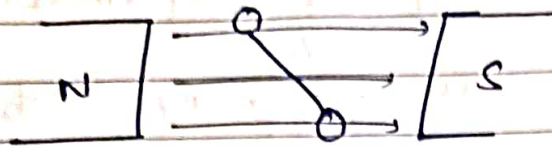


# DC MACHINES



$$E = (2Blv) \cos \theta$$

$$\text{EMF induced} = (\vec{v} \times \vec{B}) \cdot \vec{l}$$

## INTRO TO ROTATING MACHINES

$$e = \frac{d\lambda}{dt}$$

change in flux-linkage ' $\lambda$ ' result from mechanical motion

⇒ EMF is induced

⇒ Rotating Machine → generate voltage by rotating windings mechanically through a M.F. or rotate M.F. through stationary windings.

set of such windings connected together ⇒ Armature winding  
 ↓  
 windings which carry A.C. current

→ Induction or synchronous machines ⇒ armature winding on the stationary part of the circuit.

stator windings ← (STATOR)

→ DC machine → armature is on the rotating part (ROTOR)

→ second winding → carry DC current ⇒ field windings  
 ↓  
 produce main operating flux  
 ↓  
 Permanent magnets can be used instead.

## LORENTZ FORCE LAW

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$

$\downarrow$        $\downarrow$        $\downarrow$   
 $V/m$     $m/s$     $T$

in a pure electric-field system,  $\vec{F} = q\vec{E}$

in a pure magnetic system,  $\vec{F} = q(\vec{v} \times \vec{B})$

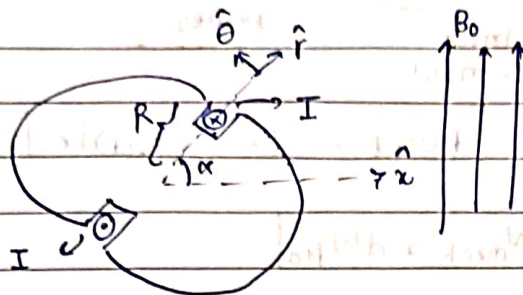
Force density,  $F_v = \rho(\vec{E} + \vec{v} \times \vec{B})$       current density,  $J = \rho v$  ( $A/m^2$ )

$$\vec{F}_V = \vec{J} \times \vec{B}$$

magnetic system force density

$$\vec{J} = \nabla \times \vec{A} \quad \vec{F}_V = \nabla (\vec{E} \cdot \vec{V} \times \vec{B})$$

e.g. -



Force per unit length on wire =  $\vec{I} \times \vec{B}$

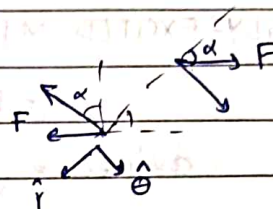
wire - ①  $\vec{F}_0 = -IB_0 l \sin \alpha \hat{\theta}$

wire - ②  $\vec{F}_0 = -IB_0 l \sin \alpha \hat{\theta}$

so,

$$F_{\theta\text{-dirn}} = -2IB_0 l \sin \alpha$$

so,  $T_{\text{net}} = (-2IB_0 l \sin \alpha)(R) = (-2IRB_0 l \sin \alpha)$



inding

carry

uit.

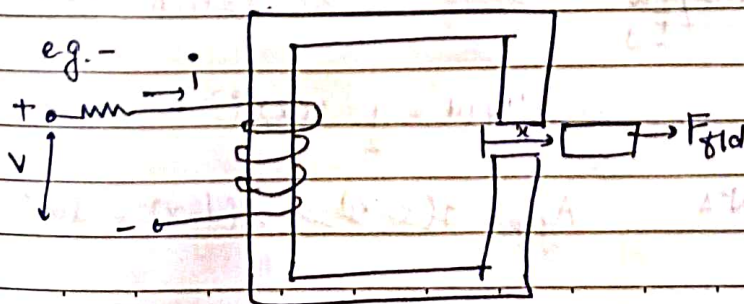
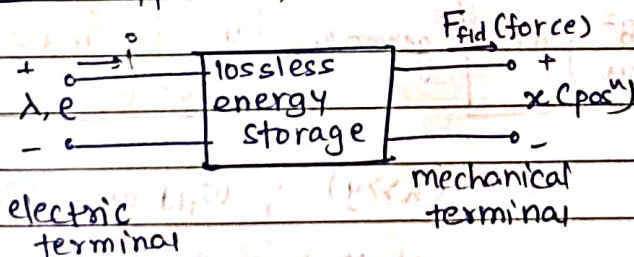
(force per unit length =  $(\vec{J} \times \vec{A}) \times \vec{B} = \vec{T} \times \vec{B}$ )

rotor  $\rightarrow$  M.F. and stator  $\rightarrow$  M.F.

These two sets attempt to align  $\rightarrow$  Torque associated with their displacement from alignment.

$\Rightarrow$  Motor :- stator MF pulls the rotor MF, and performs work.

Generator :- opposite ; rotor does work on the stator.



/m<sup>2</sup>)



Energy Conservation:  $\rightarrow$

$$\frac{dW_{fid}}{dt} = e i - f_{fid} \left( \frac{dx}{dt} \right)$$

rate of change of energy stored in M.F.      electrical power input      mechanical power output

$$e = \frac{d\lambda}{dt}$$

$$dW_{fid} = d\lambda - (f_{fid}) dx$$

$$dW_{elec} = e i dt = dW_{mech} + dW_{fid}$$

SINGLY-EXCITED M.F. systems

$$\lambda = L(x) i$$

$$dW_{mech} = f_{fid} \cdot dx$$

$$dW_{elec} = i d\lambda$$

$$dW_{fid} = i d\lambda - f_{fid} \cdot dx$$

$$\Delta W_{fid} = i(\Delta\lambda) - F_{fid}(\Delta x)$$

(energy stored in the magnetic field)

if  $dx=0$

$$dW_{fid} = i d\lambda$$

$$W_{fid} = \int i \cdot d\lambda = \int \frac{\lambda}{L(x)} d\lambda = \frac{1}{2} \frac{\lambda^2}{L(x)}$$

$$W_{fid} = \frac{1}{2} \frac{\lambda^2}{L(x)}$$

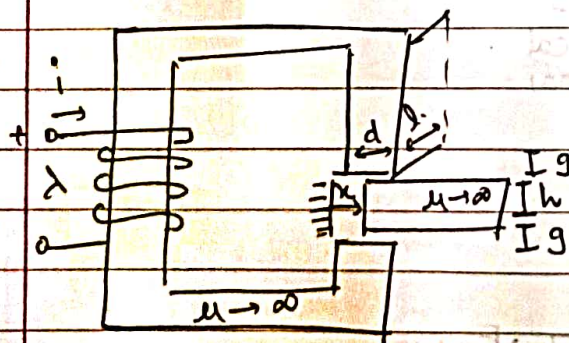
also,

$$W_{fid} = \int_V \left( \frac{B^2}{2\mu} \right) dv$$

generally  $\rightarrow$

$$W = \int_V \left( \int_0^B (\mathbf{H} \cdot d\mathbf{B}') \right) dv$$

eg.-



(h>g) ;  $W_{fid}$  as a f<sup>n</sup>c of x.

$$N=1000$$

$$g=2\text{mm}$$

$$d=0.15\text{m}$$

$$i=10\text{A}$$

$$l=0.1\text{m}$$

$$W_{fid} = \frac{1}{2} L(x) i^2$$

$$L(x) = \frac{\mu_0 N^2 A}{2g}$$

$$A_{gap} = \cancel{d(1-x)} \Rightarrow l(d-x) = ld \left( \frac{1-x}{d} \right)$$



$$L(x) = \frac{\mu_0 N^2 l d (1-x/d)}{2g}$$

$$W_{fid} = \frac{1}{2} \frac{N^2 \mu_0 l d (1-x/d)}{2g} i^2$$

### MAGNETIC FORCE AND TORQUE FROM ENERGY

$$dW_{fid}(\lambda, x) = i d\lambda - f_{fid} dx$$

mechanical force

$$dW_{fid}(\lambda, x) = \frac{\partial W}{\partial \lambda} \bigg|_x d\lambda + \frac{\partial W}{\partial x} \bigg|_\lambda dx$$

$$i = \frac{\partial W_{fid}}{\partial \lambda} \bigg|_x$$

$$f_{fid} = - \frac{\partial W_{fid}}{\partial x} \bigg|_\lambda$$

$$f_{fid} = - \frac{\partial}{\partial x} \left( \frac{1}{2} L(x) i^2 \right) = - \frac{\partial}{\partial x} \left( \frac{1}{2} \frac{\lambda^2}{L(x)} \right)$$

$$= \frac{\lambda^2}{2(L(x))^2} (L'(x))$$

$$F_{fid} = \frac{\lambda^2}{2(L(x))^2} \frac{dL(x)}{dx} = \frac{i^2}{2} \left( \frac{dL(x)}{dx} \right)$$

rotating terminal  $\Rightarrow$

$$dW_{fid}(\lambda, \theta) = i d\lambda - T_{fid} d\theta$$

$$T_{fid} = - \frac{\partial W_{fid}}{\partial \theta} \bigg|_\lambda$$

$$\text{if } \lambda = L(\theta) i \Rightarrow T_{fid} = \frac{1}{2} \frac{\lambda^2}{(L(\theta))^2} \left( \frac{dL(\theta)}{d\theta} \right)$$

$$T_{fid} = \frac{i^2}{2} \frac{d(L(\theta))}{d\theta}$$

### COENERGY

$$W'_{fid} = i\lambda - W_{fid}$$

$$W'_{fid}(i, x) = i\lambda - W_{fid}(\lambda, x)$$

$$d(i\lambda) = \lambda di + i d\lambda$$

$$dW'_{fid}(\lambda, x) = i d\lambda - f_{fid} dx$$

$$\text{so, } dW'_{fid}(i, x) = i d\lambda + f_{fid} dx$$

$$\lambda = \frac{\partial W'}{\partial i} \bigg|_x$$

$$f_{fid} = \frac{\partial W'}{\partial x} \bigg|_i$$

$$w'_{fld}(i, x) = \int_0^i \lambda(i', x) di' = \int_0^i L(w) di = \frac{1}{2} L(x) i^2$$

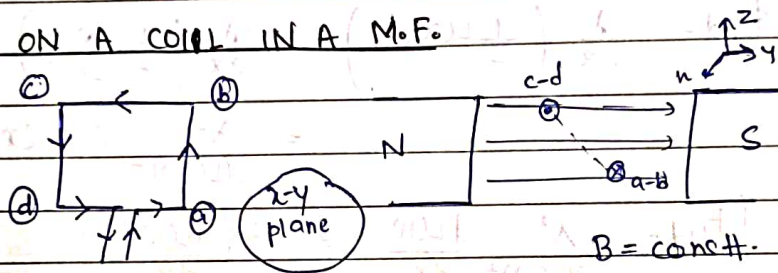
$$f_{fld} = \left. \frac{dw'}{dx} \right|_i = \left[ \frac{i^2}{2} \left( \frac{dL(x)}{dx} \right) \right]$$

and similarly,

$$T_{fld} = \left. \frac{dw'}{d\theta} \right|_i = \frac{i^2}{2} \left( \frac{dL(\theta)}{d\theta} \right)$$

$$w'_{fld} = \int_V \left( \int_0^{H_0} B \cdot dH \right) dV \quad w'_{fld} = \int_V \left( \frac{\mu H^2}{2} \right) \cdot dV$$

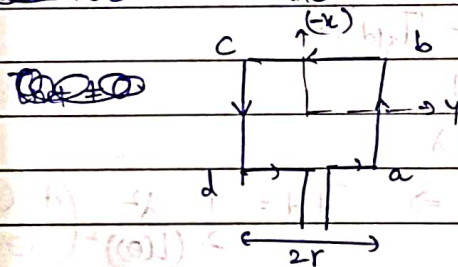
FORCE ON A COIL IN A M.F.



$B = \text{const. along } y\text{-axis}$

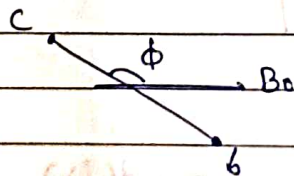
$$F_{ab} = I(\vec{r} \times \vec{B}) = I(\hat{x} \times B\hat{j}) = IB\hat{k}$$

$$F_{cd} = IB\hat{k} \quad \text{and} \quad F_{da} = -IB\hat{k}$$



$$F_{ab} = BIl(-\hat{z})$$

$$F_{cd} = BIl(\hat{z})$$

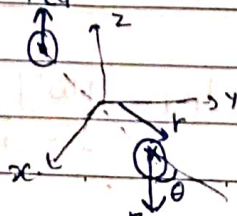


$$F_{bc} = BI(2r) \sin\phi (-\hat{x})$$

$$F_{da} = BI(2r) \sin\phi (+\hat{x})$$

$F_{bc}$  and  $F_{da}$  try to stretch the loop

(Torque)  $\rightarrow F_{ab}$  and  $F_{cd}$



$$\tau = 2rF \sin\theta$$

$$= 2r(IBl) \sin\theta$$

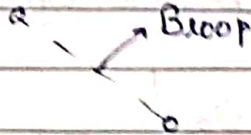
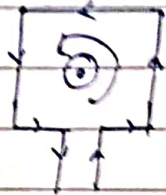


$$T_{\text{net}} = (2r) (I l B) \sin \theta = I (2rl) B \sin \theta$$

$$= (IA)(B) \sin \theta$$

$$\tau = (\vec{IA}) \times (\vec{B}) \quad \boxed{\tau = \vec{M} \times \vec{B}}$$

The loop also creates a M.F.,  $B_{\text{loop}}$



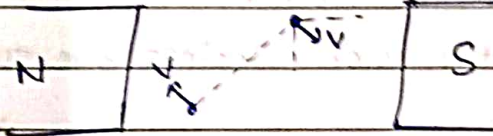
$$T_{\text{net}} = \left[ (2rl) I B \sin \theta \right]$$

$\downarrow$   
 $K B_{\text{loop}}$

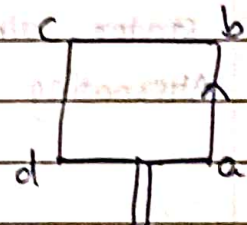
$$\boxed{\tau = K B_{\text{loop}} \times B_{\text{ext}}}$$

EMF

$$\boxed{\mathcal{E} = (\vec{v} \times \vec{B}) \cdot \vec{l}}$$



$$v = r\omega$$



$$E_{a \rightarrow b} = l(-\hat{x}) \cdot [(r\omega)(B_0) \sin \theta](-\hat{x})$$

$$\boxed{E_{a \rightarrow b} = l r \omega B_0 \sin \theta}$$

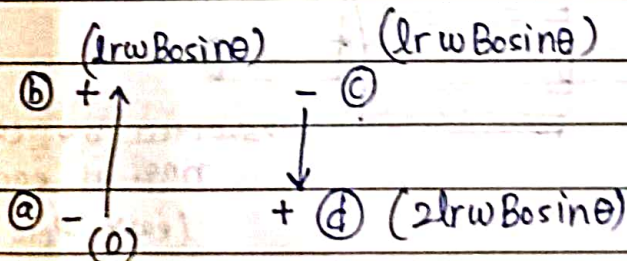
$$E_{b \rightarrow c} = (l \cos \theta (-\hat{y}) + l \sin \theta (-\hat{z})) \cdot ((r\omega)(B_0) \sin \theta (\hat{x}))$$

$= 0$

$$E_{c \rightarrow d} = l(\hat{x}) \cdot [(r\omega)(B_0) \sin \theta](+\hat{x})$$

$$\boxed{E_{c \rightarrow d} = +l r \omega B_0 \sin \theta}$$

and  $E_{d \rightarrow a} = 0$



$$\boxed{E_{\text{net}} = 2 l r \omega B_0 \sin \theta}$$

$$E = (2rl) \omega B \sin \theta$$

$$= A \omega B \sin \theta$$

$$E = \omega A B \sin \theta$$

$$\boxed{\text{EMF} = \omega A B \sin(\omega t)}$$

$\theta = 180^\circ - \phi$   $\rightarrow$  angle made by normal.