

# Examen Final – FIS1523 – Termodinámica

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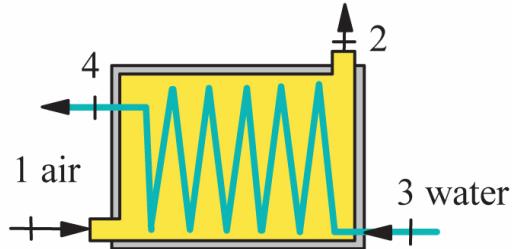
**Tiempo:** 120 minutos

## Tablas Incluidas:

- Propiedades del aire como gas-ideal
- Agua saturada – tabla de temperatura
- Agua saturada – tabla de presión
- Refrigerante 134a saturado – tabla de presión
- Refrigerante 134a supercalentado

## Problema 1

Un intercambiador de calor, como el que se muestra en la figura, se usa para enfriar un flujo de aire de 800 a 360 K, sin cambios en la presión que vale 1 MPa. El refrigerante es un flujo de agua a 15°C y 0.1 MPa. Si el agua sale como vapor saturado, ¿cuál es el cociente de los flujos de masa  $\dot{m}_{\text{agua}}/\dot{m}_{\text{aire}}$ ?

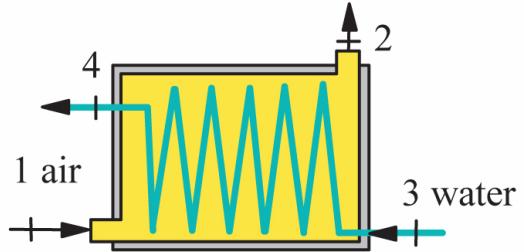


## Solución

A heat exchanger, shown in Fig. P6.85, is used to cool an air flow from 800 K to 360 K, both states at 1 MPa. The coolant is a water flow at 15°C, 0.1 MPa. If the water leaves as saturated vapor, find the ratio of the flow rates  $\dot{m}_{H_2O}/\dot{m}_{air}$

Solution:

C.V. Heat exchanger, steady flow 1 inlet and 1 exit for air and water each. The two flows exchange energy with no heat transfer to/from the outside.



Continuity Eqs.: Each line has a constant flow rate through it.

$$\text{Energy Eq.6.10: } \dot{m}_{air}h_1 + \dot{m}_{H_2O}h_3 = \dot{m}_{air}h_2 + \dot{m}_{H_2O}h_4$$

Process: Each line has a constant pressure.

Air states, Table A.7.1:  $h_1 = 822.20 \text{ kJ/kg}$ ,  $h_2 = 360.86 \text{ kJ/kg}$

Water states, Table B.1.1:  $h_3 = 62.98 \text{ kJ/kg}$  (at 15°C),

Table B.1.2:  $h_4 = 2675.5 \text{ kJ/kg}$  (at 100 kPa)

$$\frac{\dot{m}_{H_2O}}{\dot{m}_{air}} = \frac{h_1 - h_2}{h_4 - h_3} = \frac{822.20 - 360.86}{2675.5 - 62.99} = \mathbf{0.1766}$$

## Problema 2

Un dispositivo de cilindro con pistón, aislado de  $0.25 \text{ m}^3$  contiene inicialmente  $0.7 \text{ kg}$  de aire a  $20^\circ\text{C}$ . En este estado el pistón es libre de moverse. Ahora se deja entrar al cilindro aire a  $70^\circ\text{C}$  y  $500 \text{ kPa}$  desde una tubería hasta que el volumen aumenta un  $50\%$ . Considerar calores específicos constantes a temperatura ambiente.

- Encontrar la expresión que permite encontrar la temperatura final del sistema
- Si la temperatura final del sistema fuera  $308 \text{ K}$ , determinar la cantidad de masa que entró al sistema, el trabajo realizado y la entropía generada

Datos:  $R_{\text{aire}} = 0.287 \text{ kJ/kg K}$ ;  $c_p = 1.005 \text{ kJ/kg K}$ ;  $c_v = 0.718 \text{ kJ/kg K}$

## Solución

Air is allowed to enter an insulated piston-cylinder device until the volume of the air increases by 50%. The final temperature in the cylinder, the amount of mass that has entered, the work done, and the entropy generation are to be determined.

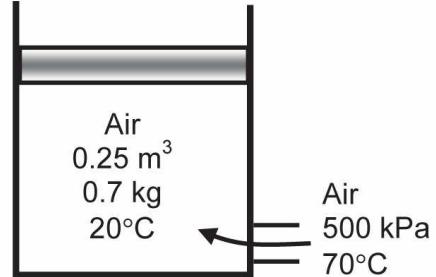
**Assumptions** 1 Kinetic and potential energy changes are negligible. 2 Air is an ideal gas with constant specific heats.

**Properties** The gas constant of air is  $R = 0.287 \text{ kJ/kg}\cdot\text{K}$  and the specific heats of air at room temperature are  $c_p = 1.005 \text{ kJ/kg}\cdot\text{K}$ ,  $c_v = 0.718 \text{ kJ/kg}\cdot\text{K}$  (Table A-2).

**Analysis** The initial pressure in the cylinder is

$$P_1 = \frac{m_1 RT_1}{V_1} = \frac{(0.7 \text{ kg})(0.287 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K})(20 + 273 \text{ K})}{0.25 \text{ m}^3} = 235.5 \text{ kPa}$$

$$m_2 = \frac{P_2 V_2}{R T_2} = \frac{(235.5 \text{ kPa})(1.5 \times 0.25 \text{ m}^3)}{(0.287 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K})T_2} = \frac{307.71}{T_2}$$



A mass balance on the system gives the expression for the mass entering the cylinder

$$m_i = m_2 - m_1 = \frac{307.71}{T_2} - 0.7$$

(c) Noting that the pressure remains constant, the boundary work is determined to be

$$W_{b,out} = P_1(V_2 - V_1) = (235.5 \text{ kPa})(1.5 \times 0.25 - 0.5)\text{m}^3 = \mathbf{29.43 \text{ kJ}}$$

(a) An energy balance on the system may be used to determine the final temperature

$$\begin{aligned} m_i h_i - W_{b,out} &= m_2 u_2 - m_1 u_1 \\ m_i c_p T_i - W_{b,out} &= m_2 c_v T_2 - m_1 c_v T_1 \\ \left( \frac{307.71}{T_2} - 0.7 \right)(1.005)(70 + 273) - 29.43 &= \left( \frac{307.71}{T_2} \right)(0.718)T_2 - (0.7)(0.718)(20 + 273) \end{aligned}$$

There is only one unknown, which is the final temperature. By a trial-error approach or using EES, we find

$$T_2 = \mathbf{308.0 \text{ K}}$$

(b) The final mass and the amount of mass that has entered are

$$m_2 = \frac{307.71}{308.0} = 0.999 \text{ kg}$$

$$m_i = m_2 - m_1 = 0.999 - 0.7 = \mathbf{0.299 \text{ kg}}$$

(d) The rate of entropy generation is determined from

$$\begin{aligned} S_{gen} &= m_2 s_2 - m_1 s_1 - m_i s_i = m_2 s_2 - m_1 s_1 - (m_2 - m_1)s_i = m_2(s_2 - s_i) - m_1(s_1 - s_i) \\ &= m_2 \left( c_p \ln \frac{T_2}{T_i} - R \ln \frac{P_2}{P_i} \right) - m_1 \left( c_p \ln \frac{T_1}{T_i} - R \ln \frac{P_1}{P_i} \right) \end{aligned}$$

### Problema 3

Una bomba de calor que opera en un ciclo de refrigeración ideal con R-134a como refrigerante es usada para calentar agua de 15 a 45 °C a razón de 0.12 kg/s. Las presiones del condensador y del evaporador son 1.4 y 0.32 MPa, respectivamente. Determinar la potencia necesaria para el funcionamiento de la bomba de calor.

### Solución

A heat pump that operates on the ideal vapor-compression cycle with refrigerant-134a is considered. The power input to the heat pump is to be determined.

**Assumptions** 1 Steady operating conditions exist. 2 Kinetic and potential energy changes are negligible.

**Analysis** In an ideal vapor-compression refrigeration cycle, the compression process is isentropic, the refrigerant enters the compressor as a saturated vapor at the evaporator pressure, and leaves the condenser as saturated liquid at the condenser pressure. From the refrigerant tables (Tables A-12 and A-13),

$$P_1 = 320 \text{ kPa} \quad \left. \begin{array}{l} h_1 = h_g @ 320 \text{ kPa} = 251.88 \text{ kJ/kg} \\ s_1 = s_g @ 320 \text{ kPa} = 0.93006 \text{ kJ/kg} \cdot \text{K} \end{array} \right\}$$

$$P_2 = 1.4 \text{ MPa} \quad \left. \begin{array}{l} h_2 = 282.54 \text{ kJ/kg} \\ s_2 = s_1 \end{array} \right\}$$

$$P_3 = 1.4 \text{ MPa} \quad \left. \begin{array}{l} h_3 = h_f @ 1.4 \text{ MPa} = 127.22 \text{ kJ/kg} \\ \text{sat. liquid} \end{array} \right\}$$

$$h_4 \cong h_3 = 127.22 \text{ kJ/kg} \quad (\text{throttling})$$

The heating load of this heat pump is determined from

$$\begin{aligned} \dot{Q}_H &= [\dot{m}c(T_2 - T_1)]_{\text{water}} \\ &= (0.12 \text{ kg/s})(4.18 \text{ kJ/kg} \cdot ^\circ\text{C})(45 - 15)^\circ\text{C} = 15.05 \text{ kW} \end{aligned}$$

and

$$\dot{m}_R = \frac{\dot{Q}_H}{q_H} = \frac{\dot{Q}_H}{h_2 - h_3} = \frac{15.05 \text{ kJ/s}}{(282.54 - 127.22) \text{ kJ/kg}} = 0.09688 \text{ kg/s}$$

Then,

$$\dot{W}_{\text{in}} = \dot{m}_R(h_2 - h_1) = (0.09688 \text{ kg/s})(282.54 - 251.88) \text{ kJ/kg} = 2.97 \text{ kW}$$

