EAMB 7004 Camadas-Limite Naturais e Dispersão de Poluentes Programa de Pós-Graduação em Engenharia Ambiental Departamento de Engenharia Ambiental, UFPR P02, 05 Nov 2021

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Prova com consulta exclusivamente ao material didático da disciplina.

NOME: Assinatura: _____

Um método de "perturbação" para as equações governantes médias sob a aproximação de Boussinesq

A notação desta prova é a mesma adotada no curso. Por isso, os símbolos usuais não serão definidos.

1 [25] Uma equação de estado consistente para as flutuações de Boussinesq e de Reynolds Suponha que vale a equação de estado linearizada

$$\frac{\rho_{\delta}}{\rho_r} = -\beta_p T_{\delta},$$

onde $\beta_p = \beta_p(T_r, p_r)$ é calculado no estado hidrostático de referência. Usando as decomposições de Boussinesq e de Reynolds para ρ e T apresentadas em aula, mostre que ela se desdobra em duas equações de estado "naturais" para as médias das flutuações de Boussinesq, e para as flutuações de Reynolds:

$$\frac{\overline{\rho_{\delta}}}{\rho_{r}} = -\beta_{p} \overline{T_{\delta}},$$
$$\frac{\rho'}{\rho_{r}} = -\beta_{p} T'.$$

Além disso, utilizando diretamente

$$\frac{\mathrm{d}\rho}{\rho} = -\beta_p \mathrm{d}T + \kappa_T \mathrm{d}p,$$

mostre que

$$\frac{\partial \rho_r}{\partial x_i} = -\rho_r \beta_p \frac{\partial T_r}{\partial x_i} + \rho_r \kappa_T \frac{\partial p_r}{\partial x_i}.$$

Note que a partir da linearlização, β_p pode ser considerado um número fixo que não varia nem com t, nem com x_i .

SOLUÇÃO DA QUESTÃO:

Basta fazer uma decomposição de Reynolds:

$$\begin{split} \frac{\rho_{\delta}}{\rho_{r}} &= -\beta_{p} T_{\delta}, \\ \rho_{\delta} &= \overline{\rho_{\delta}} + \rho', \\ T_{\delta} &= \overline{T_{\delta}} + T', \\ \overline{\rho_{\delta}} &+ \rho' &= -\beta_{p} (\overline{T_{\delta}} + T'), \\ \overline{\frac{\rho_{\delta}}{\rho_{r}}} &= -\beta_{p} \overline{T_{\delta}}, \\ \frac{\rho'}{\rho_{r}} &= -\beta_{p} T'. \end{split}$$

Em seguida,

$$\begin{split} \frac{\mathrm{d}\rho}{\rho} &= -\beta_p \mathrm{d}T + \kappa_T \mathrm{d}p, \\ \frac{\mathrm{d}\rho_r}{\rho_r} &= -\beta_p \mathrm{d}T_r + \kappa_T \mathrm{d}p_r, \\ \frac{\partial\rho_r}{\partial x_i} &= -\beta_p \rho_r \frac{\partial T_r}{\partial x_i} + \kappa_T \rho_r \frac{\partial p_r}{\partial x_i} \blacksquare \end{split}$$

2 [25] O termo de 2ª ordem da equação da continuidade

Considere a equação da continuidade e suas ordens de grandeza:

$$\underbrace{\frac{\partial \overline{\rho_{\delta}}}{\partial t}}_{\text{I}} + \underbrace{\overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}}}_{\text{II}} + \underbrace{\overline{u_{i}} \frac{\partial \overline{\rho_{\delta}}}{\partial x_{i}}}_{\text{III}} + \underbrace{\rho_{r} \frac{\partial \overline{u_{i}}}{\partial x_{i}}}_{\text{IV}} + \underbrace{\overline{\rho_{\delta}} \frac{\partial \overline{u_{i}}}{\partial x_{i}}}_{\text{V}} + \underbrace{\frac{\partial \overline{\rho' u'_{i}}}{\partial x_{i}}}_{\text{VI}} = 0.$$

Das aulas, sabemos que cada termo de IV tem ordem de grandeza $\rho_0 \tilde{u}/\ell$, e que todos os outros os termos acima (sem considerar somas) têm ordem de grandeza muito menor, $\tilde{\rho}\tilde{u}/\ell$. Reescreva portanto:

$$\underbrace{\frac{\partial \overline{\rho_{\delta}}}{\partial t}}_{I} + \underbrace{\overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}}}_{II} + \underbrace{\overline{u_{i}} \frac{\partial \overline{\rho_{\delta}}}{\partial x_{i}}}_{III} + \underbrace{\overline{\rho_{\delta}} \frac{\partial \overline{u_{i}}}{\partial x_{i}}}_{V} + \underbrace{\frac{\partial \overline{\rho' u_{i}'}}{\partial x_{i}}}_{VI} = -\underbrace{\rho_{r} \frac{\partial \overline{u_{i}}}{\partial x_{i}}}_{IV} = 0.$$

Suponha que o campo médio de velocidade é, em $1^{\underline{a}}$ aproximação, solenoidal: $\partial \overline{u_i}/\partial x_i = 0$. Mostre que

$$\frac{\partial \overline{\rho_{\delta}}}{\partial t} + \overline{u_i} \frac{\partial \overline{\rho_{\delta}}}{\partial x_i} + \overline{u_i} \frac{\partial \rho_r}{\partial x_i} + \frac{\partial \overline{\rho' u_i'}}{\partial x_i} = 0.$$

SOLUÇÃO DA QUESTÃO:

$$\begin{split} \frac{\partial \overline{\rho_{\delta}}}{\partial t} + \overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}} + \overline{u_{i}} \frac{\partial \overline{\rho_{\delta}}}{\partial x_{i}} + \overline{\rho_{\delta}} \underbrace{\frac{\partial \overline{u_{i}}}{\partial x_{i}}}_{=0} + \frac{\partial \overline{\rho' u_{i}'}}{\partial x_{i}} = -\rho_{r} \frac{\partial \overline{u_{i}}}{\partial x_{i}} = 0, \\ \frac{\partial \overline{\rho_{\delta}}}{\partial t} + \overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}} + \overline{u_{i}} \frac{\partial \overline{\rho_{\delta}}}{\partial x_{i}} + \frac{\partial \overline{\rho' u_{i}'}}{\partial x_{i}} = 0 \blacksquare \end{split}$$

3 [50] Combinando os resultados das Questões 1 e 2, deduza uma equação para o campo médio de temperatura:

$$\frac{\partial (T_r + \overline{T_{\delta}})}{\partial t} + \overline{u_i} \frac{\partial (T_r + \overline{T_{\delta}})}{\partial x_i} + \frac{\partial \overline{T'u_i'}}{\partial x_i} - \overline{u_i} \frac{\kappa_T}{\beta_p} \frac{\partial p_r}{\partial x_i} + \overline{T'u_i'} \left(-\beta_p \frac{\partial T_r}{\partial x_i} + \kappa_T \frac{\partial p_r}{\partial x_i} \right) = 0.$$

Atenção: Na dedução da equação acima, você deve desprezar um termo considerando que $\frac{\overline{\rho_{\delta}}}{\rho_{r}} \ll 1$.

SOLUÇÃO DA QUESTÃO:

$$\frac{\partial \overline{\rho_{S}}}{\partial t} + \overline{u_{i}} \frac{\partial \overline{\rho_{S}}}{\partial x_{i}} + \overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}} + \frac{\partial \rho^{r} u_{i}'}{\partial x_{i}} = 0;$$

$$\rho_{S} = -\beta_{\rho} \rho_{r} \overline{t_{S}};$$

$$\rho' = -\beta_{\rho} \rho_{r} T';$$

$$\frac{\partial \rho_{r}}{\partial t} = -\rho_{r} \beta_{\rho} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \rho_{r} \kappa_{T} \frac{\partial \rho_{r}}{\partial x_{i}}$$

$$\frac{\partial \left[-\beta_{\rho} \rho_{r} \overline{t_{S}}\right]}{\partial t} + \overline{u_{i}} \frac{\partial \left[-\beta_{\rho} \rho_{r} \overline{t_{S}}\right]}{\partial x_{i}} + \overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}} - \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$-\beta_{\rho} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} - \beta_{\rho} \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[-\beta_{\rho} \overline{t_{S}} \frac{\partial \rho_{r}}{\partial x_{i}}\right] + \overline{u_{i}} \frac{\partial \rho_{r}}{\partial x_{i}} - \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$-\beta_{\rho} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} - \beta_{\rho} \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[-\beta_{\rho} \overline{t_{S}} \frac{\partial \rho_{r}}{\partial x_{i}} + \frac{\partial \rho_{r}}{\partial x_{i}}\right] - \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$-\beta_{\rho} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} - \beta_{\rho} \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[-\beta_{\rho} \overline{t_{S}} \frac{\partial \rho_{r}}{\partial x_{i}} + \frac{\partial \rho_{r}}{\partial x_{i}}\right] - \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$-\beta_{\rho} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} - \beta_{\rho} \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[-\rho_{r} \beta_{\rho} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \rho_{r} \kappa_{T} \frac{\partial \rho_{r}}{\partial x_{i}}\right] - \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$-\beta_{\rho} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} - \beta_{\rho} \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[-\rho_{r} \beta_{\rho} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \rho_{r} \kappa_{T} \frac{\partial \rho_{r}}{\partial x_{i}}\right] - \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$-\beta_{\rho} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} + \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[-\rho_{r} \beta_{\rho} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \rho_{r} \kappa_{T} \frac{\partial \rho_{r}}{\partial x_{i}}\right] + \beta_{\rho} \frac{\partial \left[\rho_{r} T' u_{i}'\right]}{\partial x_{i}} = 0;$$

$$\rho_{r} \frac{\partial \overline{t_{S}}}{\partial t} + \overline{u_{i}} \rho_{r} \frac{\partial \overline{t_{S}}}{\partial x_{i}} + \overline{u_{i}} \left[\rho_{r} \frac{\partial \overline{t_{r}}}{\partial x_{i}} - \rho_{r} \frac{\kappa_{T}}{\partial \rho} \frac{\partial \rho_{r}}{\partial x_{i}}\right] + \left[\rho_{r} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \overline{t_{r}} \frac{\partial \rho_{r}}{\partial x_{i}}\right] + \left[\rho_{r} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \overline{t_{r}} \frac{\partial \rho_{r}}{\partial x_{i}}\right] = 0;$$

$$\frac{\partial \overline{t_{S}}}{\partial t} + \overline{u_{i}} \frac{\partial \overline{t_{r}}}{\partial x_{i}} + \overline{u_{i}} \left[\rho_{r} \frac{\partial \overline{t_{$$