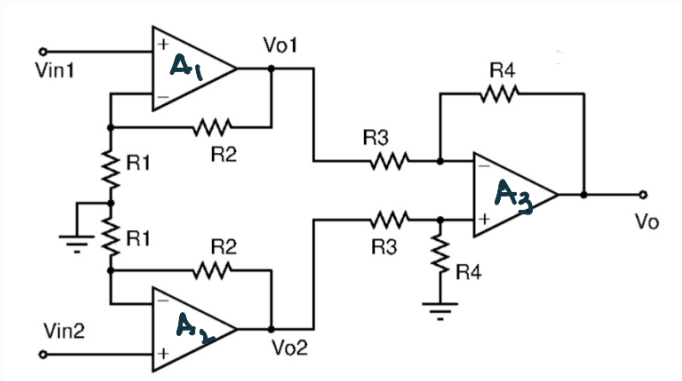


Q1.



$$R_4 = R_2 = 10k\Omega ; R_3 = R_1 = 5k\Omega$$

a.  $A_1, A_2$  are connected in non-inverting configuration

$$\text{So, } V_{o1} = \left(1 + \frac{R_2}{R_1}\right) \cdot V_{in1}$$

$$= \left(1 + \frac{R_2}{R_1}\right) \cdot (V_{cm} - V_{id} \sin(\omega t))$$

$$= \left(1 + \frac{10k}{5k}\right) \cdot (V_{cm} - V_{id} \sin(\omega t))$$

$$= 3 \cdot (V_{cm} - V_{id} \sin(\omega t)) \text{ V} - (0.5 \text{ marks})$$

$$\text{Similarly, } V_{o2} = \left(1 + \frac{10k}{5k}\right) (V_{cm} + V_{id} \sin \omega t)$$

$$= 3 \cdot (V_{cm} + V_{id} \sin(\omega t)) \text{ V} - (0.5 \text{ marks})$$

Now,  $V_{o1}, V_{o2}$  are inputs to a differential Amp. Stage

$$V_o = \frac{R_4}{R_3} (V_{o2} - V_{o1})$$

$$= 3.2 \left[ (V_{cm} + V_{id} \sin(\omega t)) - (V_{cm} - V_{id} \sin(\omega t)) \right]$$

$$= 6.4 [V_{id} \sin(\omega t)]$$

$$= 12 \cdot V_{id} \sin(\omega t) \text{ V}$$

— (0.5 marks)

b. Given  $V_{om} = 1.8\text{V}$ ,  $V_{id} = 0.3\text{V}$

If the Op-Amps were completely ideal & didn't saturate the outputs would be:

using solutions from part a -

$$V_{O1} = 5.4 - 0.9 \sin(\omega t) \text{ V}$$

$$V_{O2} = 5.4 + 0.9 \sin(\omega t) \text{ V}$$

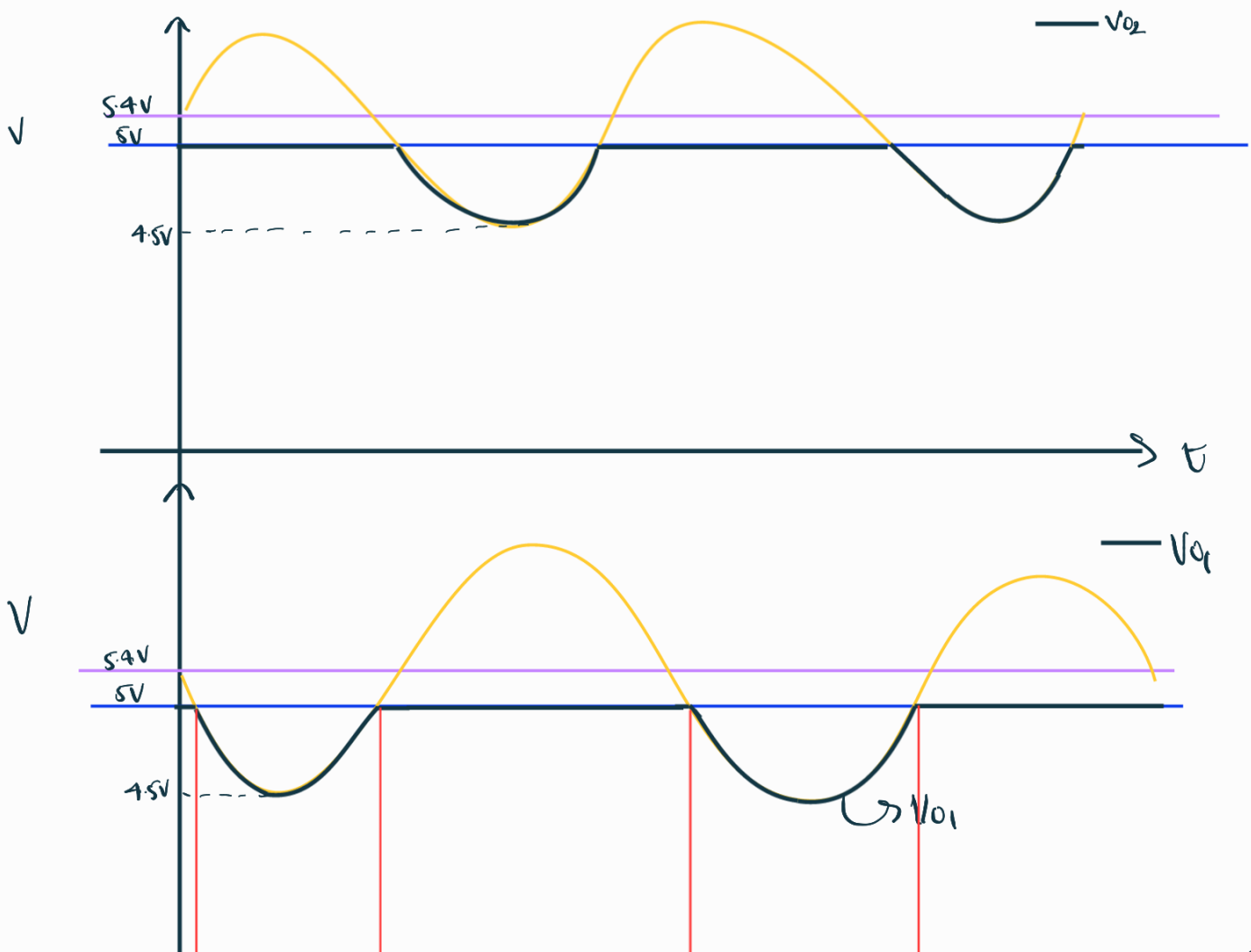
$$V_O = 3.6 \sin(\omega t) \text{ V}$$

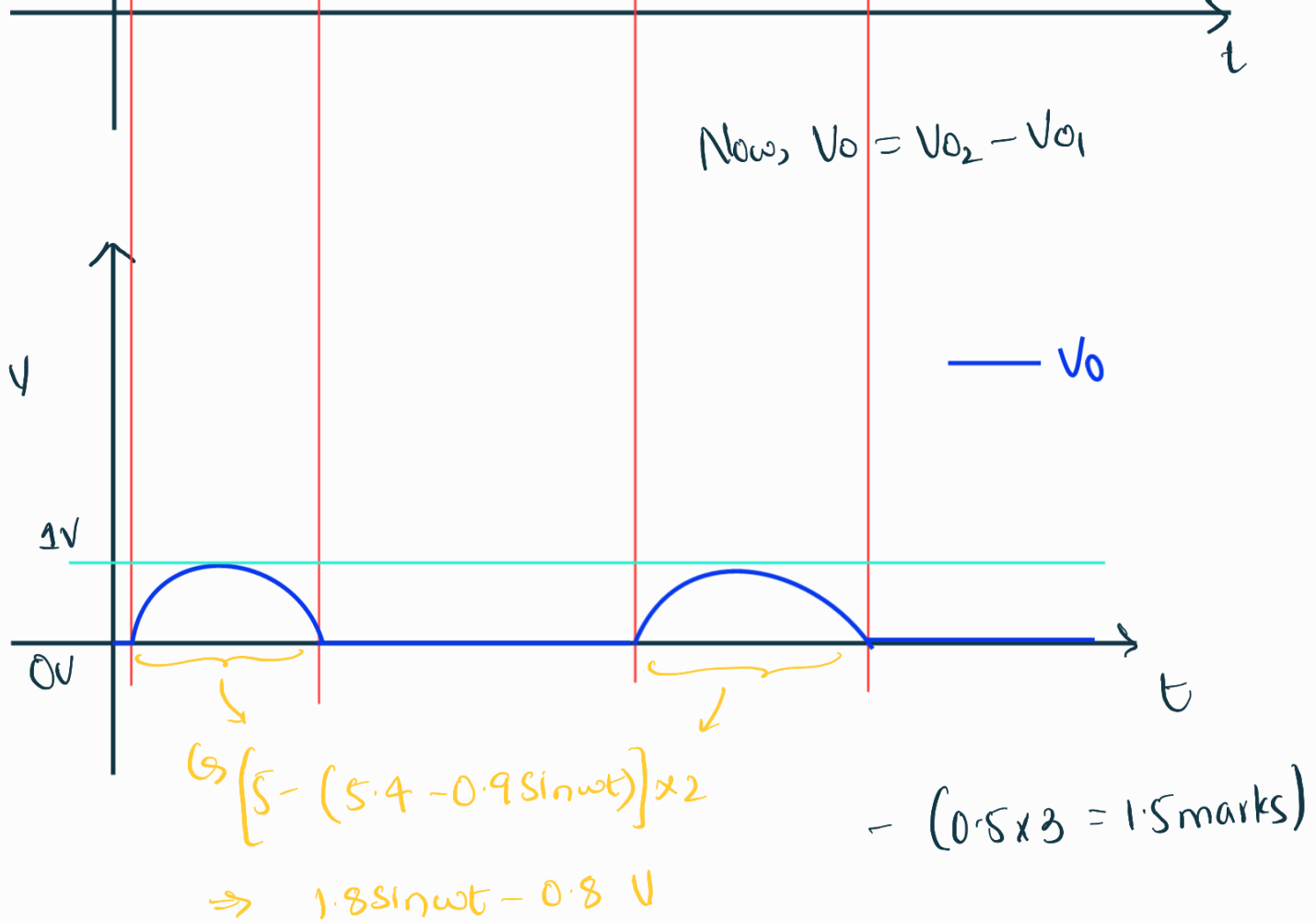
(and  $V_{omin} = 0\text{V}$ )

But, outputs all op-amps saturate at  $5\text{V}$ , (given)

So, the outputs, when drawn would be -

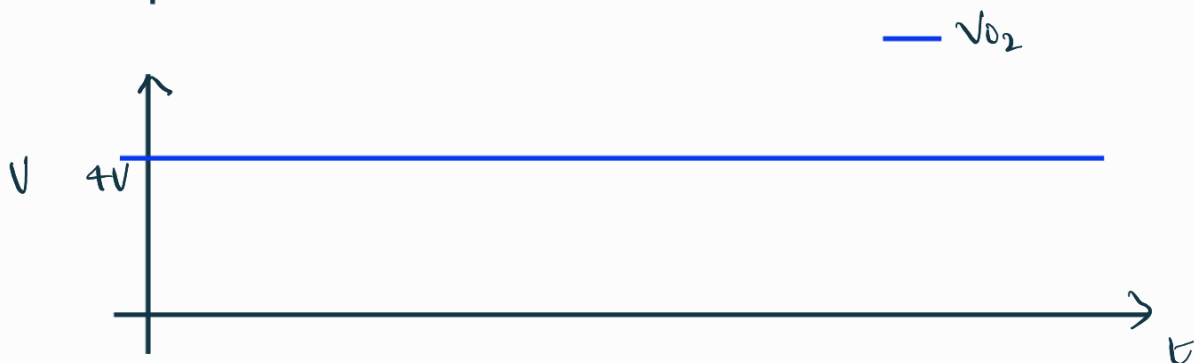
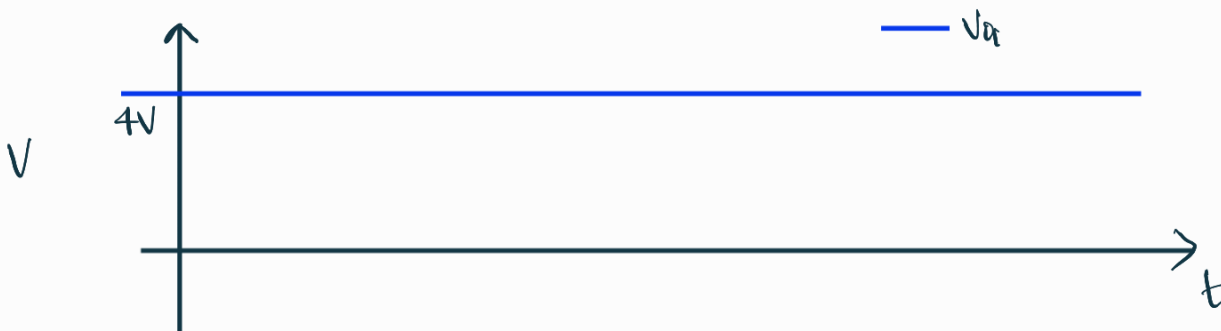
$$0\text{V} \leq V_O \leq 5\text{V}$$

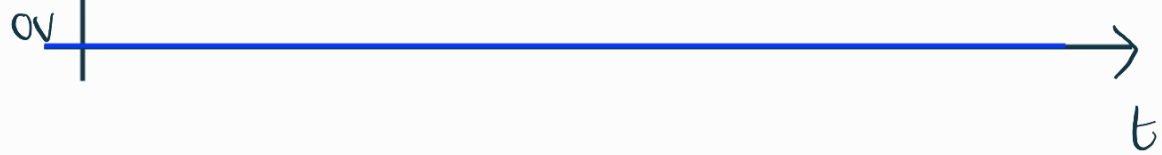




c. It is now given that, the outputs saturate at 4V but from previous parts  $V_{01}, V_{02}$  are always  $> 4V$

Hence,





— (0.5 x 3 = 1.5 marks)

Q2.

$$V_b = 0.8V \quad V_{dd} = 1.8V, \quad W/L = 9/0.36, \quad \mu_n C_{ox} = 260 \mu A/V^2$$

$$V_{TH} = 0.4V$$

Assuming  $M_1$  is in saturation

$$a. \quad I_D = \frac{\mu_n C_{ox} \cdot W}{2 \cdot L} \cdot (V_{GS} - V_{TH})^2$$

$$I_D = \frac{260 \times 10^{-6} \times 9}{2 \cdot 0.36} (0.8 - 0.4)^2$$

$$= 0.52 \text{ mA (or)} \quad 520 \mu A \quad - 0.25 \text{ marks}$$

$$V_o = V_{dd} - I_D \cdot R_D$$

$$= 1.8 - 0.52 \times 0.8 = 1.384 V \quad - 0.25 \text{ marks}$$

To check for saturation:

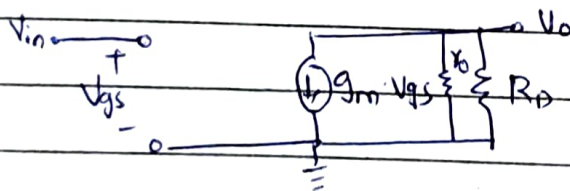
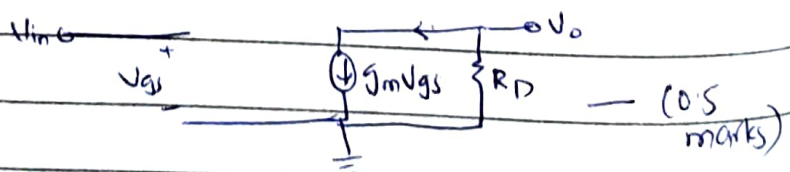
$$b. \quad V_{DS} \geq V_{GS} - V_{TH}$$

$$V_{DS} = 1.384 V, \quad V_{GS} - V_{TH} = 0.8 - 0.4 = 0.4V$$

$$V_{DS} \geq V_{GS} - V_{TH} \text{ is true.}$$

Our assumption is valid &  $M_1$  is indeed in saturation

b.

Small signal model with  $r_o \rightarrow \infty$ 

$$g_m = \frac{\partial I_D}{\partial V_{GS}} = \mu_n C_{ox} \cdot \frac{W}{L} (V_{GS} - V_T) = 2.6 \text{ mSiemens}$$

$$\text{Small Signal gain } A_v = -g_m R_D = -2.08 \quad - (0.5 \text{ marks})$$

(c)  $V_{GS} = V_D = 0.8V$

Say,  $V_{GS1} = 0.8 + 0.1 = 0.81V$

$V_{GS2} = 0.8 - 0.1 = 0.79V$

for  $V_{GS1} \rightarrow I_{D1} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS1} - V_{TH})^2$   
 $= 0.546325mA$

$V_{O1} = V_{DD} - I_{D1} \cdot R_D = 1.36294V$

for  $V_{GS2} \rightarrow I_{D2} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS2} - V_{TH})^2$   
 $= 0.494325mA$

$V_{O2} = V_{DD} - I_{D2} \cdot R_D = 1.40954V$

pk-pk output-input gain =  $\frac{V_{O2} - V_{O1}}{V_{GS2} - V_{GS1}} = -2.08$

Absolute value of gain is 2.08 & the gain is inverting  
- (2 marks)

(or) using small signal analysis

$|\Delta V_O| = g_m \cdot |\Delta I_D| \cdot R_D$   
 $= g_m R_D |\Delta V_{in}|$

$\left| \frac{\Delta V_O}{\Delta V_{in}} \right| = g_m R_D = 2.08 \leftarrow \text{Absolute value of gain}$

Also, as  $V_{in} \uparrow \rightarrow I_D \uparrow$  and  $V_O \downarrow$   
the gain is inverting.

- (2 marks)

(d) for  $R_D = 2 \times 0.8k\Omega = 1.6k\Omega$

$V_d = V_o = V_{DD} - I_D \cdot R_D = 0.968V$

$V_{GS} - V_{TH} = 0.4V$ ,  $V_{DS} \geq V_{GS} - V_{TH}$ , Hence M1  
is still in Sat.



(a) for same  $V_{GS1}, V_{GS2}$  as in the above part

$$I_{D1} = 0.546325 \text{ mA}, I_{D2} = 0.494325 \text{ mA} \text{ (same as above)}$$

$$V_{O1} = V_{DD} - I_{D1} \cdot R_D = 0.92588 \text{ V}$$

$$V_{O2} = V_{DD} - I_{D2} \cdot R_D = 1.00908$$

$$\text{pk-pk Output input gain} = \frac{V_{O2} - V_{O1}}{V_{GS2} - V_{GS1}} = -4.16$$

(08)

using small signal analysis

$$A_v = -g_m \cdot R_D = -g_m \cdot (2 \times 0.8 \text{ k}\Omega)$$

$$= -2.6 \times 2 \times 0.8 = -4.16$$

If it is assumed that ~~no~~ small signal is <sup>not</sup> present: - (1 mark)

for  $M_1$  to be in saturation  $V_{DS} \geq V_{GS} - V_{TH}$  - ①

$$V_{DS} = 1.8 - I_{D1} \cdot R_D \geq 0$$

$$= 1.8 - (0.52 \times 10^{-3}) \cdot R_D \geq 0$$

$$V_{GS} - V_{TH} = 0.4 \text{ V}$$

$$\text{from ①} \quad 1.8 - 0.52 \times 10^{-3} \times R_D \geq 0.4$$

$$0.52 \times 10^{-3} \times R_D \leq 1.4$$

$$R_D \leq \frac{1.4 \times 10^3}{0.52}$$

$$R_D \leq 2.692 \text{ k}\Omega$$

$$\therefore R_{D, \max} = 2.692 \text{ k}\Omega$$

(08)

- (1 mark)

If it is assumed that small signal is still present

$$V_{DS, \min} = V_{O1} = V_{DD} - I_{D1} \cdot R_D = 1.8 - 0.546325 \times 10^{-3} \times R_D$$

$$\text{Now,} \quad 0.546325 \times 10^{-3} \times R_D \leq 1.4$$

$$R_D \leq 2.5625 \text{ k}\Omega$$

$$\therefore R_{D, \max} = 2.5625 \text{ k}\Omega$$