Autonomous and Mobile Robotics

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Humanoid Robots 3: Balance

DIPARTIMENTO DI INGEGNERIA INFORMATICA AUTOMATICA E GESTIONALE ANTONIO RUBERTI



recap

- sufficient condition for balance: ZMP inside the support polygon
- ZMP dynamics modeled from Newton-Euler equations
- approximate model: Linear Inverted Pendulum (LIP)

$$oldsymbol{\ddot{c}^{x,y}} = rac{g^z}{c^z} \left(oldsymbol{c}^{x,y} - oldsymbol{z}^{x,y}
ight)$$

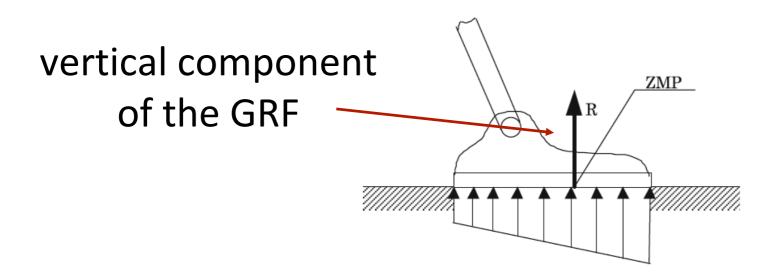
Linear Inverted Pendulum: basic scope

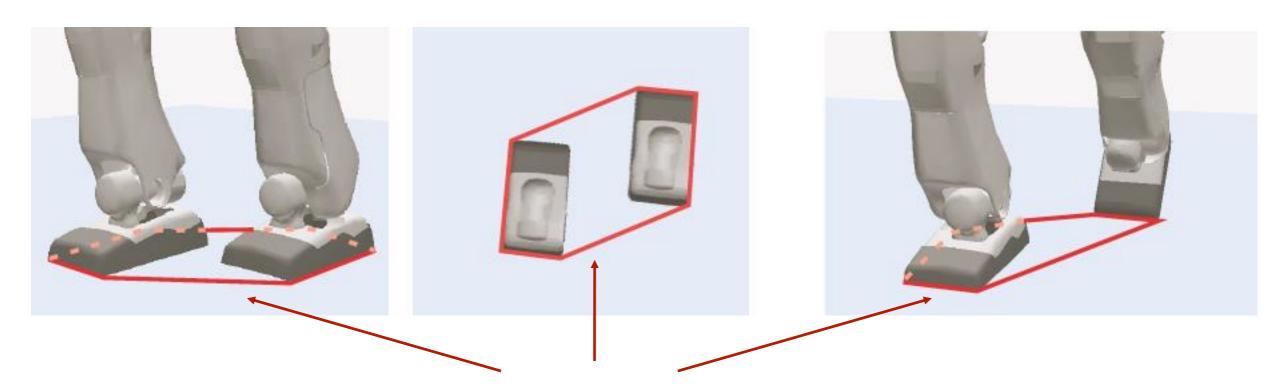
$$oldsymbol{\ddot{c}^{x,y}} = rac{g^z}{c^z} \left(oldsymbol{c}^{x,y} - oldsymbol{z}^{x,y}
ight)$$

Although extremely simplified, the LIP equation describes in first approximation the time evolution of the CoM trajectory. Moreover

- it defines a differential relationship between the CoM trajectory and the ZMP (or CMP) time evolution
- it is easier to design a controller which makes the actual CoM follow a desired behaviour
- dynamic balancing will be characterized in terms of the ZMP
- the problem will then be to understand which CoM trajectory, solution of the LIP equation, guarantees that dynamic balancing is achieved

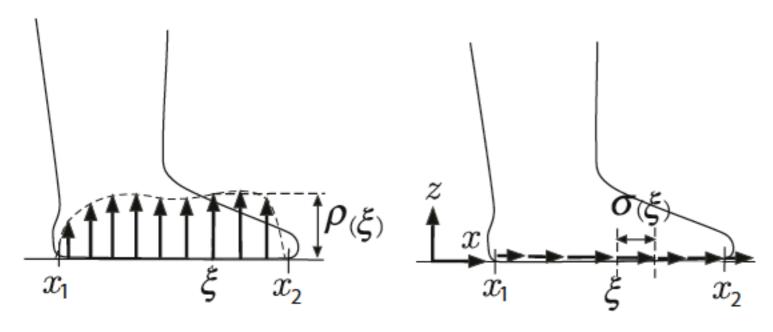
ZMP

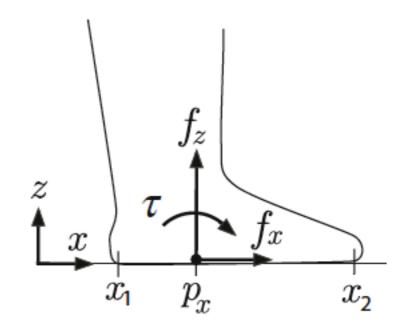




Support Polygons during Double Support

ZMP - 2D case





(a) Vertical force

(b) Horizontal force

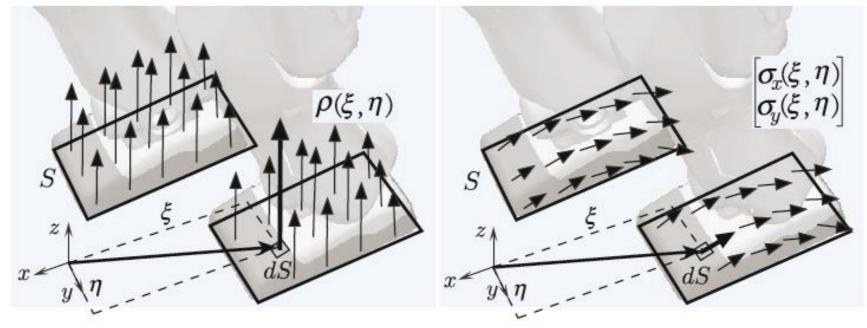
components of the GRF

$$f_x=\int_{x_1}^{x_2}\sigma(\xi)d\xi$$
 equivalent force/torque $f_z=\int_{x_1}^{x_2}
ho(\xi)d\xi$ $au(p_x)=-\int_{x_1}^{x_2}(\xi-p_x)
ho(\xi)d\xi$ $au(p_x)=0$ generic p_x specific p_x

CoP/ZMP

$$p_x = \frac{\int_{x_1}^{x_2} \xi \rho(\xi) d\xi}{\int_{x_1}^{x_2} \rho(\xi) d\xi}$$

ZMP - 3D case



(a) Vertical reaction forces

(b) Horizontal reaction forces

vertical component of the GRF

$$f_{z} = \int_{S} \rho(\xi, \eta) dS$$

$$\tau_{n}(\mathbf{p}) \equiv [\tau_{nx} \ \tau_{ny} \ \tau_{nz}]^{T}$$

$$\tau_{nx} = \int_{S} (\eta - p_{y}) \rho(\xi, \eta) dS$$

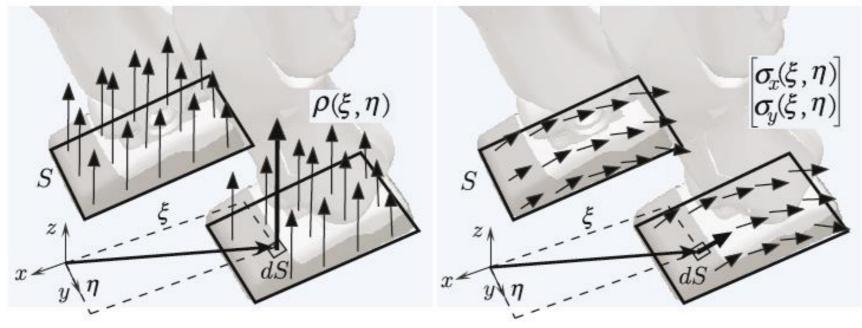
$$\tau_{ny} = -\int_{S} (\xi - p_{x}) \rho(\xi, \eta) dS$$

$$\tau_{ny} = 0$$

$$\tau_{nz} = 0.$$

$$r_{nz} = 0$$

ZMP - 3D case



(a) Vertical reaction forces

(b) Horizontal reaction forces

horizontal component of the GRF

$$f_x = \int_S \sigma_x(\xi, \eta) dS$$

$$f_y = \int_S \sigma_y(\xi, \eta) dS.$$

$$\boldsymbol{\tau}_t(\boldsymbol{p}) \equiv [\tau_{tx} \ \tau_{ty} \ \tau_{tz}]^T$$

$$\tau_{tx} = 0$$

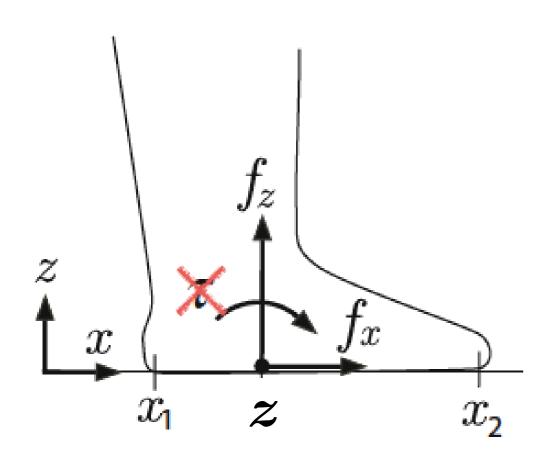
$$\tau_{ty} = 0$$

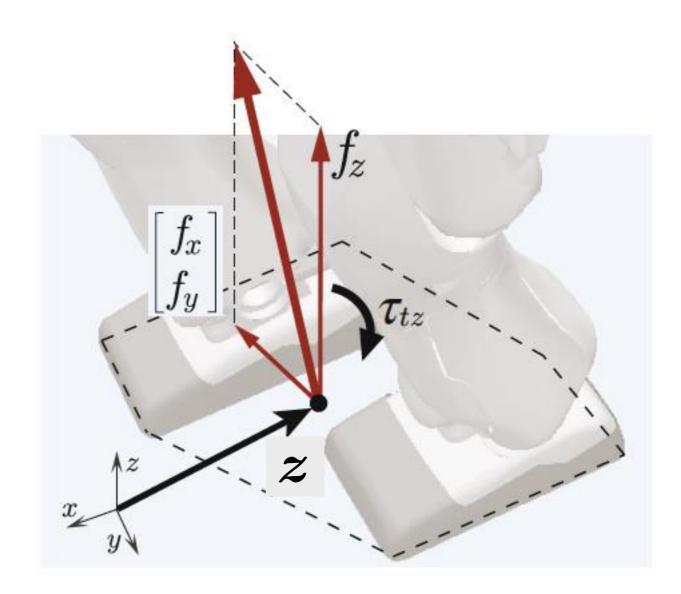
$$\tau_{tz} = \int_S \{(\xi - p_x)\sigma_y(\xi, \eta) - (\eta - p_y)\sigma_x(\xi, \eta)\} dS$$

$$\boldsymbol{\tau}_{p} = \boldsymbol{\tau}_{n}(\boldsymbol{p}) + \boldsymbol{\tau}_{t}(\boldsymbol{p})$$
$$= [0 \ 0 \ \tau_{tz}]^{T},$$

if robot moves, the z component will be different from 0

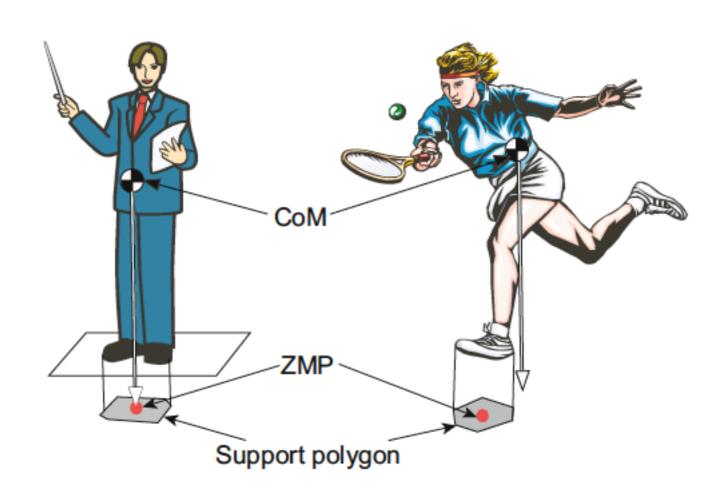
ZMP





as long as the ZMP is in the Support Polygon, the support foot will not rotate

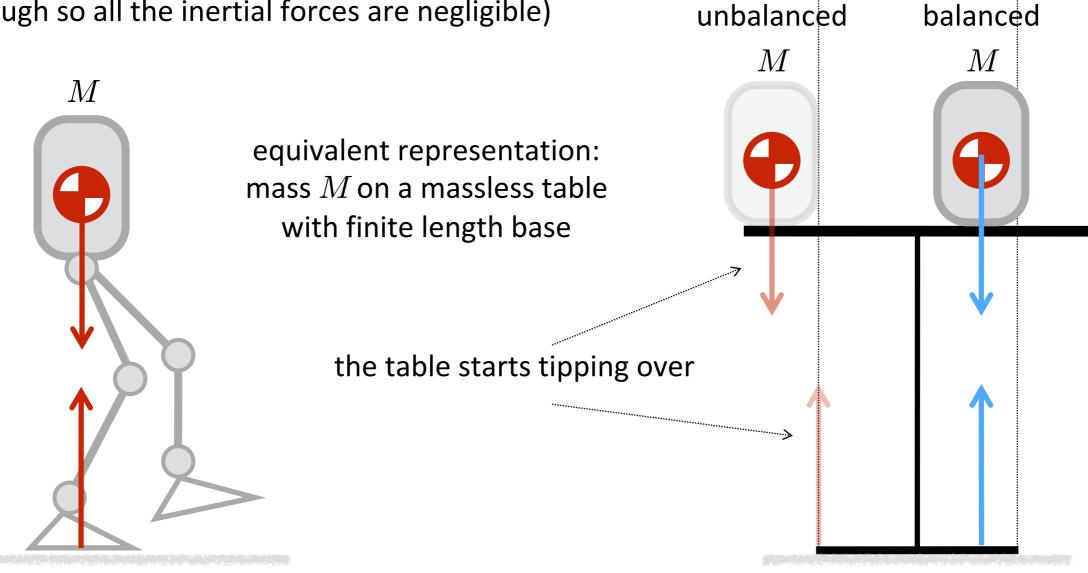
ZMP



static balance

humanoid motionless:

statically balanced robots keep the center of mass within the polygon of support in order to maintain postural stability (sufficient when the robot moves slow enough so all the inertial forces are negligible)



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if the CoM stays within these

boundaries no tipping over occurs

statically

statically

dynamic balance

Question:

how do you keep a pendulum in a non-vertical position?

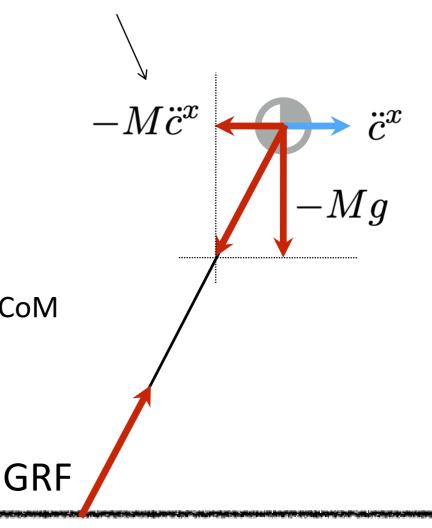
non-inertial frame (pendulum stands still in an accelerating frame)

 \ddot{c}^x acceleration -Mg gravity force \mathbf{Hyp} : no torque around the CoM

Answer:

by continuously accelerating it

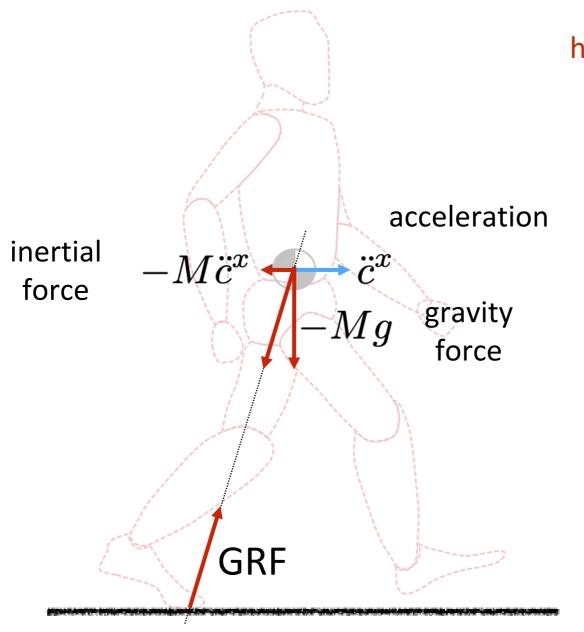
inertial force (fictitious force)



dynamic balance

humanoid walking:

the GRF will also have a component parallel to the ground; the motion requires the exchange of horizontal frictional force with the ground

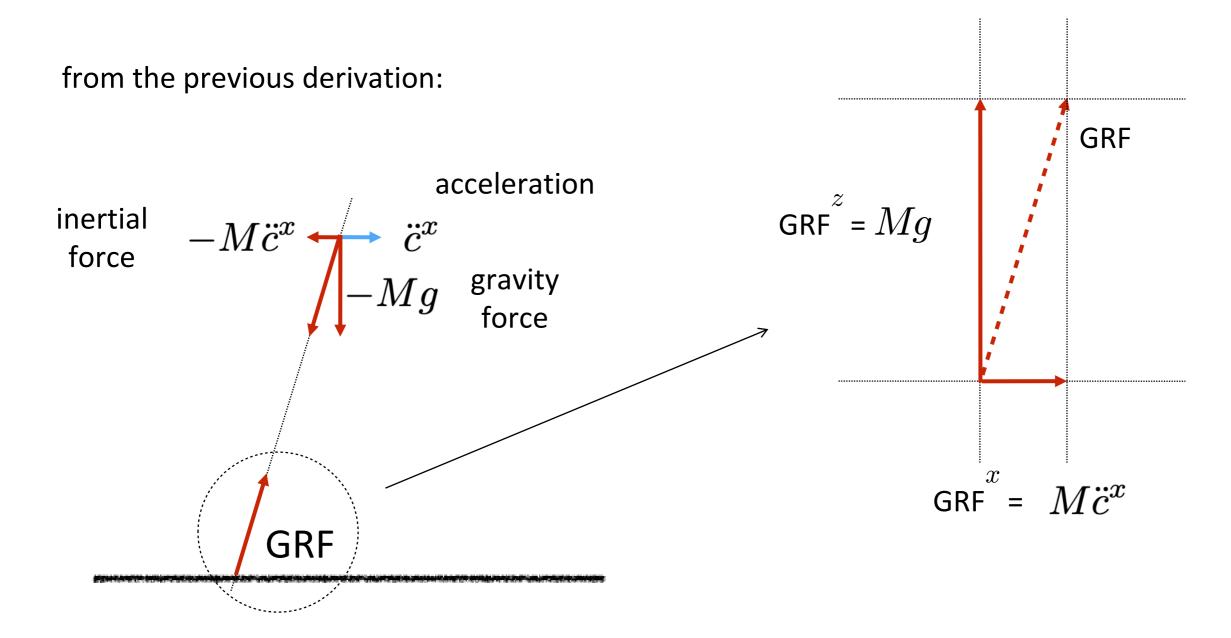


hyp: no torque around the CoM

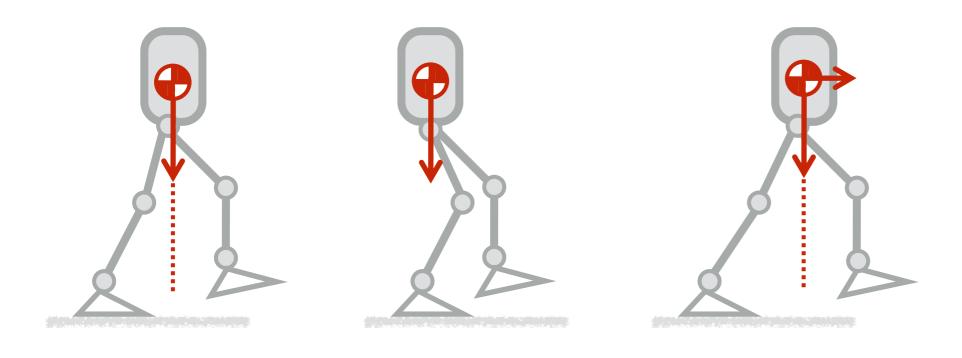
dynamic balance

Ground Reaction Force (GRF): 2D components (x,z)

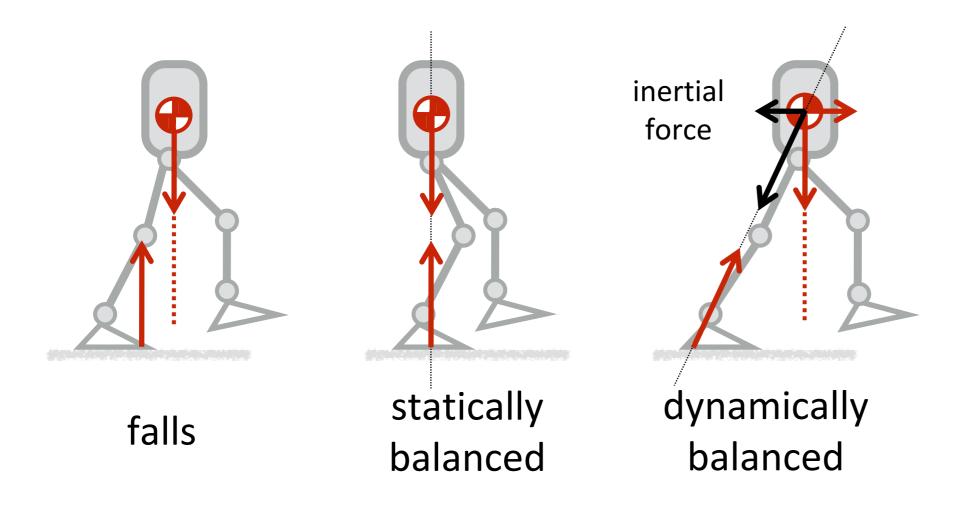
hyp: no torque around the CoM



which robot falls down?



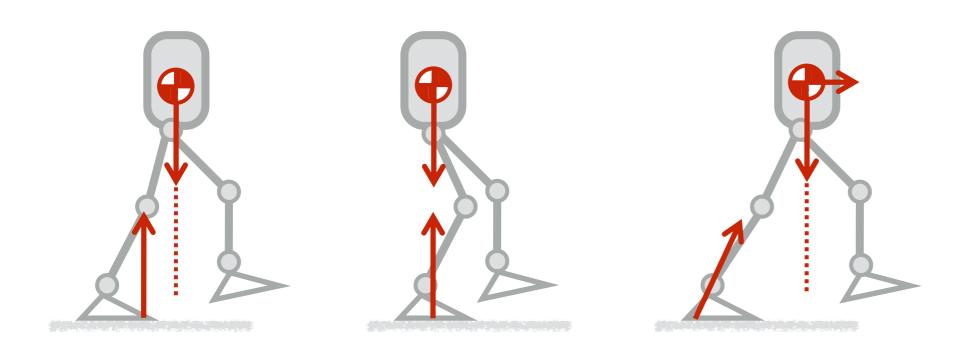
which robot falls down?



where is the ZMP?

 z^x (ZMP): point on the ground where the GRF is applied

use the dynamics equation on horizontal flat ground and neglect $m{\dot{L}}^{x,y}$



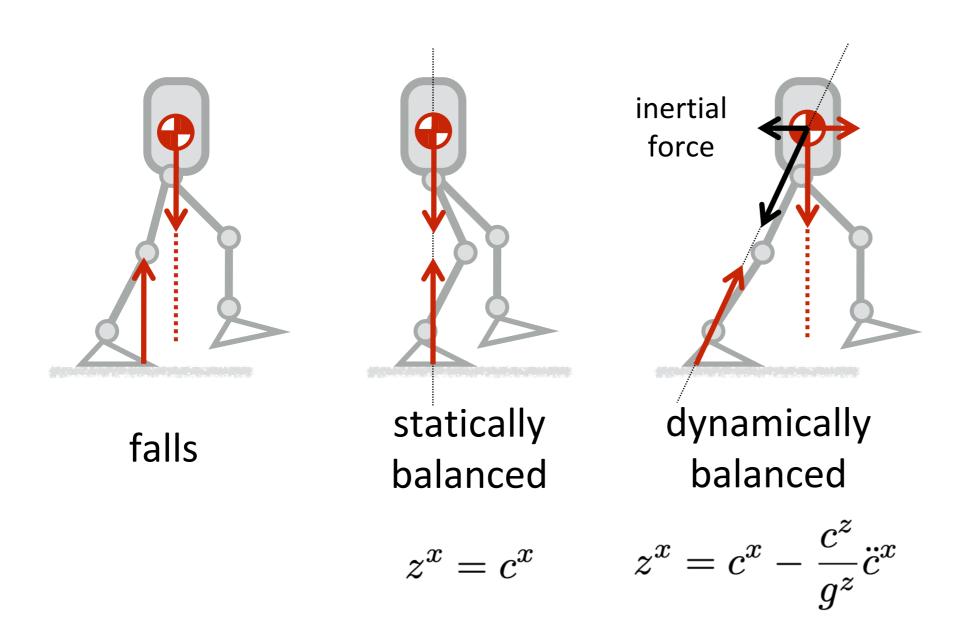
$$\frac{c^z}{\ddot{c}^z + g^z} (\ddot{\boldsymbol{c}}^{x,y} + \boldsymbol{g}^{x,y}) = (\boldsymbol{c}^{x,y} - \boldsymbol{z}^{x,y}) + \frac{\boldsymbol{S}\dot{\boldsymbol{L}}^{x,y}}{M(\ddot{c}^z + g^z)}$$

where is the ZMP?

hyp CoM at constant height $c^z = \text{constant}$

$$c^z = \text{constant}$$

LIP equation in the sagittal plane



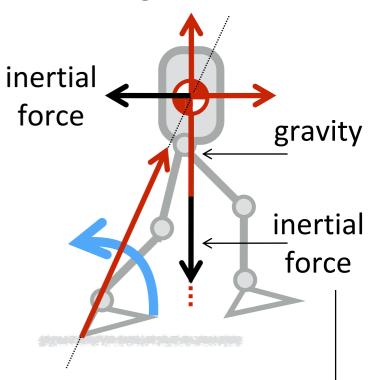
what if CoM acceleration is increased?

from the previous analysis one could think that the ZMP, increasing the CoM acceleration, would leave the support foot support, but it doesn't

- once the ZMP has reached the foot border, a rotation starts around that point
- with the rotation of the foot, the center of mass starts accelerating vertically
- with a vertical acceleration of the CoM, its height does not remain constant
- model changes, ZMP remains constant

$$z^x = c^x - \frac{c^z}{\ddot{c}^z + q^z} \ddot{c}^x$$

vertical acceleration is generated



the vertical CoM acceleration generates a vertical inertial force

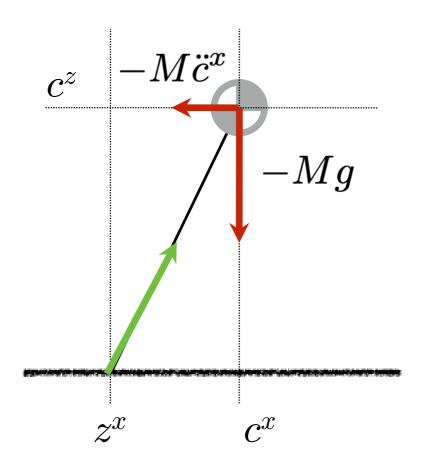
dynamically balanced

Hyp: no torque around the CoM

sum of moments around z^x

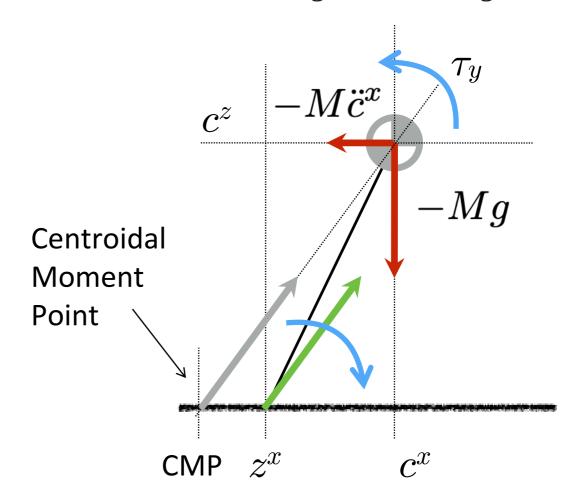
$$-Mg(c^x - z^x) + M\ddot{c}^x c^z = 0$$

$$\longrightarrow z^x = c^x - \frac{c^z}{g^z} \ddot{c}^x$$



+ torque au_y around the CoM

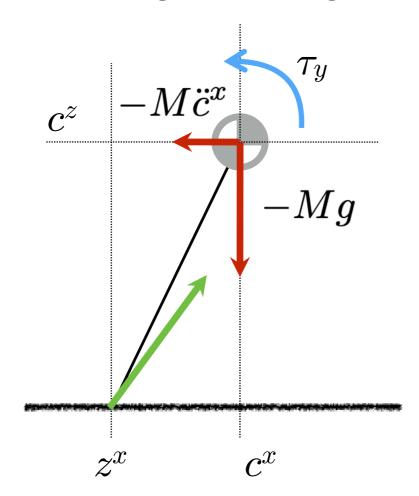
$$-Mg(c^x - z^x) + M\ddot{c}^x c^z + \tau_y = 0$$



dynamically balanced

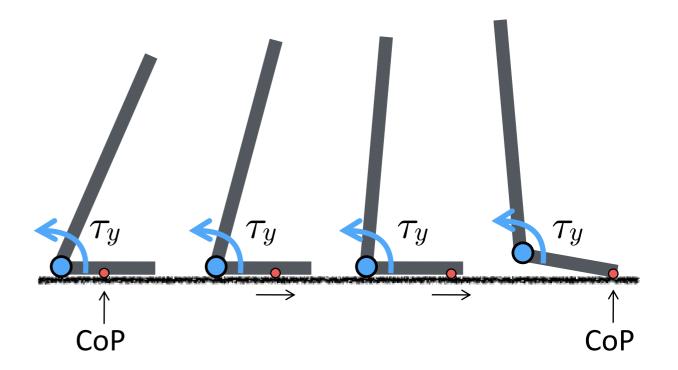
+ torque τ_y around the CoM (or equivalently an ankle torque τ_y)

$$-Mg(c^x - z^x) + M\ddot{c}^x c^z + \tau_y = 0$$



positive torque au_y (counter-clockwise) moves the Center of Pressure CoP to the right z^x is not the CoP anymore

CoP
$$=z^x+rac{ au_y}{Mg}$$



dynamically balanced locomotion

generate a gait for walking while maintaining balance

maintaining balance

assumed to be equivalent to

not tipping over the support foot

ZMP needs to stay <u>inside</u> the Support Polygon



ZMP-based criterion