



NIMRA IDRIS SIDDIQUI

17 EEB 409

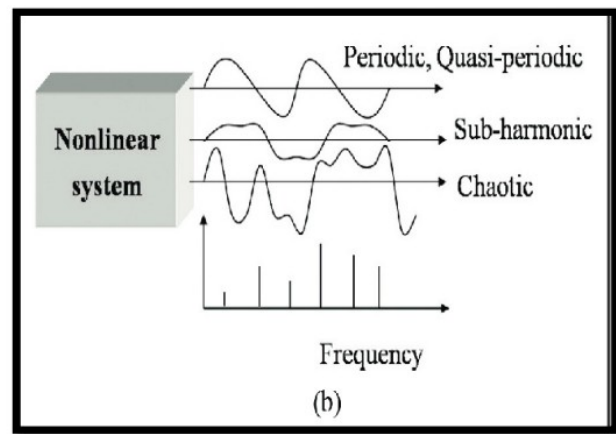
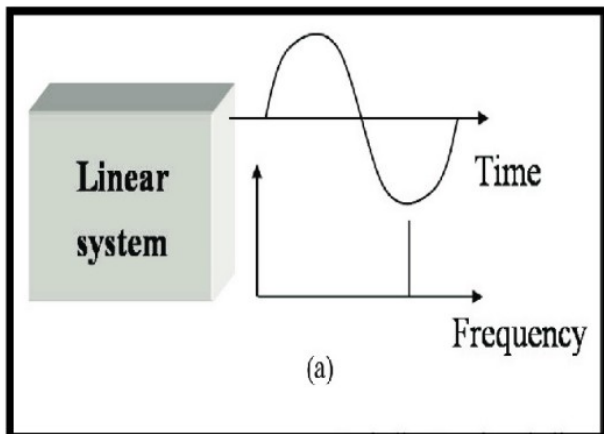
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SUBMITTED TO:

DR. MOHD RIHAN

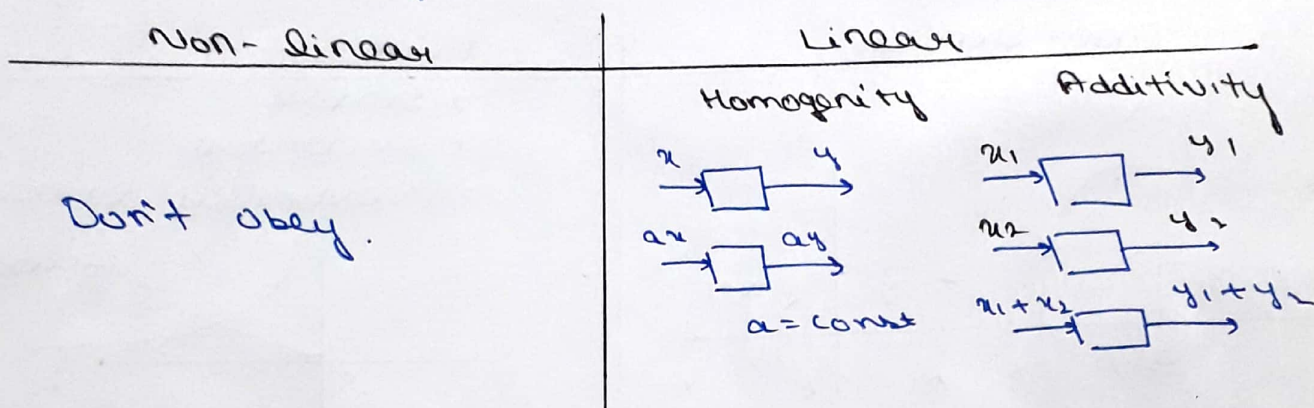
ASSIGNMENT-1



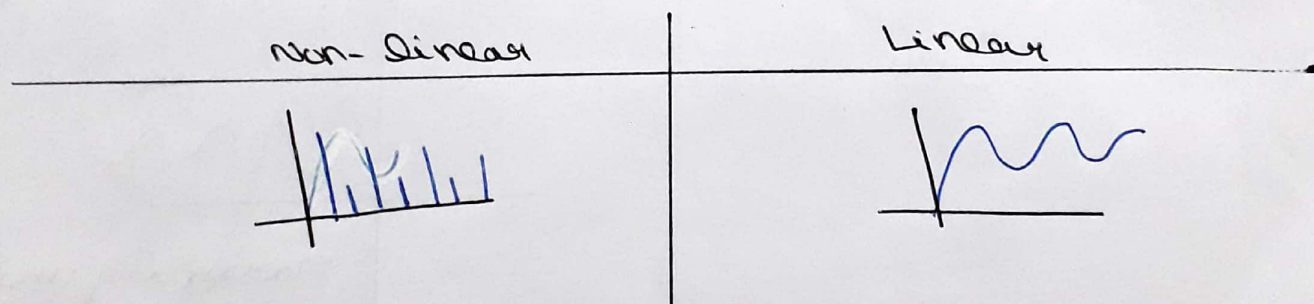
(1)

Q1 Explain the characteristic phenomena of non-linear system which makes it different from a linear system.

→ (1) The non-linear system don't follow the principle of superposition i.e homogeneity & additivity while linear system follow.



(2) Non-linear have discrete time while linear have continuous time



(3) non-linear have finite escape time i.e at finite interval of time system goes out of hand while linear control sys. have infinite time.

④

NLCs have multiple equilibrium points
i.e. $x_i = f(x_i)$, $x(0) = x^*$, $x(t) = x^*$

① which equilibrium pt. operate depend on initial condition

LCS have only one equilibrium pt

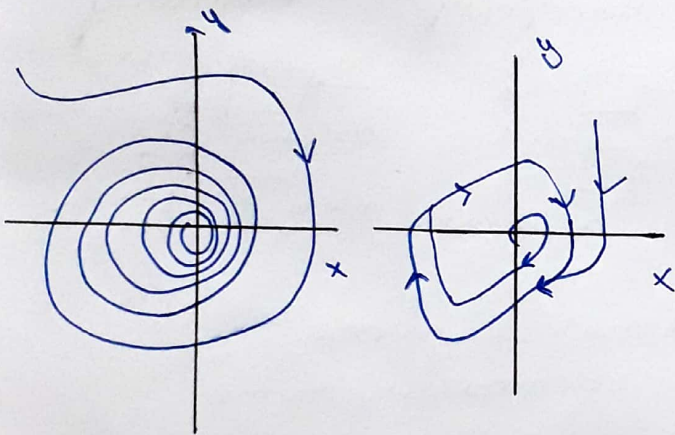
⑤

NLCs have limit cycle i.e.

→ sustained oscillation in NLCs independent of initial condition.

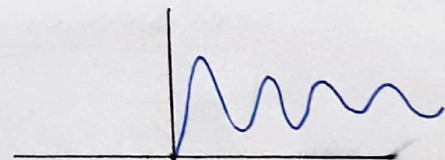
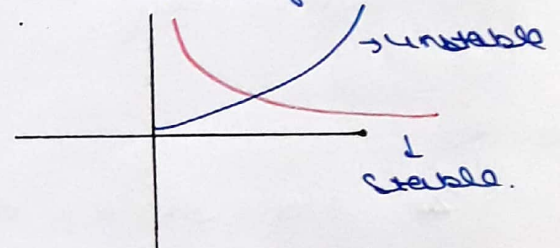
→ much more common in practical

Non-Linear



Linear

→ Stable
→ unstable
→ Marginally unstable.



Marginally unstable.

Amplitude of these oscillation depends on the initial conditions since

⑥

subharmonic, harmonic, or almost periodic oscillation.

A non linear system can oscillate with frequencies which are submultiple or multiples of its freq. It may generate an almost -

② Periodic oscillation, i.e. sum of periodic oscillations with frequencies which are not multiples of each other.

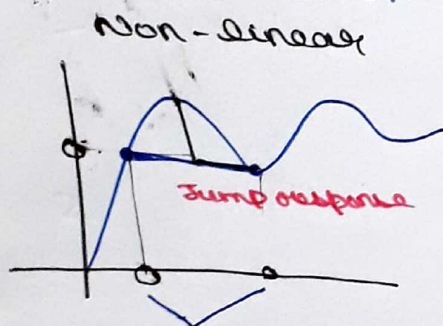
→ A stable linear system under a periodic i/t produces an o/t of same freq.

⑦ Jump response & multimodes of behaviour.

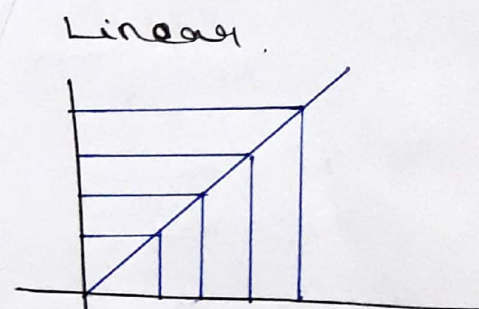
→ In NLS have multimode of behaviour.

→ NLS with increasing input, output may increase, decrease or remain same.

→ In LLS when input inc. output also increase, also when i/t dec, o/t also dec.



2 i/t may have
1 o/t



unique i/t
unique o/t

Q2 The analysis of non-linear system is different as compare to linear systems why!

Linear system →

The analysis of the L.S is done by two method

- ① State space
- ② Transfer function.

The analysis of non linear system is different from linear system because

- ① In NLS functionally output of system is not proportional to input of system
- ② In NLS there is a presence of non-linearity comes from physical limitation of the component involved.

For a non-linear system output increase up to certain limit after it become constant

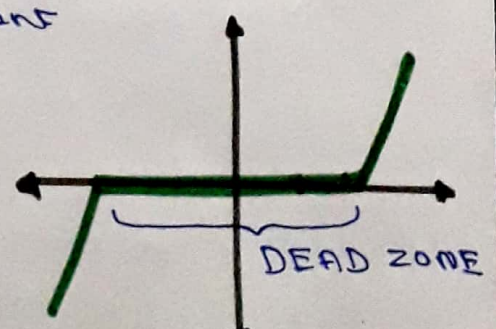
① it doesn't response to input when it reaching to saturation.

This is because types of Non-linearity Present

- ① Incidental \rightarrow present in system naturally
- ② Intentional \rightarrow Introduced artificially by an Engineer or designer to achieve certain objective

\Rightarrow Incidental non linearity comes from

- ① Saturation - Incidental.
- ② Dead Zone - It is the range of input where no output is present



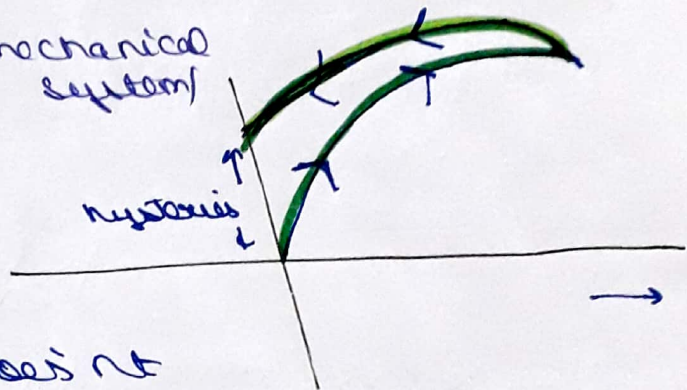
After dead zone system may respond to I/T

Due to dead zone system is NLS

3. friction $\left\{ \begin{array}{l} \text{Coulomb's fric.} \\ \text{static fric.} \end{array} \right.$

4. Backlash (mechanical system)

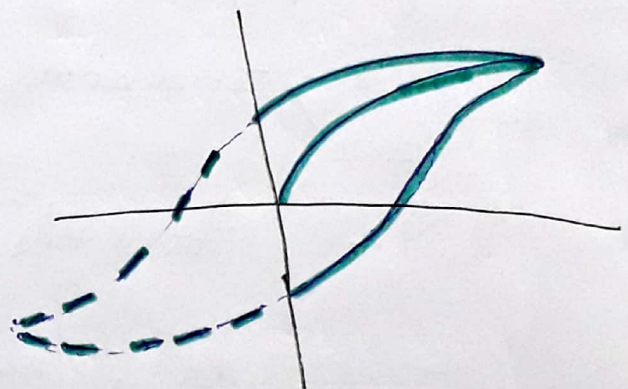
Applying mag. force.
flux is produce.



⇒ Backward curve doesn't follow forward curve

Energy supply in forward dir not ^{completely} recovered in backward dir

forward char \neq backward char.

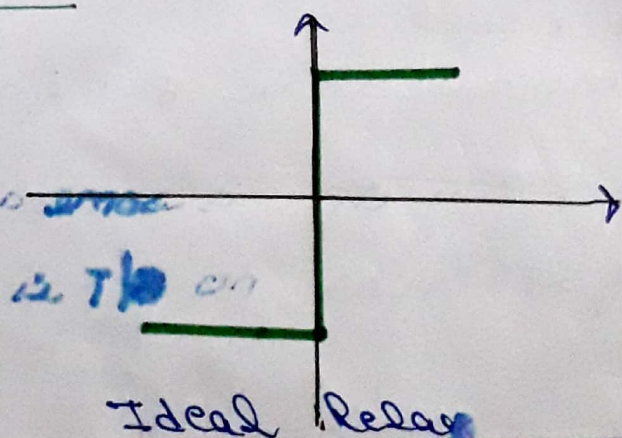


Hysteresis loss (dec. sys.)

Intentional NL

Relay

like as switch



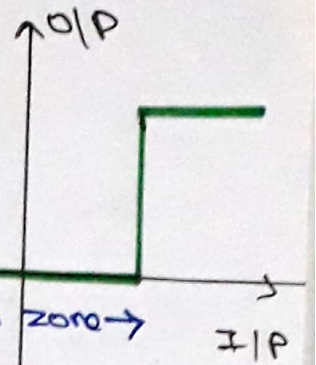
combination →

of 2 N.L i.e. dead zone + Relay

↓
incidental NL

intentional L

Relay with dead zone.

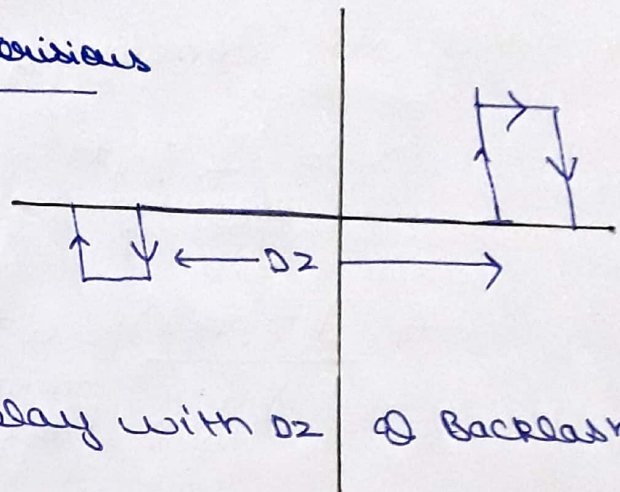


Relay + dead zone + hysteresis

incidental NL

Relay & dead zone
can consider 1.

Relay with DZ & Backlash



NLC S → NL → naturally
introduce
combination of NL

Analyzing NLS

1) Linearization

→ Developing an approximate linear model for the NL system

$\dot{x} = f(x, u, t) \rightarrow$ General mathematic of control sys
 $\dot{x}(t) = Ax(t) + bu(t) \rightarrow$ Linear time sys

NON - LINEAR SYSTEM

(4)

The analysis of NLS is by linearization

Linear approximation of non-linear Mathematical model \rightarrow

To obtain a linear mathematical model for a NLS,

consider a system where $i(t)$ is $u(t)$
 $O(t) = y(t)$

The relationship b/w $y(t)$ & $u(t)$ is given by

$$y = f(u) \quad \text{--- (1)}$$

Eqn (1) is expanded into Taylor series

$$y = f(u)$$

$$y = f(\bar{u}) + \frac{\partial f}{\partial u}(u - \bar{u}) + \frac{1}{2!} \frac{\partial^2 y}{\partial u^2}(u - \bar{u})^2 + \dots \quad \text{--- (2)}$$

where the derivatives

$$\frac{\partial y}{\partial u}, \frac{\partial^2 y}{\partial u^2} \text{ are evaluated at } u = \bar{u}.$$

Eqn (2) can be written as (neglect the infinite order terms in $u - \bar{u}$)

$$y = \bar{y} + K(u - \bar{u}) \quad \text{--- (3)}$$

$$\text{where, } \bar{y} = y(\bar{u})$$

$$K = \left. \frac{\partial y}{\partial u} \right|_{u=\bar{u}}$$

Above eqn can also be written as

$$y - \bar{y} = K(u - \bar{u}) \quad \text{--- (4)}$$

★

$$\dot{x} = f(x, u, t) \rightarrow \text{non-linear eqn}$$

TI

$$\dot{x} = f(x, u)$$

eq. pt. where $\dot{x} = 0$

imp. b/c linearization is around eq^m pt.

$$f(x_e, u_e) = 0$$

→ How to linearize non linear system?

$$\dot{x} = f(x^*, u^*) + \frac{\partial f(x, u)}{\partial x} \bigg|_{x=x^*, u=u^*} x^* + \frac{\partial f(x, u)}{\partial u} \bigg|_{x=x^*, u=u^*} u^* + \text{higher order term}$$

$$- f(x^*, u^*)$$

let the perturbation or variation is small
[valid only around the eq^m pt.]

⇒ H.O.T may be neglected

$$\dot{x}^* = \frac{\partial f(x, u)}{\partial x} \bigg|_{x=x^*, u=u^*} x^* + \frac{\partial f(x, u)}{\partial u} \bigg|_{x=x^*, u=u^*} u^*$$

let assume sys. is of 2nd order
 x_1, x_2

$$\dot{x}_1^* = \frac{\partial f_1}{\partial x_1} \bigg|_{x_1=x_1^*, x_2=x_2^*, u=u_1^*, u_2=u_2^*} x_1^* + \frac{\partial f_1}{\partial x_2} \bigg|_{x_1=x_1^*, x_2=x_2^*, u=u_1^*, u_2=u_2^*} x_2^* + \frac{\partial f_1}{\partial u_1} \bigg|_{x_1=x_1^*, x_2=x_2^*, u=u_1^*, u_2=u_2^*} u_1^* + \frac{\partial f_1}{\partial u_2} \bigg|_{x_1=x_1^*, x_2=x_2^*, u=u_1^*, u_2=u_2^*} u_2^*$$

$$+ \frac{\partial f_1}{\partial u_1} \bigg|_{u_1^*} + \frac{\partial f_1}{\partial u_2} \bigg|_{u_2^*}$$

$$\dot{x}_2 = \frac{\partial f_2}{\partial u_1} \bigg|_{\substack{u_1=u_1^*, u_2=u_2^* \\ u_1=u_1^*, u_2=u_2^*}} + \frac{\partial f_2}{\partial u_2} \bigg|_{u_2^*}$$

$$+ \frac{\partial f_2}{\partial u_1} \bigg|_{u_1^*} + \frac{\partial f_2}{\partial u_2} \bigg|_{u_2^*}$$

$$\begin{bmatrix} \dot{x}_1^* \\ \dot{x}_2^* \end{bmatrix} = \begin{bmatrix} \frac{\partial f_1}{\partial u_1} & \frac{\partial f_1}{\partial u_2} \\ \frac{\partial f_2}{\partial u_1} & \frac{\partial f_2}{\partial u_2} \end{bmatrix} \begin{bmatrix} u_1^* \\ u_2^* \end{bmatrix} + \begin{bmatrix} \frac{\partial f_1}{\partial u_1} & \frac{\partial f_1}{\partial u_2} \\ \frac{\partial f_2}{\partial u_1} & \frac{\partial f_2}{\partial u_2} \end{bmatrix} \begin{bmatrix} u_1^* \\ u_2^* \end{bmatrix}$$

$$\dot{x}(t) = A^* x^*(t) + B^* u^*(t)$$

$$\begin{bmatrix} \frac{\partial f_1}{\partial u_1} & \frac{\partial f_1}{\partial u_2} \\ \frac{\partial f_2}{\partial u_1} & \frac{\partial f_2}{\partial u_2} \end{bmatrix} \text{ defined as eqn pt.}$$

Called Jacobian responsible of converting
N.L. sys into linear sys.

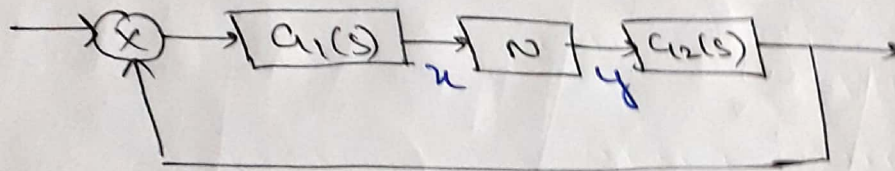
DESCRIBING FUNCTION -

- filtering effect will be significant
- neglect the harmonics
- ~~Re~~ Linearized →

2 Requirement

- 1) no. of LC \gg no. of NLS
 - 2) I/T should be sinusoidal
- Describing func. is used as linearization technique

Having 2 requirements



$$x = X \sin \omega t$$

$$y = A_0 + A_1 \sin \omega t + B_1 \cos \omega t + A_2 \sin 2\omega t + B_2 \cos 2\omega t + \dots$$

If y is symmetrical $\rightarrow A_0 = 0$
B/c of LPF of G_1 & G_2

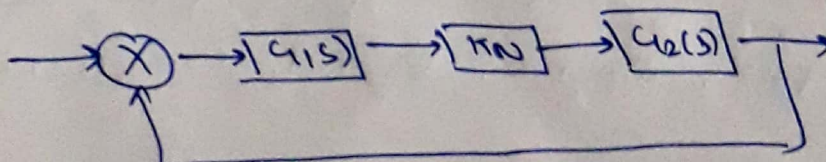
$$y = A_1 \sin \omega t + B_1 \cos \omega t$$

$$y = Y_1 \sin(\omega t + \phi)$$

$Y_1 \rightarrow$ peak of y $\phi \rightarrow$ phase diff
 $X =$ peak of x

Describing func.

$$KN = \frac{Y_1}{X} \angle \phi$$



Describing fun in NLS = Tlf func. L.C.

$$A_1, B_1$$

$$Y_1 = \sqrt{A_1^2 + B_1^2}$$

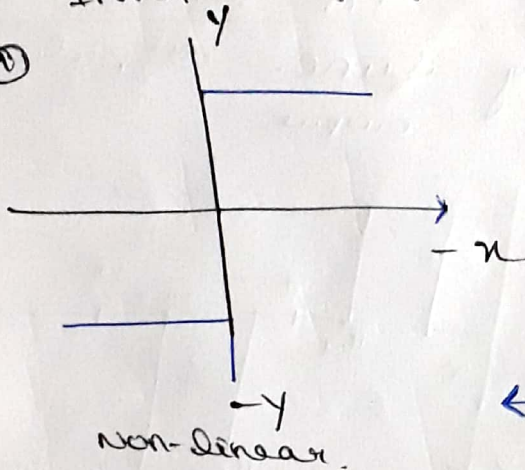
$$\Phi = \tan^{-1} \frac{A_1}{B_1}$$

$$A_1 = \frac{2}{\pi} \int_0^{2\pi} y(t) \sin \omega t \, d\omega t$$

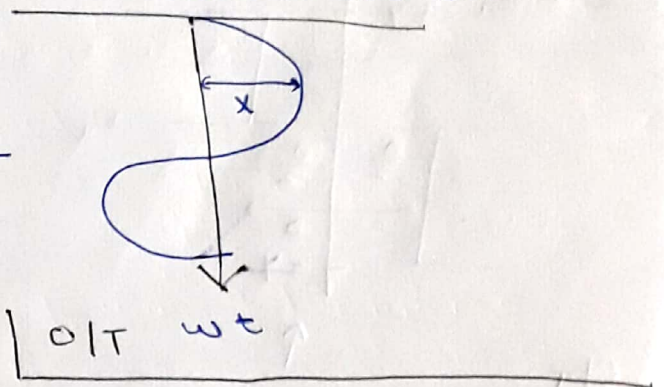
$$B_1 = \frac{2}{\pi} \int_0^{\pi} y(t) \cos \omega t \, d\omega t$$

Describing func. of an Ideal Relay

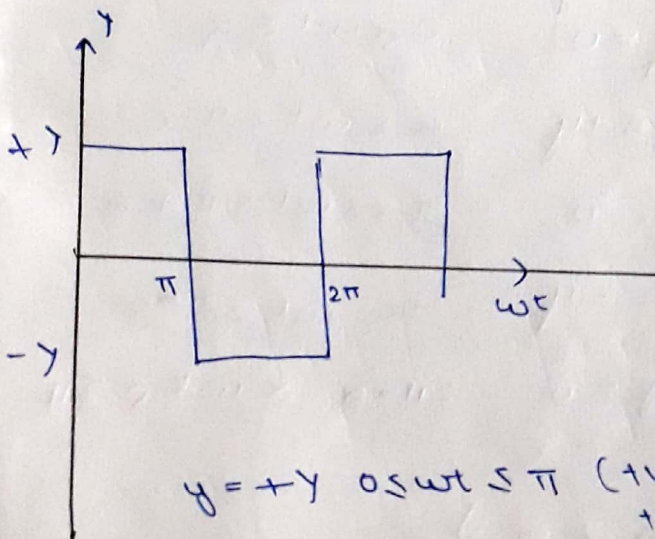
①



Apply purely sinusoidal wave to the i/t



OUTPUT



$y = +y$ $0 \leq \omega t \leq \pi$ (true for +ve cycle)
 $y = -y$ $\pi \leq \omega t \leq 2\pi$ (-ve for -ve cycle)

$$A_1 = \frac{2}{\pi} \int_0^{\pi} y \cos \omega t \, d\omega t = 0$$

$$B_1 = \frac{2}{\pi} \int_0^{2\pi} y \sin \omega t \, d\omega t$$

$$= \frac{2}{\pi} [-y \cos \omega t]_0^{\pi}$$

$$= \frac{4y}{\pi}$$

$$Y_1 = \sqrt{A_1^2 + B_1^2}$$

$$= \frac{4y}{\pi}$$

$$\phi = \tan^{-1} \frac{A_1}{B_1} = 0$$

$$KN = \frac{Y_1}{X} \angle \phi$$

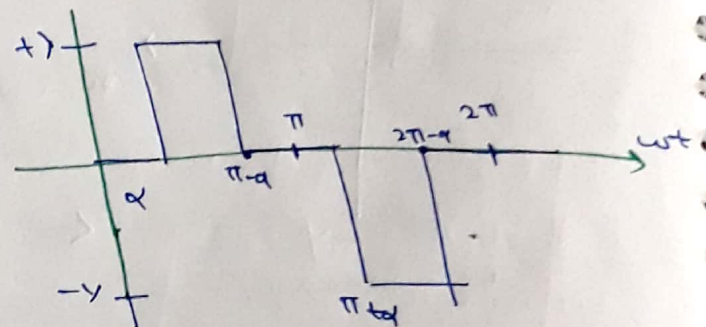
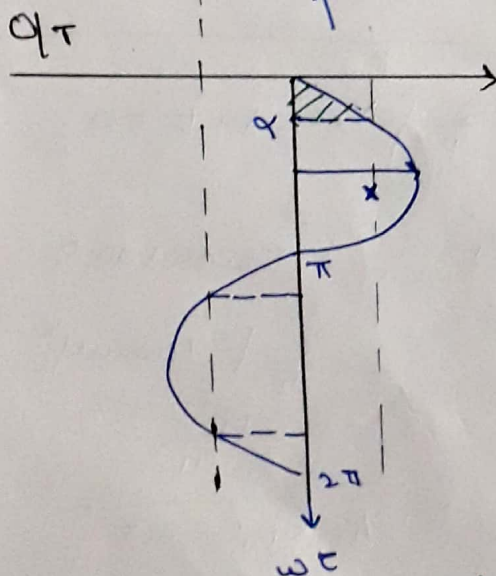
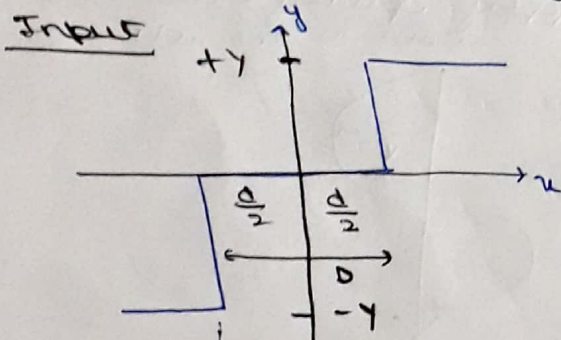
$$KN = \frac{4Y}{\pi X} \angle 0 \rightarrow \text{Ideal relay}$$

$$KN(X, \omega) = \frac{4Y}{\pi X} \angle 0$$

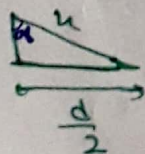
Describing func depend on

$X =$ amplit. of i/t $\left\{ \begin{array}{l} \therefore \text{describing func} \\ \omega = \text{freq. of i/t} \end{array} \right.$ is different from T/f func.

Q3 Determine describing func. of relay with a dead zone



$y = 0$	$0 \leq \omega t \leq \alpha$
$y = +Y$	$\alpha \leq \omega t \leq \pi - \alpha$
$y = 0$	$\pi - \alpha \leq \omega t \leq \pi + \alpha$
$y = -Y$	$\pi + \alpha \leq \omega t \leq 2\pi - \alpha$
$y = 0$	$2\pi - \alpha \leq \omega t \leq 2\pi$



$$\sin \alpha = \frac{d}{2X}$$

$$A_1 = \frac{2}{\pi} \int_{\alpha}^{\pi-\alpha} Y \cos \omega t d\omega t = 0$$

$$B_1 = \frac{2}{\pi} \int_{\alpha}^{\pi-\alpha} Y \sin \omega t d\omega t$$

$$= \frac{2Y}{\pi} (\cos \omega t)_{\pi-\alpha}^{\alpha} \Rightarrow \frac{2Y}{\pi} \cos \alpha - (-\cos \alpha)$$

$$B_1 = \frac{4Y \cos \alpha}{\pi}$$

$$\sin \alpha = \frac{d}{2x}, \quad \cos \alpha = \sqrt{1 - \left(\frac{d}{2x}\right)^2}$$

$$= \sqrt{\frac{x^2 - \left(\frac{d}{2}\right)^2}{x^2}}$$

$$\text{Let } \frac{d}{2x} = m$$

$$B_1 = \frac{4Y}{\pi} \sqrt{1-m^2}$$

$$\phi = \tan^{-1} \frac{A_1}{B_1} = 0$$

$$K_n(\alpha, \omega) = \frac{Y_1 \angle \phi}{x} \Rightarrow \frac{4Y \cos \alpha}{\pi x}$$

$$Y_1 = \sqrt{A_1^2 + B_1^2} \Rightarrow \sqrt{0 + \left(\frac{4Y \cos \alpha}{\pi}\right)^2}$$

$$Y = B_1$$

$$Y_1 = \frac{4Y \cos \alpha}{\pi} \text{ or } Y_1 = \sqrt{0^2 + \left(\frac{4Y \sqrt{1-m^2}}{\pi}\right)^2}$$

$$K_n(\alpha, \omega) = \frac{4Y \sqrt{1-m^2} \angle 0}{\pi x}$$

$$Y_1 = \frac{4Y}{\pi} \sqrt{1-m^2}$$

$$K_n(\alpha, \omega) = \frac{4Y}{\pi x} \sqrt{1 - \frac{d^2}{(2x)^2}} \angle 0 \quad \text{--- (3)}$$

Equation (3) is the describing function of a relay with deadzone & saturation.