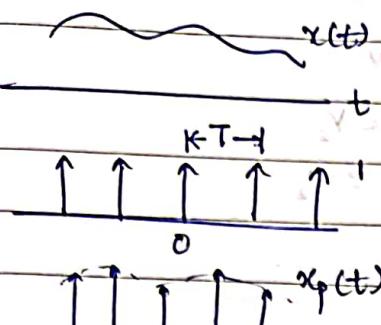


Module - ③

Impulse train Sampling \Rightarrow T: sampling period $\omega_s = \frac{2\pi}{T}$: sampling frequency



$$P(t) = \text{sampling } f^n e$$

$$x_p(t) = x(t) \cdot P(t) \quad ; \quad P(t) = \sum_{n=-\infty}^{+\infty} \delta(t-nT)$$

$$\text{using } x(t) \delta(t-t_0) = x(t_0) \delta(t-t_0)$$

$$n_p(t) = \sum_{n=-\infty}^{\infty} n(nT) \delta(t - nT)$$

$$X_p(j\omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} x(j\theta) P(j(\omega - \theta)) d\theta$$

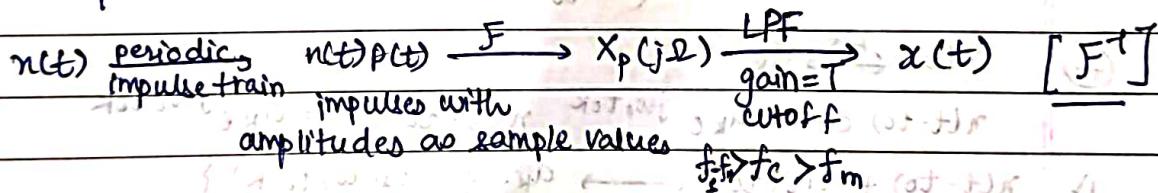
$$P(j\omega) = \frac{2\pi}{T} \sum_{k=-\infty}^{+\infty} \delta(\omega - k\omega_s)$$

convolution with an impulse simply shifts the signal.

$$x(jz) * \delta(\omega - \omega_0) = x(j(z - z_0))$$

$$x_p(j\omega) = \frac{1}{T} \sum x(j(\omega - k\Delta\omega))$$

Sampling Theorem :- $x(t)$ be a band-limited signal with $X(j\omega) = 0 \forall |\omega| > \omega_m$, then $x(t)$ is uniquely determined by its samples for $(x(nT))$



- A signal is band-limited \rightarrow there exists a max^m frequency component above which spectrum is entirely zero
- there is a limit to how fast (PHYSICAL INTERPRETⁿ) the signal changes.

Ideal low-pass filters

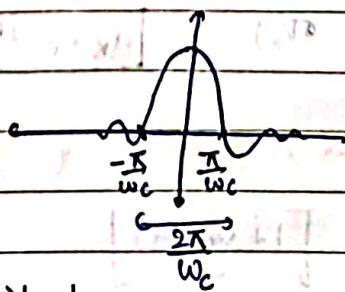
$$H(j\omega) = \begin{cases} 1 & |\omega| \leq \omega_c \\ 0 & |\omega| > \omega_c \end{cases}$$

$$h(t) = \sin \omega_c t$$

πt

non-causal (so-ly)

as we can't simply shift it to make it become causal.

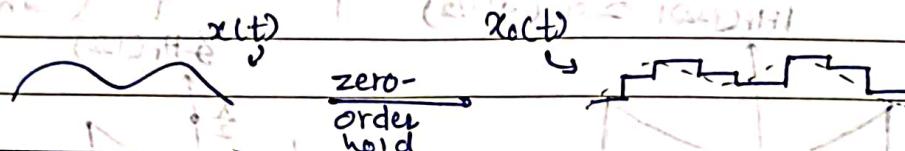


→ causal filters exhibit some level of transition band b/w the passband and stopbands since it will take time for it to shift from allowing to attenuating frequencies, as it doesn't know about future inputs ('causal')

Sample & Hold

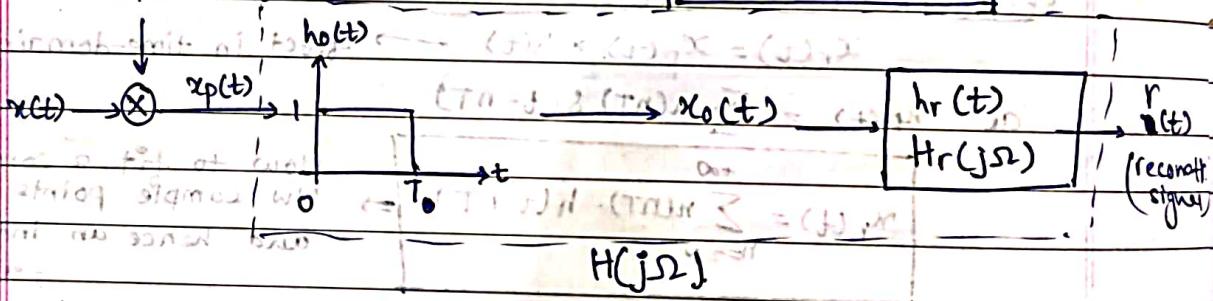
⇒ sampling theorem → band-limited signals represented by its samples.

⇒ zero-order-hold → sample and hold till the next sample is taken.



reconstruction filter → (no longer need comft. gain)
(in the passband)

$x_s(t) \rightarrow$ impulse-sampling + LSI system with a rect/L-impulse response



$H_r(j\omega)$ such that $r(t) = x(t) \Rightarrow$ cascade of $h_0(t)$ & $h_r(t)$ is the ideal LPF $H(j\omega)$ used.

$$h_0(t) \rightarrow H_0(j\omega) = \int_{-\infty}^{\infty} 1 \cdot e^{-j\omega t} dt$$

$$H_0(j\omega) = \frac{1 - e^{-j\omega T}}{\omega T} = \frac{-j\omega T}{\omega T} = \frac{j\omega T/2}{e^{-j\omega T/2}}$$

$$H_0(j\omega) = e^{-j\omega T/2} \cdot \left[\frac{2 \sin(\omega T/2)}{\omega} \right]$$

and so, as $H(j\omega) = H_0(j\omega) \cdot H_r(j\omega)$, we need,

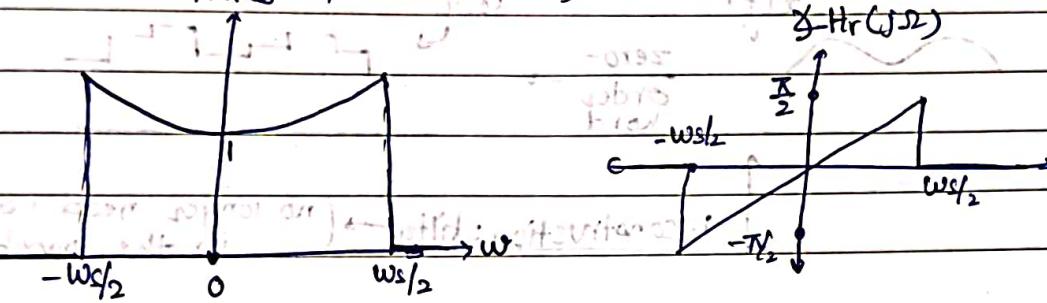
$$H_r(j\omega) = e^{j\omega T/2} / \left(\frac{2 \sin(\omega T/2)}{\omega} \right)$$

Q. - If the cutoff frequency of $H(j\omega)$ is $\omega_c = \frac{\pi}{2T}$

$$H(j\omega) = \begin{cases} 1 & \text{if } |\omega| < \omega_c = \omega_s/2 \\ 0 & \text{o/w} \end{cases}$$

Then, $H_r(j\omega) = \frac{\omega e^{j\omega T/2}}{2 \sin(\omega T/2)}$ $\Rightarrow H_r(j\omega) = (\frac{\omega}{2T}) \quad \omega > 0$
 $= 0 \quad \omega < 0$

$$|H_r(j\omega)| = \frac{(\omega T/2)}{2 \sin(\omega T/2)} = \frac{\omega}{T} \left(\frac{\omega T/2}{\sin(\omega T/2)} \right)$$



Output of a zero-order hold \rightarrow adequate sample in itself.

RECONSTRUCTION / INTERPOLATION

$$x_r(t) = x_p(t) * h(t) \rightarrow \text{effect in time-domain of LPF}$$

as $x_p(t) = \sum n(nT) \delta(t-nT)$

$$x_r(t) = \sum_{n=-\infty}^{+\infty} n(nT) \cdot h(t-nT)$$

How to fit a cont. curve b/w sample points $n(nT)$ and hence an interpolation formulae

For ideal LPF, $h(t) = \frac{\omega_c T \sin(\omega_c t)}{\pi \omega_c(t)}$

and so,

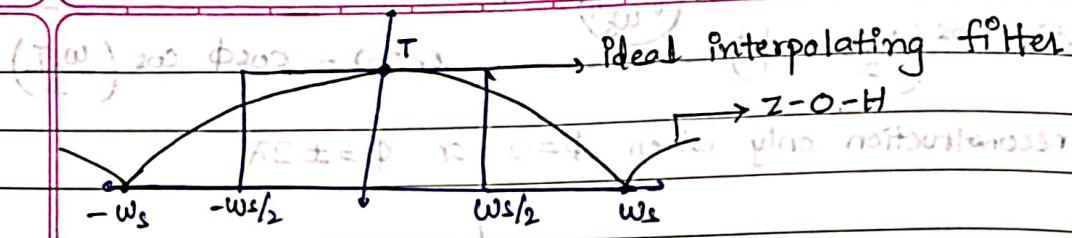
$$x_r(t) = \sum n(nT) \cdot \frac{\omega_c T \sin(\omega_c(t-nT))}{\pi \omega_c(t-nT)}$$

(band-limited interpolation)

\Rightarrow zero-order hold can also be used as an interpolation f^h , with the impulse response $h(t)$ as the interpolating f^h .

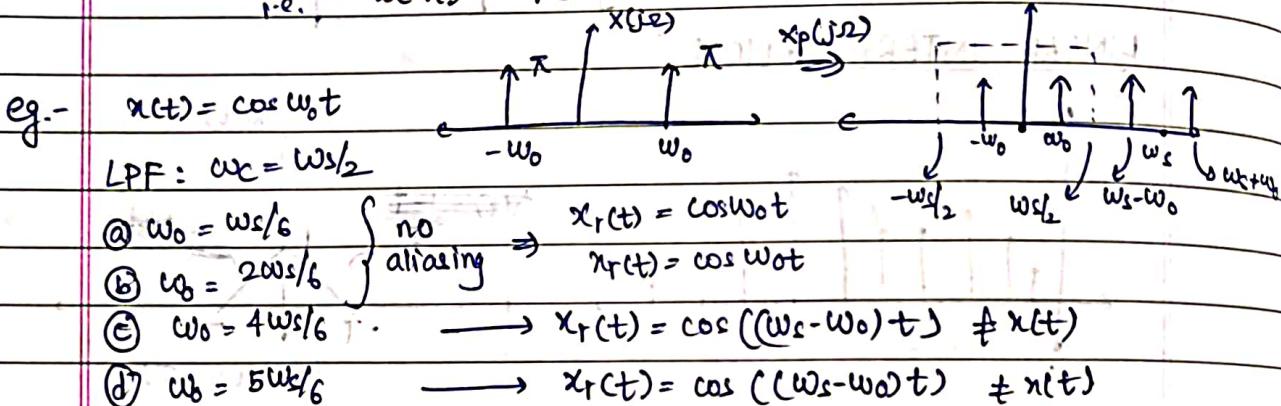
↳ interpolating f^h , $h(t) = h_0(t)$ (impulse response of LSI system)
 $\Rightarrow x_0(t) \underset{\text{approx}}{\approx} x(t)$ and so system with $\underset{\text{approx}}{\approx}$ Ideal LPF.

$$H_o(j\omega) = \left(\frac{2 \sin(\omega T/2)}{\omega} \right) e^{-j\omega T/2} \quad |H_r(j\omega)| = \frac{2 \sin(\omega T/2) \cdot T}{(-\omega T/2)}$$



⇒ NOTE :- even if $w_0 < 2w_m$, the reconstructed signal, $x_r(t)$ will be different from $x(t)$, but the value at the sampled points is same

$$\text{i.e., } x(nT) = x_r(nT) + n$$



when $w_0 = w_s \rightarrow$ The output signal is a constant \Rightarrow (1)

↳ when sampling one cycle, the samples are all equal and identical to those that would have been obtained by $w_0 = 0$ (Correct)

⇒ WHY NOT SAMPLE AT EXACTLY TWICE SAMPLING FREQUENCY.

eg.- $x(t) = \cos\left(\frac{w_c}{2}t + \phi\right) \rightarrow$ impulse sampling at $2\left(\frac{w_s}{2}\right) = w_s$

$$x_p(t) = \sum_{n=-\infty}^{+\infty} x(nT) \delta(t-nT) \quad T = \frac{2\pi}{w_s}$$

$$x_p(t) = \sum_{n=-\infty}^{+\infty} \cos\left(\frac{w_s}{2} \cdot \frac{2\pi \cdot n}{w_s} + \phi\right) \delta(t-nT)$$

$$x_p(t) = \sum_{n=-\infty}^{+\infty} (\cos \phi) \delta(t-nT)$$

Here, $x(t) = \cos\left(\frac{w_s t}{2}\right) \cos \phi - \underbrace{\sin\left(\frac{w_s t}{2}\right)}_{g(t)} \sin \phi$

and $g(NT) = \sin\left(\frac{w_s}{2} \cdot \frac{2\pi}{w_s} n\right) \sin \phi = 0 \rightarrow$ so, $x(nT) = \cos^2 \frac{w_s n}{2}$

so, $x_p(t) \xrightarrow{\text{LPF}} y_p(t) \quad Y_p(j\omega) = \{\cos \phi\} F\{(\cos w_s t)\}$

~~so, $y_p(t) = (\cos \phi) \cos\left(\frac{w_s t}{2}\right)$~~

$$x(t) = \cos\left(\frac{\omega_0 t}{2} + \phi\right) \quad \xrightarrow{v \omega_0^2} \quad x_r(t) = \cos\phi \cos\left(\frac{\omega_0 t}{2}\right)$$

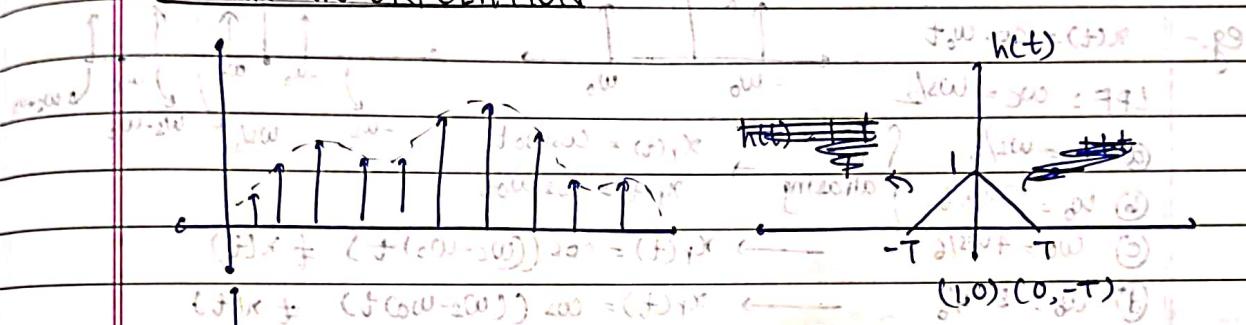
reconstruction only when $\phi=0$ or $\phi=\pm 2\pi$

$$\int e^{j\omega_0 t} dt$$

$$eg. 2) x_r(t) = \sin\left(\frac{\omega_0 t}{2}\right)$$

$$\xrightarrow{x_p(t) = 0 \text{ identically}} \boxed{x_r(t) = 0 \neq x(t)}$$

LINEAR INTERPOLATION



$$\textcircled{1} \text{ if function } H(j\omega) \text{ is real and even } \Rightarrow H(j\omega) = H(-j\omega) \quad \omega = \omega_0 \quad \text{and } \omega = -\omega_0$$

$$\text{Because } h(t) = (1-t/T)x(-T) + (t-T)x(T) \text{ is even, } h(t) = \frac{1+t/T}{2}x(-T) + \frac{1-t/T}{2}x(T)$$

$$H(j\omega) = \int_{-T}^T \left(1 + \frac{t}{T}\right) e^{-j\omega t} dt + \int_0^T \left(1 + \frac{t}{T}\right) e^{j\omega t} dt$$

$$t = -T \quad = \left[\left(1 - \frac{t}{T}\right) e^{j\omega t} \right]_0^T + \left(1 + \frac{t}{T}\right) e^{-j\omega t} dt$$

$$= \int_0^T \left(2 \cos(\omega t) - \frac{j}{T} (2j) \sin(\omega t)\right) dt = (\pm) j \omega$$

$$= -\frac{1}{T} \left[\left(-t \cos(\omega t) \right)_0^T - \frac{j}{\omega} \int_0^T \cos(\omega t) dt \right] (\pm) j \omega$$

$$= -\frac{1}{T} \left[\frac{1}{2} + \frac{j}{\omega} \left[\sin(\omega t) \right]_0^T \right]$$

$$= \frac{1}{T} \left[\frac{\sin(\omega T/2)}{\omega} \right]$$

$$h(0) * h(t)$$

$$(H(j\omega))^2 \quad H(j\omega) = H_0(j\omega) * H_0(j\omega)$$

$$(\frac{1}{T})^2 \left(\frac{\sin(\omega T/2)}{\omega} \right)^2$$

MIT 3.7736.0

$h(t)$

$$\begin{aligned}
 H(j\omega) &= \int h(t) e^{-j\omega t} dt = \int_{-T}^0 \left(1 + \frac{t}{T}\right) e^{-j\omega t} dt + \int_0^T \left(1 - \frac{t}{T}\right) e^{j\omega t} dt \\
 &\quad - \cancel{\int_{-T}^0 (2 \cos(\omega t)) \cdot dt} + \cancel{\frac{1}{T} \int_{-T}^0 t \cdot dt} \\
 &= \int_{-2}^T 2 \cos(\omega t) + \frac{1}{T} \int_{-2}^T (e^{j\omega t} - e^{-j\omega t}) \cdot t dt \\
 &= \left[1/2 [\sin(\omega t)] \right]_{-2}^T + \frac{1}{T} \int_0^T (2 \sin(\omega t)) \cdot t dt \\
 &\Rightarrow 2 \sin(\omega T) + \frac{1}{T} \left[\left[2t \cos(\omega t) \right]_{-2}^T + \frac{1}{2} \int_0^T \cos(\omega t) \right] \\
 &= 2 \sin(\omega T) + \frac{1}{T} \left[-2 \cos(\omega T) \right] + \frac{1}{T} \cdot \frac{1}{\omega^2} \sin(\omega T) \\
 &= 2 \left[\sin(\omega T) - \cos(\omega T) \right] + \frac{1}{T \cdot \omega^2} \sin(\omega T)
 \end{aligned}$$

$$h(t) = h_0^{(t)} * h_0^{(t)}$$

$$\mathcal{F}(h_0(t)) = \frac{1}{\omega/2} \sin(\omega T/2)$$

$$h_0(t)$$

$$\text{so } H(j\omega) \rightarrow$$

$$\begin{aligned}
 H(j\omega) &= \frac{1}{\omega/2} \left[\sin(\omega T/2) \right]^2 \\
 &= (\omega/2) \sin^2(\omega T/2)
 \end{aligned}$$

$$\omega = 1 \text{ rad} / \text{sec}$$

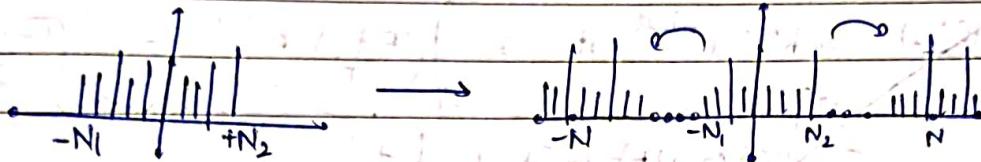
$$\omega = \pi / T = \pi / 4 \text{ rad/sec}$$

DISCRETE TIME FOURIER TRANSFORM

Consider a general seqⁿ $x[n]$ of finite durⁿ i.e.

$x[n] = 0$ for some n outside $-N_1 \leq n \leq N_2$.

$$\tilde{x}[n] = x[n] \quad \text{with period } N.$$



as $N \rightarrow \infty \Rightarrow \tilde{x}[n] \rightarrow x[n]$ for any finite n

$$\tilde{x}[n] = \sum_{k=-N}^{jK(\frac{2\pi}{N})n} a_k e^{jk\omega_0 n}$$

Note :- If $x[n] = x[n+N]$ $\omega_0 = 2\pi/N$: fundamental frequency

$e^{j(\frac{2\pi}{N})n} \rightarrow$ (periodic with period = N)

$\Phi_k[n] = e^{jk\omega_0 n} \quad k=0, \pm 1, \pm 2, \dots \rightarrow$ set of all discrete-time complex exponential signals periodic with period = N .

$$\Phi_0[n] = \Phi_N[n]$$

$\Phi_1[n] = \Phi_{N+1}[n]$ and so on, so, there are ONLY N -distinct signals

$$x[n] = \sum_k a_k \Phi_k[n] = \sum_k a_k e^{jk\omega_0 n} = \sum_{k=-N}^{jK(\frac{2\pi}{N})n} a_k e^{jk\omega_0 n}$$

and here, $a_k = \frac{1}{N} \sum_{n=-N}^{N} x[n] e^{-jk\omega_0 n}$ $\downarrow N$ successive integers

Since $\tilde{x}[n] = x[n]$ over a period that includes $-N_1 \leq n \leq N_2$

then, $a_k = \frac{1}{N} \sum_{n=-N_1}^{N_2} x[n] e^{-jk\omega_0 n} = \frac{1}{N} \sum_{n=-\infty}^{+\infty} x[n] e^{-jk\omega_0 n}$

($x[n]$ is 0 o/w)

Let $X(e^{j\omega}) = \sum_{n=-\infty}^{+\infty} x[n] e^{-jn\omega}$, Then, $a_k = \frac{1}{N} X(e^{jk\omega_0})$

proportⁿ to samples of $X(e^{j\omega})$

so, $\tilde{x}[n] = \sum_{k=-N}^{jK(\frac{2\pi}{N})n} \frac{1}{N} X(e^{jk\omega_0}) \cdot e^{jk\omega_0 n}$ $(\omega_0 = \frac{2\pi}{N} \text{ is spacing in the frequency-domain})$

$$\omega_0 = \frac{2\pi}{N} \quad \text{or} \quad \frac{1}{N} = \frac{\omega_0}{2\pi}$$

$$\tilde{x}[n] = \frac{1}{2\pi} \sum_{k=-N/2}^{N/2} x(e^{jkw_0}) \cdot e^{jknw_0}$$

as $N \rightarrow \infty$, $w_0 \rightarrow 0$

$$\sum \rightarrow \int$$

\sum over N intervals of width w_0
 \int has total width 2π

$$x[n] = \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{jw}) e^{jwn} dw \quad \rightarrow \text{inverse DTFT}$$

$$X(e^{jw}) = \sum_{n=-\infty}^{+\infty} x[n] e^{-jwn} \quad \rightarrow \text{discrete-time FT (DTFT)}$$

→ Fourier co-eff. a_k of a periodic signal $\tilde{x}[n]$ can be expressed in terms of equally-spaced samples of the F.T. of a finite-duration aperiodic signal, $x[n] = \tilde{x}[n]$ over one period & zero elsewhere.

DTFT and Sampling

$$x_c(t) = \tilde{x}(t) \circ \sum_{n=-\infty}^{+\infty} \delta(t-nT) = \sum_{n=-\infty}^{+\infty} x(t) \delta(t-nT) = \sum_{n=-\infty}^{+\infty} x(nT) \delta(t-nT)$$

Let $x_d[n] \triangleq x(nT)$

continuous time

(a C.T. Fourier T.
can be defined)

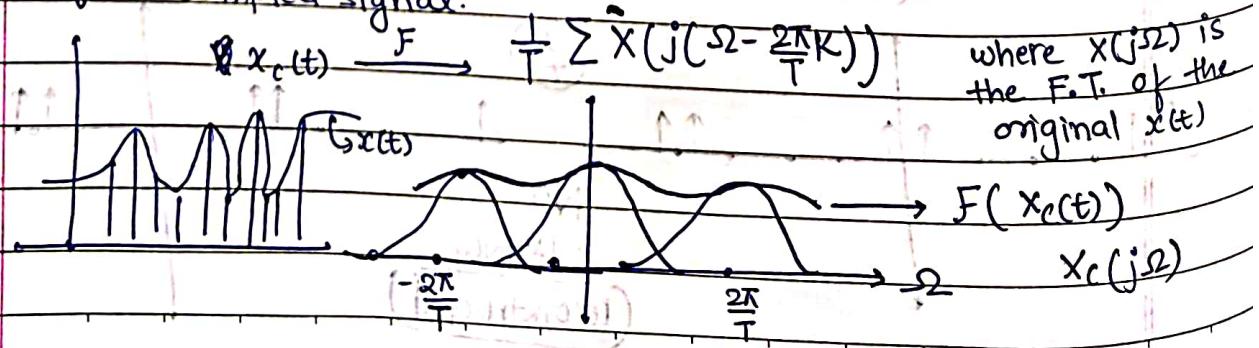
$$x_c(j\omega) = \int \left(\sum_{n=-\infty}^{+\infty} x(nT) \delta(t-nT) \right) e^{-j\omega t} dt$$

$$= \sum_{n=-\infty}^{+\infty} x(nT) e^{-jn\omega T}$$

and $X_d(e^{jw}) = \sum_{n=-\infty}^{+\infty} x[n] e^{-jwn}$

so, $X_c(j\omega) = X_d(e^{j\omega})$

So, the DTFT is just the continuous Time Fourier Transform of a sampled signal.

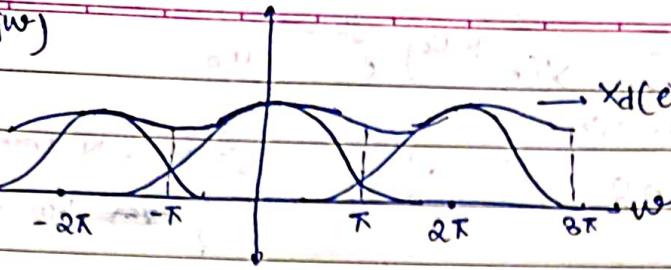


where $X(j\omega)$ is the F.T. of the original $x(t)$

$$(w = 2\pi)$$

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$$x_d(e^{jw})$$



$x_d(e^{jw})$ (looks like the same.)

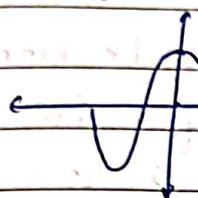
DTFT is periodic with period = 2π (in w axis)

CTFT is periodic with period = $2\pi/T$ (in ω_2) or 2π in (w)

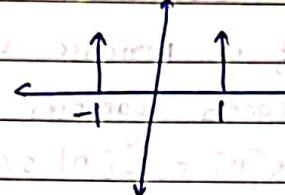
ALIASING

e.g.

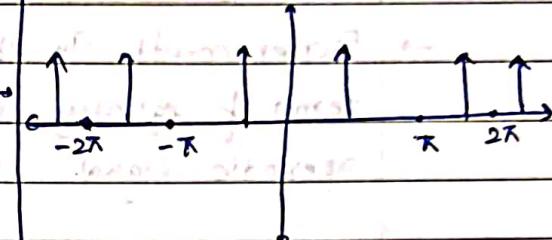
$$x_c = \cos(\omega t)$$



$$X_C(j\omega)$$



$$\text{DTFT} = \sum x_c(j(2\pi - k\omega_s))$$



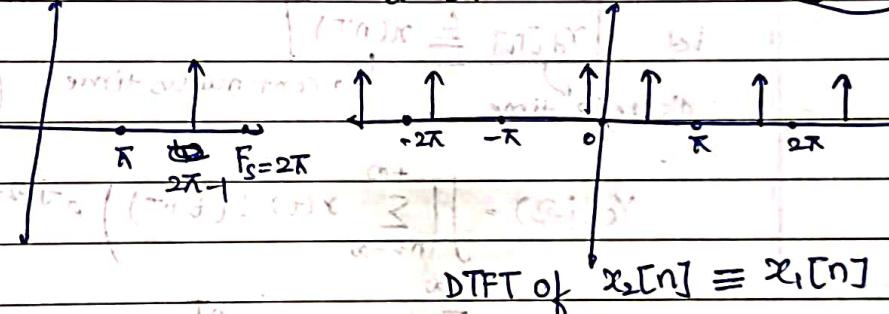
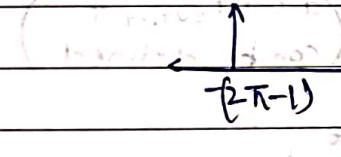
if the max. frequency, $f_m > \pi$

\Rightarrow DFT

= aliasing
in the signals

$$\text{say } x_c(t) = \cos(\omega t)$$

$$X_{2C}(2\pi) \Rightarrow$$



$$\text{DTFT of } x_c[n] \equiv x_i[n]$$

→ at a sampling rate of $T=1$, the frequencies 1 and $2\pi-1$ are indistinguishable → ALIASING

$$f_s = 2\pi$$

Nyquist criteria: $f_s - f_m > f_m$ or $f_s > 2f_m$

$$2\pi > 2(1) \quad \text{but}$$

$$2\pi < 2(2\pi-1)$$

thus, there is aliasing

if it was sampled as $f_s = 4\pi$ instead

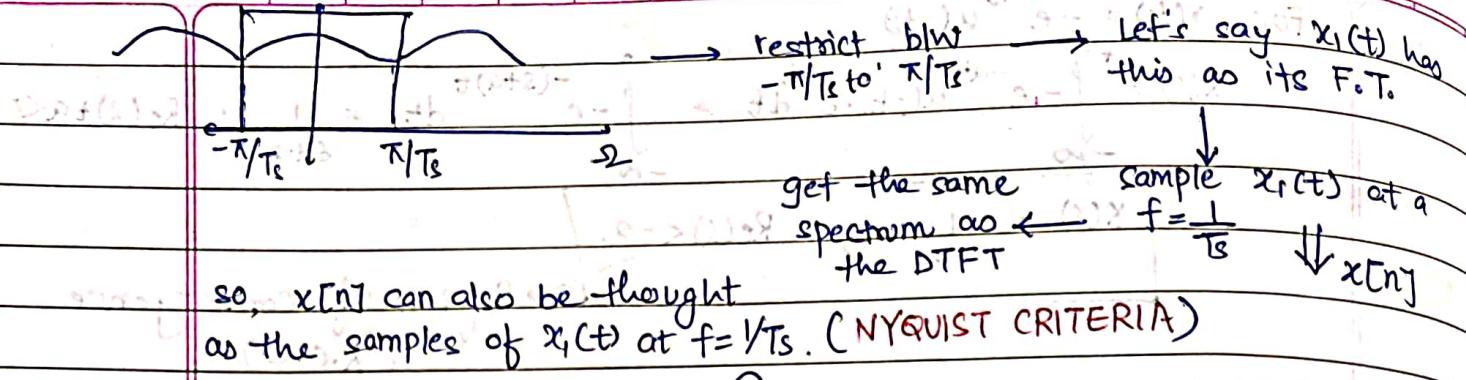
$$x_c \rightarrow \text{DTFT}$$



NO
ALIASING

(reconstructed)

DTFT



→ if we want each ω to contribute individually,

$$(\omega)_{\max.} = \pi \quad (\omega)_{\min.} = -\pi$$

MODULE - 4

Laplace Transforms

$$e^{st} \xrightarrow{\text{LTI system}} y(t) = H(s) e^{st}$$

$$y(t) = h(t) * e^{st} = \int_{-\infty}^t h(\tau) e^{s(t-\tau)} d\tau = e^{st} \int_{-\infty}^t h(\tau) e^{-s\tau} d\tau$$

if $s = j\omega \rightarrow$ F.T. ; general complex 's' → Laplace Transform

$$X(s) \triangleq \int_{-\infty}^{+\infty} x(t) e^{-st} dt \quad \text{bilateral L.T.}$$

$$s = \sigma + j\omega \quad X(\sigma + j\omega) = \int_{-\infty}^{+\infty} x(t) e^{-(\sigma+j\omega)t} dt$$

$$= \int_{-\infty}^{+\infty} (x(t) e^{-\sigma t}) e^{-j\omega t} dt = e^{-\sigma t} \int_{-\infty}^{+\infty} x(t) e^{-j\omega t} dt$$

$$= \mathcal{F}(x(t) e^{-\sigma t})$$

e.g. $x(t) = e^{-at} u(t) \quad X(j\omega) = \int_{-\infty}^{+\infty} e^{-at} u(t) e^{-j\omega t} dt = \frac{1}{j\omega + a}; a > 0$

$$X(s) = \int_{-\infty}^{+\infty} e^{-at} u(t) e^{-st} dt = \frac{1}{(s+a) + j\omega} \quad ; \quad s+a > 0$$

$$X(s) = \frac{1}{s+a} \quad ; \quad (\operatorname{Re}(s) > -a)$$

For $x(t) = -e^{-at} u(-t)$

$$X(s) = \int_{-\infty}^{+\infty} -e^{-at} u(-t) \cdot e^{-st} dt = \int_{-\infty}^0 -e^{-(s+a)t} dt = \frac{1}{s+a}; \operatorname{Re}(s) + a < 0$$

$$X(s) = \frac{1}{s+a}; \operatorname{Re}(s) < -a$$

Region of convergence
(R.O.C.)

\Rightarrow ROC: consists of those values of $s = \sigma + j\omega$ where the F.T. of $x(t) e^{-\sigma t}$ converges.

e.g. $x(t) = e^{-2t} u(t) + e^{-t} (\cos 3t) u(t)$

$$x(t) = \left[e^{-2t} + \frac{1}{2} e^{-(1+3j)t} + \frac{1}{2} e^{-(1-3j)t} \right] u(t)$$

$$\frac{1}{s+2}, \frac{1}{s+(1+3j)}, \frac{1}{s+(1-3j)} \rightarrow \frac{2s^2 + 5s + 12}{(s^2 + 2s + 10)(s + 2)}; \operatorname{Re}(s) > -1$$

$$\operatorname{Re}(s) > -2$$

$$\operatorname{Re}(s) > -1$$

$$\operatorname{Re}(s) > -1$$

poles

\Rightarrow if order of deno. $>$ num. $\Rightarrow x(s) \rightarrow 0$ as $s \rightarrow \infty$
 num. $>$ den. $\Rightarrow x(s)$ unbounded as $s \rightarrow \infty$ } zeroes / poles at ∞

e.g. $x(t) = \delta(t) - \frac{4}{3} e^{-t} u(t) + \frac{1}{3} e^{2t} u(t)$

$$x(s) = \int_{-\infty}^{+\infty} \delta(t) e^{-st} dt = \int \delta(t) \cdot 1 dt = 1 \quad \text{for any value 's'}$$

$$x(s) = 1 - \frac{4}{3} \cdot \frac{1}{s+1} + \frac{1}{3} \cdot \frac{1}{s-2} \quad \begin{cases} \operatorname{Re}(s) > 2 \\ \operatorname{Re}(s) > -1 \end{cases}$$

$$= \frac{(s-1)^2}{(s+1)(s-2)} \quad \therefore \text{neither poles nor zeroes at infinity.}$$

If the ROC does NOT include the $j\omega$ -axis, F.T. doesn't converge

$$\text{e.g. } e^{2t} u(t) \rightarrow \text{F.T. D.N.C.}$$

$$\frac{1}{s-2}; \operatorname{Re}(s) > 2$$

(n^{th} order zero \rightarrow repeated 'n' times)

Regions Of Convergence (R.O.C.)

Property 1

The ROC of $x(s)$ contains strips parallel to the jw -axis in the s -plane. This is because if $x(t) = \int_{-\infty}^{+\infty} x(s) e^{-st} dt$, then $|x(t)| \leq \int_{-\infty}^{+\infty} |x(s)| e^{-\sigma t} dt$.

ROC contains those $s=\sigma+jw$ where F.T. of $x(t)e^{-st}$ converges i.e. ROC has those values of s for which $x(t)e^{-st}$ is absolutely integrable.

$$\text{ROC: } \int_{-\infty}^{+\infty} |x(t)| e^{-\sigma t} dt < \infty$$

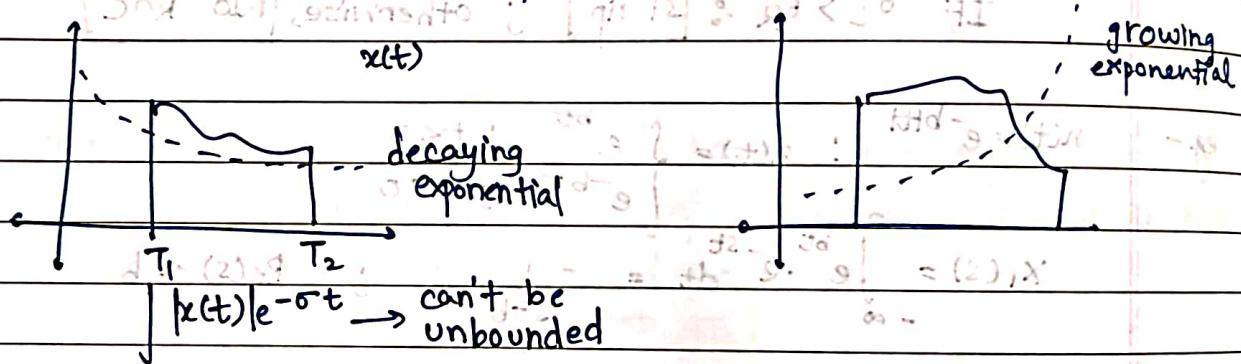
Property 2

For rational Laplace transforms, the ROC does not contain ANY POLES.

L, as $x(s) \rightarrow \infty$ at a pole, the integral doesn't converge at a pole.

Property 3

If $x(t)$ is of finite duration and absolutely integrable, then the ROC is the entire s -plane.



$$\text{Proof:- } \int |x(t)| \cdot dt < \infty \quad \text{--- (1)}$$

$$s = \sigma + jw \text{ to be in ROC, we need } \int_{T_1}^{T_2} |x(t)| e^{-\sigma t} dt < \infty \quad \text{--- (2)}$$

(1) and (2): Verify that $s=0$ is in the ROC

$$\text{For } \sigma > 0 \quad \int |x(t)| e^{-\sigma t} dt < e^{-\sigma T_1} \int |x(t)| dt \rightarrow \text{finite}$$

also bounded \rightarrow bounded

$$\text{For } \sigma < 0 \quad \int |x(t)| e^{-\sigma t} dt < e^{-\sigma T_2} \int |x(t)| dt$$

(A.P.)

Property 4

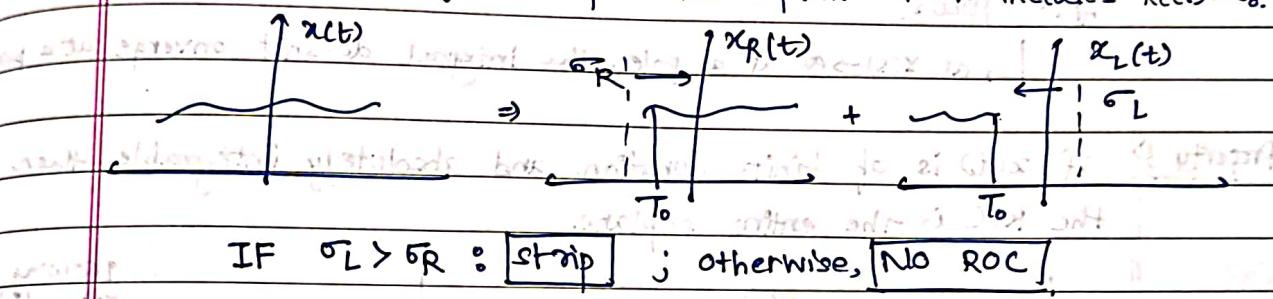
If $x(t)$ is right-sided i.e. $x(t)=0 \forall t < T_1$, and if the line $\text{Re}(s) = \sigma_0$ is in ROC, then all s for which $\text{Re}(s) > \sigma_0$ are also in the ROC.

$x(t) = e^{t^2} u(t) \rightarrow$ For no's, this signal converges)

→ Here, $x(t) = e^{-\sigma_1 t}$ for $\sigma_1 > \sigma_0$ can't grow unbounded in the left-sided domain because $x(t)$ becomes 0 after a finite time.

Property 5) If $n(t)$ is left-sided, and if the line $\text{Re}(s) = \sigma_0$ is ROC, then all s for which $\text{Re}(s) < \sigma_0$ will also be in the R.O.C.

Property 6) If $x(t)$ is two-sided and if the line $\text{Re}(s) = \sigma_0$ is in the ROC, then the ROC consists of a strip in the s -plane that includes $\text{Re}(s) = \sigma_0$.



eg.- $n(t) = e^{-bt} u(t)$: $n(t) = \begin{cases} e^{bt} & ; t < 0 \\ e^{-bt} & ; t > 0 \end{cases}$

$$X_1(s) = \int_{-\infty}^{bt} e^{bt} \cdot e^{-st} dt = -\frac{1}{s-b} ; \text{Re}(s) < b$$

$$X_2(s) = \frac{1}{s+b} ; \text{Re}(s) > -b \quad \text{so, } X(s) = \frac{1}{s+b} + \frac{1}{s-b}$$

converges only if $b > 0$

$$X(s) = \frac{-2b}{s^2 - b^2} \text{ for } -b < \text{Re}(s) < +b$$

Property 7) If the Laplace transform $X(s)$ of $x(t)$ is rational, then its ROC is bounded by poles or extends to ∞ and no poles of $X(s) \notin \text{ROC}$.

Property 8) $x(t)$ is right-sided \Rightarrow ROC is entire s -plane to right of rightmost pole.
 $x(t)$ is left-sided \Rightarrow ROC is entire s -plane to left of leftmost pole.

eg.- $X(s) = \frac{1}{(s+1)(s+2)}$

(I) (II)

$$x(s) = \frac{(s+2) - (s+1)}{(s+1)(s+2)}$$

$$= \frac{1}{s+1} - \frac{1}{s+2}$$

$$\begin{aligned} & \textcircled{1} e^{-t} u(t) - e^{-2t} u(t) \\ & \textcircled{2} -e^{-t} u(-t) \rightarrow e^{-2t} u(t) \\ & \textcircled{3} -e^{-t} u(-t) + e^{-2t} u(-t) \end{aligned}$$

INVERSE LAPLACE TRANSFORM

$$x(\sigma+j\omega) = \mathcal{F}^{-1}\{x(t)e^{-\sigma t}\}_{s=\sigma+j\omega} = X(s)$$

$$x(t)e^{-\sigma t} = \mathcal{F}^{-1}(X(s))$$

$$x(t)e^{-\sigma t} = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(\sigma+j\omega) e^{j\omega t} d\omega = (j\omega) X(s)$$

$$\text{so, } x(t) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(\sigma+j\omega) e^{(\sigma+j\omega)t} d\omega$$

$x(t)$ can be recovered from its Laplace transform, $x(\sigma+j\omega)$ by evaluating it for a set of values of $s=\sigma+j\omega$ in ROC with σ fixed and ω varying from $-\infty$ to $+\infty$.

$$x(t) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(s) e^{\sigma t} ds$$

eg.-

$$X(s) = \sum_{i=1}^n \frac{A_i}{s+a_i}$$

$\mathcal{F}^{-1}(s) \rightarrow A e^{-ait} u(t)$: if ROC is right of pole at $s=-a_i$
 $\mathcal{F}^{-1}(s) \rightarrow -A e^{-ait} u(-t)$: if ROC is left of pole at $s=-a_i$

Geometric evaluation of F.T. from pole-zero plot

$$X(s) = s-a \quad (\text{one zero})$$

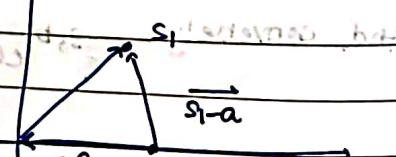
$$\swarrow$$

$$s = s_1 \rightarrow s_1 - a$$

$$s_1 - a : \text{zero at } s=a$$

$$s_1 + (-a) \rightarrow s_1 \downarrow$$

$$\text{if } X(s) = \frac{1}{s-a} \rightarrow \text{deno. by the same vector sum of } s_1 + (-a)$$



Property 8

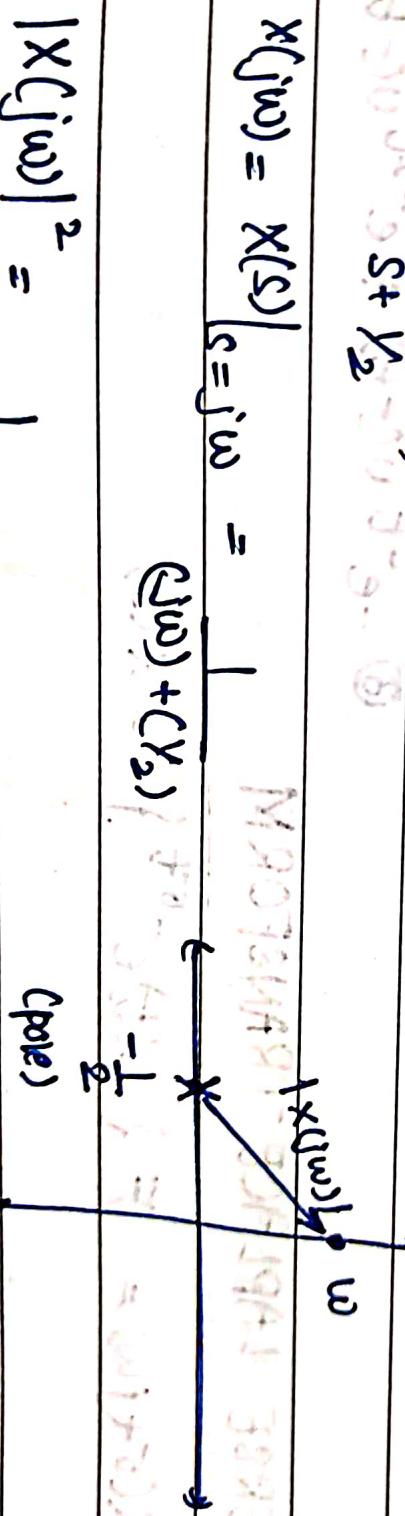
rational L.T. : $x(s) = M \frac{\prod_{i=1}^R (s-\beta_i)}{\prod_{j=1}^P (s-\alpha_j)}$

$x(s)$ at $s=s_1$: each term in product is a vector from the co

zero or the pole to the point s_1 .

$$x(s) = \frac{M}{(s-\alpha_1)(s-\alpha_2)\dots(s-\alpha_P)} \quad \text{Re}(s) > -\gamma_2$$

$x(jw) = x(s)|_{s=jw}$



$$|x(jw)|^2 = \frac{1}{w^2 + (\frac{1}{2})^2}$$

$$x(jw) = -\tan^{-1}(2w)$$