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High Level Summary

- Lead Analysts: Nick Kinnaird, James Mott
- Positron Reconstruction Method: Recon West
- Software Release: V9_11_00
- Dataset: gm2pro_daq_full_run1_60h_5033A_withfullDQC
- Histogramming Method: Weighted Ratio
- Gain Correction Method: Default in reconstruction
- Pileup Correction Method: Asymmetic shadow window, doublets only
- Lost Muon Spectrum Extraction: Triple coincidence, not included in ratio fit
- Model for CBO: Exponential envelope, frequency from tracking analysis
- Model for VW: Exponential envelope, constant frequency, not included in ratio fit
- Fit Range: $30 \,\mu\text{s} 500 \,\mu\text{s}$
- $R = -19.88 \pm 1.373 \,\mathrm{ppm} \pm syst.$ (blinding with common string)
- $\chi^2/NDF = 3052/3145$
- P value = 0.8806

Final fit function:

$$R(t) = \frac{2f(t) - f_{+}(t) - f_{-}(t)}{2f(t) + f_{+}(t) + f_{-}(t)}$$
$$f_{\pm}(t) = f(t \pm T_{a}/2)$$
$$f(t) = C(t)(1 + A\cos(\omega_{a}t + \phi))$$
$$C(t) = 1 + A_{cbo}e^{-t/\tau_{cbo}}\cos(\omega_{cbo}(t)t + \phi_{cbo})$$
$$\omega_{a} = 2\pi \cdot 0.2291 \,\text{MHz} \cdot (1 + R \times 10^{-6})$$

Chapter 1

Analysis Procedures

1.1 Key parameters in reconstruction method

Find out procedures used in 60 hr production dataset

1.2 Analysis Data Preparation Procedure

- git branch: gm2analyses branch feature/KinnairdAnalyses
- Majority of code located under gm2analyses/macros/RatioMacro
- 1. Submit jobs to OSG to run the rootTreesAndLostMuons.fcl file which produces root trees of positron hits using the ClusterTree analyzer module and coincident MIP hits using the TestCoincidenceFinder analyzer module.
- 2. Submit jobs to Fermigrid to produce histograms from root trees using the ClusterTree-ToHistsPileup.C macro in RatioMacro/HistMaking. Beyond standard threshold histograms this macro produces pileup and lost muon histograms all within the same root file.

1.3 Histogramming Procedure

Method: Weighted Ratio (threshold)

- 1. Loop through all clusters and apply an artificial deadtime (ADT) to combine hits within 6 ns into a single pulse using the same procedure and code that the pileup method uses (see below). Drop clusters with time $< 25 \,\mu s$ or time $> 600 \,\mu s$.
- 2. Histograms are constructed with ROOT's TH1F class with 149.15 ns bins from $0-699.960\,95\,\mu s$ corresponding to 4693 bins.
- 3. Randomize times by $\pm 149.15/2$ ns and fill histograms for energies > 1.7 GeV. Randomization uses ROOT's default TRandom3 class.
- 4. Fill one of the four histograms $\{u_+(t), u_-(t), v_1(t), v_2(t)\}$ as shown in Equation A.18 per cluster. The associated histogram is determined by generating a random number between 0 and 1, and comparing that number to the relative probabilities of the different weights.

- 5. Clusters filled into the $u_+(t)$ histogram have their times shifted by $t \to t T_a/2$ and clusters filled into the $u_-(t)$ histogram have their times shifted by $t \to t + T_a/2$.
- 6. T_a is known a priori to high precision from the previous experiment, and its value is taken as $1/f_a$, where f_a is 0.2291 MHz:

$$T_a \approx 4.364\,906\,\mu s$$
 (1.1)

1.4 Gain Correction Procedure

Gain correction method: Default by the Italian Calibration Team

- 1. Long term gain is corrected using out-of-fill lasers included normalization from the Source Monitor.
- 2. In-fill gain is corrected using in-fill lasers including normalization from the Source Monitor.
- 3. Short-term double pulse (SDTP) effect is not included.

1.5 Pileup Correction Procedure

Pileup correction method: Asymmetric shadow window

- 1. Create a vector of clusters per calorimeter per fill. For each cluster look for a second cluster in a window from 12-18 ns after the time of the first cluster. This corresponds to a shadow dead time (SDT) of 6 ns and a shadow gap time (SGT) of 12 ns, equal to 1 and 2 times the applied ADT respectively.
- 2. Create shadow doublets with energies and times as:

$$E_{doublet} = E_1 + E_2 \tag{1.2}$$

$$t_{doublet} = \frac{t_1 * E_1 + (t_2 - SGT) * E_2}{E_1 + E_2}$$
(1.3)

- 3. Randomize $t_{doublet}$ times by $\pm 149.15/2$ ns as in the histogramming procedure described above.
- 4. For each calorimeter construct a pileup spectrum P = doublets singlets = D S, where the singlets are subtracted at time $t_{doublet}$ as opposed to their individual times, and pulses are only added or subtracted if they are above 1.7 GeV. Subtract P off energy and threshold histograms.

- 5. For pileup subraction in the ratio method, randomly split associated doublets and singlets into 4 separate histograms as is done in the histogramming procedure described above, with times shifted accordingly. Subtract 4 pileup histograms off corresponding $\{u_+(t), u_-(t), v_1(t), v_2(t)\}$ histograms before forming the ratio.
- 6. The errors of the pileup corrected histogram were determined to be:

$$\sigma(N_{corrected}) = \sqrt{N_{corrected} + 2N_1 + 6N_4},\tag{1.4}$$

where N_1 is the number of doublets where both singlets were below threshold, and N_4 is the number of doublets where both singlets were above threshold, and this is a quantity evaluated at each time bin. (Cite this? DocDB 14830. Derive this in the appendix?) A histogram of error multipliers was created by factoring out the $N_{corrected}$ term, which is then applied to the bin errors before fitting. This is true even for the ratio errors to good approximation. (Cite this? Derive it as JP did?) Note that I did not time randomize the N_1 and N_4 entries when constructing the correct errors, which should have a negligible effect.

7. The pileup correction at the triplet/contamination level is not included. The machinery exists to apply such a correction, but it requires more work to get it correct. It has been determined not be necessary for the 60H and Run 1 data.

1.6 Lost muon spectrum extraction procedure

Method: Triple coincidence of clusters

Note that the lost muons are not included in the ratio fit because the ratio method divides out such slow effects. This is reflected by the lack of a low frequency peak in the FFT of the fit residuals for the ratio fit, whereas such a peak exists for T method fits. I include here however my method for extracting the lost muon function for possible future systematic studies.

- 1. Triple coincidence of clusters in 3 consecutive calorimeters are made with an energy cut of 100 MeV < E < 250 MeV and 5 ns < dt < 8.5 ns.
- 2. A time histogram is made with the muon cluster in the first calorimeter.
- 3. The function that would be used in the final fit is:

$$\Lambda(t) = 1 - \kappa_{loss} \int_{0}^{t} L(t')e^{(-t'/\gamma\tau_{\mu})}dt'$$
(1.5)

where L(t) is the triples histogram, and an arbitrary 10^{-6} factor has been absorbed into κ_{loss} in order to bring it to a more reasonable value (from $\mathcal{O}(10^{-10})$ to $\mathcal{O}(10^{-4})$).

1.7 Beam Dynamics: CBO Model

1. The CBO frequency as a function of time is taken from the tracking analysis, DocDB 14208. The form used is

$$\omega_{cbo}(t) = \omega_0 (1 + \Delta \omega t + Ae^{-t/\tau_A} + Be^{-t/\tau_B})$$
(1.6)

with parameters determined from station 12 in the 60H dataset and fixed in the fit as:

$$\Delta \omega = 1.86 \times 10^{-8} \,\text{ns}^{-1},$$
 $A = -0.0504,$
 $\tau_A = 73.3 \,\mu\text{s},$
 $B = -0.131,$
 $\tau_B = 16.6 \,\mu\text{s}.$

The parameter ω_0 is allowed to float in the fit and starts with a value of 2.3051 rad μ s⁻¹. The ratio method has trouble with letting the other parameters float, and fixing them to various values does not change the fit results significantly.

- 2. Because the ratio method divides out the CBO partially (reduction by a factor of ~ 5 in the FFT cbo peak amplitude), the ratio fit has a hard time fitting the CBO lifetime. Therefore τ_{cbo} is fixed to 180 μ s, determined from a T Method fit to the same data.
- 3. An exponential function is assumed for the CBO decoherence.
- 4. The N_{cbo} term is included in the fit, A_{cbo} and ϕ_{cbo} are excluded. The 2CBO term is excluded.
- 5. The final CBO function is:

$$N_{cbo}(t) = C(t) = 1 + A_{cbo}e^{-t/\tau_{cbo}}\cos(\omega_{cbo}(t)t + \phi_{cbo})$$

$$(1.7)$$

1.8 Beam Dynamics: Vertical Waist Model

1. ω_a is senstive to the width of the beam, which is characterized by the frequency

$$f_{VW} = f_{cyc} - 2f_y, (1.8)$$

$$f_y = f_{cbo} \sqrt{\frac{2f_{cyc}}{f_{cbo}} - 1}. ag{1.9}$$

In the 60H dataset $f_{VW} \approx 2.3 \,\mathrm{MHz} \approx 10 \cdot \omega_a$, an even multiple of the g-2 frequency. Because of this, the vertical waist largely cancels in the numerator of the ratio. (show this explicitly?) This combined with the time randomization to remove the fast rotation (f_{cyc}) means the vertical waist does not need to be included in the ratio fit. This is justified by the lack of a vertical waist peak in the FFT of the residuals of the fit. (mention at all how there is a very small but observable peak at very early times or omit it?)

2. If included, an exponential function is assumed for the VW decoherence as in the CBO, and the final VW term is

$$V(t) = 1 + A_{VW}e^{-t/\tau_{VW}}\cos(\omega_{VW}t + \phi_{VW})$$
(1.10)

3. ω_{VW} is assumed to be a constant value even though the CBO frequency changes vs time.

1.9 Final Fit Function

The following function is used for the final fit for each calorimeter and for the calorimeter sum:

$$R(t) = \frac{2f(t) - f_{+}(t) - f_{-}(t)}{2f(t) + f_{+}(t) + f_{-}(t)}$$
(1.11)

$$f_{\pm}(t) = f(t \pm T_a/2)$$
 (1.12)

$$f(t) = C(t)(1 + A\cos(\omega_a t + \phi)) \tag{1.13}$$

$$C(t) = 1 + A_{cbo}e^{-t/\tau_{cbo}}\cos(\omega_{cbo}(t)t + \phi_{cbo})$$
(1.14)

$$\omega_a = 2\pi \cdot 0.2291 \,\text{MHz} \cdot (1 + R \times 10^{-6}) \tag{1.15}$$

All parameters are floating except for terms in $\omega_{cbo}(t)$ and τ_{cbo} as described above.

Chapter 2

Analysis Results

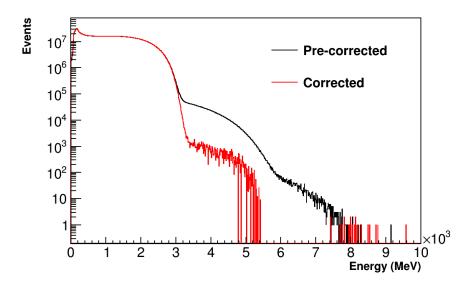
2.1 Pre-corrected and corrected energy and time spectra

Cluster Energies vs Pileup Energies



Figure $2\cdot 1$: Cluster energies in black are plotted vs pileup energies in red, for all calorimeters added together. At energies below about 2.4 GeV the pileup spectrum goes negative. In this plot the absolute value of the pileup energies is plotted, and a spike at about 2.4 GeV can be seen as a consequence of this. Due to the triplets and contamination in the pileup spectrum, the red and black curves can be seen to diverge at high energies.

Energy Spectra - Added Calos



(a) Log scale - the corrected energy spectrum goes negative around 5 GeV.

Energy Spectra - Added Calos Zoomed



(b) Linear scale - zoomed in to show the shape.

Figure $2 \cdot 2$: Plots for the pre-corrected and corrected energy spectra are shown, all calorimeters added together. Because the triplets and contamination are not accounted for, the corrected energy spectrum does not lie exactly along zero.

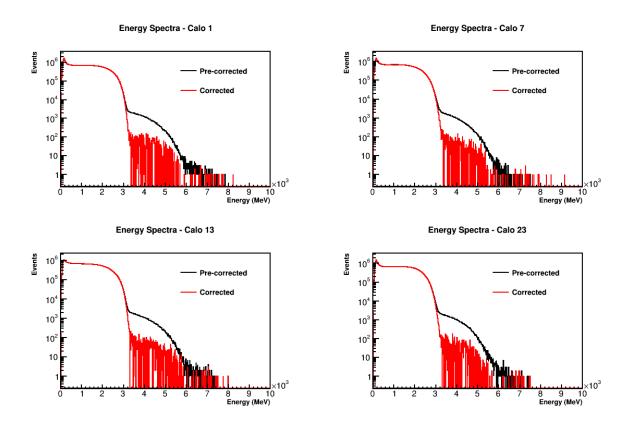


Figure $2\cdot 3$: Pre-corrected and corrected energy spectra for calorimeters 1, 7, 13, and 23 plotted on a log scale.

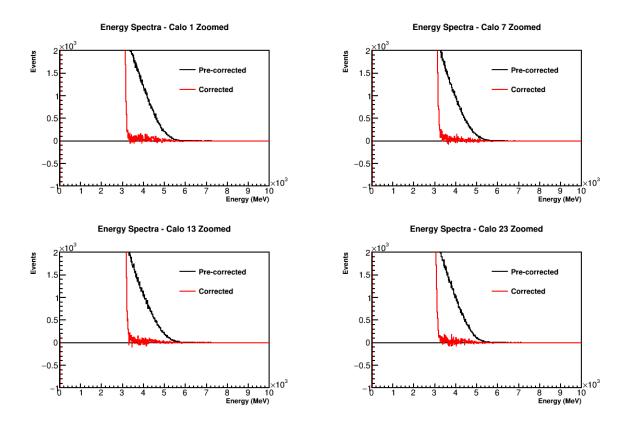


Figure 2.4: Pre-corrected and corrected energy spectra for calorimeters 1, 7, 13, and 23 plotted on a linear scale and zoomed in.

2.2 6 Parameter Ratio Fit

Full Ratio Fit

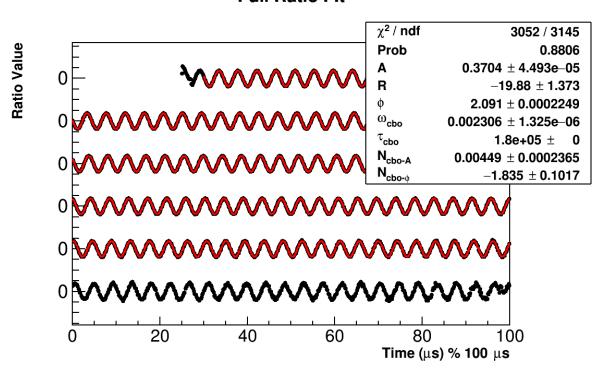
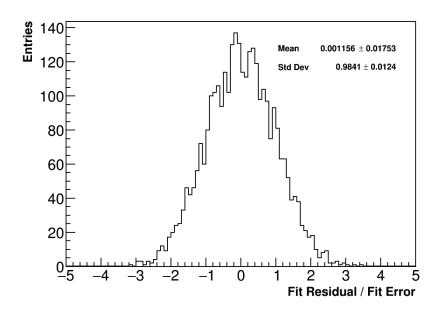


Figure 2.5: Final fit result for the 60 hour dataset. The fit includes 6 free parameters and one fixed. The x axis is in units of μ s modulo 100 μ s, with successive portions of the data points and fit shifted downwards on the plot. The parameter values in the stats box for the CBO frequency and lifetime are in units of ns. R is blinded locally. The fit ranges from 30 μ s to 500 μ s.

2.3 Residual and FFT



Full Ratio Fit Projected Pull



(c) Fit pulls projected onto the y axis. Note the Gaussian shape centered around 0 with unit width.

Figure 2.6: Residuals and pulls for the full ratio fit.



Figure 2·7: FFT of the residuals of the full ratio fit. No significant peaks remain in the ratio fit residuals after fitting with CBO terms. Overlayed are dotted lines for the g-2, CBO, and vertical waist frequencies. Peaks close to the lines are coincidental but don't line up when zoomed in.



Figure 2.8: A plot of the FFT of the residuals of the fit for the five parameter fit compared to the ratio fit. In black is the FFT for a five parameter fit, where peaks for the CBO and vertical waist can be seen as well as the g-2 peak. In red is the FFT of the full ratio fit residuals, where it has been scaled up to be visible on this plot.

2.4 Start time scans

Full Ratio Fit χ^2/NDF Vs Fit Start Time

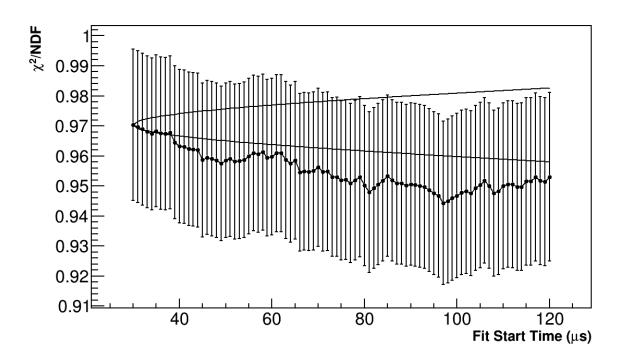


Figure 2.9: Plotted is the χ^2 per degree of freedom vs the start time of the fit. The solid lines indicate the one sigma statistically allowed difference in the fit result coming from the reduction in the data included in the fit. The error bars on the points are calculated as $\sqrt{2/NDF}$.

2.5 Stop time scans

I can produce stop time scans, and the results are consistent with the statistical significance bands, but some of the fits aren't perfect leading to some bad looking plots. Should I leave these out completely? Play more with the limits like I did to get the start time scans clean? Hack the plotting module to produce nicer looking plots? Or only include the good looking plots like R and the chi2?

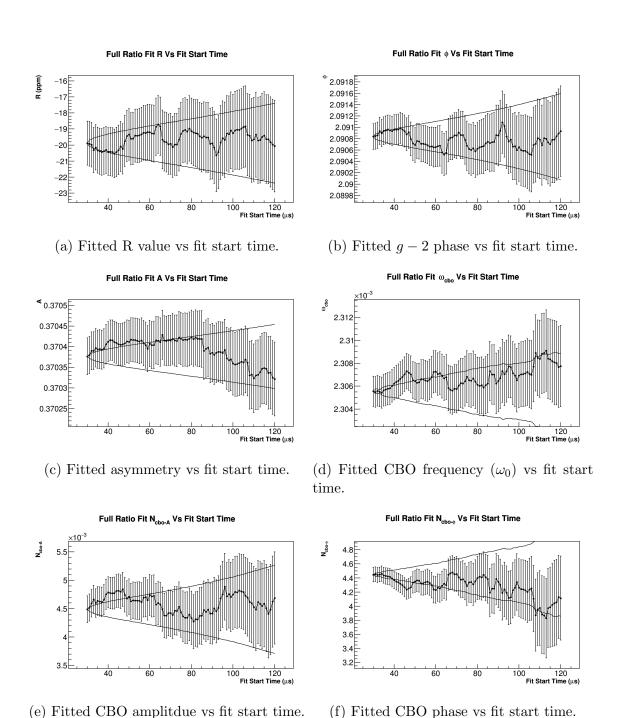


Figure $2\cdot10$: Start time scans for the free parameters in the full ratio fit. All parameters are consistently within the one sigma statistical bands.

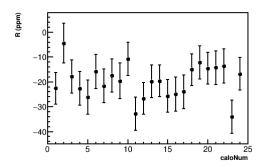
2.6 Results vs calorimeter

Full Ratio Fit χ^2/NDF Vs Calo Num



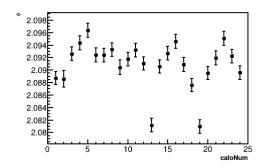
Figure 2·11: Plotted is the χ^2 per degree of freedom vs calorimeter number.

Full Ratio Fit R Vs Calo Num



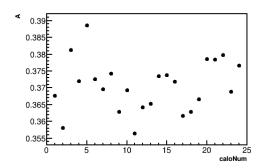
(a) Fitted R value vs calorimeter number.

Full Ratio Fit o Vs Calo Num



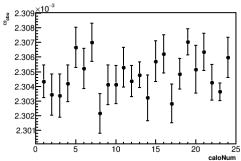
(b) Fitted g-2 phase vs calorimeter number. Calorimeters 13 and 19 lie behind the trackers leading to the different g-2 phases.

Full Ratio Fit A Vs Calo Num



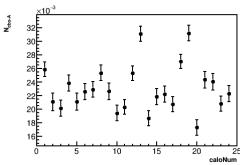
(c) Fitted asymmetry vs calorimeter number.

Full Ratio Fit $\,\omega_{cbo}^{}$ Vs Calo Num



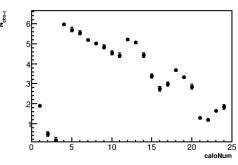
(d) Fitted CBO frequency (ω_0) vs calorimeter number.

Full Ratio Fit N_{cbo-A} Vs Calo Num



(e) Fitted CBO amplitude vs calorimeter number.

Full Ratio Fit $N_{cbo-\phi}$ Vs Calo Num



(f) Fitted CBO phase vs calorimeter number. The CBO phase varies from 0 to 2π around the ring.

Figure 2·12: Full ratio fit parameter values vs calorimeter number.

2.7 Correlation matrix for fit parameters

	A	R	ϕ	ω_{cbo}	τ_{cbo} (fixed)	N_{cbo-A}	$N_{cbo-\phi}$
A R ϕ ω_{cbo}	$\begin{array}{c} 1.0000 \\ 0.0049 \\ -0.0068 \\ -0.0166 \end{array}$	$0.0049 \\ 1.0000 \\ -0.8300 \\ -0.0204$	-0.0068 -0.8300 1.0000 0.0280	$\begin{array}{c} -0.0166 \\ -0.0204 \\ 0.0280 \\ 1.0000 \end{array}$	0.0000 0.0000 0.0000 0.0000	-0.0098 0.0207 -0.0287 0.0773	0.0233 0.0282 -0.0387 -0.8585
τ_{cbo} (fixed) N_{cbo-A} $N_{cbo-\phi}$	$ \begin{array}{r} 0.0000 \\ -0.0098 \\ 0.0233 \end{array} $	$0.0000 \\ 0.0207 \\ 0.0282$	$0.0000 \\ -0.0287 \\ -0.0387$	$0.0000 \\ 0.0773 \\ -0.8585$	$\begin{array}{c} 1.0000 \\ 0.0000 \\ 0.0000 \end{array}$	$0.0000 \\ 1.0000 \\ -0.0656$	$0.0000 \\ -0.0656 \\ 1.0000$

Table 2.1: Correlation matrix for the full ratio fit. The CBO lifetime is fixed but included in this table. The only significant correlation to R is the g-2 phase.

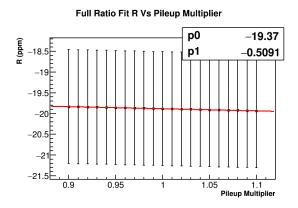
Chapter 3

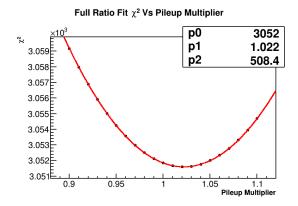
Systematic Uncertainty Evaluations

3.1 Sensitivity of ω_a to gain corrections

3.2 Sensitivity of ω_a to pileup

The systematic error on R due to the pileup construction consists primarily of two parts, the error due to misconstruction of the amplitude and the phase of the pileup. The error due to the amplitude misconstruction was calculated by scanning over a pileup multiplier parameter, from 90% of the calculated pileup amplitude to 110%, as shown in Figure 3·1. The sensitivity of R to the amplitude was determined to be 509.1 ppb per unit amplitude. The uncertainty of the pileup amplitude construction was determined by fitting a parabola to the χ^2 as a function of the pileup amplitude, and taking the width of that parabola as the uncertainty. This width is determined as the distance in X for the χ^2 to rise by 1 from the minimum, also calculated as $\sqrt{2/(\chi^2)''}$.





- (a) Sensitivity of R vs the pileup amplitude. The slope is -509.1 ppb per unit amplitude.
- (b) Plotted is the fitted χ^2 vs the pileup amplitude. The fit equation used was $p2 \times (x-p1)^2 + p0$. The minimum therefore lies at 1.022.

Figure 3·1: The significant plots to determine the pileup amplitude systematic error.

This corresponds to an uncertainty of $\sqrt{1/508.4} = 0.0444$ or 4.44%. The minimum of the χ^2 plot of 1.022 lies at approximately .5 σ away from 1, which is consistent and nice to see. Then, calculating the systematic error on R due to the pileup amplitude construction

$$\delta R_{pm} = \delta \alpha_{pm} \times \frac{dR}{d\alpha_{pm}} \tag{3.1}$$

where $\delta \alpha_{pm}$ is the uncertainty on the pileup amplitude, the systematic error on R is calculated as $0.0444 \times 509.1 \text{ pbb} = 22.6 \text{ ppb}$.

Another technique to estimate the uncertainty of the pileup amplitude construction is to look at the offset of the high energy tail of the pileup subtracted energy spectrum from zero. Because however I've applied only the doublet correction, I know that the shape of the pileup spectrum is wrong by some amount, as evidenced in $2\cdot 2$. While the pileup itself can multiplied by some scaling factor other than 1 in order to align the energy spectra slightly better, because the shape of the pileup correction is imperfect the offset calculation I believe is the wrong way to go about calculating this uncertainty in my case. The shape can be fixed by including the triplets and the doublet contamination in the shadow method, but that work is incomplete. Since the triplets are a 1% effect relative to the doublets, and the contamination is of the same order, I believe the uncertainty of 4.44% conservatively includes for this mismatch in shape and the omission of the triplets. Regardless, since the statistics of the 60H dataset is much larger than the order of the systematic effect for the pileup construction ($\mathcal{O}(1 \text{ ppm})$) vs $\mathcal{O}(10 \text{ ppb})$), this is a fine assumption.

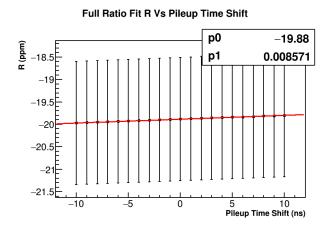


Figure 3.2: Sensitivity of R vs the pileup phase. The slope is 8.571 ppb per ns.

The error on R due to the pileup phase construction was calculated by scanning over a pileup time shift parameter, where the pileup spectrum was shifted in time by some amount before subtraction. The sensitivity of R to this parameter is shown in Figure 3.2. It is extremely unlikely that the entire pileup spectrum could be shifted by the offsets shown here, so this is a conservative estimate of the effect of the pileup phase on R. Another factor that

R (PU phase shifted) - R (no shift) Vs Fit Start Time

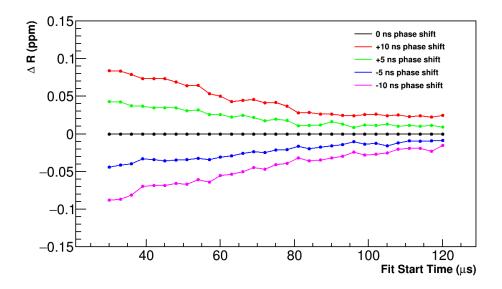


Figure 3.3: Plotted is ΔR between pileup time shifted and unshifted results vs fit start time. The black line and points are by definition 0. As the fit start time increases and the pileup reduces, the ΔR points converge to zero as they should.

the phase depends on is the energy dependence of the constructed pileup pulses, calculated as just the sum of the singlets. If the energy is miscalculated then the phase of the included pulses will be off. However, because the spatial separation is turned off in the reconstruction clustering, this is a small effect for my pileup construction method. Similarly, in the near future the Short Term Double Pulse (STDP) improvement to the laser calibration will be included also reducing this effect. For these reasons and due to the conservative nature of my phase error estimation, I leave such effects out. I then calculate the phase error as

$$\delta R_{pp} = \delta \alpha_{pp} \times \frac{dR}{d\alpha_{pp}} \tag{3.2}$$

where $\delta \alpha_{pp}$ is the uncertainty on the pileup phase. I once again very conservatively estimate the uncertainty on the pileup phase as half the artificial deadtime at 3 ns. The systematic error on R is then calculated as $3 \text{ ns} \times 8.571 \text{ pbb/ns} = 25.7 \text{ ppb}$. This is a very conservative estimate which is fine once again because of the comparison of order of statistics vs the systematic effect.

Adding these two errors in quadrature results in a systematic error on R due to the pileup as 34.2 ppb.

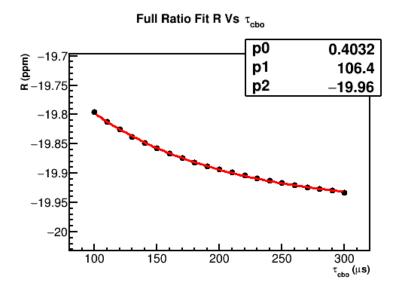


Figure 3.4: Plotted is the fitted R value as a function of the CBO lifetime, which has been fixed in the full ratio fit. The error bars have been removed from the plot in order to show the shape of the curve better. The points have been fitted to an exponential function which lines up nicely, $p_0e^{-t/p_1} + p_2$.

3.3 Sensitivity of ω_a to lost muon function shape

3.4 Sensitivity of ω_a to CBO function

3.4.1 CBO Shape

3.4.2 CBO Frequency

What about systematic errors for the cbo frequency? Should this be provided from the trackers or something that I do?

3.4.3 CBO Lifetime

Because the CBO lifetime has been fixed in the fit, there is a systematic error on R. Scanning over various values of the fixed CBO lifetime allows this error to be calculated. The resulting curve of R vs the CBO lifetime turns out not to be linear, as shown in Figure 3.4. Taking the uncertainty on the CBO lifetime as the error produced by the T Method fit, approximately $16 \mu s$, and looking at the change in R for CBO lifetime values of $180 \pm 16 \mu s$, the systematic error on R is taken as the larger of the two at 12.1 ppb.

3.5 Sensitivity of ω_a to VW function

3.6 Sensitivity of ω_a to various effects

3.6.1 g-2 Period Guess

To perform the ratio method, the g-2 period needs to be known a priori to high precision. By scanning over various g-2 period guesses the dependence of R on T_a can be determined, as shown in Figure 3.5. The systematic error can then be calculated as

$$\delta R_{period} = \delta \alpha_{period} \times \frac{dR}{d\alpha_{period}}$$
(3.3)

where $\delta \alpha_{period}$ is the uncertainty on T_a . Very conservatively taking the uncertainty as 10 ppm, the systematic error on R is calcualted as $10 \text{ ppm} \times 1.62 \times 10^{-4} \text{ ppm/ppm} = 1.62 \text{ ppb}$, which is completely negligible.

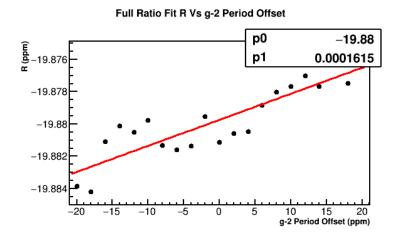


Figure 3.5: Fitted R value as a function of the ppm level offset from the guess used for the g-2 period, 1.1. Error bars have been removed from this plot, otherwise it appears as a flat line. The slope is .16 ppb per ppm offset in T_a .

3.6.2 Bin Width

The systematic uncertainty from the bin width, chosen to eliminate the fast rotation signal, was calculated by performing the histogramming and fitting stages with varying values of bin widths. The systematic uncertainty is taken as the RMS spread of the fitted R values. As shown in Figure 3.6 it is 44.5 ppb.

Full Ratio Fit R Vs Bin Width Mean -19.87 RMS 0.04453 -19 -20.5 -21 -21.5 -149 149.05 149.1 149.15 149.2 149.25 149.3 Bin Width (ns)

Figure 3.6: Plotted are fitted R values for varying bin widths ranging from 149.00 ns to 149.30 ns in steps of 5 ns.

3.6.3 Randomization

I'm not sure what the systematic error due to the randomization should be. I'm also not sure what I should take as my final answer for R. Would it just be the average of all the random seeds?

3.7 Final Systematic Uncertainty Table

3.8 Final Results

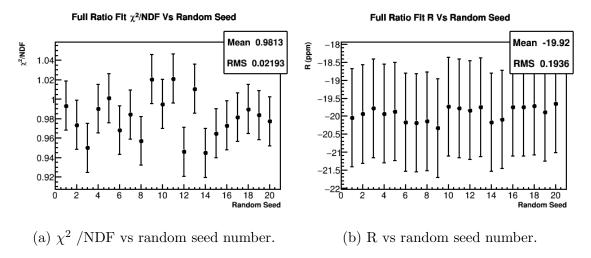


Figure 3.7: Plotted is the χ^2 /NDF and fitted R value for 20 random seeds.

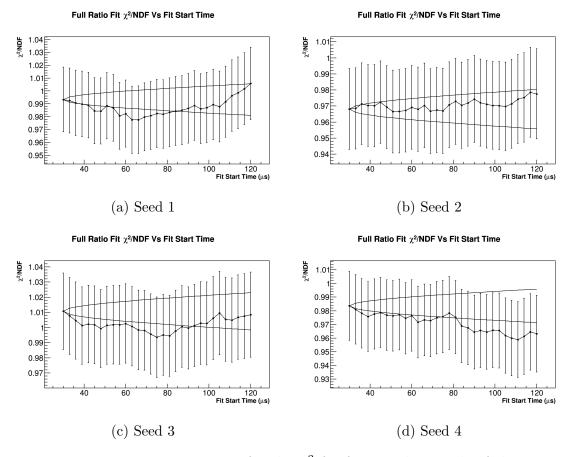


Figure 3.8: Fit start time scans for the χ^2 for four random seeds of the randomization of the same dataset. Compare to Figure 2.9. Note how the scans rise and fall at different points but are all consistent with the statistical bands.

Appendix A

Ratio Method Derivation and Fit Function

Consider the 5 parameter function:

$$N_5(t) = N_0 e^{-t/\tau} (1 + A\cos(\omega_a t + \phi)), \tag{A.1}$$

which describes some ideal dataset in histogram format. Here ϕ will be set to zero for simplicity. Now define the variables $u_+(t)$, $u_-(t)$, $v_1(t)$, and $v_2(t)$ as

$$u_{+}(t) = \frac{1}{4}N_{5}(t + T/2)$$

$$u_{-}(t) = \frac{1}{4}N_{5}(t - T/2)$$

$$v_{1}(t) = \frac{1}{4}N_{5}(t)$$

$$v_{2}(t) = \frac{1}{4}N_{5}(t),$$
(A.2)

where the 1/4 out front reflects randomly splitting the whole dataset into 4 equally weighted sub-datasets, and T is the g-2 period known to high precision, $\mathcal{O}(10^{-6})$. This corresponds to a weighting of 1:1:1:1 between the datasets. To be explicit here regarding the signs, the counts that are filled into the histogram described by u_+ have their times shifted as $t \to t - T/2$, which is what the function $N_5(t + T/2)$ describes, and vice versa for u_- . To form the ratio define the variables:

$$U(t) = u_{+}(t) + u_{-}(t)$$

$$V(t) = v_{1}(t) + v_{2}(t)$$

$$R(t) = \frac{V(t) - U(t)}{V(t) + U(t)}.$$
(A.3)

Plugging in and dividing the common terms $(N_0e^{-t/\tau}/4)$,

$$R(t) = \frac{2(1 + A\cos(\omega_a t)) - e^{-T/2\tau}(1 + A\cos(\omega_a t + \omega_a T/2)) - e^{T/2\tau}(1 + A\cos(\omega_a t - \omega_a T/2))}{2(1 + A\cos(\omega_a t)) + e^{-T/2\tau}(1 + A\cos(\omega_a t + \omega_a T/2)) + e^{T/2\tau}(1 + A\cos(\omega_a t + \omega_a T/2))}.$$
(A.4)

Now set $\omega_a T/2 = \delta$, and note that T is really

$$T = T_{guess} = \frac{2\pi}{\omega_a} + \Delta T,$$

$$\Delta T = T_{guess} - T_{true}.$$
(A.5)

Being explicit,

$$\delta = \frac{\omega_a}{2} T_{guess} = \frac{\omega_a}{2} (\frac{2\pi}{\omega_a} + \Delta T) = \pi + \pi \frac{\Delta T}{T_{true}} = \pi + \pi (\delta T), \tag{A.6}$$

and δ can be redefined as

$$\delta = \pi(\delta T),\tag{A.7}$$

by flipping the sign of any cosine terms that contain δ .

Then, using the trig identity

$$\cos(a \pm b) = \cos(a)\cos(b) \mp \sin(a)\sin(b) \tag{A.8}$$

so that

$$\cos(\omega_a t \pm \delta) = \cos(\omega_a t) \cos \delta \mp \sin(\omega_a t) \sin \delta$$

$$\approx \cos(\omega_a t) (1 - \delta^2) \mp \sin(\omega_a t) \delta$$

$$\approx \cos(\omega_a t),$$
(A.9)

since $\delta \sim O(10^{-5})$, the ratio becomes

$$R(t) \approx \frac{2(1 + A\cos(\omega_a t)) - (1 - A\cos(\omega_a t))(e^{-T/2\tau} + e^{T/2\tau})}{2(1 + A\cos(\omega_a t)) + (1 - A\cos(\omega_a t))(e^{-T/2\tau} + e^{T/2\tau})}.$$
 (A.10)

Expanding

$$e^{\pm T/2\tau} = 1 \pm \frac{T}{2\tau} + \frac{1}{2} \left(\frac{T}{2\tau}\right)^2 \pm \dots,$$
 (A.11)

repacing and simplifying,

$$R(t) \approx \frac{A\cos(\omega_a t) - C(1 - A\cos(\omega_a t))}{1 + C(1 - A\cos(\omega_a t))},$$
(A.12)

where

$$C = \frac{1}{16} \left(\frac{T}{\tau}\right)^2 \approx 2.87 * 10^{-4}.$$
 (A.13)

Using the expansion

$$f(x) = \frac{1}{1+x} = 1 - x + x^2 - \dots, \quad |x| < 1,$$
(A.14)

and since C is small, the denominator can be manipulated such that

$$R(t) \approx (A\cos(\omega_a t)) - C(1 - A\cos(\omega_a t)))(1 - C(1 - A\cos(\omega_a t)))$$

$$\approx A\cos(\omega_a t) - C + CA^2\cos^2(\omega_a t),$$
(A.15)

after dropping terms of $\mathcal{O}(C^2)$ and higher. In practice the last term is ommitted since it has a minimal effect on the fitted value of ω_a [cite], and one arrives at

$$R(t) \approx A\cos(\omega_a t) - C,$$
 (A.16)

the conventional 3 parameter ratio function.

In order to avoid approximations one can instead weight the counts in the histograms as

$$u_{+}(t): u_{-}(t): v_{1}(t): v_{2}(t) = e^{T/2\tau}: e^{-T/2\tau}: 1:1,$$
 (A.17)

so that

$$u_{+}(t) = \frac{e^{T/2\tau}}{2 + e^{T/2\tau} + e^{-T/2\tau}} N_{5}(t + T/2)$$

$$u_{-}(t) = \frac{e^{-T/2\tau}}{2 + e^{T/2\tau} + e^{-T/2\tau}} N_{5}(t - T/2)$$

$$v_{1}(t) = \frac{1}{2 + e^{T/2\tau} + e^{-T/2\tau}} N_{5}(t)$$

$$v_{2}(t) = \frac{1}{2 + e^{T/2\tau} + e^{-T/2\tau}} N_{5}(t).$$
(A.18)

(These factors out front aren't so far off from 1/4 since $e^{\pm T/2\tau} \approx e^{\pm 4.35/2*64.4} \approx 1.034, .967.$) Then instead R(t) becomes

$$R(t) = \frac{2(1 + A\cos(\omega_a t)) - (1 - A\cos(\omega_a t + \delta)) - (1 - A\cos(\omega_a t - \delta))}{2(1 + A\cos(\omega_a t)) + (1 - A\cos(\omega_a t + \delta)) + (1 - A\cos(\omega_a t + \delta))},$$
(A.19)

where the $e^{\pm T/2\tau}$ terms out front now cancel. Using Equation A.9 again and this time avoiding approximations in δ ,

$$R(t) = \frac{2A\cos(\omega_a t)(1+\cos\delta)}{4+2A\cos(\omega_a t)(1-\cos\delta)},$$
(A.20)

after simplifying. In the limit that

$$\delta = \pi(\delta T) \to 0 \tag{A.21}$$

since δT is small,

$$R(t) \approx A \cos(\omega_a t),$$
 (A.22)

with the only approximation being made at $\mathcal{O}(\delta^2) \sim \mathcal{O}(10^{-10})$.

Finally, while the 3 parameter ratio function suffices for fits to data containing slow modulations, it does not suffice for faster oscillation features. In that case it is more useful to fit with the non-approximated or simplified version of the ratio,

$$R(t) = \frac{v_1(t) + v_2(t) - u_+(t) - u_-(t)}{v_1(t) + v_2(t) + u_+(t) + u_-(t)},$$

$$= \frac{2f(t) - f_+(t) - f_-(t)}{2f(t) + f_+(t) + f_-(t)},$$
(A.23)

where

$$f(t) = C(t)(1 + A\cos(\omega_a t + \phi))$$

 $f_{\pm}(t) = f(t \pm T_a/2),$ (A.24)

and C(t) can encode any other effects in the data that need to be fitted for, such as the CBO,

$$C(t) = 1 + A_{cbo}e^{-t/\tau_{cbo}}\cos(\omega_{cbo}t + \phi_{cbo}). \tag{A.25}$$

Additionally, any other fit parameters such as A or ϕ can be made a function of t. Using the non-approximated form for the final fit function gives greater confidence in the fit results for the high precision ω_a extraction necessary for the experimental measurement.

Appendix B

Ratio Method Errors