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EE114 Power Engineering - I

Assignment 03

- **Question 1:** The magnetic circuit shown in Fig. 1 has dimensions $A_e = A_g = 9 \text{ cm}^2$, $g = 0.050 \text{ cm}$, $l_c = 30 \text{ cm}$ and $N = 500$ turns. Assume the value $\mu_r = 70,000$ for core material. (a) Find the reluctances R_e and R_g . For the condition that the magnetic circuit is operating with $B_c = 1.0 \text{ T}$, find (b) the flux ϕ and (c) the current i .

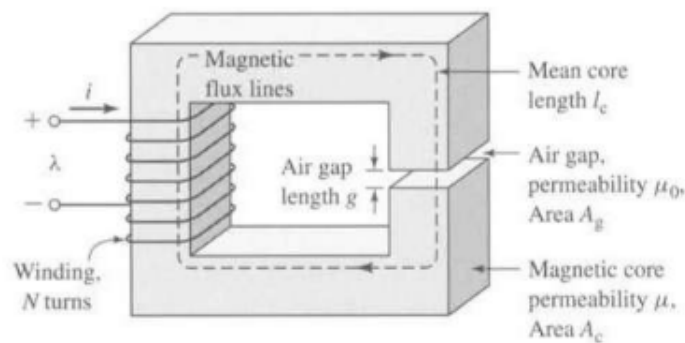


Figure 1

- **Question 2:** Find the flux ϕ and current for Question 1 if (a) The number of turns is doubled to $N = 1000$ turns while the circuit dimensions remains the same. (b) if the number of turns remains same ($N = 500$ turns) and the gap is reduced to 0.040 cm .
- **Question 3:** The relative permeability of the core material for the magnetic circuit of Fig. 1 is assumed to be $\mu_r = 70000$ at a flux density of 1.0 T . (a) For this value of μ_r , calculate the inductance of the winding. (b) Calculate the inductance under the assumption that the relative permeability is equal to 2900. Derive your conclusions from these problems (a) and (b).
- **Question 4:** For the magnetic circuit of Fig. 1. find (a) the inductance L , (b) the magnetic stored energy W for $B_c = 1.0 \text{ T}$, and (c) the induced voltage e for a 60 Hz time varying core flux of the form $B_c = 1.0 \sin(\omega t)$ where $\omega = 2\pi 60$.
- **Question 5:** Assume the core material in Fig. 1 is M-5 electrical steel. (a) Find the current i required to produce $B_c = 1.0 \text{ T}$. ($H_c = 11 \text{ A-turns/m}$) (b) Find the current i required to produce $B_c = 1.6 \text{ T}$. ($H_c = 71 \text{ A-turns/m}$) (c) By what factor does the current have to be increased to result in this factor of 1.6 increase in flux density?

- **Question 6:** A magnetic circuit with a single air gap is shown in Fig. 2. The core dimensions are:

$$A_c = 1.8 \times 10^{-3} \text{ m}^2 \quad l_c = 0.6 \text{ m} \quad g = 2.3 \times 10^{-3} \text{ m} \quad N = 83 \text{ turns}$$

Assume that the core is of infinite permeability and neglect the fringing effect. (a) Calculate the reluctance of the core and that of the air gap.

For a current of $i = 1.5 \text{ A}$, calculate (b) the total flux ϕ (b) the flux linkage λ (c) coil inductance L .

- **Question 7:** The magnetic circuit of Fig. 3 consists of a core and a moveable plunger of width l_p , each of permeability μ . The core has cross-sectional area A_c and mean length l_c . The overlap area of the two air gaps A_g is a function of the plunger position x and can be assumed to vary as

$$A_g = A_c \left(1 - \frac{x}{X_0} \right)$$

You may neglect the fringing effect at the air gap and use approximation consistent with magnetic-circuit analysis.

(a) Assume infinite permeability, derive an expression for the magnetic flux density in the air gap B_g as a function of the winding current I and as the plunger position is varied ($0 \leq x \leq 0.8X_0$). What is the corresponding flux density in the core?

(b) Repeat part (a) for a finite permeability.

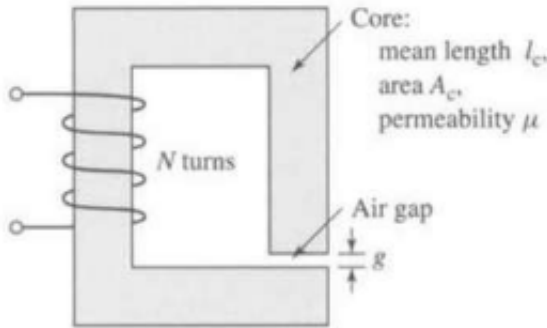


Figure 2

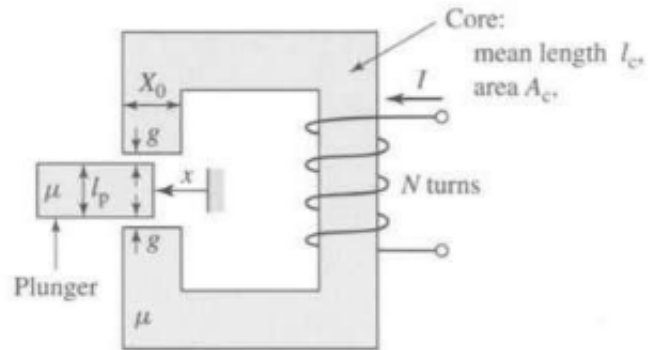


Figure 3

- **Question 8:** The magnetic circuit of Fig 4. consists of rings of magnetic material in a stack of height h . The rings have inner radius R_i and outer radius R_o . Assume that the iron is of infinite permeability and neglect the effects of magnetic leakage and fringing. For:

$$R_i = 3.4 \text{ cm}$$

$$R_o = 4.0 \text{ cm}$$

$$h = 2 \text{ cm}$$

$$g = 0.2 \text{ cm}$$

Calculate:

(a) the mean core length and the cross sectional area.

(b) Reluctance of the core and air gap.

if $N = 65$ turns, calculate:

(c) the inductance.

(d) current i required to operate at an air-gap flux density of $B_g = 1.35\text{T}$.

(e) Corresponding flux linkage of the coil.

- **Question 9:** A square voltage wave having a fundamental frequency of 60 Hz and equal positive and negative half cycles of amplitude E is applied to a 1000-turn winding surrounding a closed iron core of $1.25 \times 10^{-3}\text{m}^2$ cross section. (a) Sketch the voltage, winding flux linkage and the core flux as a function of time. (b) Find the maximum permissible value of E if the maximum flux density is not to exceed 1.15 T.

- **Question 10:** The inductor of Fig. 5 has following dimensions.

$$A_c = 1.0\text{cm}^2$$

$$l_c = 15\text{cm}$$

$$g = 0.8\text{mm}$$

$$N = 480 \text{ turns}$$

Neglect fringing effect and leakage flux.

(a) Calculate inductance. ($\mu_r = 1000$)

(b) This inductor is connected to 60 Hz voltage source. Calculate the RMS inductor voltage corresponding to peak core flux density of 1.5 T. Calculate the RMS current and the peak stored energy.

- **Question 11:** Consider the magnetic circuit of Fig. 6. This structure, known as a pot-core, is typically made in two halves. The N -turn coil is wound on a cylindrical bobbin and can be easily inserted over the central post of the core as the two halves are assembled. Because the air gap is internal to the core, provided the core is not driven excessively into saturation, relatively little magnetic flux will "leak" from the core, making this a particularly attractive

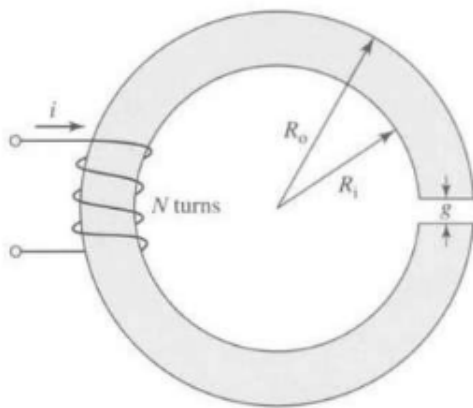


Figure 4

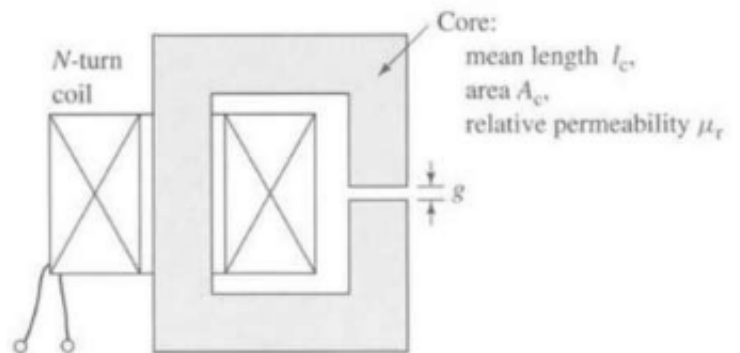


Figure 5

- (b) Find the mutual inductances between the three pairs of windings.
- (c) Find the voltage induced in winding 1 by time-varying currents $i_a(t)$ and $i_b(t)$ in windings A and B. Show that this voltage can be used to measure the imbalance between two sinusoidal currents of the same frequency.

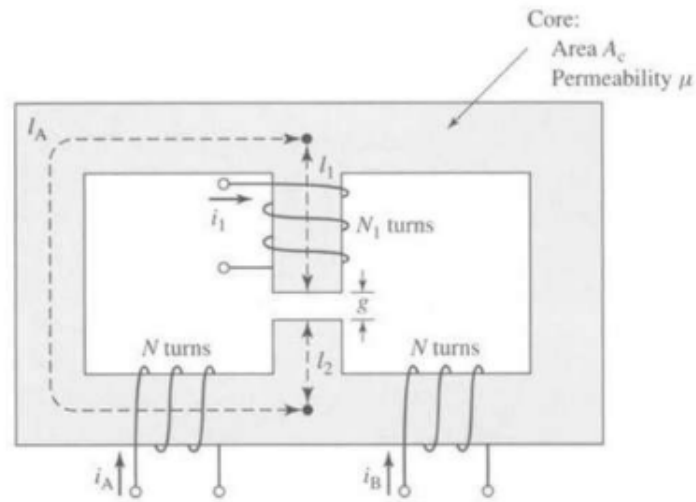


Figure 8

- **Question 14:** Solve for I_1 , I_2 and V_o in Fig.9.

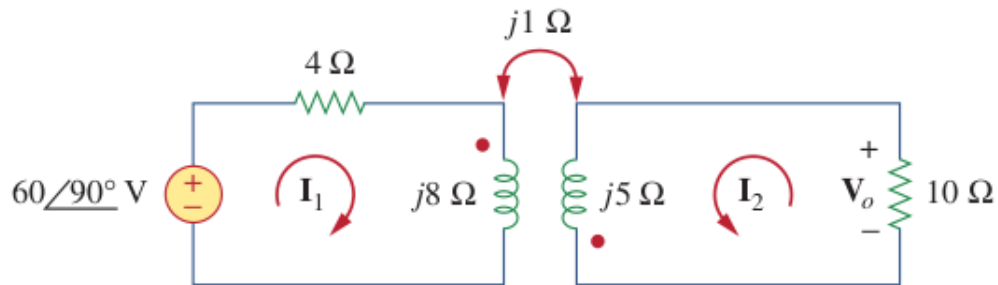


Figure 9