

# Precision Control of an Autonomous Surface Vessel



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# Agenda



- ▶ **Introduction**
  - Use Case
- ▶ **System Description**
- ▶ **Model**
  - Reference Frames
  - Model Equations
  - Model Verification
- ▶ Control Approach
- ▶ Sensor Fusion
- ▶ Inner Controller
- ▶ Outer Controller
- ▶ Results
- ▶ Conclusion

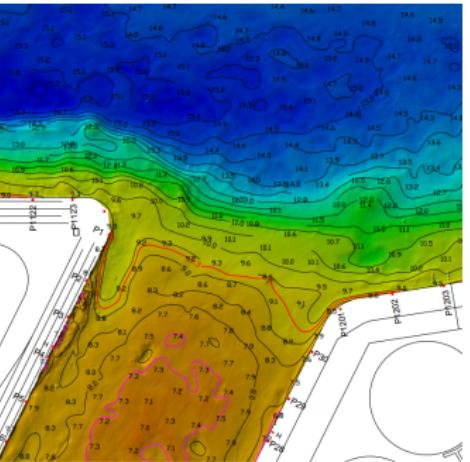
# Introduction



- ▶ What is an Autonomous Surface Vessel (ASV)
- ▶ Bathymetric Measurements
- ▶ Control of an ASV

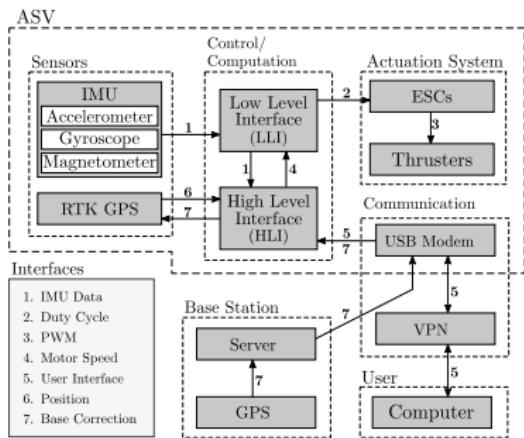
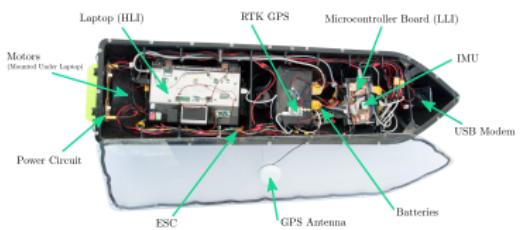
# Introduction

## Use Case



- ▶ Depth map used by Port of Aalborg
  - ▶ Problem: No recent knowledge of depths of the port
  - ▶ Solution: Automate smaller unmanned vessel

# System Description

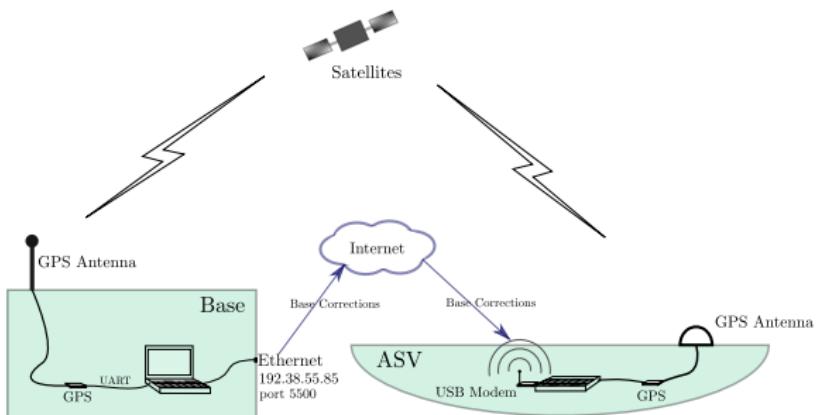


# System Description

## RTK GPS

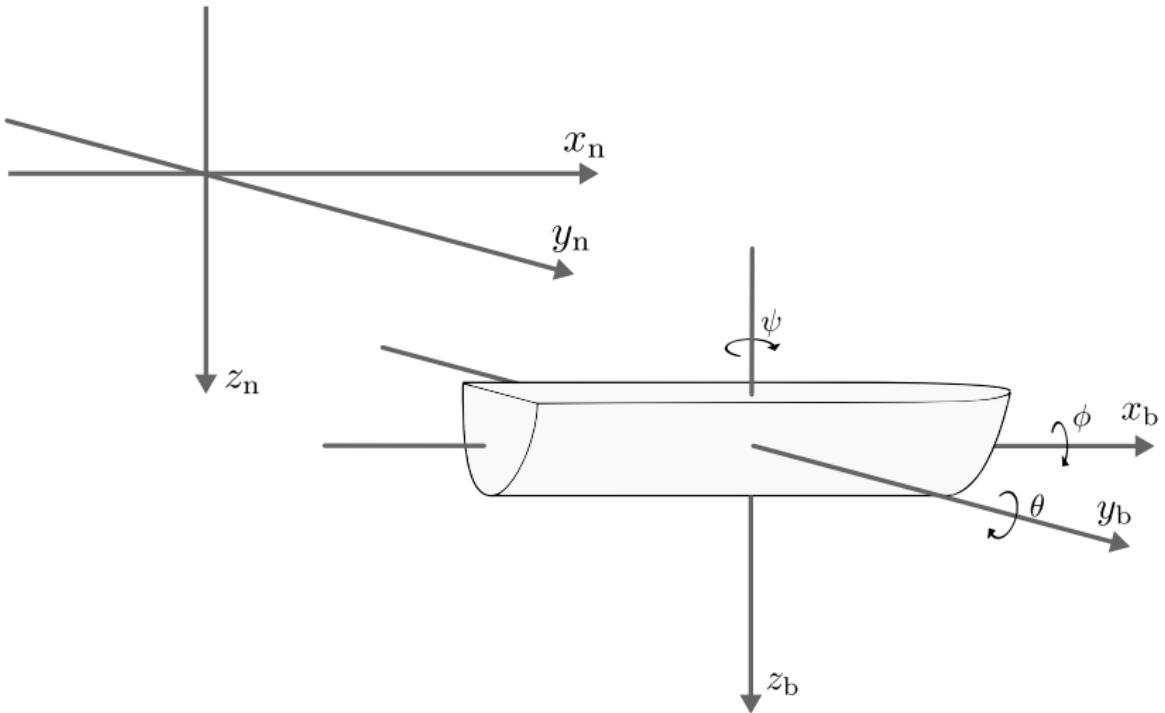


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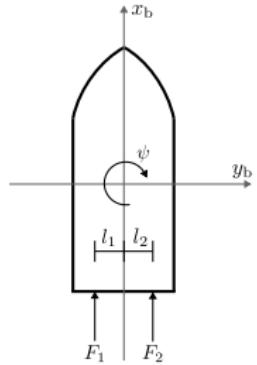
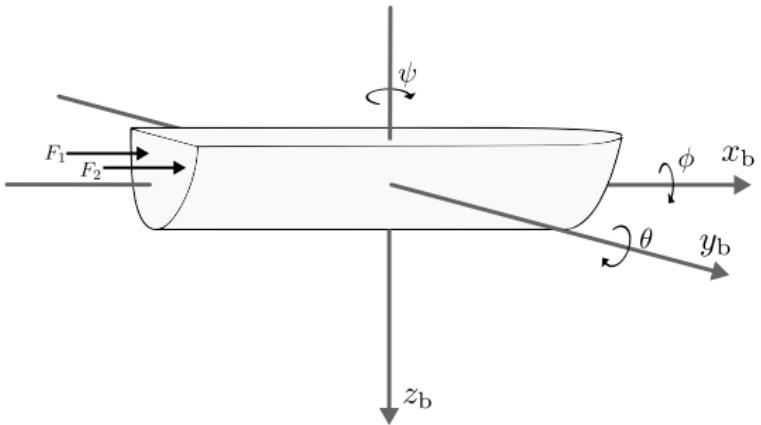
# Model

## Reference Frames



# Model

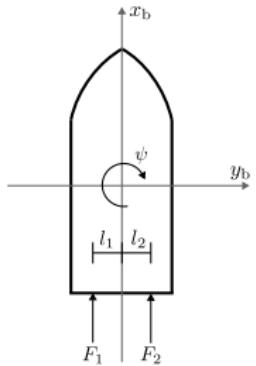
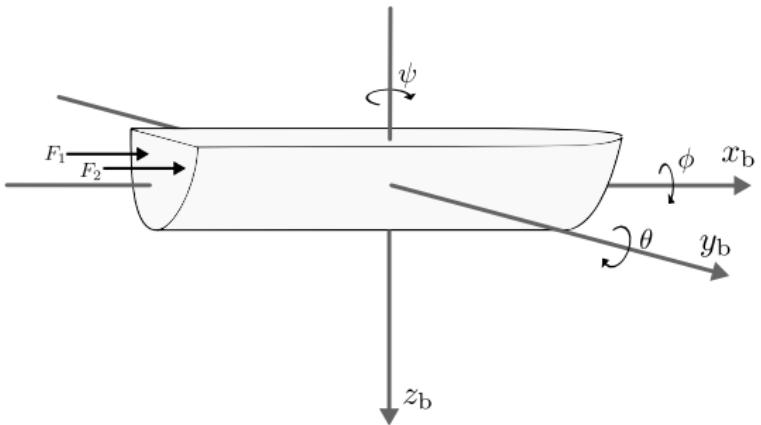
## Model Dynamics



- ▶ Rigid Body Dynamics
- ▶ Hydrostatics
- ▶ Hydrodynamics

# Model

## Rigid Body Dynamics

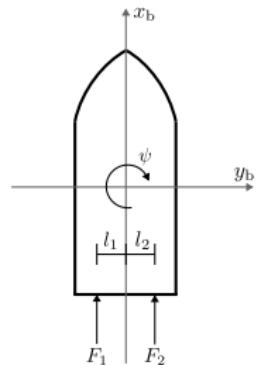
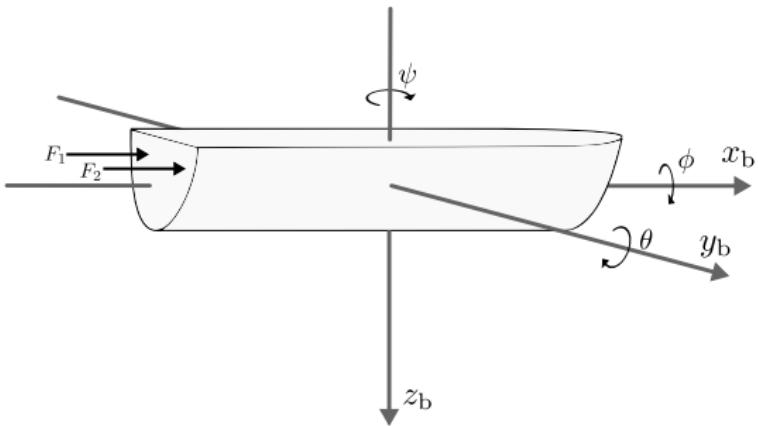


$$\sum F = m\ddot{x}$$

$$\sum \tau = I\ddot{\theta}$$

# Model

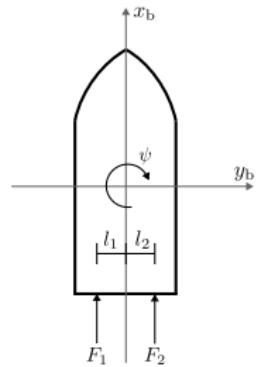
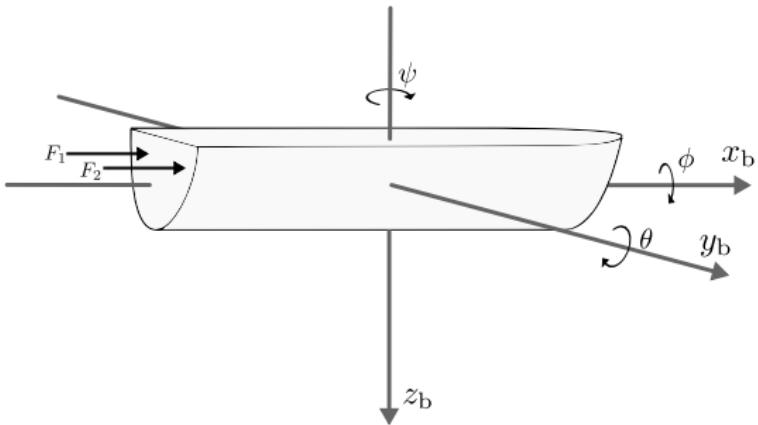
## Hydrostatics



- ▶ Buoyancy Force

# Model

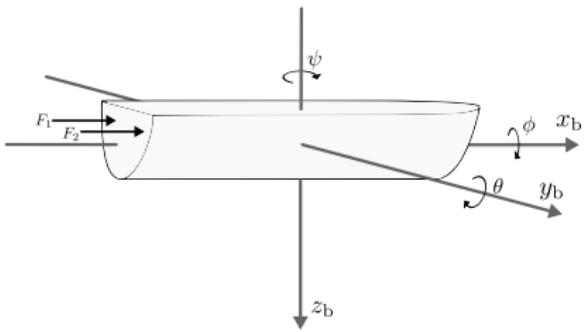
## Hydrodynamics



- ▶ Added mass
- ▶ Viscous Damping

# Model

## Model Equations



$$m\ddot{x}_b = F_1 + F_2 - d_{\dot{x}_b} \dot{x}_b + F_{x_b}$$

$$m\ddot{y}_b = -d_{\dot{y}_b} \dot{y}_b + F_{y_b}$$

$$m\ddot{z}_b = -d_{\dot{z}_b} \dot{z}_b + F_{z_b}$$

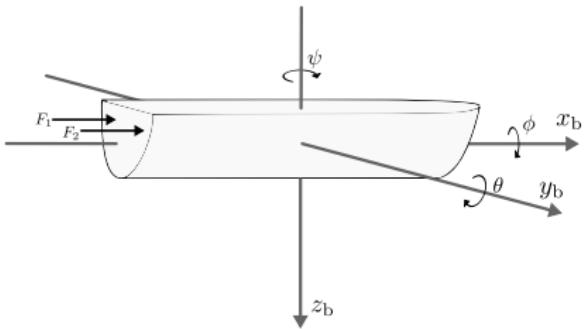
$$I_x \ddot{\phi} = -d_{\dot{\phi}} \dot{\phi} + T_\phi$$

$$I_y \ddot{\theta} = -d_{\dot{\theta}} \dot{\theta} + T_\theta$$

$$I_z \ddot{\psi} = F_1 I_1 - F_2 I_2 - d_{\dot{\psi}} \dot{\psi}$$

# Model

## Linearized Model Equations



$$m\ddot{x}_b = F_1 + F_2 - d_{\dot{x}_b} \dot{x}_b$$

$$m\ddot{y}_b = -d_{\dot{y}_b} \dot{y}_b$$

$$m\ddot{z}_b = -d_{\dot{z}_b} \dot{z}_b - \rho g A_w p \tilde{z}_n$$

$$I_x \ddot{\phi} = -d_{\dot{\phi}} \dot{\phi} - \rho g V \overline{GM_T} \cdot \phi$$

$$I_y \ddot{\theta} = -d_{\dot{\theta}} \dot{\theta} - \rho g V \overline{GM_L} \cdot \theta$$

$$I_z \ddot{\psi} = F_1 l_1 - F_2 l_2 - d_{\dot{\psi}} \dot{\psi}$$

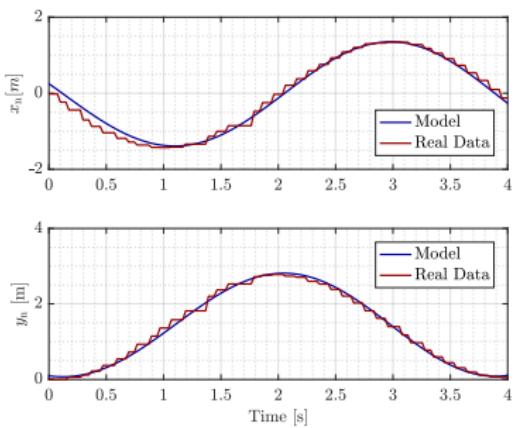
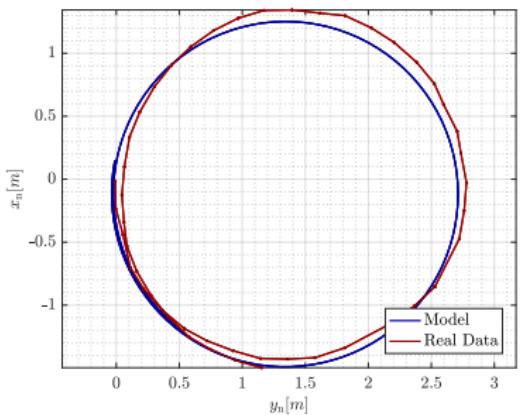
# Model

## Model Verification



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### ► Verified Nonlinear Model

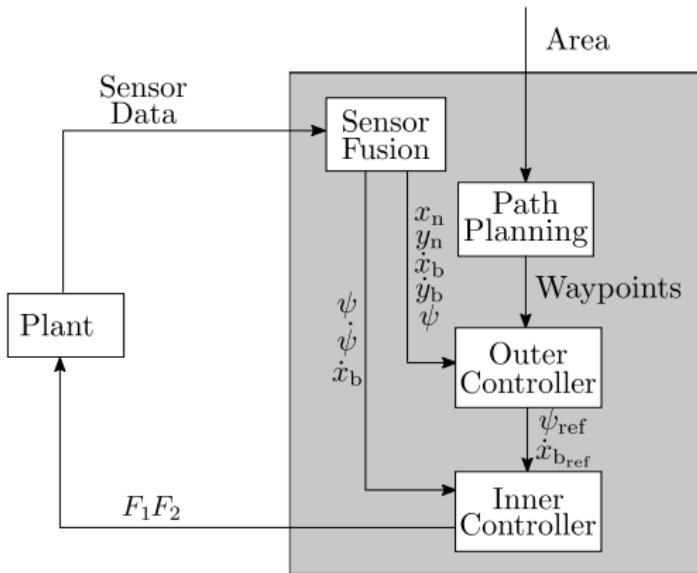


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  - Attitude Kalman Filter
  - Position Kalman Filter
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- ▶ Outer Controller
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- ▶ Conclusion

# Control Approach



# Sensor Fusion

## Kalman Filter Structure



# Sensor Fusion

## Attitude Kalman Filter



$$\hat{\mathbf{x}}_{\text{att}}(k+1) = \mathbf{A}_{\text{att}} \hat{\mathbf{x}}_{\text{att}}(k) + \mathbf{B}_{\text{att}} \mathbf{u}(k) + \mathbf{w}_{\text{att}}(k)$$

$$\mathbf{y}_{\text{att}}(k) = \mathbf{C}_{\text{att}} \hat{\mathbf{x}}_{\text{att}}(k) + \mathbf{v}_{\text{att}}(k)$$

$$\mathbf{Q}_{\text{att}} = \text{diag}(\sigma_{\phi}^2, \sigma_{\theta}^2, \sigma_{\psi}^2, \sigma_{\dot{\phi}}^2, \sigma_{\dot{\theta}}^2, \sigma_{\dot{\psi}}^2, \sigma_{\ddot{\phi}}^2, \sigma_{\ddot{\theta}}^2, \sigma_{\ddot{\psi}}^2)$$

$$\mathbf{R}_{\text{att}} = \text{diag}(\sigma_{\phi,\text{acc}}^2, \sigma_{\theta,\text{acc}}^2, \sigma_{\psi,\text{mag}}^2, \sigma_{\dot{\phi},\text{gyro}}^2, \sigma_{\dot{\theta},\text{gyro}}^2, \sigma_{\dot{\psi},\text{gyro}}^2)$$

$$\hat{\mathbf{x}}_{\text{att}} = [\phi \quad \theta \quad \psi \quad \dot{\phi} \quad \dot{\theta} \quad \dot{\psi} \quad \ddot{\phi} \quad \ddot{\theta} \quad \ddot{\psi}]^T$$

$$\mathbf{y}_{\text{att}} = [\phi_{\text{acc}} \quad \theta_{\text{acc}} \quad \psi_{\text{mag}} \quad \dot{\phi}_{\text{gyro}} \quad \dot{\theta}_{\text{gyro}} \quad \dot{\psi}_{\text{gyro}}]^T$$

$$\mathbf{u} = [F_1 \quad F_2]^T$$

# Sensor Fusion

## Attitude Kalman Filter



$$\mathbf{A}_{\text{att}} = \begin{bmatrix} 1 & 0 & 0 & T_s & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & T_s & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & T_s & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & T_s & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & T_s & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & T_s \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & T_s \\ 0 & 0 & 0 & -\frac{d_\phi}{I_x} & 0 & 0 & -T_s \frac{d_\phi}{I_x} & 0 & 0 \\ 0 & 0 & 0 & 0 & -\frac{d_\theta}{I_y} & 0 & 0 & -T_s \frac{d_\theta}{I_y} & 0 \\ 0 & 0 & 0 & 0 & 0 & -\frac{d_\psi}{I_z} & 0 & 0 & -T_s \frac{d_\psi}{I_z} \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \quad \mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

# Sensor Fusion

## Attitude Kalman Filter



$$\hat{\mathbf{x}}_{\text{att}}(k+1|k) = \mathbf{A}_{\text{att}} \hat{\mathbf{x}}_{\text{att}}(k|k) + \mathbf{B}_{\text{att}} \mathbf{u}(k)$$

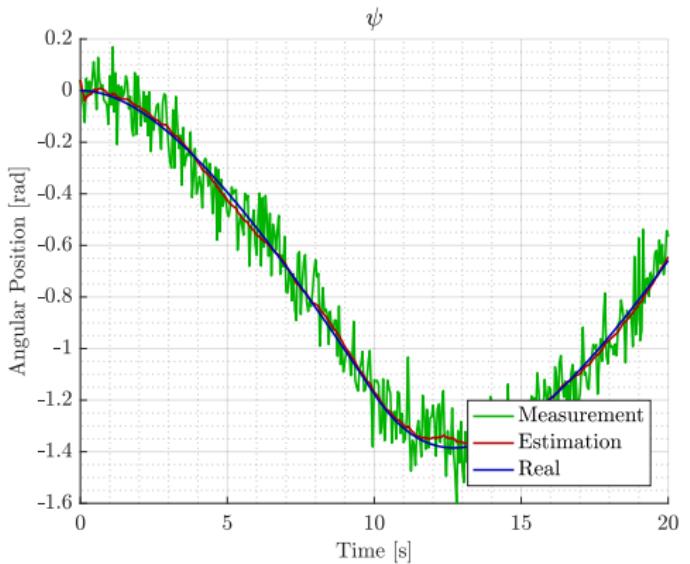
$$\mathbf{P}_{\text{att}}(k+1|k) = \mathbf{A}_{\text{att}} \mathbf{P}_{\text{att}}(k|k) \mathbf{A}_{\text{att}}^T + \mathbf{Q}_{\text{att}}$$

$$\hat{\mathbf{x}}_{\text{att}}(k+1|k+1) = \hat{\mathbf{x}}_{\text{att}}(k+1|k) + \mathbf{K}(k+1) [\mathbf{y}_{\text{att}}(k+1) - \mathbf{C}_{\text{att}} \hat{\mathbf{x}}_{\text{att}}(k+1|k)]$$

$$\mathbf{P}_{\text{att}}(k+1|k+1) = \left[ \mathbf{I} - \mathbf{K}(k+1) \mathbf{C}_{\text{att}}^T \right] \mathbf{P}_{\text{att}}(k+1|k)$$

# Sensor Fusion

## Attitude Kalman Filter



# Sensor Fusion

## Position Kalman Filter



$$\begin{aligned}\hat{\mathbf{x}}_{\text{pos}}(k+1) &= \mathbf{A}_{\text{pos}}(k)\mathbf{x}_{\text{pos}}(k) + \mathbf{B}_{\text{pos}}\mathbf{u}(k) + \mathbf{w}_{\text{pos}}(k) \\ \mathbf{y}_{\text{pos}}(k) &= \mathbf{C}_{\text{pos}}\hat{\mathbf{x}}_{\text{pos}}(k) + \mathbf{v}_{\text{pos}}(k)\end{aligned}$$

$$\begin{aligned}\mathbf{Q}_{\text{pos}} &= \text{diag}(\sigma_{x_n}^2, \sigma_{y_n}^2, \sigma_{x_b}^2, \sigma_{y_b}^2, \sigma_{\ddot{x}_b}^2, \sigma_{\ddot{y}_b}^2) \\ \mathbf{R}_{\text{pos}} &= \text{diag}(\sigma_{x_{n,\text{GPS}}}^2, \sigma_{y_{n,\text{GPS}}}^2, \sigma_{\ddot{x}_{b,\text{acc}}}^2, \sigma_{\ddot{y}_{b,\text{acc}}}^2)\end{aligned}$$

$$\hat{\mathbf{x}}_{\text{pos}} = [x_n \quad y_n \quad \dot{x}_b \quad \dot{y}_b \quad \ddot{x}_b \quad \ddot{y}_b]^T$$

$$\mathbf{y}_{\text{pos}} = [x_{n,\text{GPS}} \quad y_{n,\text{GPS}} \quad \ddot{x}_{b,\text{acc}} \quad \ddot{y}_{b,\text{acc}}]^T$$

$$\mathbf{u} = [F_1 \quad F_2]^T$$

# Sensor Fusion

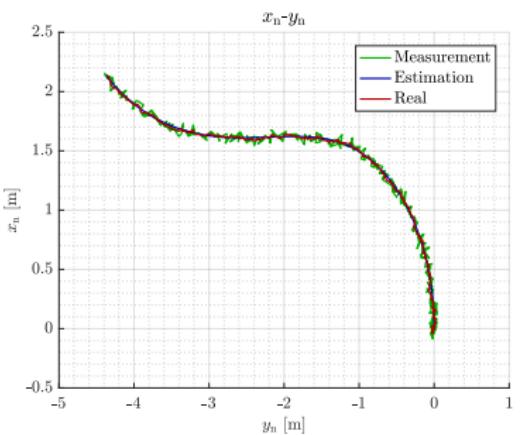
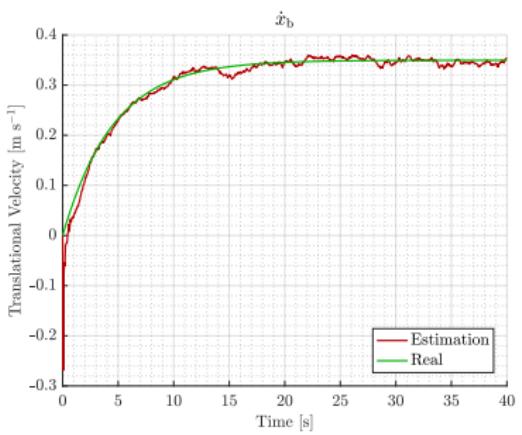
## Position Kalman Filter



$$\mathbf{A}_{\text{pos}}(\phi(k), \theta(k), \psi(k)) = \begin{bmatrix} 1 & 0 & T_s \mathbf{R}_b^n(1,1) & T_s \mathbf{R}_b^n(1,2) & 0 & 0 \\ 0 & 1 & T_s \mathbf{R}_b^n(2,1) & T_s \mathbf{R}_b^n(2,2) & 0 & 0 \\ 0 & 0 & 1 & 0 & T_s & 0 \\ 0 & 0 & 0 & 1 & 0 & T_s \\ 0 & 0 & -\frac{d_x}{m} & 0 & -T_s \frac{d_x}{m} & 0 \\ 0 & 0 & 0 & -\frac{d_y}{m} & 0 & -T_s \frac{d_y}{m} \end{bmatrix}$$

# Sensor Fusion

## Position Kalman Filter

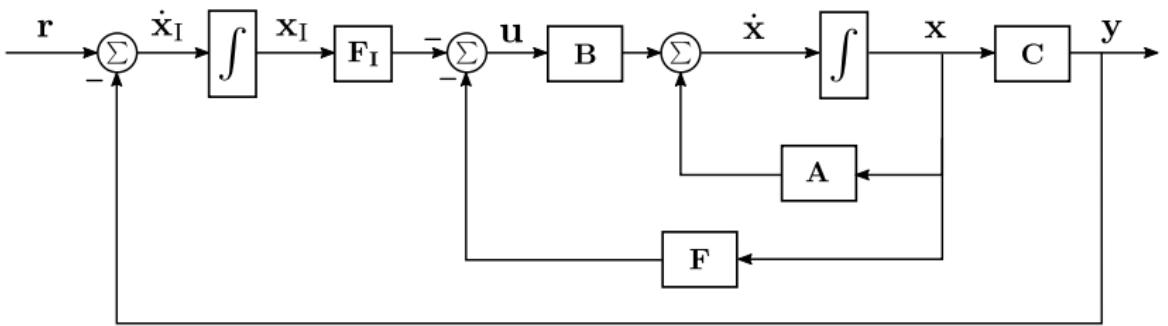


# Agenda

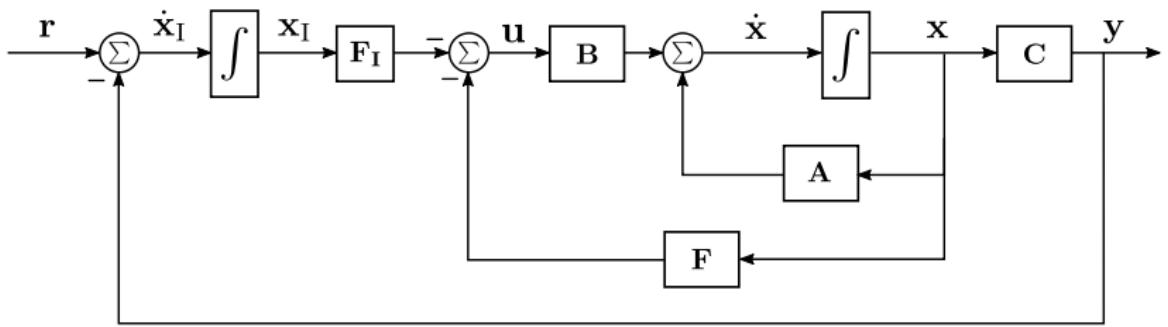


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# Inner Controller



# Inner Controller



- ▶ Linear Quadratic Regulator
- ▶  $\mathcal{H}_\infty$  Controller

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



- ▶ Suboptimal  $\mathcal{H}_\infty$  controller

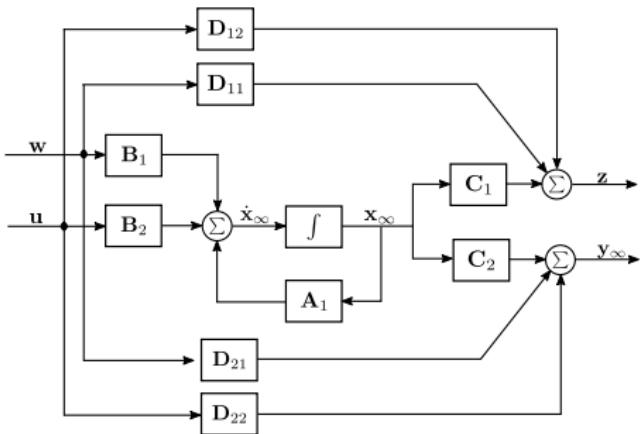
Find an internally stabilizing controller that provides a closed loop  $\mathcal{H}_\infty$  norm less than some bound  $\gamma$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



### ► System structure



$$\dot{\mathbf{x}}_\infty(t) = \mathbf{A}_1 \mathbf{x}_\infty(t) + \mathbf{B}_1 \mathbf{w}(t) + \mathbf{B}_2 \mathbf{u}(t)$$

$$\mathbf{z}(t) = \mathbf{C}_1 \mathbf{x}_\infty(t) + \mathbf{D}_{11} \mathbf{w}(t) + \mathbf{D}_{12} \mathbf{u}(t)$$

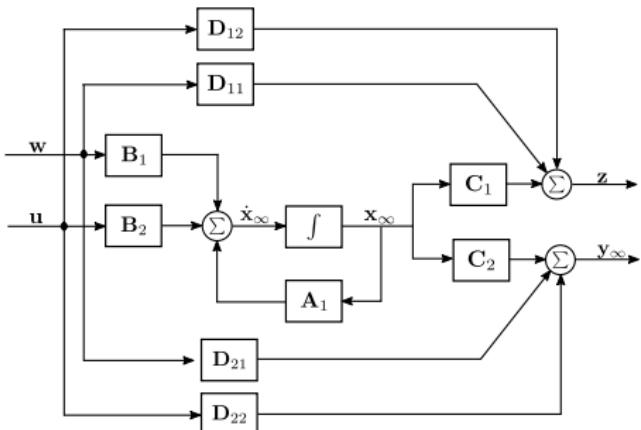
$$\mathbf{y}_\infty(t) = \mathbf{C}_2 \mathbf{x}_\infty(t) + \mathbf{D}_{21} \mathbf{w}(t) + \mathbf{D}_{22} \mathbf{u}(t)$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



### ► System structure



$$\mathbf{u}(t) = [F_1 \quad F_2]^T$$

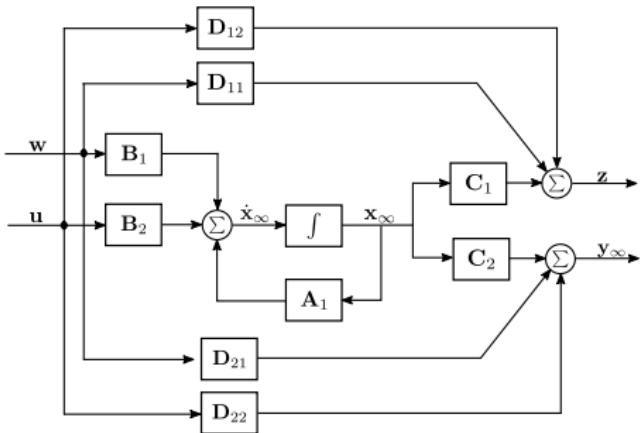
# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



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### ► System structure



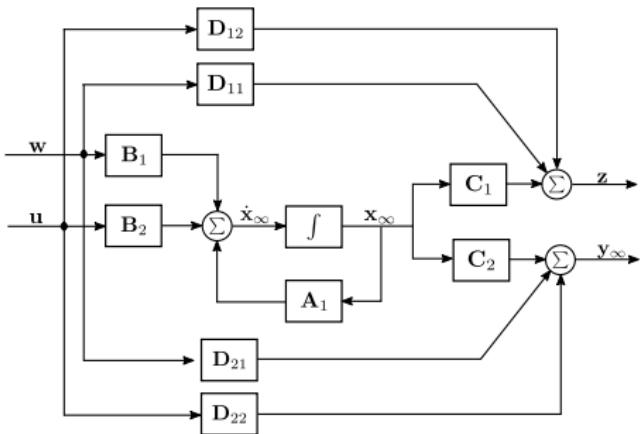
$$\mathbf{w}(t) = [\psi_{\text{ref}} \quad \dot{x}_{\text{b,ref}} \quad F_{\text{wc}} \quad \tau_{\text{wc}} \quad F_{\text{wave}} \quad \tau_{\text{wave}} \quad n_{\psi} \quad n_{\dot{x}_{\text{b}}}]^T$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



### ► System structure



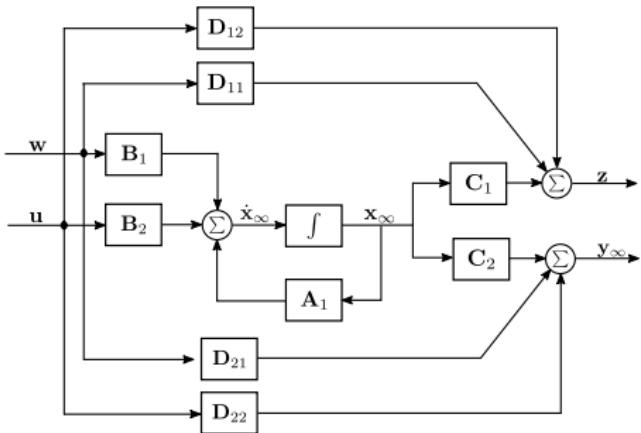
$$\mathbf{y}_\infty(t) = [\psi \quad \dot{x}_b \quad \mathbf{x}_I^T]^T$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



### ► System structure



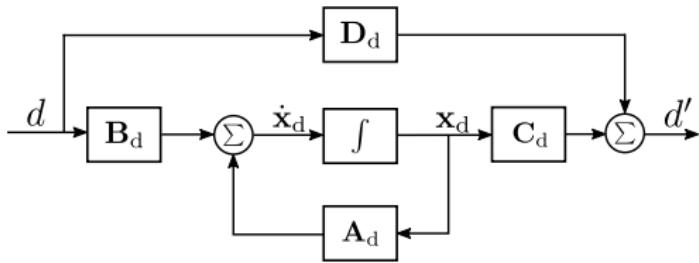
$$\mathbf{x}_\infty(t) = \begin{bmatrix} \psi & \dot{\psi} & \dot{x}_b & x_{int_\psi} & x_{int_{\dot{x}_b}} & x_{F_{wc}} & x_{T_{wc}} & x_{F_{wave}} & x_{T_{wave}} & x_{n_\psi} & x_{n_{\dot{x}_b}} \end{bmatrix}^T$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



- ▶ Disturbance model



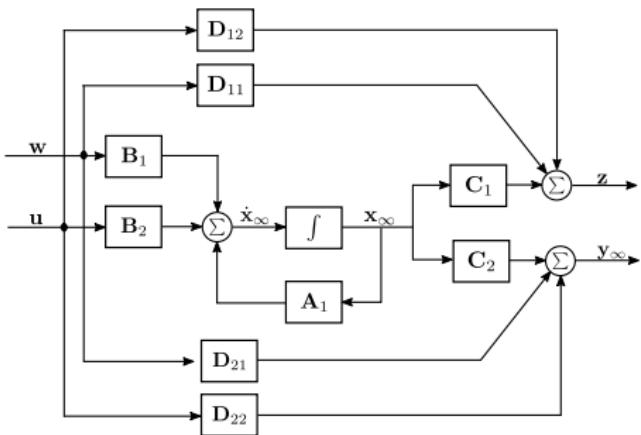
$$\frac{d'}{d} = \frac{a}{s+a} \rightarrow \dot{d}' = -ad' + ad \rightarrow \begin{cases} \dot{x}_d = -ax_d + ad \\ d' = x_d \end{cases}$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



### ► System structure



$$\mathbf{z}(t) = [\mathbf{x}_\infty^T \quad \mathbf{u}^T]^T$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



- Controller design parameters ( $\gamma$ ,  $\mathbf{C}_1$ ,  $\mathbf{D}_{12}$ )

$$\mathbf{C}_1 = \begin{bmatrix} \mathbf{W}_x & \mathbf{0}_{3 \times 2} & \mathbf{0}_{3 \times 2} & \mathbf{0}_{3 \times 2} & \mathbf{0}_{3 \times 2} \\ \mathbf{0}_{2 \times 3} & \mathbf{W}_I & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 3} & \mathbf{0}_{2 \times 2} & \mathbf{W}_{w_c} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 3} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{W}_{wave} & \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 3} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{W}_{noise} \\ \mathbf{0}_{2 \times 3} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 3} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} & \mathbf{0}_{2 \times 2} \end{bmatrix} \quad \mathbf{D}_{12} = \begin{bmatrix} \mathbf{0}_{2 \times 3} \\ \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 2} \\ \mathbf{0}_{2 \times 2} \\ \mathbf{W}_u \end{bmatrix}$$

# Inner Controller

## $\mathcal{H}_\infty$ Controller Design



- ▶ Feedback gain

$$\mathbf{X}_\infty = Ric \begin{bmatrix} \mathbf{A} & \gamma^{-2} \mathbf{B}_1 \mathbf{B}_1^T - \mathbf{B}_2 \mathbf{B}_2^T \\ -\mathbf{C}_1^T \mathbf{C}_1 & -\mathbf{A}^T \end{bmatrix}$$

$$\mathbf{F}_\infty = -\mathbf{B}_2^T \mathbf{X}_\infty$$

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# Inner Controller

## Linear Quadratic Controller Design



# Inner Controller

## Comparison of the Controllers



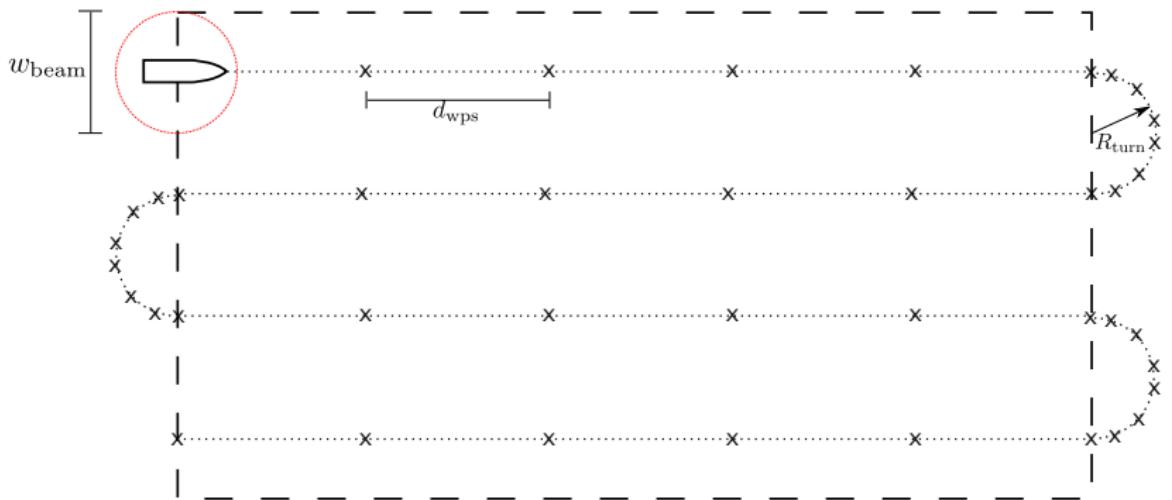
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- ▶ **Outer Controller**
  - Path Generation Algorithm
  - Path Following Algorithm
- ▶ **Results**
  - Controller Results
  - Implementation Results
- ▶ **Conclusion**

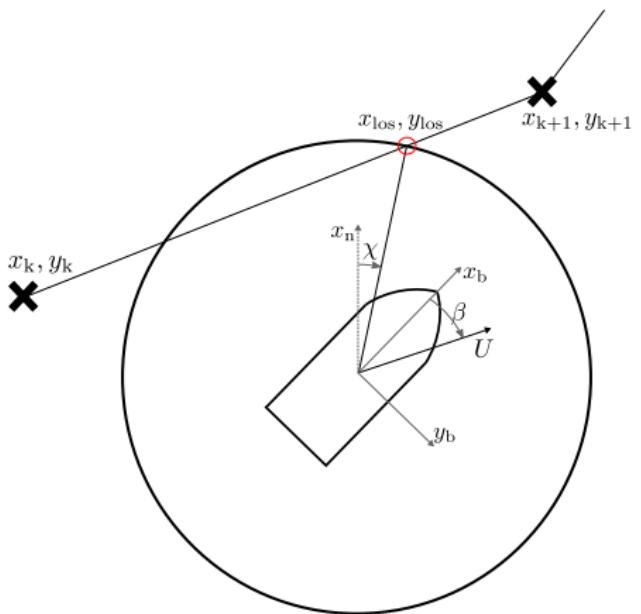
# Outer Controller

## Path Generation Algorithm



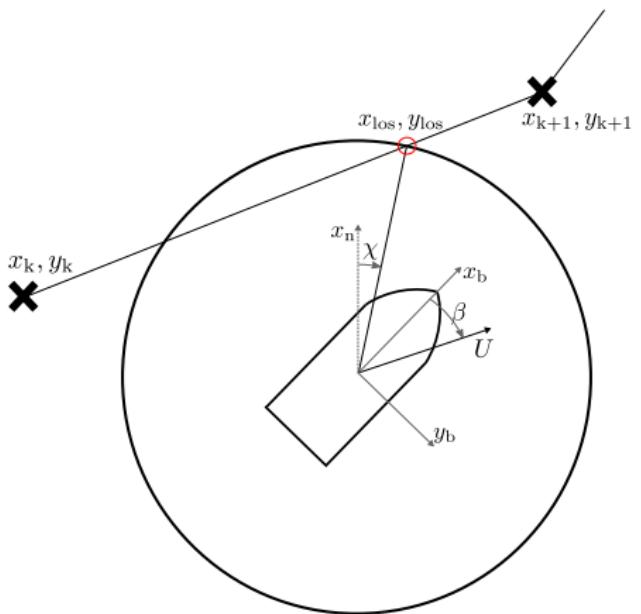
# Outer Controller

## Path Following Algorithm



# Outer Controller

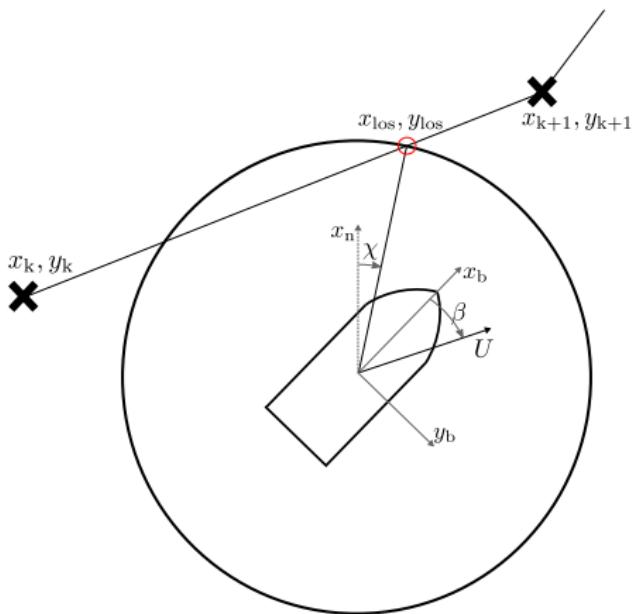
## Path Following Algorithm



$$\chi = \arctan \left( \frac{y_{\text{LOS}} - y_n}{x_{\text{LOS}} - x_n} \right)$$

# Outer Controller

## Path Following Algorithm

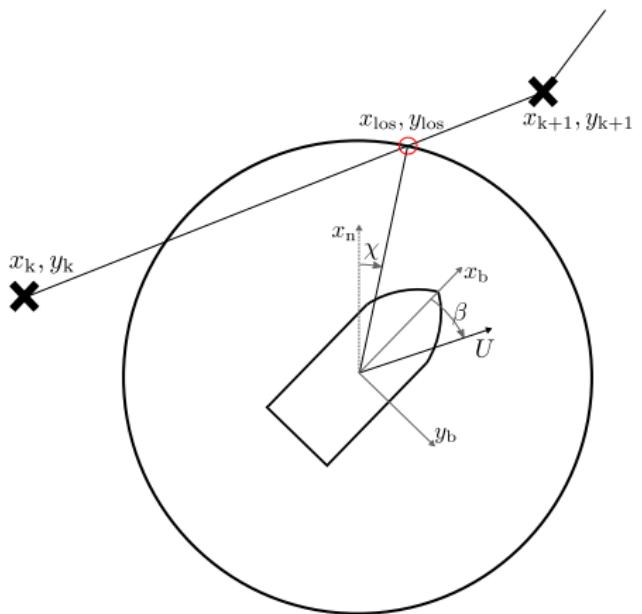


$$\chi = \arctan \left( \frac{y_{\text{LOS}} - y_n}{x_{\text{LOS}} - x_n} \right)$$

$$\beta = \arctan \left( \frac{\dot{y}_b}{\dot{x}_b} \right)$$

# Outer Controller

## Path Following Algorithm



$$\chi = \arctan \left( \frac{y_{\text{LOS}} - y_n}{x_{\text{LOS}} - x_n} \right)$$

$$\beta = \arctan \left( \frac{\dot{y}_b}{\dot{x}_b} \right)$$

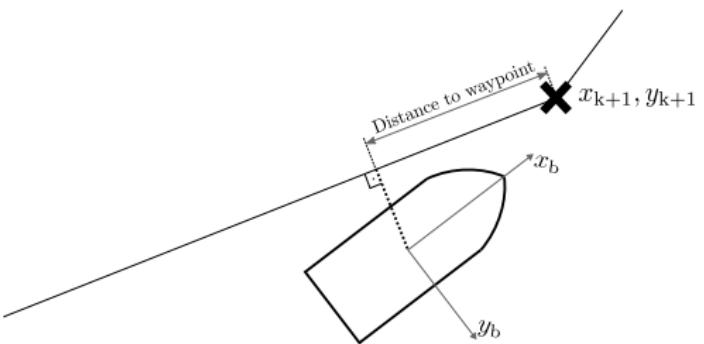
$$\psi_{\text{ref}} = \chi - \beta$$

# Outer Controller

## Path Following Algorithm



- ▶ Change active waypoints

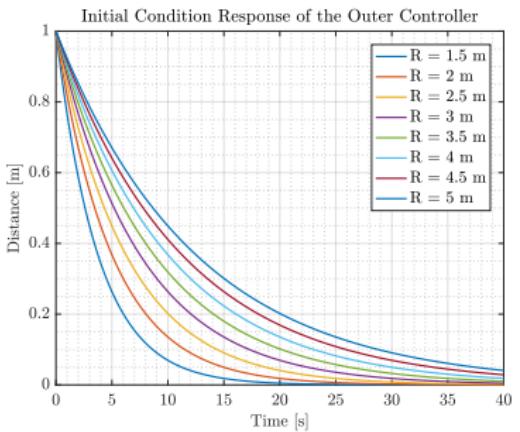
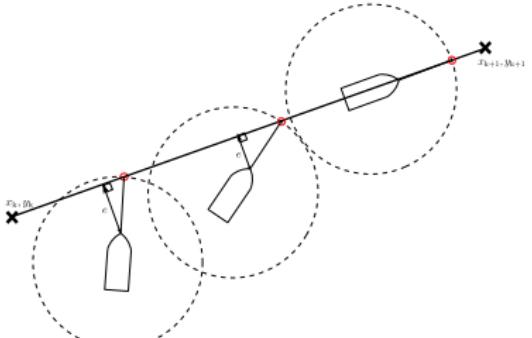


# Outer Controller

## Path Following Algorithm



- ▶ Convergence to the path

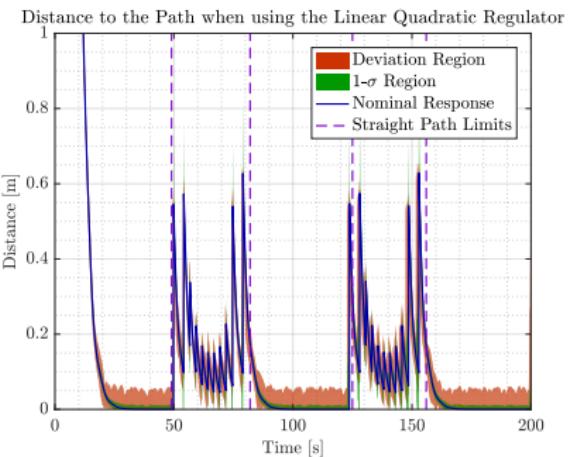
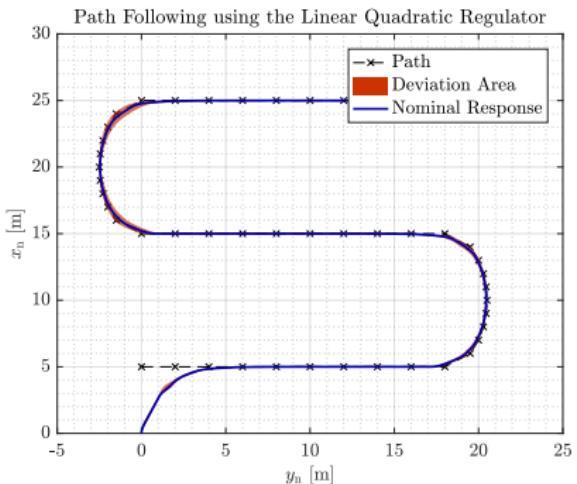


# Results

## Controller Results



### ► LQR as inner controller

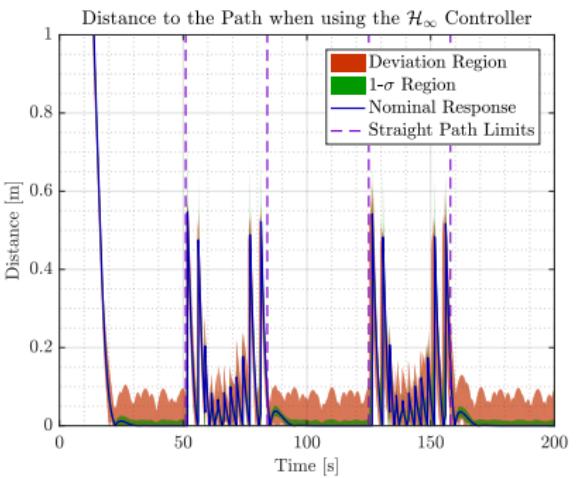
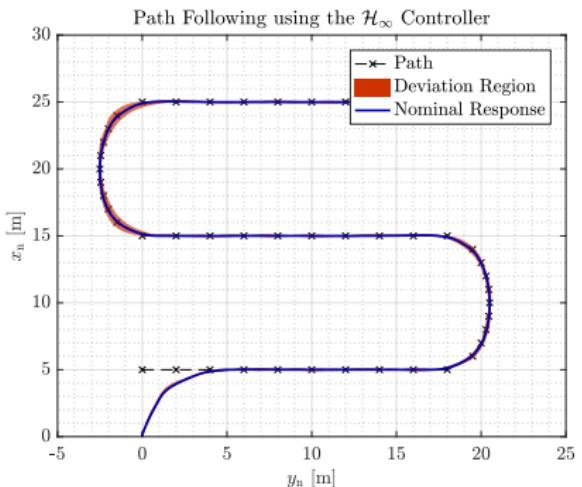


# Results

## Controller Results



- ▶ Robust controller as inner controller

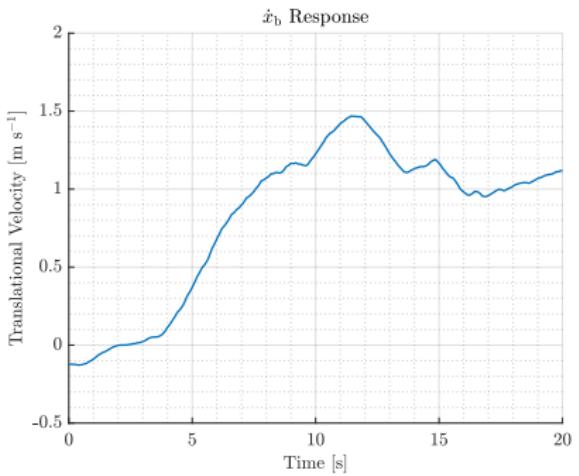
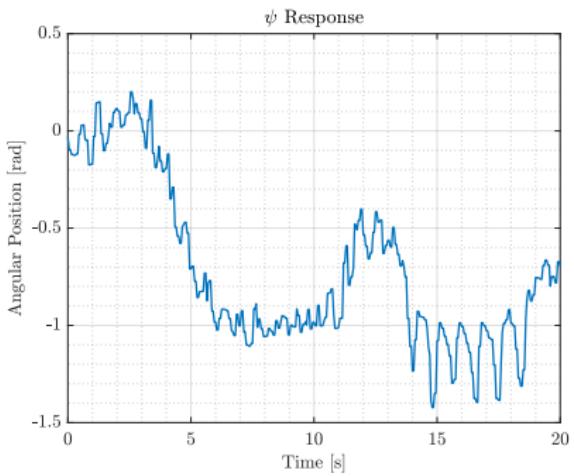


# Results

## Implementation Results



### ► Inner controller test



# Conclusion



- ▶ The estimator has been tuned and tested through simulation.
- ▶ The controller has also been analyzed though simulations that include disturbances, noise and varying parameters.
- ▶ The simulated results have not been fully replicated in the real vessel, but they show a promising behavior of the control system.

# Precision Control of an Autonomous Surface Vessel



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