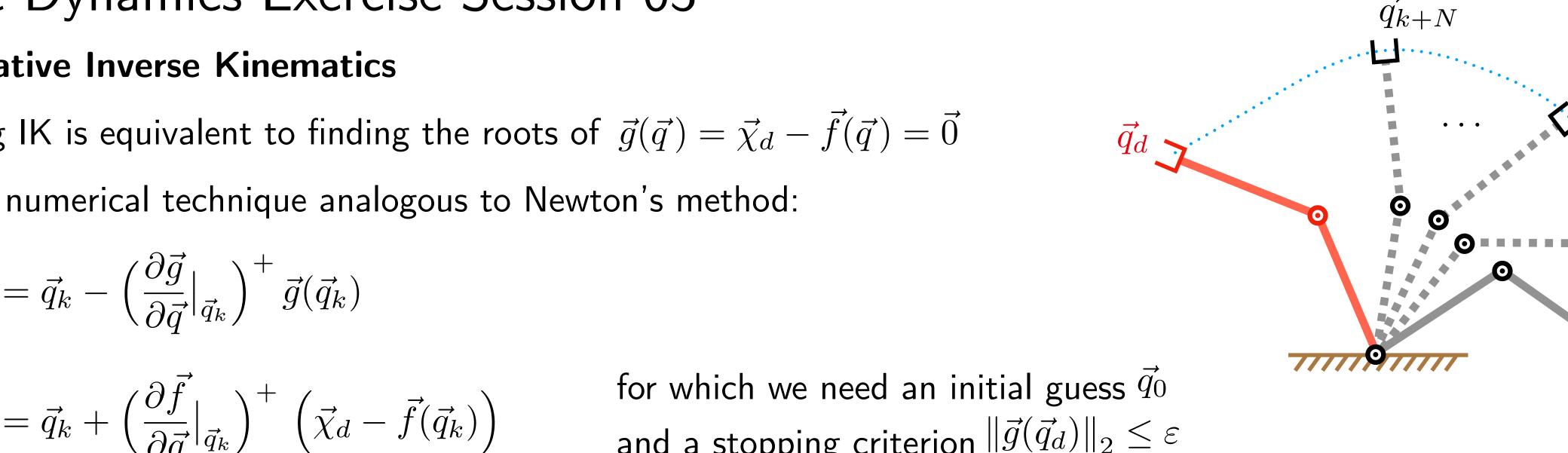
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How to properly compute the pose error:





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How to properly compute the pose error:

$$\Delta \vec{\chi}_{\mathcal{I}\mathcal{E}} = \begin{bmatrix} \vec{I}\vec{r}_{IE^*} - \vec{I}\vec{r}_{IE}(\vec{q}) \\ \Phi_{\mathcal{I}\mathcal{E}^*} \boxminus \Phi_{\mathcal{I}\mathcal{E}}(\vec{q}) \end{bmatrix} \propto \begin{bmatrix} \vec{I}\vec{v}_{IE} \\ \vec{I}\vec{\omega}_{\mathcal{I}\mathcal{E}} \end{bmatrix}$$



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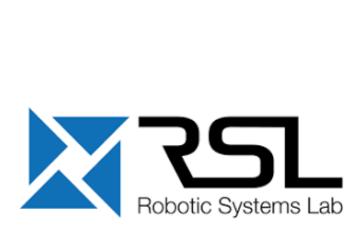
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How to properly compute the pose error:

$$\Delta \vec{\chi}_{\mathcal{I}\mathcal{E}} = \begin{bmatrix} I \vec{r}_{IE^*} - I \vec{r}_{IE}(\vec{q}) \\ \Phi_{\mathcal{I}\mathcal{E}^*} \boxminus \Phi_{\mathcal{I}\mathcal{E}}(\vec{q}) \end{bmatrix} \propto \begin{bmatrix} \mathcal{I} \vec{v}_{IE} \\ \mathcal{I} \vec{\omega}_{\mathcal{I}\mathcal{E}} \end{bmatrix} \implies \text{use } J_0 \text{ instead of } J_A$$



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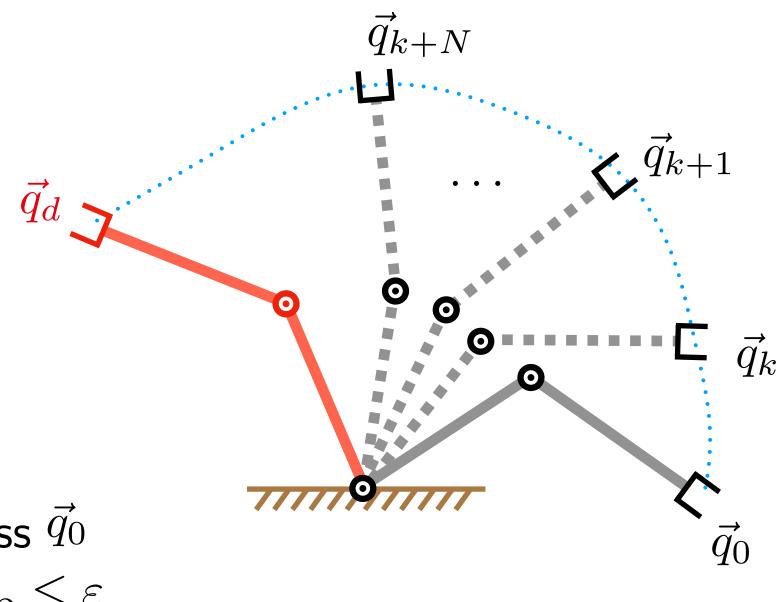
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 $\square$ : Boxminus: shortest "path" between orientations (minus does not work in orientation space)





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 pose error  $\underline{\wedge}$ 



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 $q_{k+N}$ 

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Given 
$$C_{\mathcal{I}\mathcal{E}},\,C_{\mathcal{I}\mathcal{E}^*}$$
 :

$$\varepsilon \vec{\varphi}_{\varepsilon \varepsilon^*} = \text{RotMat2RotVec}(C_{\varepsilon \varepsilon^*})$$

$$_{\mathcal{I}}\vec{\varphi}_{\mathcal{E}\mathcal{E}^*} = C_{\mathcal{I}\mathcal{E}} \,_{\mathcal{E}}\vec{\varphi}_{\mathcal{E}\mathcal{E}^*} = \text{RotMat2RotVec}(C_{\mathcal{I}\mathcal{E}^*} \, C_{\mathcal{I}\mathcal{E}}^{\top}(\vec{q}))$$





Given a reference trajectory defined by 
$$\vec{\chi}_d(t) = \begin{bmatrix} \vec{\mathcal{I}} \vec{r}_{IE^*} \\ \Phi_{\mathcal{I}\mathcal{E}^*} \end{bmatrix}$$
,  $\vec{w}_d(t) = \begin{bmatrix} \vec{\mathcal{I}} \vec{v}_{IE^*} \\ \vec{\mathcal{I}} \vec{\omega}_{\mathcal{I}\mathcal{E}^*} \end{bmatrix}$ 



Given a reference trajectory defined by 
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,  $\vec{w}_d(t) = \begin{bmatrix} \vec{\iota} \vec{v}_{IE^*} \\ \vec{\iota} \vec{\omega}_{\mathcal{I}\mathcal{E}^*} \end{bmatrix}$ 

Control law 
$$\dot{\vec{q}} = J^+ \underbrace{\begin{bmatrix} \vec{v}_{IE} \\ \vec{\tau} \vec{\omega}_{\mathcal{I}\mathcal{E}} \end{bmatrix}}_{\vec{w}(t)}$$



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, where  $\vec{w}(t) = \vec{w}_d(t) + \underbrace{K_p}_{>0} \Delta \vec{\chi}_{\mathcal{I} \mathcal{E}}$  we require feed forward reference if the desired pose is not constant



### 3) Kinematics Motion Control

Given a reference trajectory defined by 
$$\vec{\chi}_d(t) = \begin{bmatrix} \vec{\mathcal{I}} \vec{r}_{IE^*} \\ \Phi_{\mathcal{I}\mathcal{E}^*} \end{bmatrix}, \ \vec{w}_d(t) = \begin{bmatrix} \vec{\mathcal{I}} \vec{v}_{IE^*} \\ \vec{\mathcal{I}} \vec{\omega}_{\mathcal{I}\mathcal{E}^*} \end{bmatrix}$$

Control law 
$$\dot{\vec{q}} = J^+ \underbrace{\begin{bmatrix} \vec{v}\vec{v}_{IE} \\ \vec{z}\vec{\omega}_{\mathcal{I}\mathcal{E}} \end{bmatrix}}_{\vec{w}(t)} \text{, where } \vec{w}(t) = \vec{w}_d(t) + \underbrace{K_p}_{>0} \Delta \vec{\chi}_{\mathcal{I}\mathcal{E}} \text{ if the desired pose is not constant}$$
 relates "changes": ( )  $\sim \Delta$ 

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we require feed forward reference

Reason why this works: error dynamics  $\Delta \dot{\vec{\chi}}_{IE} + K_p \Delta \vec{\chi}_{IE} = \vec{0}$ 



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$$\Deltaec{\chi}_{\mathcal{I}\mathcal{E}} oec{0}$$
 as  $t o\infty$   $ec{\chi}_{\mathcal{I}\mathcal{E}}(t) oec{\chi}_{d}(t)$ 

