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## Specific capacitance of Nb/AIO<sub>x</sub>/Nb Josephson junctions with critical current densities in the range of 0.1–18 kA/cm<sup>2</sup>



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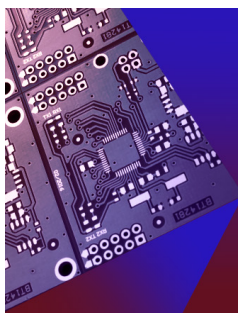


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# Specific capacitance of Nb/AlO<sub>x</sub>/Nb Josephson junctions with critical current densities in the range of 0.1–18 kA/cm<sup>2</sup>

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The specific capacitance  $C_s$  of Nb/AlO<sub>x</sub>/Nb Josephson tunnel junction has been measured by means of the superconducting quantum interference device (SQUID) resonance technique. We have investigated the junctions with critical current densities  $J_c$  in the range of 0.1–18 kA/cm<sup>2</sup> and found that  $1/C_s$  linearly depends on a logarithm of  $J_c$ . This suggests that the barrier thickness is moderately uniform in the junction area and increases continuously during growth. The results also show that increasing  $J_c$  reduces time constants of the junction. © 1995 American Institute of Physics.

The specific capacitance  $C_s$  of a Josephson tunnel junction is one of its most important parameters, since many characteristics of Josephson devices are related to  $C_s$  of the junction. Its critical current density  $J_c$  (or specific-normal-conductance  $G_n$ ) dependence is especially important because  $J_c/C_s$  (or  $G_n/C_s$ ) determines both the plasma frequency  $\omega_p = \sqrt{2\pi J_c/\Phi_0 C_s}$ , where  $\Phi_0$  is the magnetic flux quantum, and the RC time constant  $\tau_{CR} = C_s/G_n$ , which determine the response time of the junction.<sup>1</sup> Because both  $J_c$  and  $C_s$  are functions of barrier thickness  $d$ ,  $C_s$  is related to  $J_c$ . In most applications of Josephson junctions, an appropriate estimate of  $C_s$  is required for the design of devices and circuits. Moreover, the relationship between  $C_s$  and  $J_c$  (or  $G_n$ ) will give valuable information about the structure of the tunnel barrier.<sup>2</sup> Recently, van der Zant *et al.*<sup>2</sup> have investigated  $C_s$  of Nb/AlO<sub>x</sub>/Nb junctions for a wide range of  $J_c$ , using Fiske mode resonances in one-dimensional arrays of Josephson junctions. They have reported that  $C_s$  increases linearly with increasing  $J_c$ . In this paper, the results of  $C_s$  measurements of Nb/AlO<sub>x</sub>/Nb junctions with  $J_c$  in the range of 0.1–18 kA/cm<sup>2</sup> will be described. We have used a superconducting quantum interference device (SQUID) resonance technique<sup>3,4</sup> and found that  $1/C_s$  linearly depends on  $\log J_c$  and  $\log G_n$ .

A method described by Magerlein<sup>4</sup> which utilizes resonance in SQUIDs due to junction capacitance and loop inductance, was used for determining  $C_s$ . The inset of Fig. 1 shows the equivalent circuit of the SQUIDs used here. Six symmetric two-junction SQUIDs with different junction sizes and loop inductances were fabricated on each chip in order to obtain various resonant voltages  $V_r$  and  $\beta_L = 2I_c L/\Phi_0$ , where  $I_c$  is the critical current of the junction and  $2L$  is the loop inductance of the SQUID. The SQUIDs consisted of Nb/AlO<sub>x</sub>/Nb trilayers, in which the thicknesses of Nb electrodes and the Al normal layer were 200 nm and less than 6 nm, respectively. An evaporated SiO film (350 nm) was used as an insulating layer for all devices. Additional damping resistance was not used in our SQUIDs. All measurements were performed at 4.2 K.

In the current-voltage characteristics of symmetric two-junction SQUIDs, a resonant step appears at the voltage,

$$V_r = \Phi_0/2\pi\sqrt{LC_sS}, \quad (1)$$

where  $S$  is the area of one junction.<sup>3,4</sup> To determine the  $C_s$ , three parameters, resonant voltage  $V_r$ , loop inductance  $2L$  and junction area  $S$ , are necessary. The loop inductance  $2L$  was obtained from the modulation period of the critical current by injection of control currents. The error in  $2L$  is estimated to be less than  $\pm 6\%$ . This error is mainly due to the frequency dependence of the London penetration depth.<sup>5</sup> As Tuckerman and Magerlein<sup>3</sup> mentioned, generally the peak voltage of the resonance step does not agree with the resonant voltage  $V_r$ , which was determined by curve fitting to the current-voltage characteristics as described in Refs. 3 and 4. Measured  $V_r$  varied from 0.5 to 0.7 mV, which means that resonant frequency was in the range of 240–340 GHz. We estimate the error in  $V_r$  to be less than  $\pm 8\%$ . We determined the junction area  $S$  from the normal conductance of SQUIDs. It is assumed that the specific normal conductance  $G_n$  is uniform in a whole wafer region. We have determined  $G_n$  by the average of those of  $10 \times 10 \mu\text{m}^2$  junctions in the same wafer and then estimated  $S$  from a ratio of SQUID conduc-

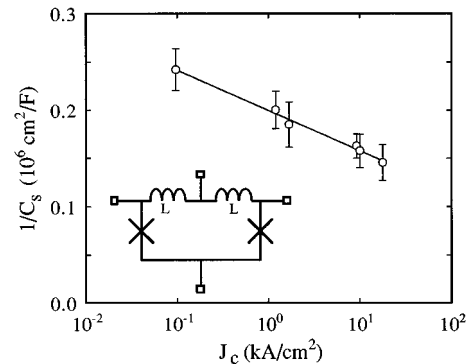


FIG. 1. The relationship between specific capacitance  $C_s$  and critical current density  $J_c$ . The solid line is a least squares fit,  $1/C_s = 0.20 - 0.043 \log_{10} J_c$ , where  $C_s$  is in  $\mu\text{F}/\text{cm}^2$  and  $J_c$  is in  $\text{kA}/\text{cm}^2$ . The inset shows an equivalent circuit of the symmetric two-junction SQUID used here.

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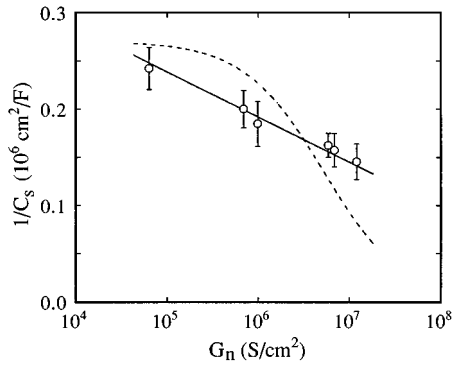


FIG. 2. The relationship between specific capacitance  $C_s$  and specific normal conductance  $G_n$ . The solid line is a fit using Eqs. (2) and (3) with  $\phi=1.5$  eV and  $\epsilon_r=4$ . The dashed line,  $C_s=3.7+0.70\times 10^{-6}G_n$ , is the dependence reported in Ref. 2.

tance to  $G_n$ . Thus, the total error in each measurement of  $C_s$  amounted to less than  $\pm 22\%$ . Finally,  $C_s$  was determined as the average of 3–8 data obtained from one wafer, so the error in  $C_s$  is estimated to be  $\pm 8\%$  to  $\pm 13\%$ .

The stray capacitance is expected to be 5–10 fF depending on the SQUID configuration, assuming that dielectric constant of SiO is 5.7. Because this is much smaller than junction capacitance, we neglect the contribution of the stray capacitance.

We defined  $J_c$  as the maximum  $I_c/S$  of individual junctions in the same wafer, since the Josephson critical current  $I_c$  can easily be reduced by an external noise.  $J_c$  is assumed to be uniform over a wafer.

The result of the  $C_s$  measurements is plotted in Fig. 1. It is found that  $1/C_s$  linearly depends on  $\log J_c$ . This logarithmic relationship is predicted by a simple model in which thickness and barrier height of the insulator are uniform in the junction area and the thickness increases continuously during growth.<sup>2</sup> The solid line in Fig. 1,  $1/C_s = 0.20 - 0.043 \log_{10} J_c$ , is a least squares fit. Here,  $C_s$  is in  $\mu\text{F}/\text{cm}^2$  and  $J_c$  is in  $\text{kA}/\text{cm}^2$ . For  $J_c < 10$   $\text{kA}/\text{cm}^2$ , the  $C_s$  obtained are close to those reported earlier<sup>2,6–8</sup> and consistent with the results of analysis of subgap current-voltage characteristics.<sup>9</sup> However, in the high  $J_c$  region, the  $J_c = 18$   $\text{kA}/\text{cm}^2$  junction showed a smaller  $C_s$  than those reported in Ref. 2.

For comparison with theory, the dependence of  $C_s$  on  $G_n$  is more important than that on  $J_c$ , because tunnel theory directly predicts  $G_n$  as a function of  $d$ . We then obtain  $J_c$  from the  $I_c R_n$  product. Generally, the  $I_c R_n$  product depends on the thickness of the normal layer, the gap of the electrodes, and the transparency of the barrier.<sup>10,11</sup> The result in Fig. 1 is replotted in Fig. 2 as the relationship between  $1/C_s$  and  $G_n$ . The logarithmic relation is evident. According to tunnel theory,<sup>12</sup> specific tunnel conductance  $G_n$  through an insulator with uniform thickness and uniform barrier height is given as

$$G_n = \frac{e^2}{4\pi\hbar d^2} \left( \frac{4\pi d \sqrt{2m\phi}}{\hbar} - 1 \right) \exp \left( - \frac{4\pi d \sqrt{2m\phi}}{\hbar} \right), \quad (2)$$

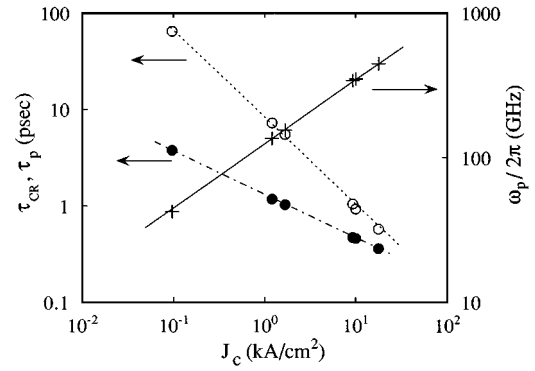


FIG. 3. The plasma frequency  $\omega_p$  (crosses), the RC time constant  $\tau_{CR}$  (open circles), and the plasma time constant  $\tau_p = 1/\omega_p$  (solid circles) as functions of critical current density  $J_c$ .

where  $\phi$  is the barrier height,  $m$  is the mass of a free electron, and  $\hbar$  is Planck's constant. The specific capacitance is given as a function of  $d$ ,

$$C_s = \epsilon_0 \epsilon_r / d, \quad (3)$$

where  $\epsilon_0$  is vacuum permittivity and  $\epsilon_r$  is relative dielectric constant. Using Eqs. (2) and (3) we calculate the dependence of  $C_s$  on  $G_n$  with adjustable parameters of  $\phi$  and  $\epsilon_r$ . The solid line in Fig. 2 is a fit with  $\phi=1.5$  eV and  $\epsilon_r=4$ . This is not an exact logarithmic relation but is approximately  $1/C_s = 0.47 - 0.047 \log_{10} G_n$ , where  $C_s$  is in  $\mu\text{F}/\text{cm}^2$  and  $G_n$  in  $\text{S}/\text{cm}^2$ . The value of  $\phi$ , 1.5 eV, is very close to that reported by Adelerhof *et al.*<sup>13</sup> We do not know the  $\epsilon_r$  of aluminum oxide in Nb/AlO<sub>x</sub>/Nb junctions. Note that the reported value of  $\epsilon_r$  of Al<sub>2</sub>O<sub>3</sub> is about 9 at a few hundred GHz,<sup>14</sup> which is larger than the value obtained,  $\epsilon_r=4$ .

The dashed line in Fig. 2,  $C_s = 3.7 + 0.70 \times 10^{-6} G_n$ , is the experimental result reported by van der Zant *et al.*<sup>2</sup> (we modified their original equation,  $C_s = 3.7 + 0.37 J_c$ , using their assumption of  $I_c R_n = 1.9$  mV). As they described, a linear dependence of  $C_s$  on  $J_c$  (or  $G_n$ ) is predicted by a model in which the barrier is assumed to be a mixture of a one monolayer oxide with thickness  $t_0$  and a two monolayer oxide with thickness  $2t_0$ . Certainly, the assumption that the thickness of the insulator is uniform and increases continuously during growth is somewhat impractical.<sup>2,11</sup> However, the assumption that the barrier consists of only two parts, oxides with thickness of  $t_0$  and  $2t_0$  is also an oversimplification. The barrier AlO<sub>x</sub> in Nb/AlO<sub>x</sub>/Nb junctions is not a single crystal film and a “monolayer” thickness depends on crystal direction. For example, the monolayer thickness of Al<sub>2</sub>O<sub>3</sub> varies from 0.41 nm for (1100) to 1.3 nm for (0001). Our experimental result suggests that a continuously variable-thickness model is more suitable for our junctions than a one- and two-monolayers-thickness model, at least for  $J_c$  of 0.1–18  $\text{kA}/\text{cm}^2$ . We cannot explain the cause of the difference between our data and those in Ref. 2, which appear to be within experimental error in the low- $J_c$  region. This is an interesting question and further investigations, including studies on growth mechanism of aluminum oxide,<sup>15,16</sup> are required.

In Fig. 3,  $\omega_p$  and  $\tau_{CR}$ , calculated using the measured

$J_c$ ,  $G_n$ , and  $C_s$ , are shown. The plasma time constant  $\tau_p = 1/\omega_p$ , relating to turn-on delay,<sup>1</sup> is also plotted. It is clearly shown that  $\tau_{CR}$  and  $\tau_p$  decrease and  $\omega_p$  increases monotonically with increasing  $J_c$ . In other words, the increase of  $J_c$  overcomes the increase of  $C_s$  and, consequently, results in the reduction of time constants.

In summary, we have measured  $C_s$  of Nb/AlO<sub>x</sub>/Nb tunnel junctions with  $J_c$  ranging from 0.1–18 kA/cm<sup>2</sup> using a SQUID resonance technique and obtained the logarithmic dependence,  $1/C_s = 0.20 - 0.043 \log_{10} J_c$  and  $1/C_s = 0.47 - 0.047 \log_{10} G_n$ . These results suggest that the thickness of the tunnel barrier is moderately uniform and increases continuously during growth. We have obtained a good agreement with conventional tunnel theory, assuming  $\phi = 1.5$  eV and  $\epsilon_r = 4$  for the barrier in our Nb/AlO<sub>x</sub>/Nb junctions. The obtained values of  $\tau_{CR}$  and  $\tau_p$  show that increasing  $J_c$  improves the response time of the junction.

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