

Wide Band Receiver Calibration

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1 Introduction

The object is to identify methods for calibration and perform calibration for multiple receiver system using an open source hardware. By calibration we mean, estimating the phase and amplitude changes to signal due RF signal conditioning units such as low-noise amplifiers, active bandpass filters and other components within the HW at transmitter and receiver for received signal. Once the HW contributions have been estimated, we can estimate the channel between the transmitter and receiver. We will be utilizing the below components for attempting calibration processes.

- Single Ettus USRP X410 unit [1]
- Single omnidirectional antenna
- Patch antenna with atleast 4 receive patches
- RF cables to connect the USRP to the antennas
- 20db attenuators
- CPU for sample collection
- ethernet cable to connect USRP to CPU

We will be utilizing 1 Transmit antenna (omnidirectional) and 4 receive antennas (patch antenna) to transmit/receive reference signals for calibration process.

The following terms will be used interchangably but they represent the same thing.

source : transmitter

sensor : receiver

Tx : Transmitter

Rx : Receiver

Sequence of steps:

1. Determine layout requirement of Tx and Rx antennas
2. Collect wireless transmission data between Tx and Rx
3. Collect wired transmission data with direct connection between the Tx and Rx port of the USRP
4. Perform Frequency Error Estimation and frequency correction
5. Determine stable points in the calibration data after phase unwrapping
6. Fix errors in unwrapping using outlier detection
7. Leakage detection **NOT SURE HOW TO VERIFY THIS**
8. Perform SAGE Algorithm to extract LoS component (Time Delay and Phase+Amplitude of signal)
9. Using the LoS signal phase to perform final calibration (and determine phase contributions from the receiver)
10. Using MUSIC algorithm to verify the correctness of the calibration data

2 Layout Requirement of Tx and Rx antennas

We begin by first identifying the reference signal properties and the receiver/sensor dimensions.

- Center Frequency $f_c : 5.725 \text{ Ghz}$
- Wavelength of source signal $\lambda = \frac{c}{f_c} = \frac{3 \times 10^8}{5.725 \times 10^9} \approx 0.052 \text{ meters}$
- Separation between sensors $L_a : 0.2 \text{ meter}$

We then consider the assumptions listed in Appendix A, that will be factored in for layout requirement. It is recommended to follow through the details provided in the Appendix to recognize the reason for these assumptions.

- Assumption 4 requires us to use sensors in a single array, hence we use the patch antenna as seen in Figure 1a. The 2nd reason for using patch antenna (instead of single Rx) is the possibility of using MUSIC algorithm to verify calibration data accuracy.
- Assumption 1 requires us to ensure the source and sensor is in the same plane. For this arrangement to be met, we ensure that the Tx and Rx are placed on the table with equal height. The height may not be exactly equal but within the error of few cms should be ok.
- Assumption 2 requires us to ensure the separation between the source and sensor are such that we can utilize the far field approximation. Referring to the equation provided in Appendix B, the Tx-Rx separation or Rayleigh distance must be greater than 1.54 meters.

$$\text{Rayleigh distance } d_R = \frac{2L_a^2}{\lambda} = \frac{2(0.2)^2}{0.052} \approx 1.54 \text{ meters}$$

- Assumption 3 requires no-mutual coupling between the receivers. The USRP X410 unit is assumed to have decent shielding between the different receivers.
- Assumption 6 requires us to ensure a clear LoS path. The quality of the LoS signal also depends on the Fresnel Zone clearance. Referring to the equation provided in Appendix C, the distance from the floor to the LoS path or the Fresnel Zone radius must be greater than 0.15 meters.

$$\text{Radius of first Fresnel Zone } F_1 = 8.656 \sqrt{\frac{d_R \times 10^6}{f_c}} = 8.656 \sqrt{\frac{1.629 \times 10^6}{5.725 \times 10^9}} \approx 0.15 \text{ meters}$$

The LoS requirement implies we need to separate out the LoS component from the multipath using the SAGE algorithm. More details are provided in section 7



(a) Patch Antenna

(b) Cabling from patch to USRP

Figure 1: Path Antenna Setup utilizing middle 4 patches

For our setup as seen in Figure 2, the Tx bench to Rx bench separation was set to 1.629 meters and the height from floor to Tx/Rx bench level is 0.5 meters. The Tx-Rx separation is greater than bench separation, and the LoS height is greater than the bench height. This ensures both Rayleigh distance ($> 1.54m$) and Fresnel Zero radius ($> 0.15m$) are both met

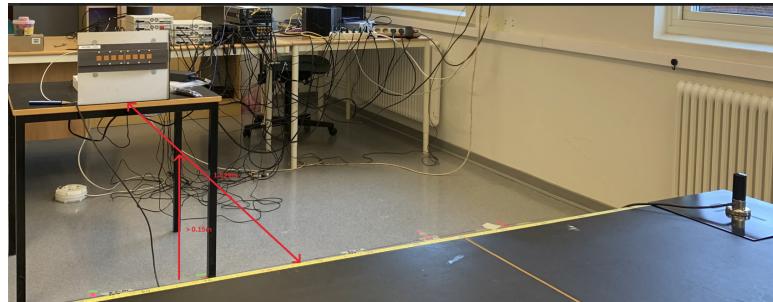


Figure 2: Measurements to check layout requirements

Apart from the critical aspects, there are some non-critical considerations that will help with calibration process. When we do unwrapping of the phase for visualization, it will be useful to ensure that the distance to the receiver for every adjacent position doesn't exceed by 1 wavelength (or 2π in radians). Based on the adjacent wrapped phase value, we can know if unwrapping is required or not. The other aspect is to ensure we have a minimum difference of atleast 0.1 wavelength (or 0.2π in radians) to reduce impact of human error on calibration data.

Reference Code : ArrangementCalculator.m

[Room for Improvement] Unfortunately, while deciding the arrangement for calibration data, the minimum difference was missed resulting in higher error near the middle. We opted for 10cm sliding length, when the calculations suggest value higher than 13cm. Given that we use 10cm as sliding length, the max length on either sides of the table calculates to be 104cm. We limited ourselves to 100cm. But if we opted for 13cm sliding length, then we will be limited to 77cm limits on either side of the mid point.

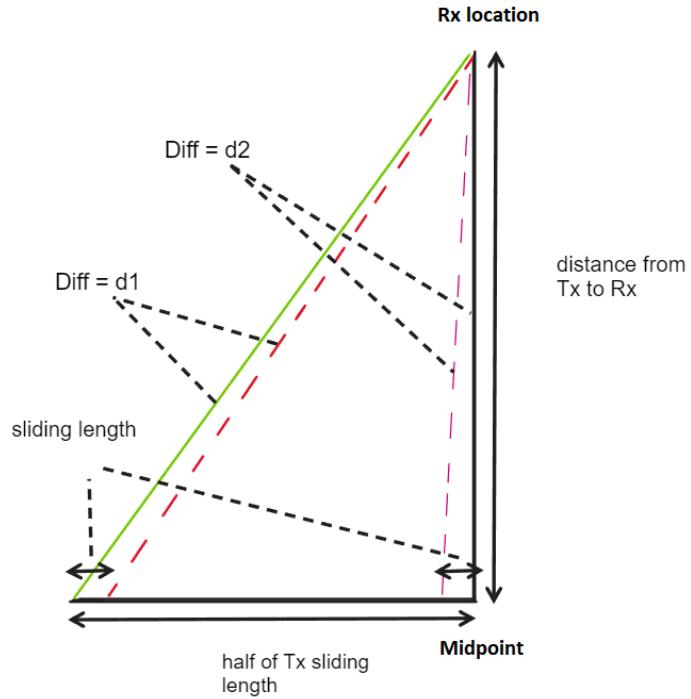


Figure 3: Visual understanding of min/max difference d_2 , d_1

This will all make more sense when you cover subsequent sections.

3 Data Collection

3.1 Tx-Rx Antenna setup

Having identified the apparatus setup requirements, now we attempt to collect data to perform the calibration. Collecting data for a single position of Tx and Rx antenna wont give us confidence on accuracy of calibration results. Rather we can attempt to collect multiple data points and ensure we see similar calibration results for all data points. For this we will attempt to slide the Tx antenna in parallel to patch antenna board orientation and collect the data at periodic position intervals. Arrange a couple of benches as shown in Figure 1b or Figure 4. Ensure that the center of the row of benches is in same position as the center of the patch antenna; to obtain equal measurements on either sides. Note down the measurement from one end to the center of the bench row setup as shown in Figure 4

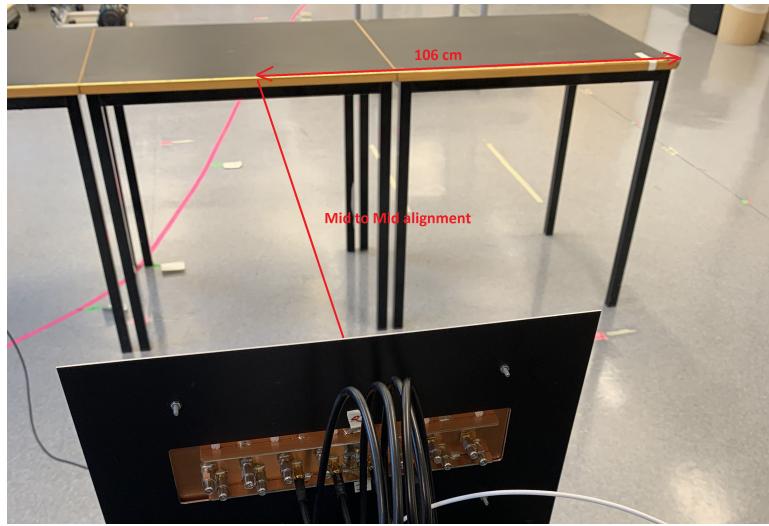


Figure 4: Mid point measurement

Once you have the bench row arrangement completed, we measure the Tx antenna bottom plate physical dimensions. The measurement values are shown in Figure 5

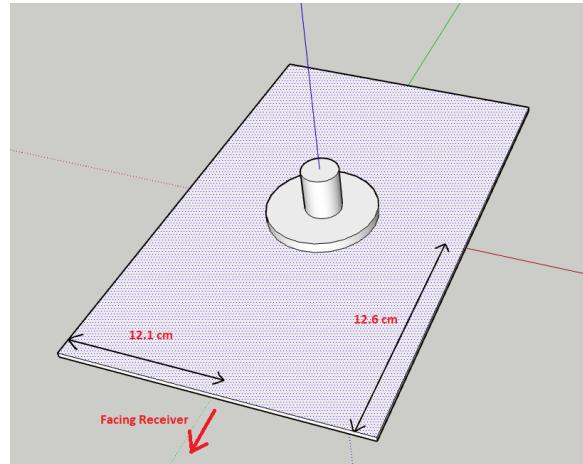


Figure 5: Tx antenna on metal plate

We will utilize the sliding approach to collect multiple data points, as shown in Figure 6. For this, we mark from the left to right, a 10cm interval and attempt to collect a set of measurements for every 10 cm shift in Tx antenna. The more the measurements, the more datapoints we have, the more is our confidence on the calibration data. Too narrow a separation will result in higher inaccuracies due to human error, hence 10cm seems to be a decent interval.

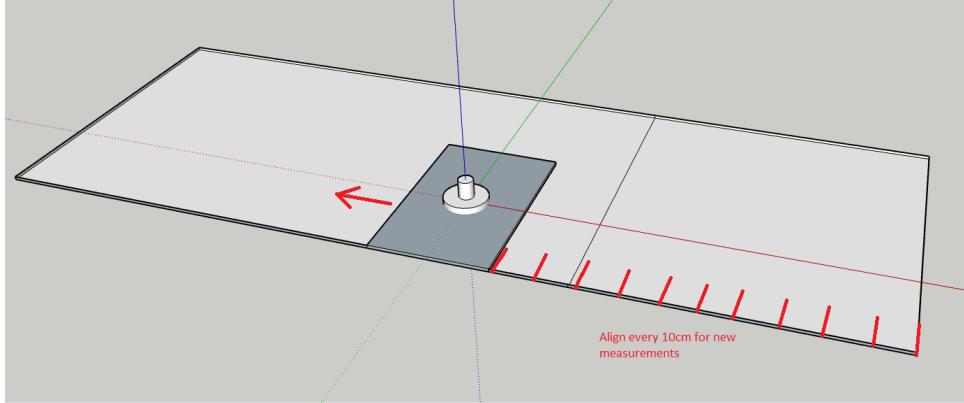


Figure 6: Sliding Tx Antenna

[Room for Improvement] One important consideration (to ensure lower error in the calibration data around mid) is while placing the Tx antenna as various positions, the mid position is as aligned to mid of the table setup. For our arrangement, unfortunately, this was not factored in. You can see from Table 1, for Sr No 10, 11 the mid value of DtMfN was not as close to 0 as possible. To improve this, it would be better to start from the mid and go sideways or start from left position that ensures we reach mid as we slide from left to right.

3.2 Cabling details

Now we turn our attention to rf cable connections between USRP and Tx-Rx antennas. Refer to Figure 7 for the details. The Tx port will be connected directly to the omnidirectional antenna.



Figure 7: Patch antenna to USRP

3.3 USRP Configuration

Center frequency : 5.725 Ghz

Waveform Type : OFDM (Appendix E)

Reference Signal : Zadoff Chu sequence (Appendix D)

Subcarrier spacing : **FILL**

Number of subcarriers : 1024

Sampling rate : 2ns

Tx gain : 55 dB

Rx gain : 45 dB

We will use the above configuration to collect OTA signal (Over The Air) as well as direct Tx to Rx feed BB data (Back-to-Back). To collect BB data, refer to Figure 8 as an example for Tx to Rx3 case. We need to collect the same for Tx to Rx0, Tx to Rx1 and Tx to Rx2.

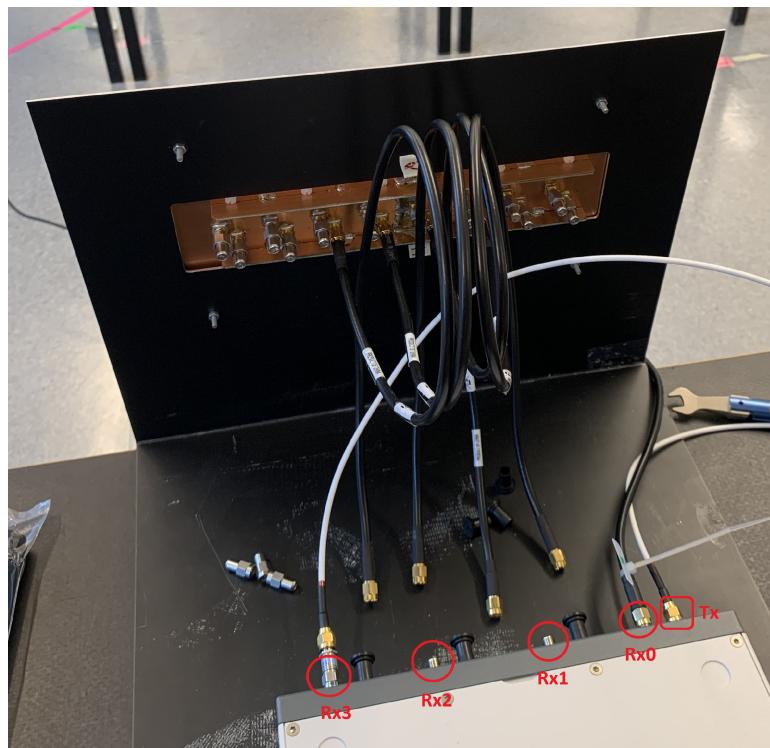


Figure 8: Back to Back Data collection Tx to Rx3 connection example

3.4 Table of positional data

Using the sliding approach (Figure 6), we collect all the necessary information shown in Table 1.

Patch Antenna and Tx Antenna bottom plate info :

Distance from left of Tx Antenna plate to Tx Antenna = 12.1 cm

Distance from front of Tx Antenna plate to Tx Antenna = 12.6 cm

Distance from left of Table to Center = 106cm

Shortest Distance from the center of Rx panel to Tables = 162.9cm

Shortest Distance from the center of Rx panel to Tx Antenna = $162.9 + 12.6 = 175.5$ cm

Distance between each patch in Rx Patch Antenna = 6.67 cm

Acronyms :

DfL : Distance from Left of the tables to tx antenna bottom plate

DtAfL : Distance to AntennaTx from Left of the tables

DtMfN : Distance to Mid from Tx Antenna position (+ve if Tx Antenna location to left of Mid else -ve)

DtMoR : Distance to Mid of Receiver (Hypotenuse) from Tx Antenna

DoA : Direction of Arrival w.r.t direction \perp to patch antenna plane

Dt1P : Distance to first Rx Patchh Antenna from Tx Antenna

Dt2P : Distance to second Rx Patch Antenna from Tx Antenna

Dt3P : Distance to third Rx Patch Antenna from Tx Antenna

Dt4P : Distance to forth Rx Patch Antenna from Tx Antenna

SrNo	DfL (cm)	DtAfl (cm)	DtMfn (cm)	DtMoR (cm)	DoA (radian)	DoA (degree)	Dt1P (cm)	Dt2P (cm)	Dt3P (cm)	Dt4P (cm)
1	0	12.1	93.9	199.0414	0.9781	-33.959	193.4554	197.1794	200.9034	204.6274
2	10	22.1	83.9	194.5237	1.0526	-29.6904	189.5706	192.8727	196.1747	199.4768
3	20	32.1	73.9	190.4244	1.1229	-25.6625	186.0937	188.9808	191.868	194.7551
4	30	42.1	63.9	186.7711	1.1897	-21.8352	183.0517	185.5313	188.0109	190.4905
5	40	52.1	53.9	183.5905	1.2536	-18.174	180.4715	182.5508	184.6302	186.7095
6	50	62.1	43.9	180.9073	1.3153	-14.6388	178.38	180.0649	181.7497	183.4346
7	60	72.1	33.9	178.7441	1.3752	-11.2068	176.8006	178.0963	179.3919	180.6876
8	70	82.1	23.9	177.1199	1.4338	-7.8492	175.7542	176.6647	177.5751	178.4856
9	80	92.1	13.9	176.0496	1.4914	-4.549	175.2565	175.7852	176.314	176.8427
10	90	102.1	3.9	175.5433	1.5486	-1.2717	175.7652	175.6173	175.4693	175.3214
11	100	112.1	-6.1	175.606	1.6056	1.9942	175.258	175.49	175.722	175.954
12	110	122.1	-16.1	176.2369	1.6628	5.2715	175.3182	175.9307	176.5431	177.1556
13	120	132.1	-26.1	177.4302	1.7206	8.5832	175.9378	176.9327	177.9277	178.9226
14	130	142.1	-36.1	179.1744	1.7794	11.9522	177.1035	178.4841	179.8647	181.2453
15	140	152.1	-46.1	181.4537	1.8397	15.4071	178.797	180.5681	182.3393	184.1104
16	150	162.1	-56.1	184.2484	1.9018	18.9652	180.9985	183.1651	185.3317	187.4983
17	160	172.1	-66.1	187.5352	1.9663	22.6608	183.6825	186.251	188.8194	191.3879
18	170	182.1	-76.1	191.2889	2.0338	26.5283	186.8225	189.8001	192.7777	195.7553
19	180	192.1	-86.1	195.4826	2.105	30.6077	190.391	193.7854	197.1798	200.5742
20	190	202.1	-96.1	200.0886	2.1806	34.9393	194.3615	198.1796	201.9976	205.8157

Table 1: Antenna position details

Full table of details can be referred to at DATA SHEET

Few Pointers :

- The calculations are limited to 4 decimal places

4 Frequency Error Detection and Correction

Reference Code : FrequencyErrorAndCorrection_v1.m

Frequency error can be easily identified by checking the phase difference between consecutive time samples. If we observe a linear increment or decrement in phase, then the contribution to this error in phase is the frequency error. The error from each channel is shown in Figure 9

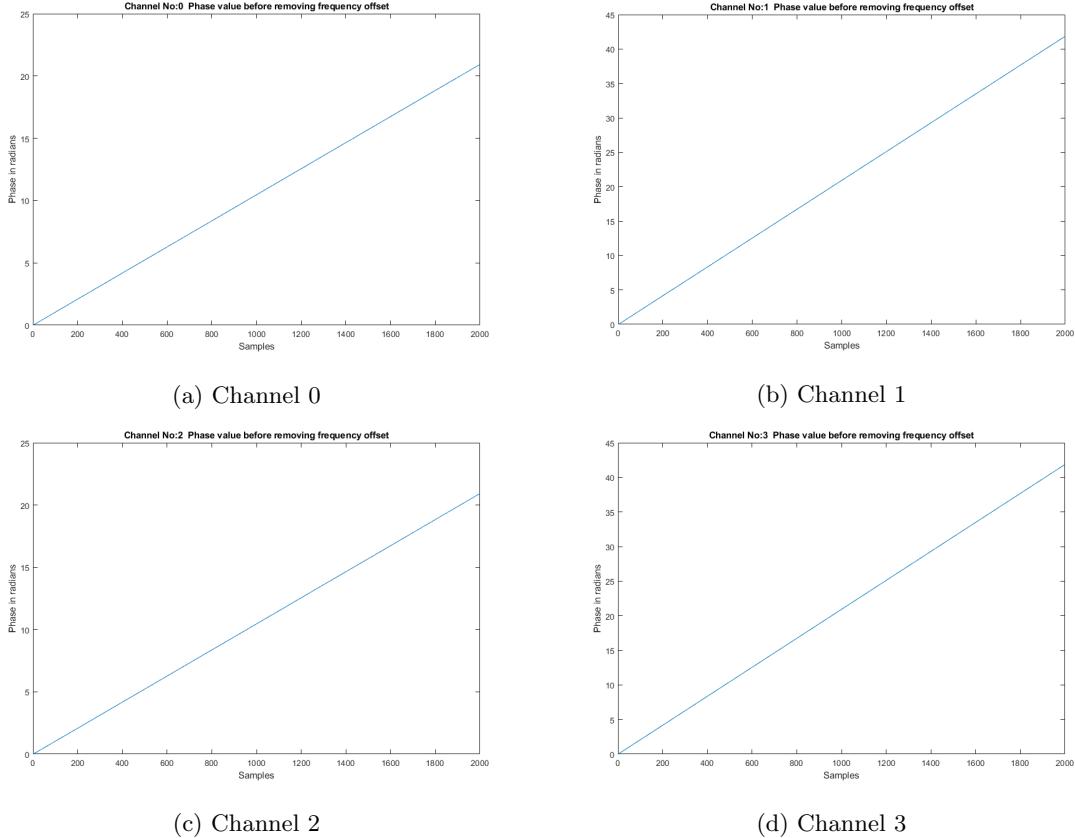


Figure 9: Plotting phase error using B2B data

We used a concept of phase unwrapping to see a clear increment and plot beyond the limit of $[-\pi \ \pi]$

We first determine the frequency error by determine the slope of the line. This can be easily computed using polyfit. Using the determined frequency error, we can remove the error by reversing the effect. The phase error after removing frequency error is shown in Figure 10

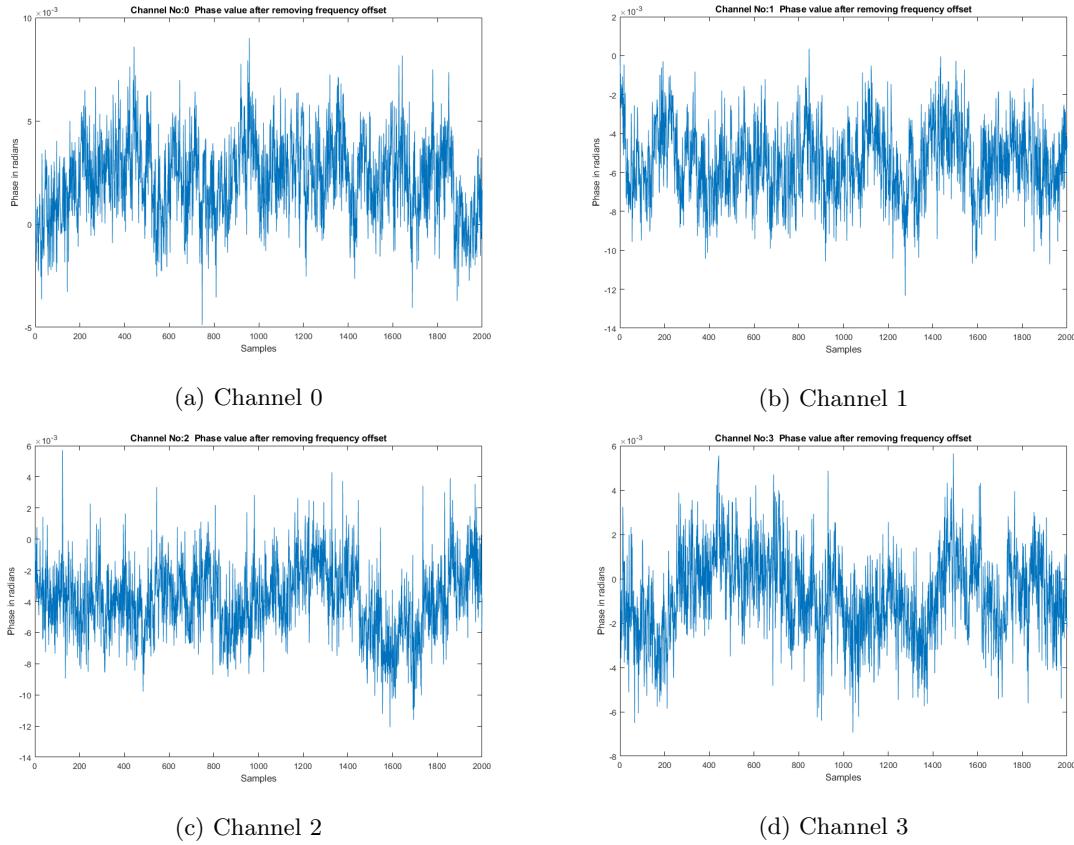


Figure 10: Plotting phase error after frequency error removal

As we can see, the phase error has now dropped to max of 10^{-2} and has stochastic behavior over time.

5 Stable stationary point detection for Channel Estimation

Reference Code : KNN_Clustering_v1.m

While sliding the Tx antenna, the received signal will observe some phase jitter either due to physical obstruction, or actual antenna movement movement. It takes few secs to stabalize after completing the antenna placement hence selecting the stable points for calibration at every step is necessary. The Figure 11 gives a good view of phase jitters.

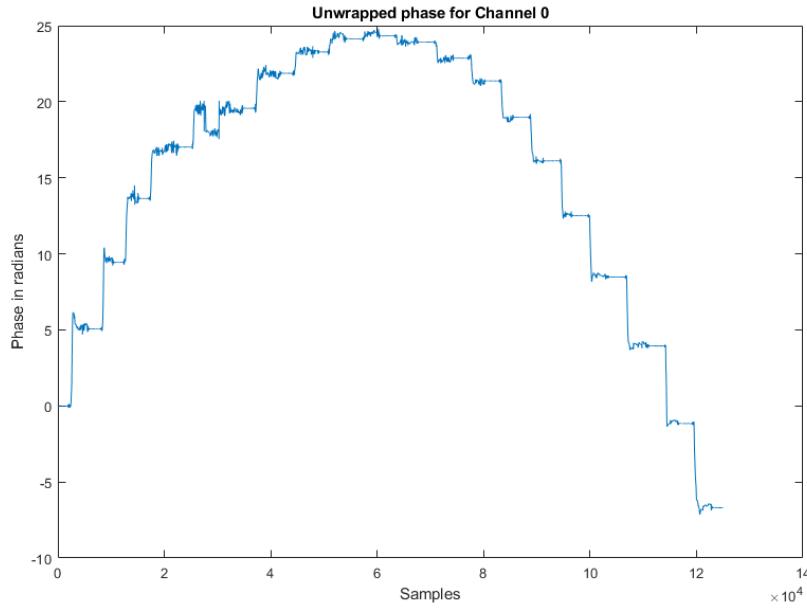


Figure 11: Sample of Phase Jitter

The stable points can either be choosen manual through visual inspection or you can use a customized KNN Clustering algorithm. This algorithm requires you to provide the percentage of time the antenna was in a stationary position with no interference/obstruction (RatioStableVsMovement) and the number of stable points (NumCenters). Below is the summary but you can refer to Appendix F for more details

Summary of Algorithm :

- Introduce the concept of window, which is 1 or more secs of consecutive ofdm samples.
- Provide two values, Number of stable points (eg 20) and Percentage of time in stable region (eg 0.5).
- The Acceptance Rate Limit should be less than percentange of time in stable region
- By selecting window time (window width), utilize sliding window (slide 1sec for new window) to pick different set of ofdm samples for each window (window sample)
- Utilize the mean and variance of the phase value of all ofdm samples in a window (mean value, variance value)
- Perform KNN Clustering using the mean value of all window samples and number of centroids equal to number of stable points.
- Reject bad window samples based on (eg highest variance) of all the window samples

- Increase strictness of sample quality (eg using sum of points to centroid distance or sumd) to meeting Acceptance Rate Limit
- Pick window width based on highest number of surviving samples but meeting Acceptance Rate Limit
- Select the nearest sliding window index to the centroid (stable window index)
- Repeat for all channels and take average index value as final stable window index (number of indexes equal to number of stable points equal to number of clusters)
- Select the mid ofdm sample for all stable window indexes

The locations of the stable positions picked up by the above algorithm can be seen in Figure 12

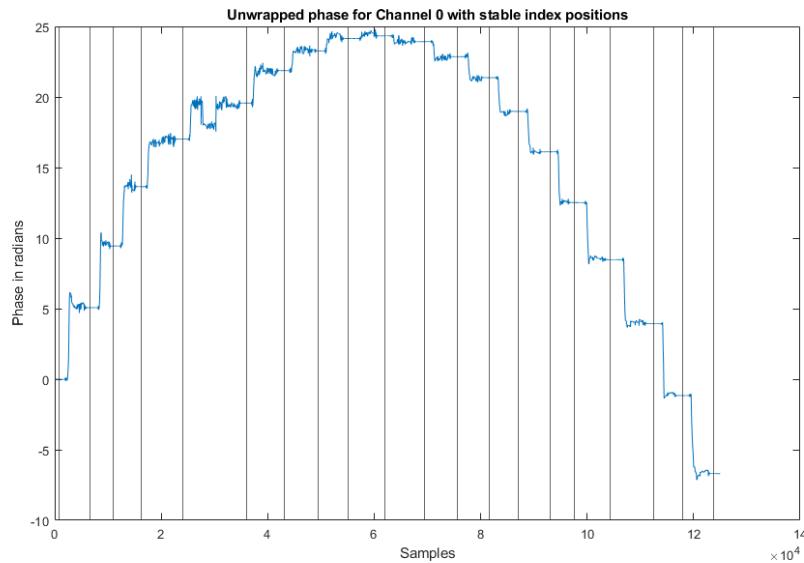


Figure 12: Vertical plot of Stable Positions

6 Unwrapping error removal using outlier detection

Reference Code : OutlierDetectorAndPhaseCorrector_v1.m

This process is not necessary to complete the calibration process, but helps with obtaining the right unwrapped phase. The more the number of receive antennas, the better is the error removal process. Figure 13 shows a good example of unwrapping error in Channel 3. The blue indicates wrapped phase and orange points indicates unwrapped phase. Carefully observing the overlapping instance to non-overlapping instance near 500, you will see a jump of more than π which makes it difficult to know if this was due to wrapping or not. Observing other samples gives clue on what the phase is.

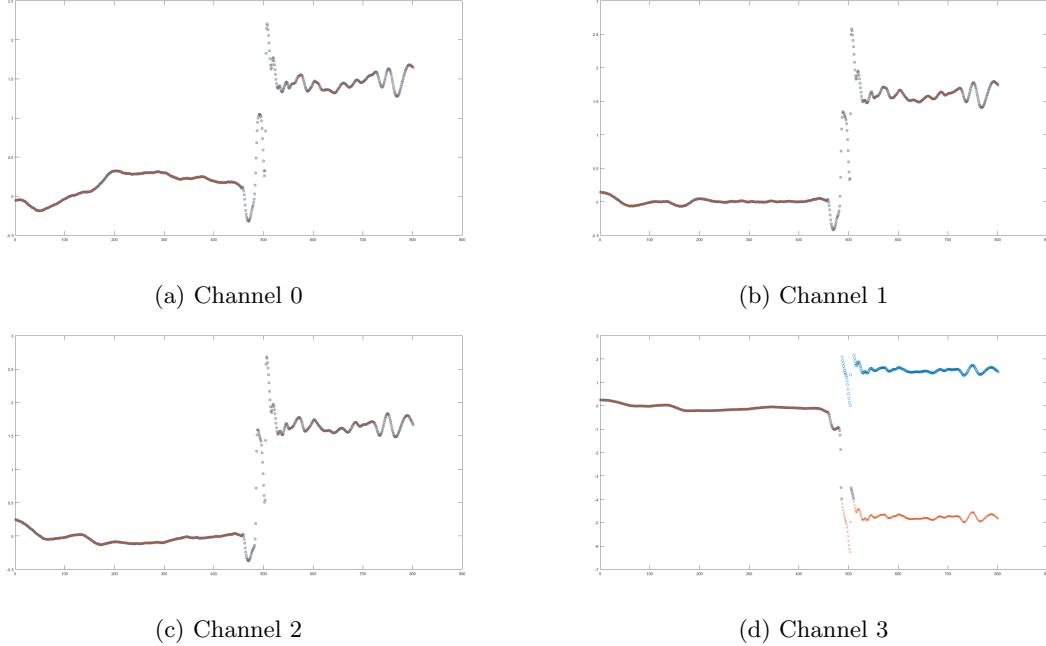


Figure 13: Unwrapping Error Example

The one advantage of using multiple receive antennas simultaneously; it becomes easier to detect outliers. Note that for SAGE algorithm below we utilize the original signal but for unwrapping the LoS phase, we need to rely on adjust phase for unwrapping identified earlier and hence detecting outliers is critical. For the SAGE algorithm we only utilize 1 data point for every Tx antenna location hence we don't have a gradual phase transition plots from SAGE. Figure 14 shows the corrected

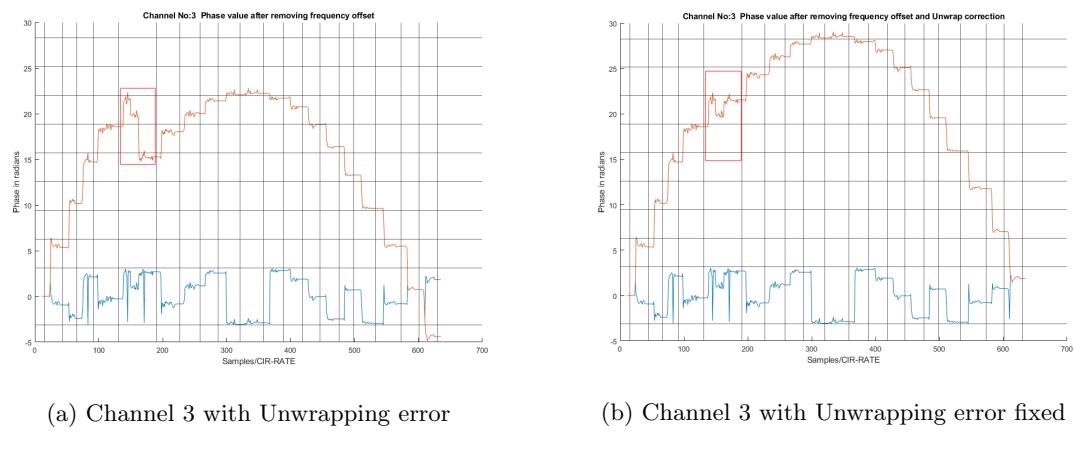


Figure 14: Unwrapping Error Fixed

7 LoS Separation

As indicated by Assumption 6, we need the LoS signal characteristics to perform calibration. We start with describing the signal model following the SAGE algorithm.

7.1 Signal Model

Lets denote the time-varying channel transfer function as $h(k; t)$ where $k \in [1, \dots, 1024]$ indicates the indexes of the subcarriers/tones. h is measured as

$$h(k, t) = \frac{y(k; t)}{x(k)} \quad (1)$$

where y and x denote the received and transmitted signals respectively in the frequency domain. The time varying channel impulse response (CIR) $h(\tau; t)$ is then calculated by performing inverse Fourier transform to $h(k; t)$

In an indoor environment, the receiver is expected to receive multipath components from the source emitting wireless signals. Each multipath component will consist of a delay, and a complex amplitude; and we can represent the signal model with time varying multipath components as

$$h(\tau; t) = \sum_{\ell=1}^{L(t)} \alpha_{\ell}(t) \delta(\tau - \tau_{\ell}(t)) \quad (2)$$

$h(\tau; t)$: Time varying channel impulse response

$\alpha_{\ell}(t)$: time varying complex amplitude

$\delta(\tau - \tau_{\ell}(t))$: time varying delay of the ℓ th multipath component.

$L(t)$: number of MPCs observed for the snapshot at time instant t

The channel parameters to be estimated are $\boldsymbol{\theta} = [\alpha_{\ell}(t), \tau_{\ell}(t), L(t)]$ where $\ell = 1, \dots, L(t)$ and $t = t_1, \dots, t_M$ with M being the number of measurement shaphshots.

Since there is no relationship between the shaphshots, we can modify the parameter estimation problem to a single snapshot at a time

$$\boldsymbol{\theta} = [\alpha_{\ell}, \tau_{\ell}, L] \quad (3)$$

The equation for received signal (single shaphshot) can be written as

$$y(k) = h(k) \cdot x(k) = \sum_{\ell=1}^L \alpha_{\ell} \cdot x(k) \cdot e^{-j2\pi(k-1)\tau_{\ell}/K} + n(k) \quad (4)$$

$y(k)$: Received signal for the k th subcarrier

$x(k)$: Transmitted signal (calibration signal) for the k th subcarrier

$n(k)$: AWGN

Rewriting above equation in vector form by stacking all subcarrier terms into single vector

$$\mathbf{y} = \sum_{\ell=1}^L \alpha_{\ell} \mathbf{x}(\tau_{\ell}) + \mathbf{n} \quad (5)$$

We were able to convert Equation 14 into an optimization problem described by Equation 17. Unfortunately, above Equation 5 will result in an intractable ¹ likelihood function if we attempt the similar optimization steps (steps described between Equation 16 and 17). We need to employ iterative methods to separate out the multipaths which is discussed in next section.

Estimation problem :

$$\min_{\Theta} \left\| \mathbf{y} - \sum_{\ell=1}^L \alpha_{\ell} \mathbf{x}(\tau_{\ell}) \right\|^2 \quad (6)$$

Comparison to Equation 17, $\mathbf{A}_m \rightarrow \mathbf{y}$, $\alpha_l \rightarrow \mathbf{M}$, $\mathbf{A} \rightarrow \mathbf{x}$

¹Intractable means unsolvable and this is due to aggregation of multipath components in a single received sample

7.2 SAGE implementation

Below are the steps while implementing the SAGE algorithm. For more mathematical details, please refer to Appendix G and H

$$\mathbf{x}(\tau_i) = [x(1) \cdot e^{-j2\pi(0)\tau_i/K} \quad x(2) \cdot e^{-j2\pi(1)\tau_i/K} \quad \dots \quad x(K) \cdot e^{-j2\pi(K-1)\tau_i/K}]'$$

1. **Initialize all complex amplitudes to zero.** $\alpha_l = 0$

Reason [Step 1 in SAGE algorithm] : We need to initialize the variables to some value before applying iterative optimization. For the very first optimization process, the LOS component will be the strongest and we hope that the optimization will be able to narrow down on the right time delay and complex amplitude.

2. **Estimate the i-th multipath component, considering the other multipath as known parameters.** Hence \mathbf{y}_i becomes

$$\mathbf{y}_i = \mathbf{y} - \sum_{l \neq i} \alpha_l \mathbf{x}(\tau_l) \quad (7)$$

Reason [Step 1 in SAGE algorithm] : We have chosen the i-th multipath parameters τ_i, α_i to optimize on.

Reason [Step 2 + 3 in SAGE algorithm] : Remember that SAGE algorithm requires “admissible hidden-data space”. By subtraction all the other multipath components, we focus only just 1 path. This leaves us with only two parameters τ_i, α_i . We perform E-step using last computed values or initialized values.

3. **Apply maximization to estimate the parameter**

$$\hat{\tau}_i = \max_{\tau_i} \|\mathbf{x}(\tau)^H \mathbf{y}_i\| \quad (8)$$

Reason [Step 4 in SAGE algorithm] : We apply M-step. **how to explain the derivation of this beyond intuition? Can I say that the autocorrelation property of Zadoff Chu sequences ensure maximum value for right time delay**

Note that SAGE algorithm helps determine a local minima. Since we need to determine a global minimum, we perform numerical search. We attempt all integer values and utilize the optimization function to narrow to few decimal places in accuracy. The numerical search will target the strongest signal.

4. Determine remaining parameter

$$\hat{\alpha}_i = \mathbf{x}(\hat{\tau}_i)^H \mathbf{y}_i / \|\mathbf{x}(\hat{\tau}_i)\|^2 \quad (9)$$

Reason : With \mathbf{y}_i , we only have two parameters to estimate (τ_i, α_i) . Since we have already performed optimization on one of the parameters τ_i , the remaining one α_i can be determined in closed form.

Proof:

$$\begin{aligned} \mathbf{y}_i &= \mathbf{y} - \sum_{l \neq i} \alpha_l \mathbf{x}(\tau_l) \approx \hat{\alpha}_i \mathbf{x}(\hat{\tau}_i) \\ \Rightarrow \mathbf{x}(\hat{\tau}_i)^H \hat{\alpha}_i \mathbf{x}(\hat{\tau}_i) &= \mathbf{x}(\hat{\tau}_i)^H \mathbf{y}_i \quad \text{premultiplying both sides by } \mathbf{x}(\hat{\tau}_i)^H \\ \Rightarrow \hat{\alpha}_i \mathbf{x}(\hat{\tau}_i)^H \mathbf{x}(\hat{\tau}_i) &= \mathbf{x}(\hat{\tau}_i)^H \mathbf{y}_i \quad \hat{\alpha}_i \text{ is a scalar hence re-ordering terms} \\ \Rightarrow \hat{\alpha}_i \|\mathbf{x}(\hat{\tau}_i)\|^2 &= \mathbf{x}(\hat{\tau}_i)^H \mathbf{y}_i \\ \Rightarrow \hat{\alpha}_i &= \mathbf{x}(\hat{\tau}_i)^H \mathbf{y}_i / \|\mathbf{x}(\hat{\tau}_i)\|^2 \end{aligned}$$

5. Repeat step 2 for all multipath

Reason : For every iteration, we choose a different index set (all parameters pertaining to one path), estimate the parameters, subtract out the path and continue to next path.

6. Repeat step 3 a few times until you deem it accurate enough

Reason : There is a possibility of residual energy even if we attempted to remove a significant portion of energy from each multipath. More iterations helps reduce this residual energy

The successive peak removal as part of SAGE algorithm can be clearly seen in Figure
The retrieved LoS Components from SAGE is shown in Figure 16

WE DONT GET NEAT TRANSITIONS, MUST BE SOME INDEXING PROBLEM

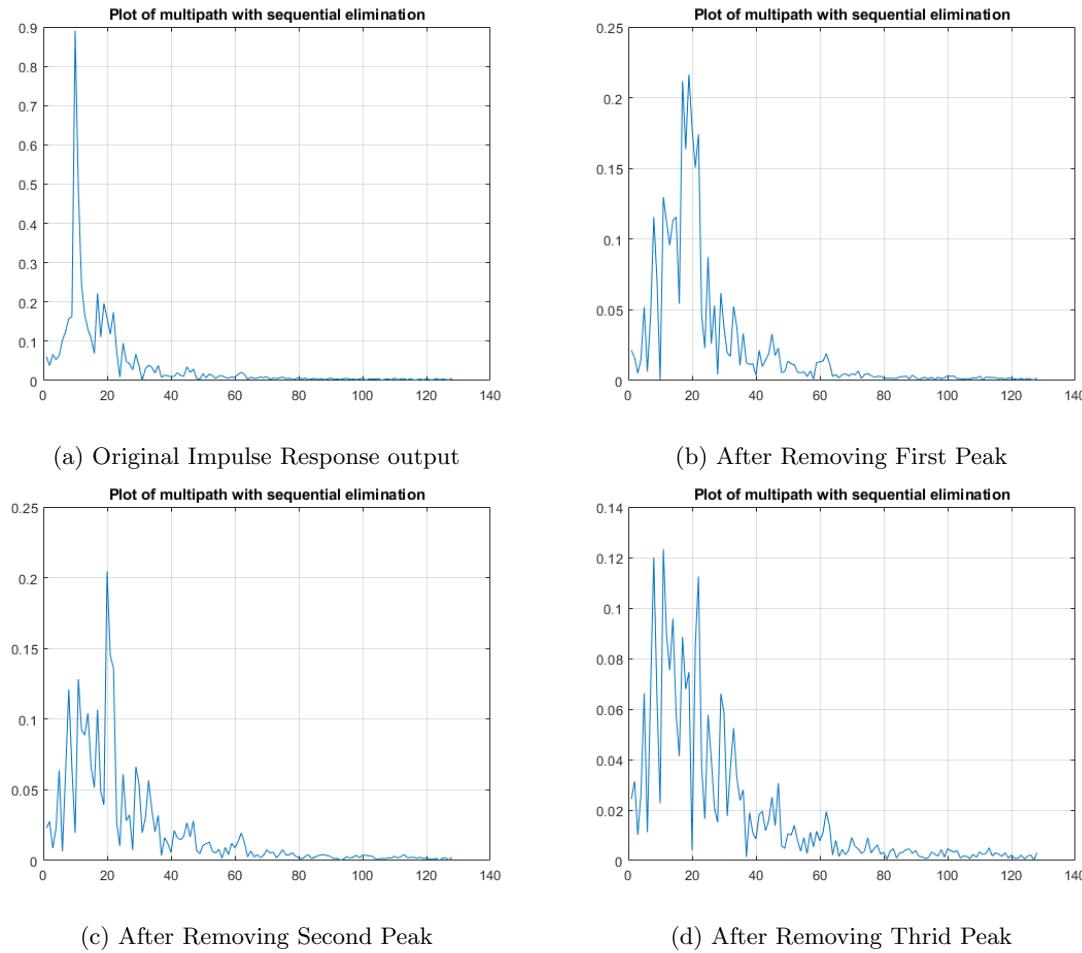


Figure 15: SAGE Algorithm Successive Peak Removal

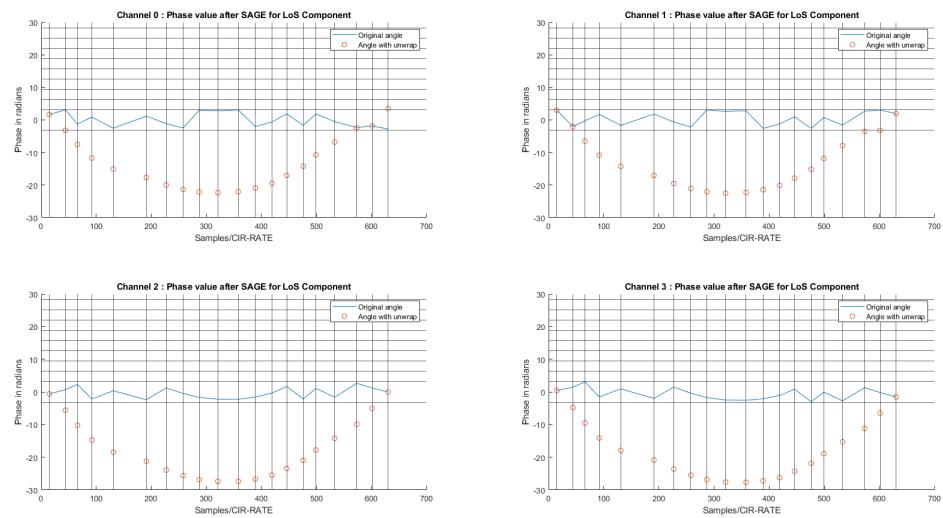


Figure 16: LoS Components after SAGE

8 Calibration

Now we shall use

A Summary of Calibration algorithm and simplification

The sensor array calibration paper[2] covers in detail calibration algorithm, starting with the most generic problem statement of using n sources and m sensors. This section will identify the assumptions/approximations made by the paper followed by simplifying the problem statement to suit our needs and the relevant equations.

In order to obtain the phase difference w.r.t reference sensor, we use the below equation

$$a(\psi_i, \theta_j) = e^{j\omega_o \tau_i(\theta_j)} \quad (10)$$

ψ_i : sensor coordinate position such as value of x, y and z-axis in 3D space

θ_i : direction of arrival such as value of azimuth and elevation angle in 3D space

τ_i : time delay which is a function of θ_i

Solving the system of equations in 3D space would be quite complex and require lots of accurate/high precision sensor data. Instead we can opt to simplify the equation by assuming the source and sensors in a single plane and far field approximation.

Assumption 1 : Sensor and source in a single plane

Reason : 3D space can be reduced to 2D space

Assumption 2 : Wavefront follows far field approximation

Reason : Easier to compute the relative distance from source to different sensors

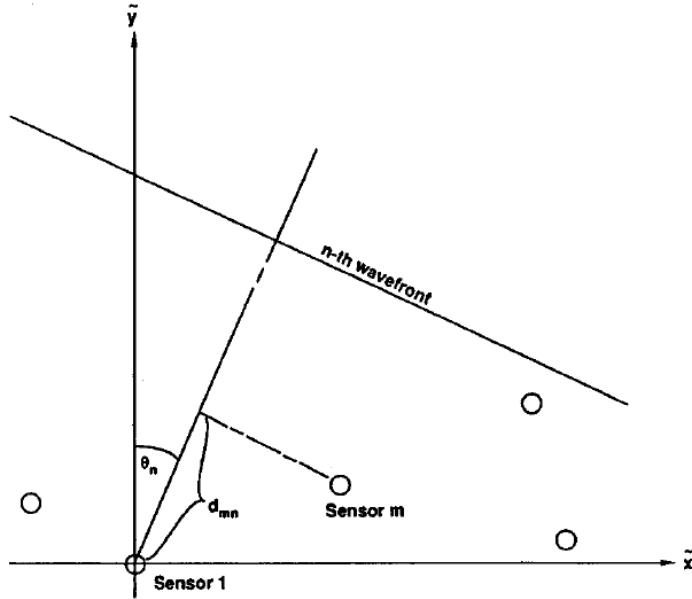


Figure 17: Problem geometry [3]

Assumption 1 and 2 simplifies the calculations for relative time delays of received signal across sensors. The Figure 17 will help understand how the time delays are derived. Assuming Sensor 1 as reference, the delay of the signal from source n on the sensor m can be expressed by below equation

$$\tau_m(\theta_n) = -d_{mn}/c = -\frac{1}{c}(x_m \sin \theta_n + y_m \cos \theta_n) \quad (11)$$

n : Index for source

m : Index for sensor

$\tau_m(\cdot)$: Time delay of received signal on Sensor m w.r.t reference sensor (Sensor 1)

d_{mn} : Distance from Sensor m to reference sensor in the direction of source n

(x_m, y_m) : Coordinates of sensor m also represented as ψ_m

θ_n : Direction of Arrival (DOA) of source n relative to y-axis

c : Propagation velocity or the speed of light

Rewriting sensor coordination positions as an array

$$\boldsymbol{\psi} = [\psi_1, \psi_2, \dots, \psi_m]^T = [(x_1, y_1), (x_2, y_2), \dots, (x_m, y_m)]^T$$

Rewriting in vector form to represent phase vector,

$$\mathbf{a}(\boldsymbol{\psi}, \theta_j) = [e^{j\omega_o \tau_1(\theta_j)}, e^{j\omega_o \tau_2(\theta_j)}, \dots, e^{j\omega_o \tau_m(\theta_j)}] \quad (12)$$

Note, we have only represented the phase contributions based on physical location of sources. We still need to factor in phase and amplitude contributions by each sensor that may or may not be related to other sensors. We will introduce a matrix to describe exactly these characteristics.

$\mathbf{M} \in \mathbb{C}^{m \times m}$: Calibration matrix comprising of mutual coupling coefficients between sensor elements and the gain and phase terms of each sensor (or channel)

For a single signal arriving from θ , the complex envelope of the received signal vector,

$$\mathbf{r}(t) = \mathbf{M} \cdot \mathbf{a}(\boldsymbol{\psi}, \theta_j) \cdot s(t) + \mathbf{e}(t) \quad (13)$$

While performing experiments, what is known to us is the received signal $\mathbf{r}(t)$ and the complex envelop of the source signal $s(t)$. What we need to determine is calibration matrix \mathbf{M} and phase vector $\mathbf{a}(\boldsymbol{\psi}, \theta_j)$ or to be more specific, we need to determine $\boldsymbol{\psi}$, but θ is known. We will come back to how θ can be calculated in our case. The zero mean additive Gaussian noise vector $\mathbf{e}(t)$ is not known and cannot be measured.

Performing summation on Equation 13 for N samples over time, we get

$$\begin{aligned} \sum_{t=1}^N \mathbf{r}(t) &= \sum_{t=1}^N \left(\mathbf{M} \cdot \mathbf{a}(\boldsymbol{\psi}, \theta_j) \cdot s(t) + \mathbf{e}(t) \right) \\ &= \mathbf{M} \cdot \mathbf{a}(\boldsymbol{\psi}, \theta_j) \cdot \sum_{t=1}^N s(t) + \sum_{t=1}^N \mathbf{e}(t) \\ &= \mathbf{M} \cdot \mathbf{a}(\boldsymbol{\psi}, \theta_j) \cdot \alpha N + \sum_{t=1}^N \mathbf{e}(t) \end{aligned}$$

$$\frac{1}{\alpha N} \sum_{t=1}^N \mathbf{r}(t) = \mathbf{M} \cdot \mathbf{a}(\psi, \theta_j) + \frac{1}{\alpha N} \sum_{t=1}^N \mathbf{e}(t) \quad (14)$$

$$\mathbf{a}_m(\theta_j) = \mathbf{M} \cdot \mathbf{a}(\psi, \theta_j) + \mathbf{n}_j \quad (15)$$

$\mathbf{a}_m(\theta_j)$: Steering vector for a calibration source at location θ_j

\mathbf{n}_j : zero-mean Gaussian distribution but with different covariance $\zeta^2 \mathbb{I}$ as $\mathbf{e}(t)$ where \mathbb{I} is identity matrix of size $n \times n$

Equation 15 is a linear problem, but because \mathbf{n}_j is not a measurable quantity, we have to rely on stochastic approaches such as utilizing probability density function. We can easily formulate the optimization equation (because noise is zero-mean Gaussian) but we need to ensure that signal from different sources do not overlap when received by a sensor. We can achieve this by collecting the received signal at every sensor after transmitting from all n sources but in temporally disjoint fashion. In other words, transmit only one source at a time, and measure the signal at the sensor, before transmitting from the next source.

$$\max_{\mathbf{M}, \psi} p(\mathbf{a}_m(\theta_1), \mathbf{a}_m(\theta_2), \dots, \mathbf{a}_m(\theta_n) | \mathbf{M}, \psi, \zeta^2) = \max_{\mathbf{M}, \psi} \frac{1}{(\pi \zeta^2)^{nm}} e^{-\frac{1}{\zeta^2} \sum_{j=1}^n \|\mathbf{a}_m(\theta_j) - \mathbf{M} \cdot \mathbf{a}(\psi, \theta_j)\|^2} \quad (16)$$

We can simplify the above equation by taking log but also convert a maximizing problem to a minimizing problem by taking the negative log. The constant terms can be ignored as they dont contribute to optimization.

$$\min_{\mathbf{M}, \psi} \left(-\log(p(\cdot)) \right) = \min_{\mathbf{M}, \psi} \left(- \left(\log \left(\frac{1}{(\pi \zeta^2)^{nm}} \right) - \frac{1}{\zeta^2} \sum_{j=1}^n \|\mathbf{a}_m(\theta_j) - \mathbf{M} \cdot \mathbf{a}(\psi, \theta_j)\|^2 \right) \right)$$

getting rid of constant additive terms

$$= \min_{\mathbf{M}, \psi} \left(\frac{1}{\zeta^2} \sum_{j=1}^n \|\mathbf{a}_m(\theta_j) - \mathbf{M} \cdot \mathbf{a}(\psi, \theta_j)\|^2 \right)$$

getting rid of constant multiplicative terms

$$= \min_{\mathbf{M}, \psi} \left(\sum_{j=1}^n \|\mathbf{a}_m(\theta_j) - \mathbf{M} \cdot \mathbf{a}(\psi, \theta_j)\|^2 \right)$$

expanding summation term and swapping order within modulus square

$$= \min_{\mathbf{M}, \psi} \|\mathbf{M} \cdot \mathbf{a}(\psi, \theta_1) - \mathbf{a}_m(\theta_1)\|^2 + \dots + \min_{\mathbf{M}, \psi} \|\mathbf{M} \cdot \mathbf{a}(\psi, \theta_n) - \mathbf{a}_m(\theta_n)\|^2$$

converting additive vector terms into matrix multiplication + Frobenius Norm

$$= \min_{\mathbf{M}, \psi} \|\mathbf{M} \mathbf{A}(\psi) - \mathbf{A}_m\|_{\textcolor{red}{F}}^2$$

$$\mathbf{A}_m = [\mathbf{a}_m(\theta_1), \mathbf{a}_m(\theta_2), \dots, \mathbf{a}_m(\theta_n)]$$

$$\mathbf{A}(\psi) = [\mathbf{a}(\psi, \theta_1), \mathbf{a}(\psi, \theta_2), \dots, \mathbf{a}(\psi, \theta_n)]$$

Optimization problem (changed order of terms, outcome doesnt change) :

$$\min_{\mathbf{M}, \psi} \|\mathbf{A}_m - \mathbf{M} \mathbf{A}(\psi)\|_{\textcolor{red}{F}}^2 \quad (17)$$

We cannot solve the optimization problem unless the number of measurements is equal to or exceeds the unknowns, or in other words, the number of equations must be equal to or exceed the number of unknowns

M : This is a $m \times m$ matrix implying $m \times m = m^2$ terms and hence m^2 unknowns. But we also have to keep in mind this is complex matrix, resulting in two unknowns (real + imaginary) for every element in the matrix. This gives us a total of $2m^2$ (real) unknowns.

ψ : The coordinates of the m sensors are not known, and hence $2m$ (real) unknowns.

\mathbf{A}_m : This is known and will give us $m \times n$ independent measurements, but if we factor in both real and complex, we get $2mn$ (real) known measurements.

To ensure a possible solution, we can represent the condition as an inequality expression

$$2mn \geq 2m^2 + 2m \quad (18)$$

and also **\mathbf{A}_m** needs to be full rank!

Assumption 3 : No mutual coupling between sensor elements

Benefit : Reduces the number of unknowns for system of equations

The sensors or in our case the USRP receivers are assumed to have good shielding and hence negligible coupling. This will convert **M** into diagonal matrix instead of full matrix thereby reducing the number of (real) unknowns from $2m^2$ to $2m$. Rewriting the inequality expression18 as

$$2mn \geq 2m + 2m \quad (19)$$

Assumption 4 : Sensor antennas are in single array

Reason : Reduces the number of unknowns for system of equations

Note this is different from phase array antennas where all the antennas feed to a single receiver; here we have antenna patches on a single board and each patch is connected to a different receiver. This simplifies the problem statement by reducing the number of unknowns from 2 coordinate values to single distance between antenna patches reducing the **ψ** unknown contribution from $2m$ to m . Rewriting the inequality expression19 as

$$2mn \geq m + m \Rightarrow n \geq 1 \quad (20)$$

This gives us the ability to perform calibration using just 1 source! But do notice that we had implicitly assumed that the direction of arrival θ is known, and hence must be clearly listed as an assumption.

Assumption 5 : Direction of Arrival is known

Reason : Reduces the number of unknowns for system of equations

The derivations so far has assumed a single signal from source to sensor, but unfortunately we cannot assume a pure LoS signal from source to the sensor under most environment conditions, and especially not true in indoor environment that has high likelihood of reflective surfaces for carrier frequency we are operating at.

Assumption 6 : Only LoS signal from source to sensor.

Reason : Derivation described earlier doesn't consider multipath case

Like any wireless signal reception, timing synchronization is very critical to know the delay between the transmit and receive signal for our calibration data.

Assumption 7 : Timing information can be accurately determine

Reason : Receiving multiple samples for a fix setup requires accurate timing synchronization

B Far field approximation

Far field sources results in planar wavefronts making it easier to compute the distance from the source in relation to other sensors. The minimum distance between the source and sensors to approximate the wavefront to be planar instead of spherical can be obtained using Rayleigh distance formula,

$$d_R = \frac{2L_a^2}{\lambda} \quad (21)$$

d_R : Separation between the source and sensor

L_a : Largest separation between the sensors

λ : wavelength of transmitted signal

C Fresnel Zone Clearance

Fresnel zones are regions within which if we have a reflecting surface or an obstruction, it will impact the quality of LoS signal. There are two properties that we should be aware of

1. Reflecting surface : If we have a reflecting surface within the first fresnel zone, the multipath reflected off the surface might distractively combine with LoS signal
2. Obstruction near LoS : Obstruction of free path around LoS reduces the strength of the LoS signal (**HOW TO EXPLAIN THIS USING TEXT REFERENCES**) due to Huygens–Fresnel principle of propagating waves.

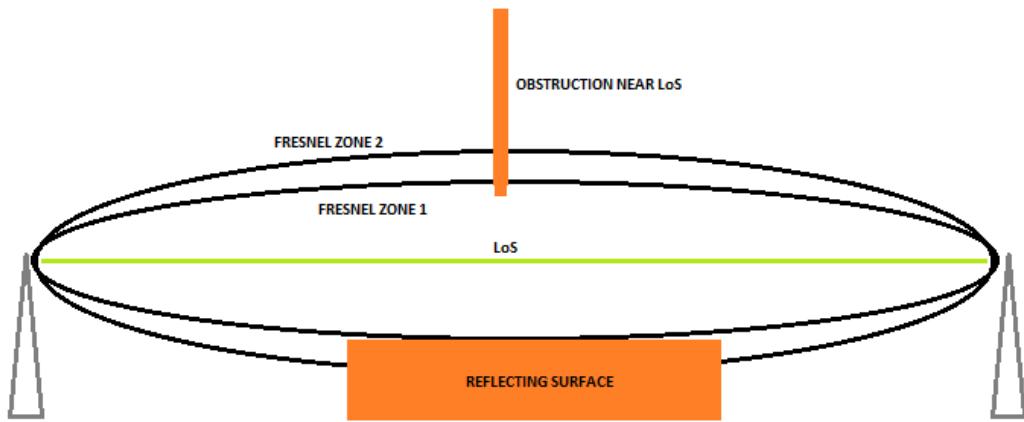


Figure 18: Fresnel Zone

Radius of the first Fresnel Zone is given by

$$F_1 = 8.656 \sqrt{\frac{d_R \times 10^6}{f_c}} \quad (22)$$

d_R : Separation between the source and sensor

f_c : Source signal center frequency

D Constant amplitude continuous wave calibration signal source

We will use Zadoff Chu sequence to generate the desired source signal that meets the requirement of constant amplitude continuous wave signal [4] and has desirable properties. The sequence needed to generate the calibration signal is described by below equation

$$s_q[n] = e^{-j\pi q \frac{n(n+1)}{\mathcal{N}_{zc}}} \quad (23)$$

\mathcal{N}_{zc} : Length of the sequence (odd number)

q : Root index whose value $\in (1, 2, \dots, \mathcal{N}_{zc} - 1)$

$n = (0, 1, 2, \dots, \mathcal{N}_{zc})$: sequence index

The desirable property of zero cyclic autocorrelation makes it very useful in time synchronization, or to time the exact start of the sequence in the received signal.

E Signalling Mode

As we are working with UWB signal, we will use OFDM scheme to transmit multiple narrow band signals but aggregate them to form a 400Mhz wide band signal. The Figure 19 20 below gives a summary of the transmitter and receiver processes, except the constellation mapping is replaced with zadoff chu sequence at transmitter, with match filter in the receiver. This is because we are not sending data but pure reference signal for proper synchronization and channel estimation. You can also refer to [5], [6] for better understanding.

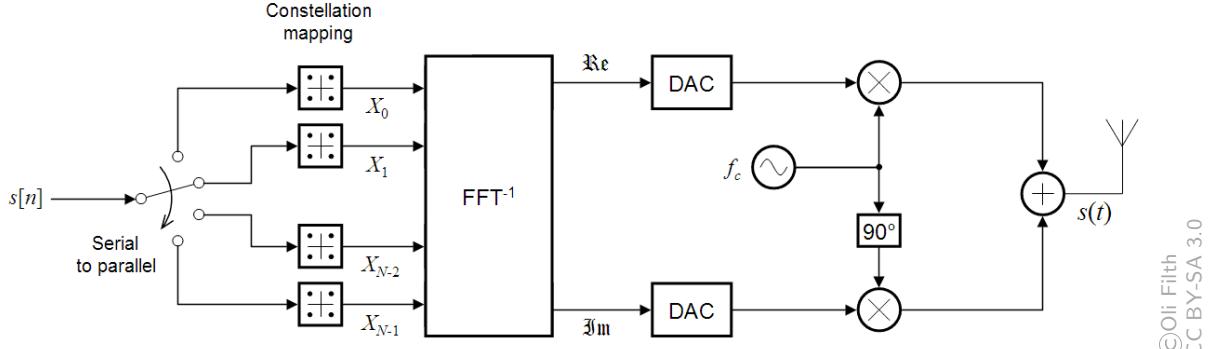


Figure 19: OFDM Transmitter

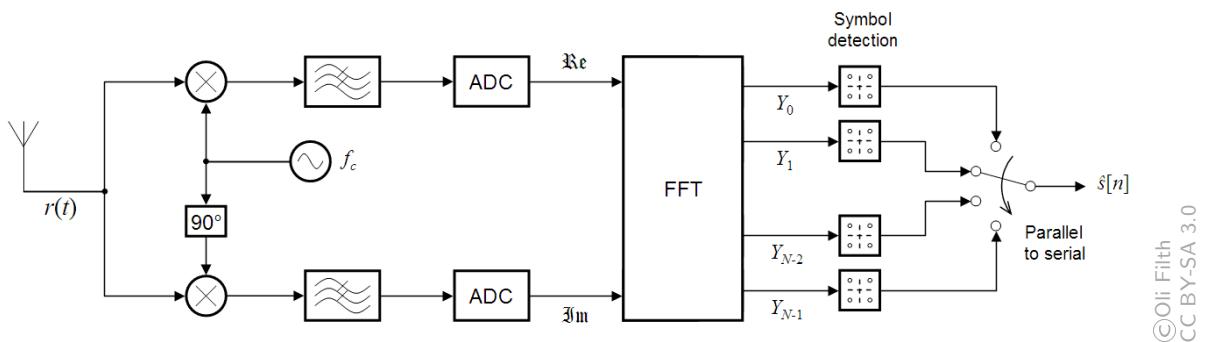


Figure 20: OFDM Receiver

Since we are dealing with multiple subcarriers to implement a UWB signal, we need to determine how many subcarriers should we select. Keep in mind that we need to send a known reference or calibration signal, and since we are going to use Zadoff Chu sequences to generate the desired source signal, we need to follow the requirements listed as part of Equation 23. N_{zc} needs to be an odd number but an even number of subcarriers is desired to perform FFT optimally. We have 1024 subcarriers with sequence length of 813 (the rest are padded with zeros)

F KNN Clustering Algorithm for Stable Point Detection

We use a sliding window whose width increases from 1 sec to 13 secs with increment of 2 (selecting only odd secs window size). For each window width we compute the mean and variance of the window samples as we slide from start to the end, moving 1 sec at a time.

If all the windows were considered, it would mean acceptance rate of 100%, but this shouldnt be greater than RatioStableVsMovement. We need a way to penalize/deselect the windows with high jitter. What we have from KNN clustering function is the centroid location, which centroid each data sample belongs to and the sum of points to centroid distances (sumD).

For a given target of sumD (using SumDLimit variable), we can attempt to reject data samples (window sample) whose variance is max, one window at a time and cross check if we go below SumDLimit. The surviving window samples are considered as accepted, but if higher than RatioStableVsMovement percentage, we will need to tighten requirement by lowering down SumDLimit value (we reduce by factor of 10).

Once we are below RatioStableVsMovement, we note down the number of surviving samples. We then repeat this for higher window width ($1 \rightarrow 3 \rightarrow 5 \rightarrow \dots$). While attempting higher window width, if there is any instance where SumDLimit had to be lowered from previous value, we restart from window width 1 and repeat again. This is to ensure equal strictness (SumDLimit value) to all window sizes.

We then note the number of surviving window samples for each window width. The number of surviving window samples will follow a concave shape, meaning there is one window size that will give us max value. We store the window samples and centroid values for this window size, and we pick the window index that is closest to the centroid. This is basically the best stable point!

We repeat the above steps for each channel, take the average of index value across all channels and round it to the nearest integer. This gives us the best stable point across all channels.

G Expectation-Maximization Method

The Expectation-Maximization (EM) method[7],[8],[9] is one of the early iterative methods that works by iteratively maximizing the conditional log-likelihood of a single Unobservable Complete ¹ data space rather than maximizing the intractable likelihood function for the measured data. EM method in simplest form can be described as iteration between E-step and M-step described below

1. Expectation step (E step):

$$Q(\boldsymbol{\theta}|\boldsymbol{\theta}^{(t)}) = \mathbb{E}_{\mathbf{X}|\mathbf{Y},\boldsymbol{\theta}}[\log L(\boldsymbol{\theta}; \mathbf{Y}, \mathbf{X})] = \sum_{\mathbf{X}} P(\mathbf{X}|\mathbf{Y}, \boldsymbol{\theta}^{(t)}) \log(P(\mathbf{Y}, \mathbf{X}|\boldsymbol{\theta}))$$

2. Maximization step (M step):

$$\boldsymbol{\theta}^{(t+1)} = \max_{\boldsymbol{\theta}} Q(\boldsymbol{\theta}|\boldsymbol{\theta}^{(t)})$$

Y : Observed incomplete data (sometimes referred to output)

X : Unobserved complete data

θ : Unknown parameters

t : iteration count

The EM method suffers from a drawback of slow convergence. The optimization step above needs to be performed on entire observed data space **Y** and across all parameters **θ** simultaneously.

The Space-Alternating Generalized Expectation-Maximization (SAGE) Algorithm [10] [11] solves the drawback via updating the parameters sequentially by alternating between several hidden spaces.

¹ “Unobserved Complete” implies (“Unobserved”) not all variables that describes the model are observable (or measurable) and (“Complete”) for those variables that are observable, we have complete information.

H Space-Alternating Generalized Expectation-Maximization Algorithm

The below steps are directly picked up from [10] with slight change in notations to compare with EM method.

For $t = (0, 1, \dots)$, iterate through the below steps...

1. Choose an index set $\mathbf{S} = \mathbf{S}^t$
2. Choose an admissible hidden-data space $X^{\mathbf{S}^t}$ for $\theta_{\mathbf{S}^t}$
3. E-step : Compute $Q(\theta_{\mathbf{S}^t}; \theta^t)$ using step 4
4. M-step :

$$\theta_{\mathbf{S}^t}^{t+1} = \max_{\theta_{\mathbf{S}^t}} Q(\theta_{\mathbf{S}^t}; \theta^t) \quad (24)$$

$$\theta_{\tilde{\mathbf{S}}^t}^{t+1} = \theta_{\tilde{\mathbf{S}}^t}^t \quad (25)$$

To represent subspace, we need to introduce indexing, or assign one index to each parameter
 $\Phi(\cdot)$: Original function to maximize

$\theta = [\theta_1, \theta_2, \dots, \theta_p]'$: Unknown parameters (same as EM but enumerating for index set)

\mathbf{S} : Index set which is a subset of θ , represents selected parameters for optimization

$\tilde{\mathbf{S}}$: Index set which is a subset of θ , represents parameters not selected for optimization (value is fixed)

$\theta = [\theta_{\mathbf{S}}, \theta_{\tilde{\mathbf{S}}}]'$

$\mathbf{X}^{\mathbf{S}}$: Random vector considering the available parameter $\theta_{\mathbf{S}}$ **CHECK DEFINITION**

Identifying the admissible hidden-data space is important for SAGE algorithm to work.

Lets consider a probability density function $f(y, x; \theta)^1$

$$\begin{aligned} f(y, x; \theta) &= f(y|x; \theta)f(x; \theta) && \dots \text{Product rule} \\ &= f(y|x; \theta_{\mathbf{S}}, \theta_{\tilde{\mathbf{S}}})f(x; \theta) && \dots \text{Separating sets} \\ &= f(y|x; \theta_{\tilde{\mathbf{S}}})f(x; \theta) && \dots \text{True only if } ^2 f(y|x; \theta_{\tilde{\mathbf{S}}}) \perp\!\!\!\perp \theta_{\mathbf{S}} \end{aligned}$$

Definition for “Admissible hidden-data space” : A random vector $\mathbf{X}^{\mathbf{S}}$ with probability density function $f(x, \theta)$ is an admissible hidden-data space with respect to $\theta_{\mathbf{S}}$ for $f(y; \theta)$ if the joint density of $\mathbf{X}^{\mathbf{S}}$ and \mathbf{Y} satisfies

$$f(y, x; \theta) = f(y|x; \theta_{\tilde{\mathbf{S}}})f(x; \theta) \quad (26)$$

In other words, $\mathbf{X}^{\mathbf{S}}$ must be a complete-data space for $\theta_{\mathbf{S}}$ given that $\theta_{\tilde{\mathbf{S}}}$ is known.

¹Semicolon Notation : $f(\mathbf{a}; \mathbf{b})$: A function f that depends on variables \mathbf{a} and parameters \mathbf{b} . Parameter is similar to variable but stays fixed when we use the function.

² $\perp\!\!\!\perp$: Independent of

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