

ES3J1 Group 3 Report

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Question 1

The output produced by the motor is not smooth, so to obtain its model that can be analysed using control system theory, a filter needs to be designed.

The filter (and thus, the model) tuning was done according to the brief. The process followed the steps outlined below:

1. The filter coefficient was set to the simplest low-pass transfer function $\frac{1}{0.1s+1}$ to start smoothing the motor output, obtained by applying the step input. An example filter performance is shown in *Figure 1*.

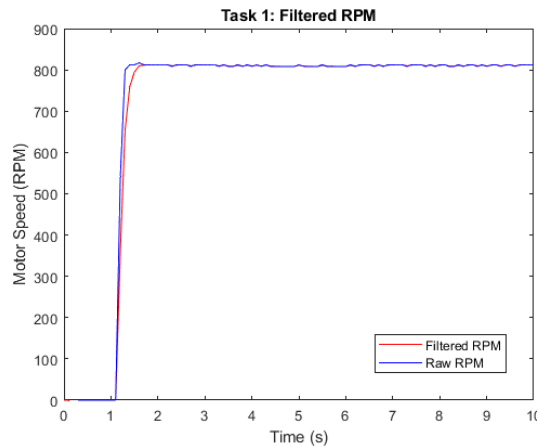


Figure 1: Low-pass filter's impact on the signal.

2. The motor circuit, as set up in the brief, was assembled; the motor and Arduino were connected to the circuit and a link was established to the Simulink workspace.
3. The motor was run using the MATLAB hardware add-on. The signal could be traced as going from the workspace input, through the PWM converter block and into the Arduino. The PWM signal generated by the Arduino then propagated through the circuit to power the motor, which had its encoder linked to the Arduino – this signal was then converted into motor revolutions per minute (RPM) in the workspace and the obtained results were designated as the output. The input into the system and the output of the motor (in RPM) was saved to the workspace for further analysis.
4. System Identification Toolbox (SIT) was used, with the input being the signal prior being processed by the PWM block and the output being the motor's RPM.
5. In SIT the analysis was set for the transfer function to have no zeroes and one pole – this was identified by inspection, using the unfiltered transfer function output, as the step input produced a first order response.
6. The obtained transfer function was scaled by dividing both the numerator and the denominator by the step time ($T_s = 0.1$).

7. The obtained transfer function was plotted against the unfiltered motor output to verify the model accuracy. If proven significantly inaccurate, the design process was repeated until a fitting filter that produced a smooth transfer function was obtained.

The resulting transfer function's step response is shown in *Figure 2* (titled as "Computed (SIT)").

An alternative method for tuning the transfer function was also explored, as the steady state value of the produced function did not exactly match the motor output on the graph. The new tuning approach was found in [1] and was executed in the following steps:

1. Steps 1-3 were repeated from the previous method: a simple low-pass filter was set up, the motor circuit was assembled and the motor response to a step input was saved to the workspace.
2. Find the maximum gain reached by the output. This is regarded as the absolute – or steady state – gain. The value recorded was 834.
3. The time constant for the response was calculated. This was defined as the time to reach 63.2% of the steady-state value. In this case, a value of 528.76 RPM needed to be reached. The time to reach this value was calculated to be 1.185s. As the step was applied at $t = 1$ s, the time constant was therefore $\tau = 1.185 - 1 = 0.185$ s.
4. Using the standard first order transfer function model:

$$G(s) = \frac{Y(s)}{X(s)} = \frac{K}{\tau s + 1}$$

and substituting the values calculated, a final transfer function was obtained:

$$G(s) = \frac{834}{0.185s + 1}$$

The resulting transfer function's step response is shown in *Figure 2* (titled as "Graphical").

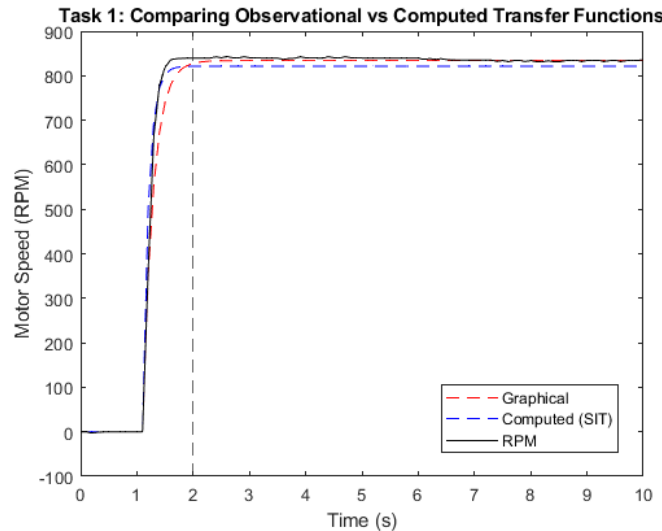


Figure 2: Step responses of transfer functions

The performance of the both functions were compared by calculating the mean-squared errors (MSEs) ϵ for each in a given timeframe:

- Transient-state error ($0 < t \leq 2$): the computed transfer function MSE was found to be $\epsilon_{ts-c} = 3.77 \times 10^4$, while the graphically-found transfer function's MSE was found to be $\epsilon_{ts-g} = 1.66 \times 10^4$. Overall, the MSE was 227% higher using the SIT-calculated transfer function than the graphically-calculated transfer function.

- Steady-state error ($t > 2$): the SIT-calculated transfer function's MSE during the steady-state operation was found to be $\epsilon_{ss-c} = 243.0$ and the graphically-found transfer function's MSE during steady-state operation was $\epsilon_{ss-g} = 17.6$. Overall, there was a 1381% increase in the MSE value of the SIT-calculated transfer function compared to the graphically-calculated transfer function.
- Overall error ($t > 0$): the total MSE for the SIT-calculated transfer function was $\epsilon_{T-c} = 3.94 \times 10^3$ while the overall MSE for the graphically-calculated transfer function was $\epsilon_{T-g} = 1.66 \times 10^3$. Overall, the total MSE was 237% larger for the SIT-calculated transfer function than for the graphically-generated function.

Having evaluated the errors, further tasks were performed using the graphically-generated transfer function, as it outperformed the SIT-generated function on every timeframe and better fit the specifications.

Upon observation of the motor function, the motor had a 0.1 second delay, thus the transfer function needed to be multiplied by $e^{-0.1s}$ to account for this delay.

The final design allowed for the produced output to be a smooth 1st order response, which enabled further analysis and tuning of the system in the subsequent tasks.

The open-loop Simulink model used to obtain the results discussed in this section is shown in *Figure 3*.

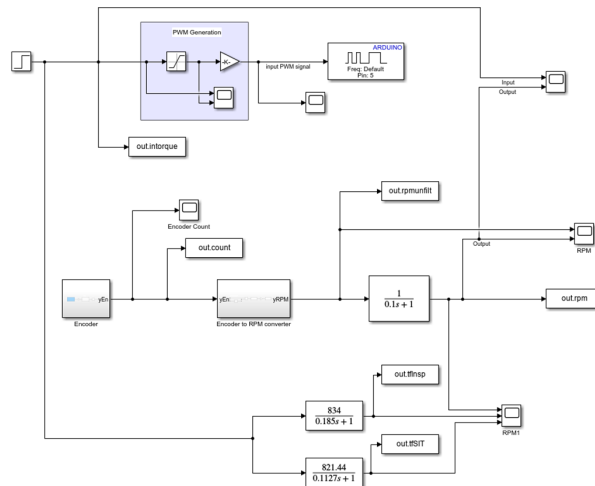


Figure 3: The model used to obtain the measures

Question 2

Using the transfer function obtained in Question 1, closed-loop analysis of the system was used to obtain the required constants for proportional-integral (PI) control. The Ziegler-Nichols method was chosen due to its ease of implementation.

An initial PI system was created with K_p and K_i both set to zero. K_p was slowly increased in increments of 0.001, until consistent oscillations were produced in response to a step input. At $K_p = 0.016$, constant oscillations occurred. The system response using the oscillatory K_p is shown in *Figure 4*.

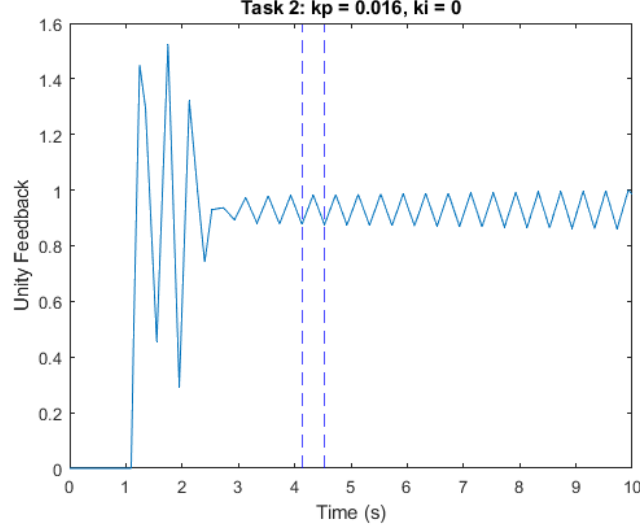


Figure 4: The oscillatory graph used in the Ziegler-Nichols tuning

The peak-to-peak time was measured to obtain the ultimate time period $P_u = 0.407$ s, giving an ultimate gain of $K_u = 0.016$.

The Ziegler Nichols tuning equations were applied to obtain the controller values of K_p and K_i . The response of the system using the calculated K_p and K_i is shown in Figure 5. An important consideration is that the produced K_i value produced unstable step responses, so it was scaled down by an order of magnitude of two to obtain a stable plot.

$$K_p = 0.45 * K_u = 0.45 * 0.016 = 0.0072$$

$$K_i = 0.83 * P_u = 0.83 * 0.407459 = 0.338$$

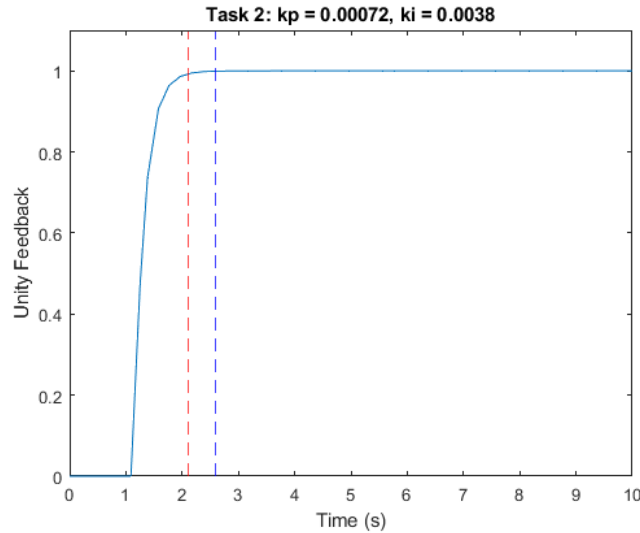


Figure 5: The step response with scaled K_i , obtained from Ziegler-Nichols method.

The K_p and K_i values were then adjusted by multiplying both by the sample time $T_s = 0.1$ s to produce $K_p = 0.00072$ and $K_i = 0.0338$.

Upon testing these values, the output displayed violent oscillations. Hence, K_i was once again scaled down by a magnitude of 10. When implemented, this produced the step response depicted in Figure 6.

Whilst the settling time was within the required parameters, the peak time exceeded the 1 second requirement, hence K_i was increased to 0.0005.

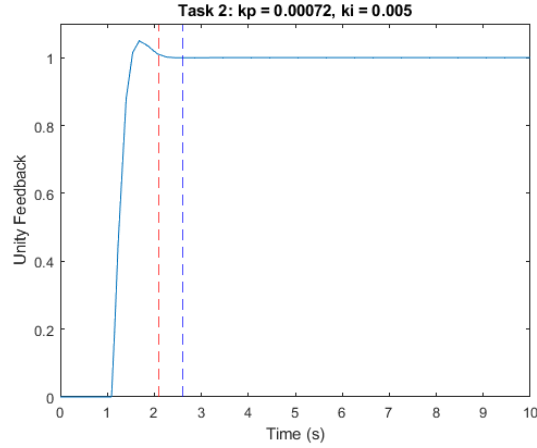


Figure 6: Step response of an adjusted K_i to meet the response requirements.

Finally, for open loop analysis, a step input of magnitude 1 was used. However, in a closed-loop system a reference speed was required. Hence, a block of gain $K = 834$ (the steady state gain, observed in open loop analysis) was used to scale the output. The step response of the tuned model is shown in Figure 7.

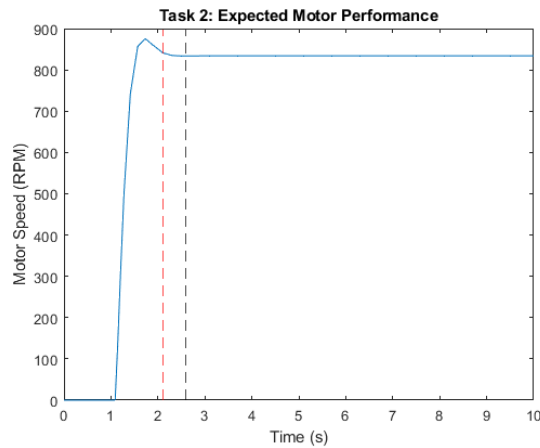


Figure 7: Step response, expected from the motor.

The Simulink model that was used to generate the plots is presented in Figure 8.

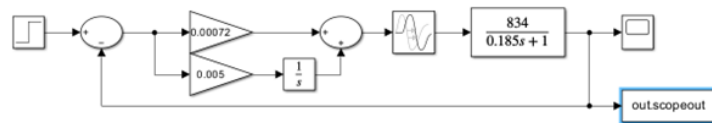


Figure 8: The model used to obtain the plots.

Question 3

To fully test the performance of your PI controller, the Desired Motor Speed (Reference) should cover a substantial range of practical motor speed. Critically comment on your results. Include any results you deem essential to support your findings. Also, do remember to comment on the expectation (Task 2) versus reality (Task 3) of the implementation.

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Question 4

Using what you have learned throughout this module (and beyond such as non-linearities effect, etc), try to improve the performance of the DC motor whether from the modelling side or the control design side. Feel free to explore and be adventurous in this exercise (as long as the safety precaution is adhered to ensure you do not damage the DC motor and the Arduino Uno). If required, revisit back all the steps from Tasks 1 to 3. Remember that in an actual engineering work, there is always room for improvement and the process is always iterative.

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References

- [1] “Control Tutorials for MATLAB and Simulink - PI Control of DC Motor Speed — ctms.engin.umich.edu,” https://ctms.engin.umich.edu/CTMS/index.php?aux=Activities_DCmotorB, [Accessed 01-May-2023].