Computer exercise 3

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1 Part 1

1.1 Question 1a

Plot the realizations of Y^1 and Y^2 and make a phase plot of (Y^1, Y^2) . Repeat for $\sigma = 0.10, 0.20, 0.30$ and 0.40. Comment on the effect of adding noise to the equations.

Figure 1 shows the realizations of Y^1 and Y^2 for $\sigma = 0$. We see nice and repeated signal for both after $T \gtrsim 6$.

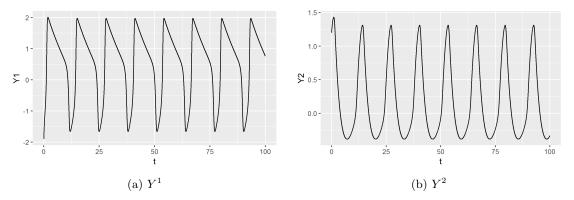


Figure 1: Realized values of Y^1 and Y^2 for $\sigma = 0$

Figure 2 shows the phase plot of (Y^1, Y^2) . Again we see some initial stabilization, but afterward the signal repeats with no variation (as $\sigma = 1$).

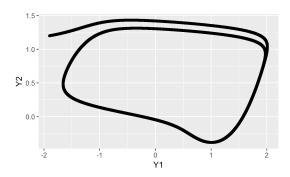


Figure 2: Phase Plot Y^1 and Y^2 for $\sigma = 0$

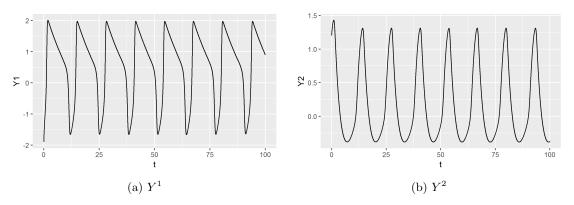


Figure 3: Realized values of Y^1 and Y^2 for $\sigma=0.10$

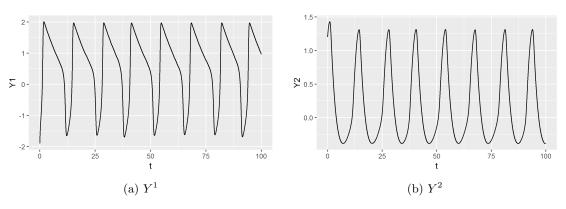


Figure 4: Realized values of Y^1 and Y^2 for $\sigma=0.20$

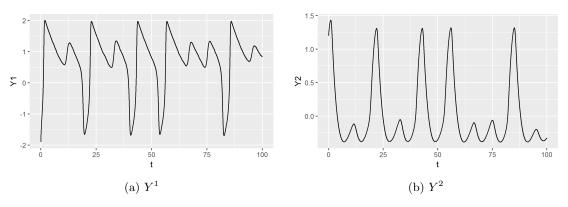


Figure 5: Realized values of Y^1 and Y^2 for $\sigma=0.30$

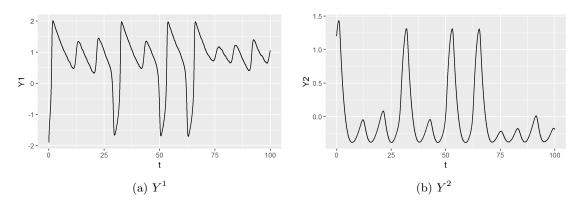


Figure 6: Realized values of Y^1 and Y^2 for $\sigma=0.40$

We repeat for $\sigma = 0.10, 0.20, 0.30$ and 0.40 as shown in Figures 3 to 6, and phase plots shown in Figure 7.

We see that it is still quite stable for $\sigma < 0.20$, but at $\sigma = 0.30$ the system begins to switch between two phases, in a non-obvious way. At $\sigma = 0.40$ the phases become even more chaotic.

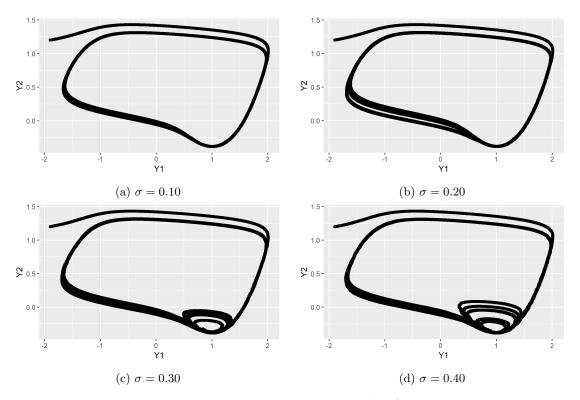


Figure 7: Phaseplots values of (Y^1, Y^2)

1.2 Question 1b

Let $\sigma = 0.10$ and simulate using the approximation. Partition the phase plane in 100×100 equal cells. Count the number of trajectories that passes through each cell. Repeat for $\sigma = 0.20, 0.30$ and 0.40.

Which extra information does the plot contain, compared to the standard phase-plot?

What we have plotted in Figure 8 is count heatmap, and not the number of time a trajectory passes through each cell. We think that the count heatmap is more informative, as it can reveal the speeds of the trajectories at each cell. Higher counts could indicate slower moving passes of the cell.

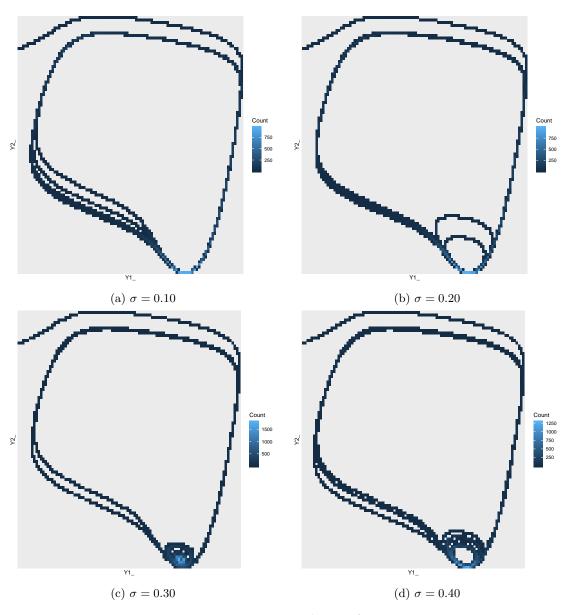


Figure 8: Realized values of Y^1 and Y^2 for $\sigma = 0.20$

2 Part 2

We start our analysis with a exploration and some descriptive statistics of the source data. Figure 9 shows correlations in the input data. We emphasize some insights:

- 1. All four room temperatures, $yT_1, \dots yT_4$, are quite strongly linearly correlated.
- 2. The ambient temperature, T_a seems to cause a lower bound on the room temperatures $yT_1, \dots yT_4$. I.e. when it is hot outside, it will also be hot inside, which makes good sense, as there are no cooling units in the building.
- 3. The solar radiation, G_v , seems to cause a lower bound on the ambient temperature. I.e. when the sun is shining strong, it will be warmer, which also makes good sense. With the above in mind, this also influences the inside temperatures.
- 4. The heaters influence influences the inside temperature, $yT_1, \dots yT_4$, but from this visualization, I argue, that it is not possible to see a difference. I.e. even though the northern circuit heater (Ph_1) is closer to room 1 and 2 (yT_1, yT_2) , the correlation is almost the same as with the southern circuit heater Ph_2 .

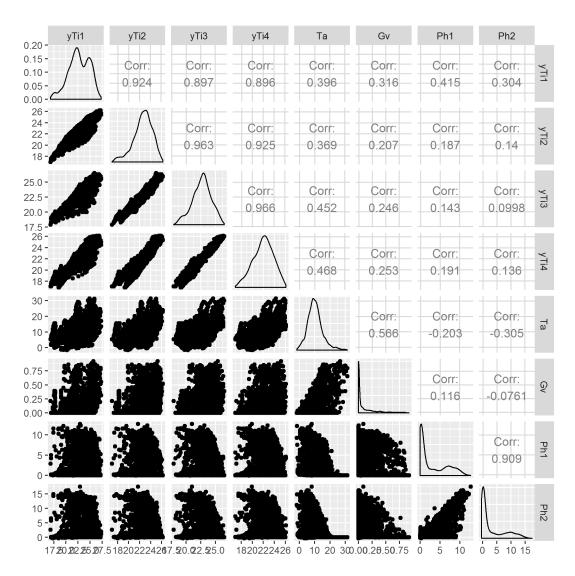


Figure 9: Correlations in input data

2.1 Question 2a

We modified the CTSM-R-model to include the 5 basis spline functions. For the initial guess for the 5 new parameters a_1, \ldots, a_5 we simply use 1 and $[10^{-5}; 10^5]$ for the bounds. Figure 10 shows the difference before and after the modification over the time of day. Table 1 shows the improvement in MSE before and after the modification.

Model	MSE
Before modification	0.0852
After modification	0.0635

Table 1: Mean Squared Error (MSE) before and after modification.

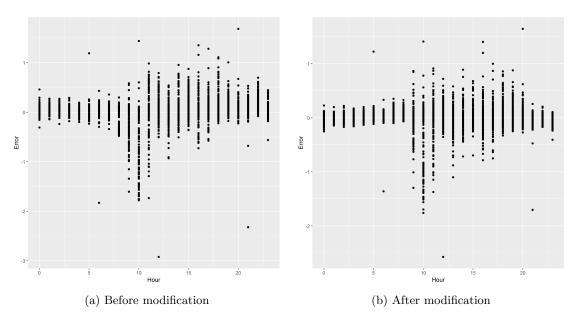


Figure 10: Error over time of day before and after modification.

2.2 Question 2b

In this section, we explore some improvements to the model from 2a. Concrete we will consider the following two improvements:

- 1. Incorporate heat transfer to/from nearby rooms. We think this could improve the model since the rooms share walls which surely can transfer heat.
- 2. Incorporate heat transfer directly between thermal mass and the ambient air. This idea arowse since we are at the second floor, and a lot of the thermal mass of the building could be exposed to the ambient air.

For the first improvement to be considered we have the following SDE-system:

$$dT_i = C_i^{-1} \left(R_{ia}^{-1} (T_a - T_i) + R_{in}^{-1} (T_n - T_i) + R_{im}^{-1} (T_m - T_i) + \Phi + A(t) G_v \right) dt + \sigma_1 dw_1$$
 (1)

$$dT_m = C_m^{-1} \left(R_{im}^{-1} (T_i - T_m) \right) dt + \sigma_2 dw_2$$
 (2)

Where $A(t) = \sum_{k=1}^{N} a_k b s_k(t)$, and R_{in} is the thermal resistance between the current and nearby room, with temperature T_n . We run our expiriment on room i = 1 with the nearby room set to n = 2. After several tries we were unable to estimate parameters, even though we provided good initial guess for the

new parameters (including a_1, \ldots, a_k). Further analysis showed that it is espacially the A(t)-term that causes the computational challange. We therefore chose to replace A(t) with Aw (as in the original model proposed in the exercise) and benchmark our improved model against the model before the modification made in Section 2.1.

The output of the parameter estimation is shown in Figure 11. We see the value of our new parameter $R_{in} = 25$ and is considered significant. This is also visible in the MSE for T_i which is 0.0810 for our improved model compared to the original unmodified model with MAE for $T_i = 0.0852$.

```
Coefficients:
                                                   Pr(>|t|)
                                                                  dF/dPar
                                                                           dPen/dPar
           Estimate
                      Std. Error
                                       t value
Ti10
         2.3603e+01
                      1.8113e-01
                                    1.3031e+02
                                                 0.0000e+00
                                                               4.1622e-02
                                                                               0.0004
TmO
         1.0088e-11
                      1.0187e-10
                                    9.9036e-02
                                                 9.2112e-01
                                                               0.0000e+00
                                                                               0.0000
         1.0621e-02
                      9.4214e-03
                                    1.1274e+00
                                                 2.5967e-01
                                                               1.8185e-02
                                                                              -0.0275
Αw
Сi
         1.5823e+01
                      1.0765e+00
                                    1.4698e+01
                                                 0.0000e+00
                                                               1.2370e+01
                                                                               0.0000
Cm
         1.2422e-01
                      1.5652e-02
                                    7.9365e+00
                                                 2.8866e-15
                                                              -6.4670e-02
                                                                               0.0000
e 1
        -1.2899e+01
                      2.0008e+01
                                   -6.4469e-01
                                                 5.1918e-01
                                                              -3.2200e-02
                                                                               0.0000
Ria
         3.9138e+01
                      2.3833e+00
                                    1.6422e+01
                                                 0.0000e+00
                                                               1.3814e+01
                                                                               0.0000
Rim
         4.1409e+01
                      7.9690e-03
                                    5.1962e+03
                                                 0.0000e+00
                                                               1.4823e+00
                                                                               0.0000
Rin
         2.5025e+01
                      6.6420e-03
                                    3.7677e+03
                                                 0.0000e+00
                                                               5.1819e+00
                                                                               0.0000
sigma1
        -1.7608e+00
                      2.4410e-02
                                    7.2135e+01
                                                 0.0000e+00
                                                               4.0577e-02
                                                                               0.0000
        4.8581e+00
                      1.0346e-01
                                    4.6956e+01
                                                 0.0000e + 00
                                                               1.5232e-01
                                                                               0.0002
sigma2
Correlation of coefficients:
        Ti10
               TmO
                      Αw
                             Ci
                                    Cm
                                           e 1
                                                 Ria
                                                        Rim
                                                               Rin
                                                                      sigma1
TmO
        -0.01
        -0.02
              -0.05
Αw
Ci
        -0.05
               0.36
                      0.03
Cm
         0.04 - 0.25
                     -0.02
                            -0.75
         0.00
              -0.08
                      0.09
                            -0.07
                                    0.02
e 1
Ria
         0.05
             -0.35
                     -0.05
                            -1.00
                                    0.75
                                           0.00
Rim
        -0.05
               0.36
                     -0.09
                             0.99
                                   -0.76
                                          -0.06
                                                -0.99
Rin
        -0.01
              -0.02
                      0.11
                             0.04
                                   -0.68
                                          0.04
                                                -0.05
                                                        0.04
         0.04
              -0.05
                     -0.02
                            -0.26
                                          -0.11
                                                 0.27
                                                       -0.26
sigma1
                                    0.45
                                                              -0.40
sigma2
       -0.05
               0.34
                      0.03
                             0.92
                                   -0.89
                                         -0.04 -0.92
                                                        0.92
                                                               0.33 -0.42
```

Figure 11: Parameter estimates for Improved Model 1

For the second improvement we further modify the SDE to the following. I.e. we include a new parameter R_{ma} for the heat transfer between the thermal mass and the ambient temperature.

$$dT_i = C_i^{-1} \left(R_{ia}^{-1} (T_a - T_i) + R_{in}^{-1} (T_n - T_i) + R_{im}^{-1} (T_m - T_i) + \Phi + A(t) G_v \right) dt + \sigma_1 dw_1$$
 (3)

$$dT_m = C_m^{-1} \left(R_{im}^{-1} (T_i - T_m) + R_{ma}^{-1} (T_a - T_m) \right) dt + \sigma_2 dw_2 \tag{4}$$

Unfortunately this does not improve the model, as the CTSM-algorithm terminales after only 6 iterations with MAE = 0.1305.

2.3 Question 2c

In this section we present a multi-room model that describes the heat dynamics of the 4 rooms that we got measurements from.

In order to simplefy the model we make some assumptions:

- 1. The thermal resistance between the air and thermal mass is the same for all rooms, denoted R_m . This is assumed since all the rooms are on the same floor, and it seem likely that the floor is made of the same material in all the rooms.
- 2. The thermal resistance between the internal air and the outside is the same for room 1 and 4 (R_o) , and room 2 and 3 (R_h) . This is assumed since both room 1 and 2 are offices close to the outside, while room 2 and 3 seem like hallway and is more central in the building.

- 3. The thermal capacity is the same for room 1 and 4 (C_o) , and room 2 and 3 (C_h) . This is assumed since both room 1 and 4 are offices of similar size, while room 2 and 3 seem like hallway and of larger, but similar size.
- 4. We estimate the window area size for each room $(A_{w,1}, \ldots, A_{w,4})$ independently of the time, but allows for different window areas (and directions of the windows) for each window.

$$dT_1 = C_o^{-1} \left(R_o^{-1} (T_a - T_1) + R_m^{-1} (T_m - T_1) + \Phi_1 + A_{w,1} G_v \right) dt + \sigma_1 dw_1 \tag{5}$$

$$dT_2 = C_h^{-1} \left(R_h^{-1} (T_a - T_2) + R_m^{-1} (T_m - T_2) + \Phi_1 + A_{w,2} G_v \right) dt + \sigma_2 dw_2 \tag{6}$$

$$dT_3 = C_h^{-1} \left(R_h^{-1} (T_a - T_3) + R_m^{-1} (T_m - T_3) + \Phi_2 + A_{w,3} G_v \right) dt + \sigma_3 dw_3 \tag{7}$$

$$dT_4 = C_o^{-1} \left(R_o^{-1} (T_a - T_4) + R_m^{-1} (T_m - T_4) + \Phi_2 + A_{w,4} G_v \right) dt + \sigma_4 dw_4$$
(8)

$$dT_m = C_m^{-1} \left(\sum_{i=1}^4 R_m^{-1} (T_i - T_m) \right) dt + \sigma_5 dw_5$$
 (9)

Finally we present one last multi room model that takes into account the inter-room heat transfer we saw significant in the previous section. For this we introduce 3 new parameters to estimate: $R_{n,1,2}$, $R_{n,2,3}$, $R_{n,3,4}$. In this $R_{n,j,k}$ is the thermal resistance between room j and k. The SDE for the system is shown in eq. (10).

$$dT_{1} = C_{o}^{-1}(R_{o}^{-1}(T_{a} - T_{1}) + R_{n,1,2}^{-1}(T_{2} - T_{1}) + R_{m}^{-1}(T_{m} - T_{1}) + \Phi_{1} + A_{w,1}G_{v})dt + \sigma_{1}dw_{1}$$

$$dT_{2} = C_{h}^{-1}(R_{h}^{-1}(T_{a} - T_{2}) + R_{n,1,2}^{-1}(T_{1} - T_{2}) + R_{n,2,3}^{-1}(T_{3} - T_{2}) + R_{m}^{-1}(T_{m} - T_{2}) + \Phi_{1} + A_{w,2}G_{v})dt + \sigma_{2}dw_{2}$$

$$dT_{3} = C_{h}^{-1}(R_{h}^{-1}(T_{a} - T_{3}) + R_{n,2,3}^{-1}(T_{2} - T_{3}) + R_{n,2,3}^{-1}(T_{2} - T_{3}) + R_{n,3,4}^{-1}(T_{4} - T_{3}) + R_{m}^{-1}(T_{m} - T_{3}) + \Phi_{2} + A_{w,3}G_{v})dt + \sigma_{3}dw_{3}$$

$$dT_{4} = C_{o}^{-1}(R_{o}^{-1}(T_{a} - T_{4}) + R_{n,3,4}^{-1}(T_{3} - T_{4}) + R_{n,3,4}^{-1}(T_{m} - T_{4}) + \Phi_{2} + A_{w,4}G_{v})dt + \sigma_{4}dw_{4}$$

$$dT_{m} = C_{m}^{-1}\left(\sum_{i=1}^{4} R_{m}^{-1}(T_{i} - T_{m})\right)dt + \sigma_{5}dw_{5}$$

This model takes quite some time to run on standard commodity hardware, but show slightly better overall performance as shown by the MSE results in Table 2. It is worth noticing that T_1 is actual a little worse, while T_2, \ldots, T_4 is quite better, releatively speaking.

N	Model / MSE	Multi room model 1	Multi room model 2
	T_1	0.0836	0.1021
	T_2	0.0304	0.0241
	T_3	0.0373	0.0173
	T_4	0.0373	0.0234
	Mean	0.0472	0.0417

Table 2: Mean Squared Error (MSE) for the multi room models.

```
Coefficients:
        Estimate Std. Error
                                t value Pr(>|t|)
        2.3584e+01 2.4516e-01
                                  96.1986 < 2.2e-16 ***
T10
        2.2234e+01
                    1.1898e-01
                                 186.8673 < 2.2e-16 ***
T30
        2.2771e+01
                    9.4945e-02
                                 239.8396 < 2.2e-16 ***
        2.2005e+01
                                 252.5609 < 2.2e-16 ***
T40
                    8.7128e-02
        1.8840e-02
                    4.3778e-03
                                  4.3035 1.695e-05 ***
        6.7601e+00
                    1.0759e+00
                                   6.2832 3.442e-10 ***
Aw1
Aw2
        3.8781e+00
                    8.5857e-01
                                   4.5169 6.339e-06 ***
        8.2243e+00
                    7.7850e-01
                                  10.5643 < 2.2e-16 ***
AwЗ
                    7.3707e-01
        8.2784e+00
                                  11.2315 < 2.2e-16 ***
Aw4
Ch
        5.1066e+01
                    9.6463e-01
                                   52.9383 < 2.2e-16 ***
\mathtt{Cm}
        5.1049e-02
                    2.9864e-03
                                   17.0940 < 2.2e-16 ***
       3.7258e+01
                    7.3398e-01
                                   50.7619 < 2.2e-16 ***
Co
е1
       -4.9983e+00
                    1.9962e-03 -2503.8741 < 2.2e-16
       -4.9989e+00
                    6.1805e-04 -8088.2422 < 2.2e-16 ***
e2
e3
       -4.9990e+00
                    9.7036e-04 -5151.6560 < 2.2e-16 ***
       -4.9989e+00
                    6.5796e-04 -7597.6671 < 2.2e-16 ***
е4
        2.8874e+00
                                  64.7433 < 2.2e-16 ***
R.h
                    4.4598e-02
Rm
        1.9949e+02
                    2.9903e+00
                                   66.7127 < 2.2e-16 ***
Rn12
        1.0531e+00
                    4.0271e-02
                                   26.1515 < 2.2e-16 ***
        4.1390e+01
                    2.8227e-01
                                 146.6301 < 2.2e-16 ***
Rn23
Rn34
        8.8741e+00
                    1.0321e-01
                                  85.9849 < 2.2e-16 ***
        2.6021e+00
                    4.8616e-02
                                  53.5234 < 2.2e-16 ***
Ro
sigma1 -1.5331e+00
                    1.5072e-02
                                -101.7157 < 2.2e-16 ***
sigma2 -2.5629e+00
                    2.5395e-02
                                -100.9209 < 2.2e-16 ***
sigma3 -3.2397e+00
                    5.9319e-02
                                  -54.6156 < 2.2e-16 ***
sigma4 - 2.4894e + 00
                    2.5982e-02
                                  -95.8112 < 2.2e-16 ***
       6.7289e+00
                    3.2759e-02
                                  205.4069 < 2.2e-16 ***
sigma5
Signif. codes: 0 '*** 0.001 '** 0.01 '* 0.05 '.' 0.1 ' ' 1
```

Figure 12: Parameter estimates for Multi room model 2

The full parameter estimation for *Multi room model 2* is shown in Figure 12. Again it is visible from the output, that the additional parameters, $R_{n,1,2}$, $R_{n,2,3}$, $R_{n,3,4}$, are significant.