# Carburisation by CO<sub>2</sub>?

**David Young** 



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#### **REACTION WITH CO<sub>2</sub>**

Alloys: Fe-9Cr, P91, P92

Gas: Ar-20CO<sub>2</sub>

T: 650°C

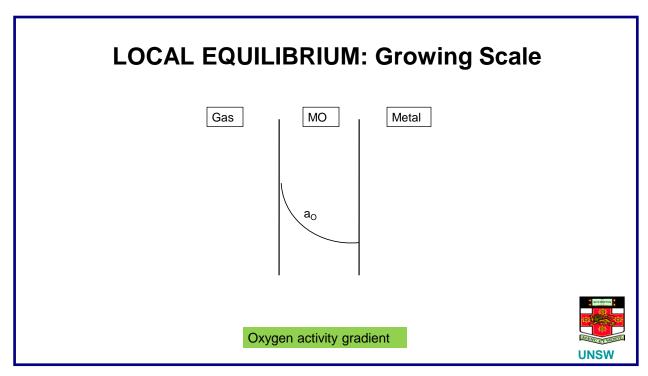
 $p_{O_2}$ = 10<sup>-7</sup> atm,  $a_C$  = 10<sup>-15</sup>

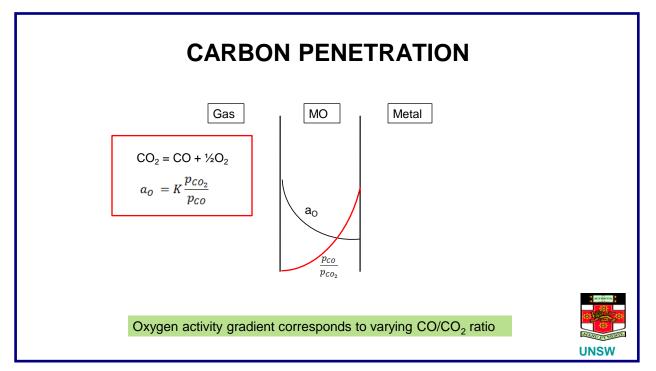
 $7\underline{Cr} + 3\underline{C} = Cr_7C_3$ 

For 9 Cr steel, need  $a_{Cr} \sim 10^{-2}$ 

The required carbon activity is 10<sup>13</sup> times higher than the gas can provide!







#### **CARBON PENETRATION**

Gas

 $CO_2 = CO + \frac{1}{2}O_2$ 

 $a_O = K \frac{p_{CO_2}}{p_{CO}}$ 

MO

Metal

 $2CO = CO_2 + C$ 

 $a_C = K \frac{p_{CO}^2}{p_{CO_2}}$ 

Oxygen activity gradient corresponds to varying CO/CO<sub>2</sub> ratio

 $p_{CO_2}$ 

 $\mathbf{a}_{\text{O}}$ 



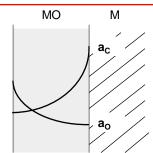
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#### **CARBON PENETRATION II**

$$2CO = CO_2 + C$$

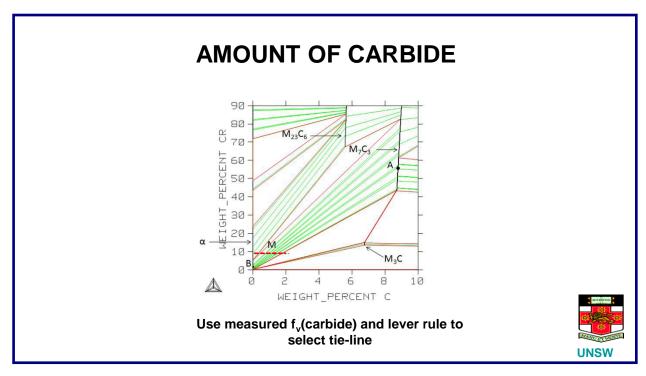
$$a_C = K \frac{p_{CO}^2}{p_{CO}}$$

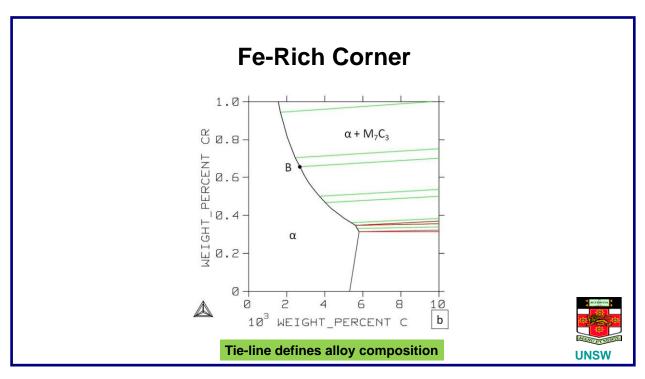
Gas

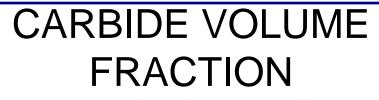


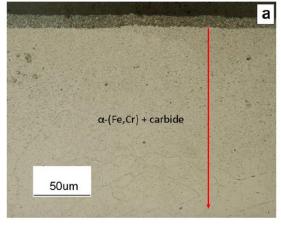
**CONCLUSION:** Carbon activity increased within/beneath oxide scale



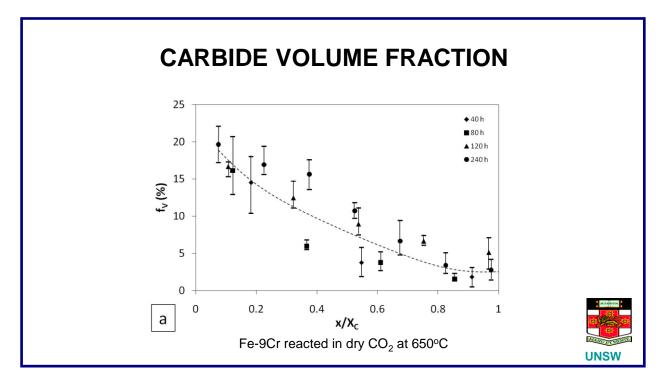












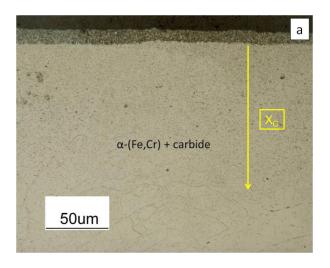
# TEST $a_{C}$ CALCULATION

Method	a <sub>C</sub>
Scale-alloy Equilibrium	0.47
From measured f <sub>V</sub>	0.43



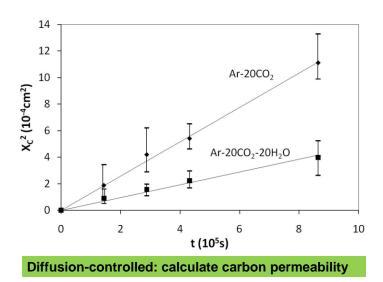
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#### **CARBURISATION KINETICS**











#### **CARBON PERMEABILITY**

$$X_C^2 = 2k_p t$$

$$k_p = \varepsilon \frac{N_C^{(s)} D_C}{\nu N_{Cr}^{(0)}}$$

$$N_C^{(s)}D_C = 6.5 \times 10^{-11} \text{ cm}^2 \text{ s}^{-1}$$

Use independently measured  $\mathbf{D}_{\mathbf{C}}$  to calculate  $\mathbf{N}_{\mathbf{C}},$  hence  $\mathbf{a}_{\mathbf{C}}$ 



## **VERIFY a<sub>C</sub> CALCULATION**

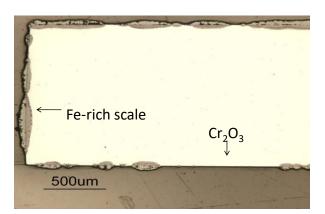
Method	$a_{C}$
Scale-alloy Equilibrium	0.47
From measured $f_V$	0.43
From carburisation rate	0.25

CONCLUSION: Carbon beneath oxide scale supersaturates with respect to gas, but represents local equilibrium



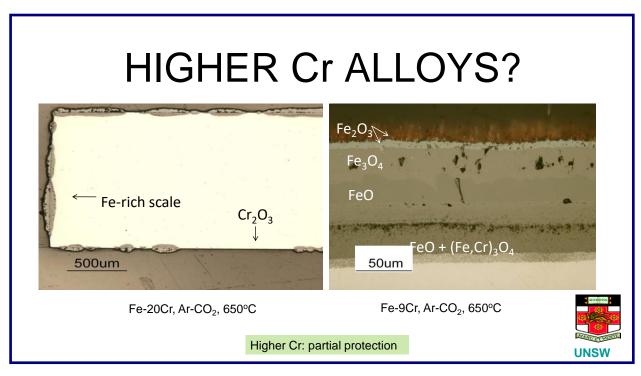
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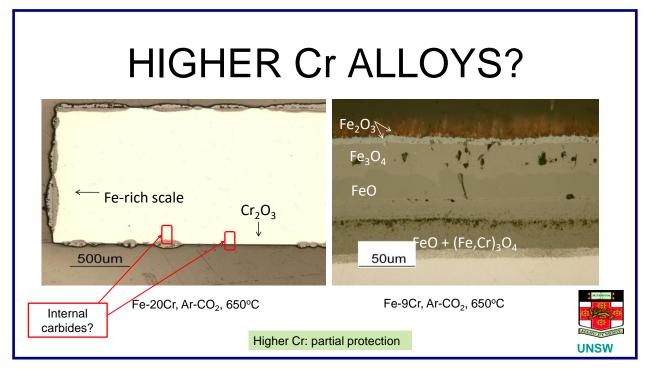
# HIGHER Cr ALLOYS?



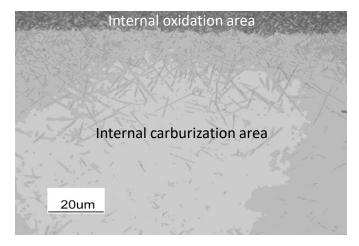
Fe-20Cr, Ar-CO<sub>2</sub>, 650°C







#### Carbides in Fe-20Cr at 650°C

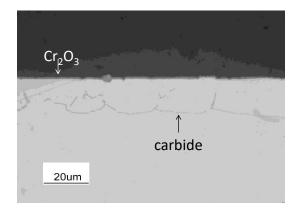


Under iron-rich oxide nodule



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## Carbides in Fe-20Cr at 650°C



Under chromia scale



# IINTERFACE a<sub>C</sub> UNDER Cr<sub>2</sub>O<sub>3</sub>

Method  $a_{C}(Dry)$ 

FeO-alloy Equilibrium 0.47

Cr<sub>2</sub>O<sub>3</sub>-alloy Equilibrium >10<sup>4</sup>

From measured  $f_V$  0.1

From carburisation rate 0.01

CONCLUSION: Oxide scale provides partial, transient protection against carburisation



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#### How Does C Penetrate Oxide Scale?

#### BACKGROUND KNOWLEDGE

- Diffusion of Cr or O in Cr<sub>2</sub>O<sub>3</sub> along grain boundaries
- C is "insoluble" in Cr<sub>2</sub>O<sub>3</sub>
- PROPOSAL: C moves via oxide grain boundaries



# Atom Probe Tomography

Mill very fine tips from oxide

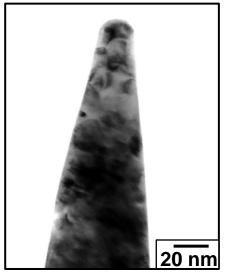
Cr<sub>2</sub>O<sub>3</sub> scale

Alloy



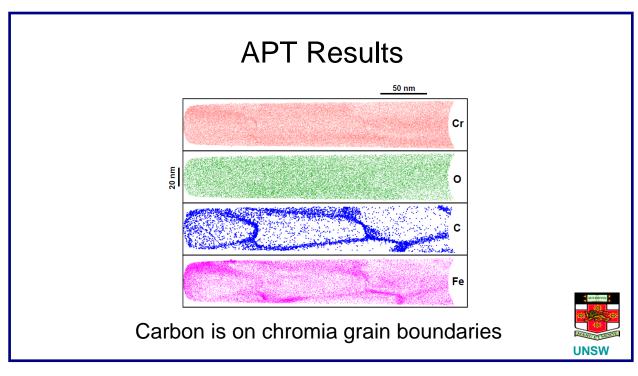
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#### FIB MILLED TIP FOR ATOM PROBE



Bright field TEM view





# CO<sub>2</sub> Corrosion of 9Cr Steels: Questions

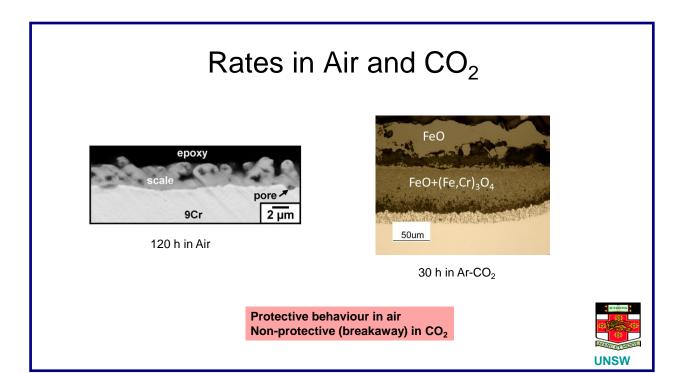
What is the rate compared with air oxidation? Why is the oxide scale in two layers? Why is the interface between them at the former steel surface?

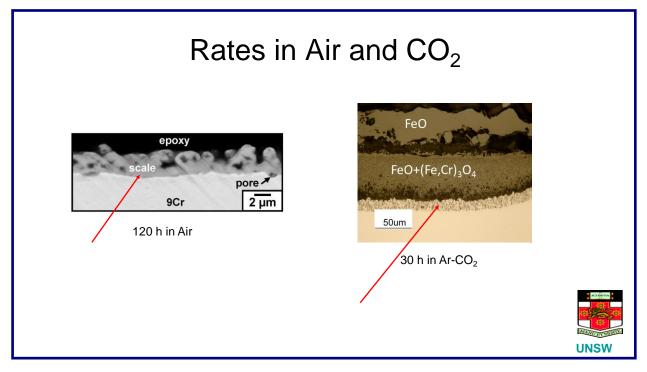
What transports across the scale, metal or oxygen? What controls the scaling rate?

> Why does internal carburisation occur? How fast is it, and what controls its rate?



UNSW





#### External or Internal Cr Oxide

$$N_{\rm Cr}\left({\rm crit}\right) = \left(\frac{\pi_g N_0^s D_0 V_{\rm m}}{{}_{3D_{\rm Cr}} V_{\rm OX}}\right)^{1/2}$$

Same alloy, same T, but:

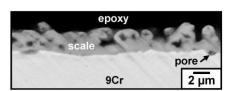
 $N_{\text{Cr}}$ 

 $N_{Cr}$ 

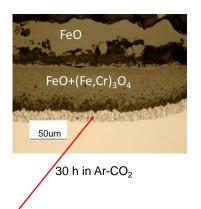


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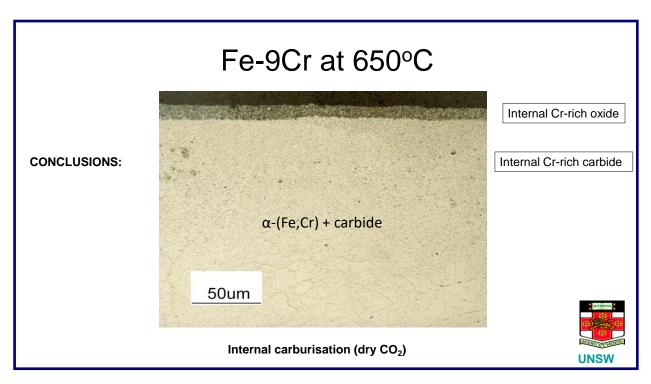
# Rates in Air and CO<sub>2</sub>

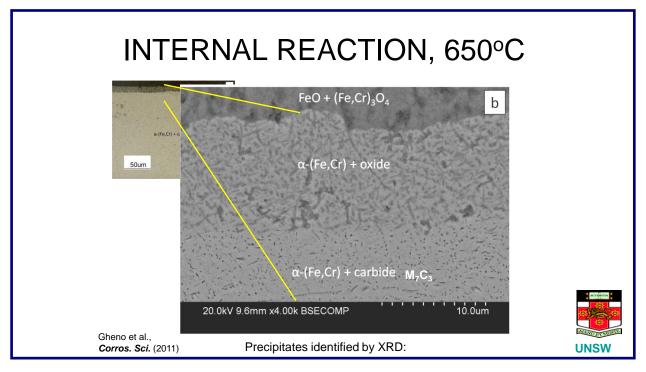


120 h in Air

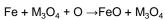




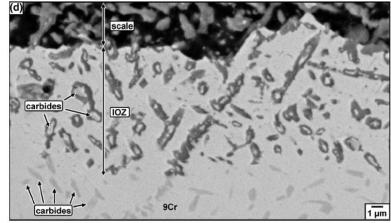








 $M_7C_3 + \underline{O} \rightarrow M_3O_4 + \underline{C}$ 



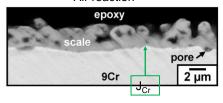
Carbides oxidised in place; Cr-rich oxides end up in inner scale



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# Explains why 9Cr alloy nonprotective in $CO_2$

Air reaction

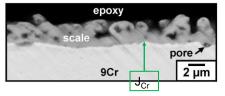


Enough Cr to diffuse to surface and form:

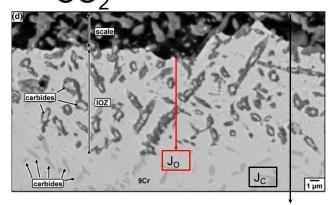


# Explains why 9Cr alloy nonprotective in

Air reaction



Enough Cr to diffuse to surface and form: External Cr-rich scale



- Fast inward C diffusion
- C reacts with:
- Result:
- Consequence:



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## CO<sub>2</sub> Corrosion of 9Cr Steels: Questions

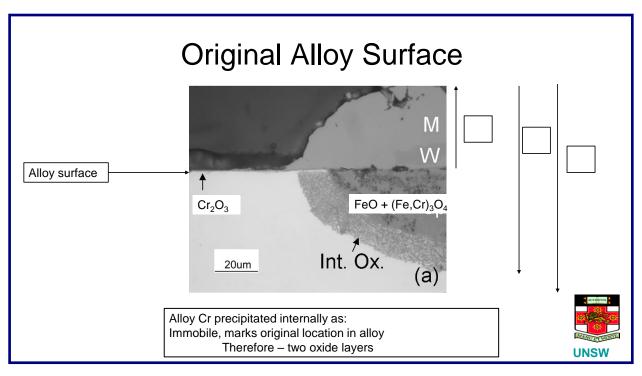
What is the rate compared with air oxidation? ok Why is the oxide scale in two layers? Why is the interface between them at the former steel surface?

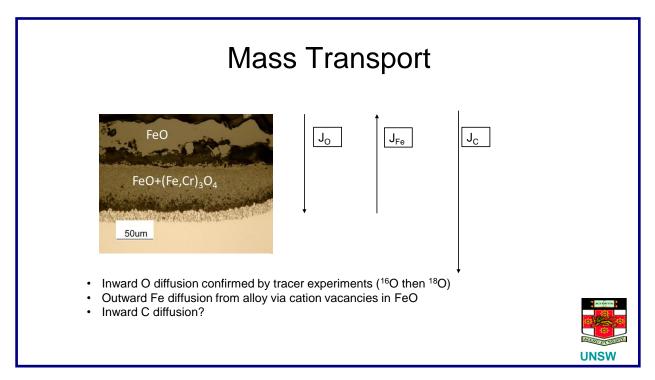
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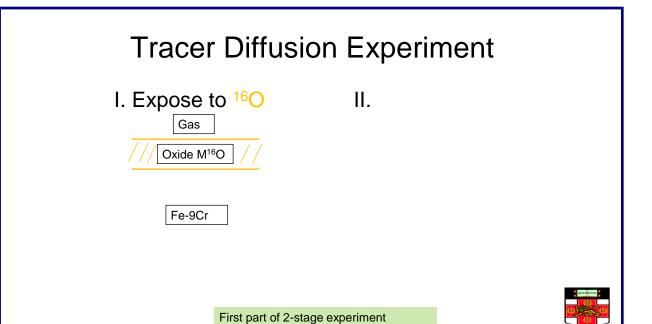
> Why does internal carburisation occur? How fast is it, and what controls its rate?

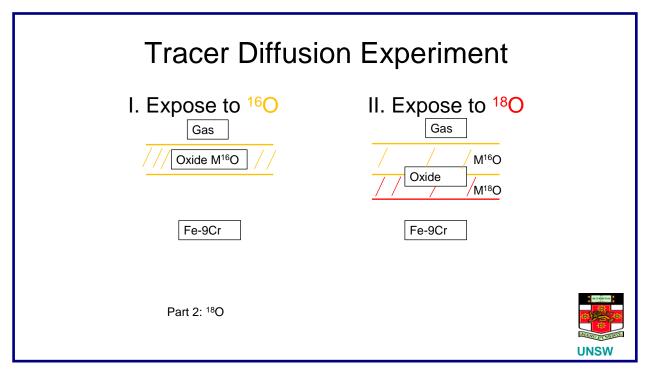


**UNSW** 

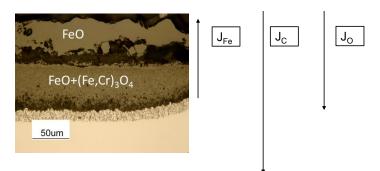








# Mass Transport Mechanisms

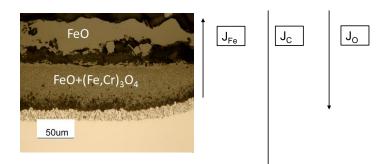


- Inward O diffusion confirmed by tracer experiments (<sup>16</sup>O then <sup>18</sup>O)
- · Outward Fe diffusion from alloy via cation vacancies in FeO
- · Inward C diffusion?



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# Mass Transport Mechanisms



- · Outward Fe diffusion from alloy via cation vacancies in FeO
- Inward C diffusion?
- · Inward O diffusion?



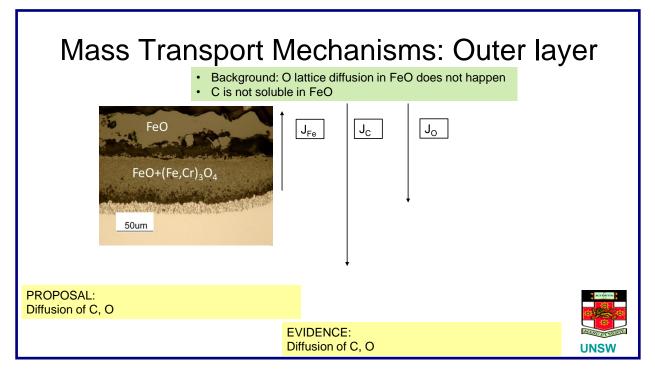
# Mass Transport Mechanisms: Outer layer FeO+(Fe,Cr)<sub>3</sub>O<sub>4</sub> J<sub>Fe</sub> J<sub>C</sub> J<sub>O</sub>

- Background: O lattice diffusion in FeO does not happen
- · C is not soluble in FeO

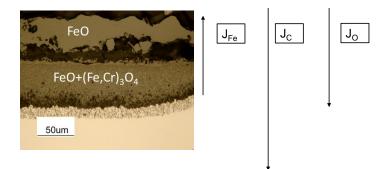
50um



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# Mass Transport Mechanisms: Inner Layer



Inner layer is fine-grained, 2-phase and porous



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# CO<sub>2</sub> Corrosion of 9Cr Steels: Questions

What is the rate compared with air oxidation? OK

Why is the oxide scale in two layers?

Why is the interface between them at the former steel surface?

What transports across the scale, metal or oxygen?

What controls the scaling rate?

Why does internal carburisation occur?

How fast is it, and what controls its rate?

OK





# **Next Time**

Alloy design to resist CO<sub>2</sub> attack

