

Article

IoT-Enabled High Efficiency Smart Solar Charge Controller with Maximum Power Point Tracking—Design, Hardware Implementation and Performance Testing

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Abstract: Amid growing demand for solar photovoltaic (PV) energy, the output from PV panels/cells fails to deliver maximum power to the load, due to the intermittency of ambient conditions. Therefore, utilizing maximum power point tracking (MPPT) becomes essential for PV systems. In this paper, a novel internet of things (IoT)-equipped MPPT solar charge controller (SCC) is designed and implemented. The proposed circuit system utilizes IoT-based sensors to send vital data to the cloud for remote monitoring and controlling purposes. The IoT platform helps the system to be monitored remotely. The PIC16F877A is used as a main controller of the proposed MPPT-SCC besides implementing the perturb and observe (P&O) technique and a customized buck-boost converter. To validate the proposed system, both simulation and hardware implementation are carried out by the MATLAB/SIMULINK environment and laboratory set up, respectively. The proposed MPPT-SCC can handle the maximum current of 10 A at 12 V voltage. Results show that the efficiency of the proposed system reaches up to 99.74% during a month of performance testing duration.

Keywords: internet of things (IoT); MPPT charge controller; solar charge controller (SCC); perturb and observe (P&O); microcontroller-based SCC; MATLAB/SIMULINK; PV system

1. Introduction

Energy sources are facing rapid transitions around the world. This shifting trend between fossil fuels and renewable energy is mainly being steered by the growing energy demand, environmental concerns, and call for green technology. While fossil fuels could continue to offer nearly 80% of total energy demand until 2040, renewable generation envisages capturing more than 50% of the demand thereafter, with an existing annual growth rate of 2.5% [1]. This notion reveals an obvious interest in and potential of renewable energy for future energy demand. Among the potential renewable energy sources (RESs), including solar energy, wind energy, bioenergy, hydro energy, geothermal energy, marine energy etc., solar energy has risen as one of the top three most powerful forms of RESs.

The International Renewable Energy Agency (IRENA) reported that the aggregate sum of 6586 terawatt hour (TWh) power generated from renewable energy sources in 2018. Sustainable hydro represented about 4149 TWh (63%), trailed by wind energy at 1263 TWh (19%), solar energy at 562 TWh (9%), bioenergy at 523 TWh (8%), geothermal energy at 88 TWh (1%) and marine energy at 1 TWh [2].

Despite the rapid expansion of solar energy uses, the non-linearity characteristics of solar cells pose a major challenge to harness the maximum power from the solar energy. Particularly, the current-voltage (I-V) and power-voltage (P-V) curves of the solar photovoltaic (PV) system hold a nonlinear property that highly depends on solar irradiance, temperature and load [3]. Based on the fluctuation of irradiance and temperature, the voltage and current continually vary the expected maximum output power from the PV system. This nonlinear nature of the PV panel brings down the energy conversion ability and boosts the system installation cost. To overcome the hindrance of nonlinearity, PV panels must be operated at maximum power point (MPP) under varying atmospheric circumstances [4–7]. Several maximum power point tracking (MPPT) techniques have been developed for the solar charge controller (SCC) and studied to track this MPP of the solar cell. For example, perturb and observe (P&O) [8–17], incremental conductance (IC) [18–23], genetic neural algorithm [24–26] and fuzzy logic control (FLC) are studied [27–29] that can operate the solar PV panel at MPP with relatively higher efficiency. However, among them, the P&O algorithm is popular for its simplicity and high efficiency. SCC with MPPT utilizes the output of the PV panel (i.e., the voltage and current) to produce the pulse width modulation (PWM) signal to control the boost converter's output [30]. Without a controller circuit, a PV panel can accomplish MPPT, but an efficient power transfer may not be often ensured, resulting in a higher power loss, whereas an MPPT-SCC can transfer more than 90% of the PV panel power to the battery [31].

However, available MPPT-SCCs in the market are inconvenient, expensive, and antiquated. Their operating process is usually complex for urban and non-technical people. Additionally, no smart data monitoring features were adopted in those controllers. To meet the current demand for energy, an efficient way of energy harvesting and distributing is very important. In modern societies, to meet the balance between supply and demand, sometimes load-shedding or shifting is needed. A standalone solar PV system that is equipped with any kind of backup energy storage, such as a battery, can produce the required power for the loads. Batteries are regarded as the highest effective source for home energy supply in isolated as well as rural regions [32]. Besides, due to the trend of the smart city, smart buildings, smart homes, smart gadgets, and the economical use of electricity without hampering human comfort [33,34], a smart device is needed that can harness and distribute the energy in an algorithmic way from the PV system. Therefore, the need for an efficient MPPT-SCC is sensed more than any time.

In this paper, an efficient SCC with IoT features is presented. Particularly, a charge controller prototype is designed with a 10-bit PIC16F877A microcontroller [35], having a flexible and sufficient I/O pin, 8 K flash program memory, and 356 bytes data memory. As a motivation, the prototype is equipped with the IoT platform to send vital data to the webserver for remote monitoring and controlling. The data are continuously sent to the cloud for further analysis and also for monitoring the status of the PV system using the website or mobile apps. These data can also be used to determine any possible faults of either PV system, batteries, or MPPT-SCC. Finally, a modified buck-boost converter is used to effectively deliver the harvested power from the solar panel to the load. The proposed MPPT-SCC is designed with an external device charging unit, real-time data monitoring display, and the IoT-based sensors to redefine the controller with time features. The proposed controller is computationally modeled and simulated with MATLAB/SIMULINK environment, and also, practically implemented with a laboratory set up, to learn its real-time performance improvement over the prominent charge controllers.

This paper is structured as follows. Section 2 captures a brief overview of the state of the MPPT solar charge controller. A brief outline of the P&O algorithm followed by the modeling of the PV array with MPPT technique is explained in Section 3. The proposed system is presented in Section 4.

The complete simulation and experimental setup with the specifications of each module is presented in Sections 5 and 6, respectively, to validate the proposed MPPT-SCC system. The manuscript concludes with the results, which are accompanied by a thorough analysis.

2. Current Research Trends of MPPT Solar Charge Controller

Different techniques and algorithms are being used in developing the MPPT-SCC. Despite their variety in operating principles, a common objective of the previous and recent research works is to improve the MPPT efficiency at a low cost, without hampering daily energy consumption routines. Tawfik Radjai et al. [36] presented a fuzzy logic controller based on a newly modified P&O MPPT technique with an adaptive duty cycle, which showed 98% efficiency. The authors presented both the simulation and hardware design of the prototype by using a CUKDC-DC converter and a SunTech STP085B PV module. Similarly, Ankur Bhattacharjee et al. [12] developed and validated a MPPT battery charger to use in PV applications. The authors proposed a vanadium redox flow battery (VRFB) instead of lead-acid and Li-ion batteries, and used a three-stage constant current constant voltage (CC-CV) topology and found 94.5% efficiency to charge the VRFB. Anil S. Hiwale et al. [11] implemented a hardware prototype with 87% efficiency using the P&O algorithm. Here, the controller generates the pulse width modulation (PWM) signal and controls the buck converter to extract the power from the PV module. John Macaulay et al. [13] proposed a fuzzy logic controller-based variable step size P&O MPPT technique for the standalone PV system. An enclosed emulated PV system including DC power source, boost converter, and a DSPACE card is used to implement the presented system. The tracking efficiency is improved by 0.38% compared to the existing algorithm. Unal Yilmaz et al. [37] have recently presented a fuzzy logic and PI controller MPPT-SCC for the PV system to rapidly charge the battery, reduce the losses, and improve the battery life cycle. The complete system was established and examined in the MATLAB/SIMULINK environment and provided 94.8–99.4% efficiency. In an earlier work, Rahul Dubey [38] reported a 99% efficient simulation model of a neural network MPPT controller integrated with a hysteresis current controlled inverter (HCCI) for a PV system. Jubaer Ahmed et al. [10] also reported an improved P&O MPPT algorithm for higher efficiency. Using the MATLAB/SIMULINK environment, the authors reported an overall improvement of 2% for their 99.2% efficient MPPT.

In summary, available MPPT-SCCs in the market do not support any IoT-based smart features, neither are they cost-effective and user friendly for use by urban and non-technical people. Therefore, the requirements of these features and higher efficiency have been the key criteria of SCC development in a more efficient way of energy harvesting and distributing.

3. Modeling of the PV Array and MPPT Techniques

Some factors dominate the output of PV cells, such as solar irradiance, temperature, shadows, and dirt. The literature review shows some interesting models of solar cells [39,40]. The single diode model and the double diode model are very popular electrical models for the solar cell. Comparing with the double diode model, the single diode model is efficient as well as simple to design, including the low value of series resistance, and have an ideal diode factor that can provide improvement in the results of PV cells [36]. Hence, a single diode PV model is used in this research work. A simplified equivalent single diode electrical model of solar cells is illustrated in Figure 1. The respective I-V curve relation can be represented by Equation (1).

$$I = I_{sc} - I_o \left[\exp\left(\frac{V + R_S I}{\frac{N_s K T}{q} a}\right) - 1 \right] - \left(\frac{V + R_S I}{R_{sh}} \right) \quad (1)$$

where I_{sc} is the short circuit current, I_o denotes the saturation current, the diode ideality constant is a , N_s is the series-connected cell, T is the temperature of the PN junction, $K = 1.38 \times 10^{-23} \text{ J/K}$ is the Boltzman constant, $q = 1.6 \times 10^{-19} \text{ C}$ is the charge of an electron, and R_S , and R_{sh} are the series

and shunt resistance of the array, respectively. If the thermal voltage of the array, $V_t = \frac{N_s K T}{q}$ then, Equation (1) can be rewritten as:

$$I = I_{sc} - I_0 \left[\exp\left(\frac{V + R_S I}{V_t a}\right) - 1 \right] - \left(\frac{V + R_S I}{R_{sh}} \right) \quad (2)$$

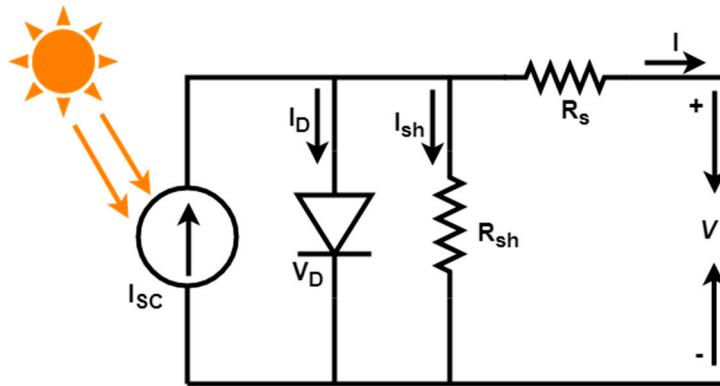


Figure 1. Equivalent single diode electrical model of a solar cell.

The most common and very popular MPPT techniques are perturb and observe (P&O) and incremental conductance (IC). To implement the MPPT in solar panels, the P&O algorithm is the simplest and cheap solution. This algorithm can easily adapt to both the software and hardware platform [16]. Therefore, the P&O algorithm (Algorithm 1) is chosen here to implement the proposed system. P&O works based on the disruption of panel array voltage. Figure 2a illustrates the P–V curve when the P&O algorithm is active. The output power of an MPP SCC is oscillating continuously around the MPP. By reducing the perturbation step rate, the oscillations of the P–V curve can be minimized.

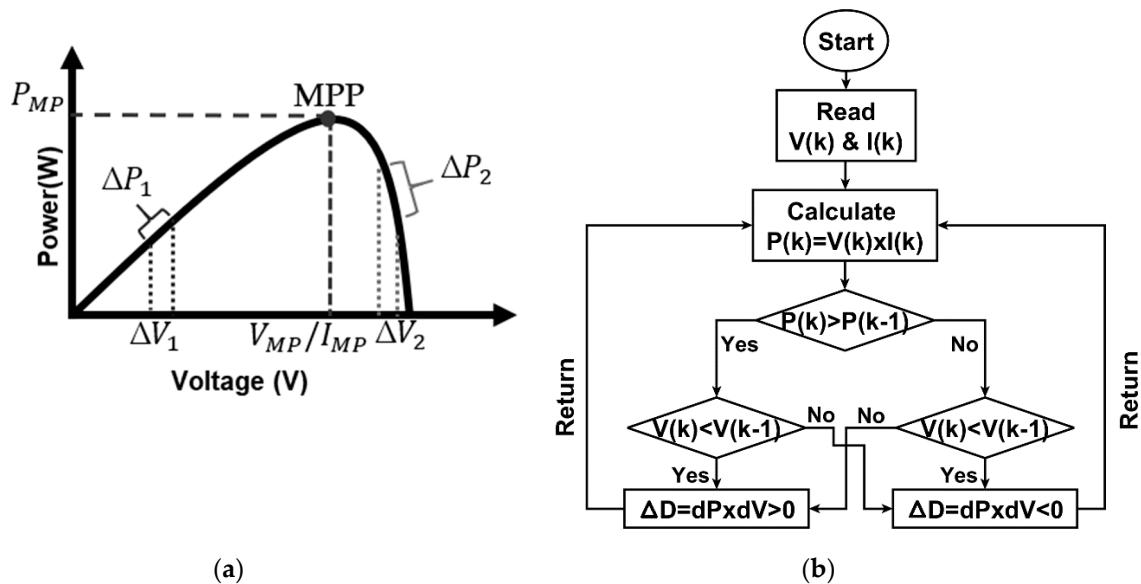


Figure 2. (a) P–V curve of a solar PV array on P&O (b) proposed flowchart of P&O algorithm.

Algorithm 1 Proposed P&O algorithm:

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State 1: Start
State 2: Measure Variables  $V(k)$  and  $I(k)$ 
State 3: Estimate power:  $P(k) = V(k) \times I(k)$ 
State 4: Call previous power  $P(k-1)$  and voltage  $V(k-1)$ 
State 5: Estimate the changed power 'dP' and changed voltage 'dV':
     $dP = P(k) - P(k-1)$  and  $dV = V(k) - V(k-1)$ .
State 6:
    If,  $dP = 0$ 
    Else  $\Delta D = dP \times dV > 0$ 
    Else  $\Delta D = dP \times dV < 0$ 
    } Then step forward to State 7.
State 7: Return.

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Figure 2b illustrates the proposed flowchart of the P&O algorithm. Following State 5, the dP represents a small change in power, while the variation of the voltage is denoted by dV . According to Figure 2a, when the voltage is decreased, then, the power of the MPP increases; similarly, the power of MPP increases when the voltage is increased. This is the core concept behind the P&O algorithm. The algorithm equates the current power reading, P_k , with the previous power reading, P_{k-1} , after the execution of each increase in the panel operating voltage. The voltage would increase if the power raised; otherwise, it shifts the direction or decreases the voltage through the switching duty cycle. Until the MPP is touched, this process will be repeated at each MPP monitoring phase [31].

4. Proposed System Architecture

The proposed system is divided into two sections. One is a simulation section, and another is an experimental setup. In the experimental setup, a modified buck-boost converter is developed and used. Similarly, in the simulation section, a mathematical model of the buck-boost converter is designed, and the complete system of the proposed design is simulated.

The principal structure of the prototype hardware is presented by a block diagram shown in Figure 3. To achieve the highest energy productivity, the solar PV panel must work at MPP. The complete prototype of the proposed charge controller is shown in Figure 4. The input power source is the 85 W PV module. The state of the input voltage and current is sent to the microcontroller through the corresponding interfaced sensors. A modified buck-boost converter is used as an MPPT controller between the PV panel and battery. The load is connected to the battery. To monitor the system activities, a liquid crystal display (LCD) is connected to the microcontroller. As mentioned before, an IoT communication module is used for the remote monitoring system. In this project, a Bluetooth device is used as an IoT interface communication module, while other modules, such as the global system for mobile (GSM) module or Wi-Fi module, can also be used for IoT connection.

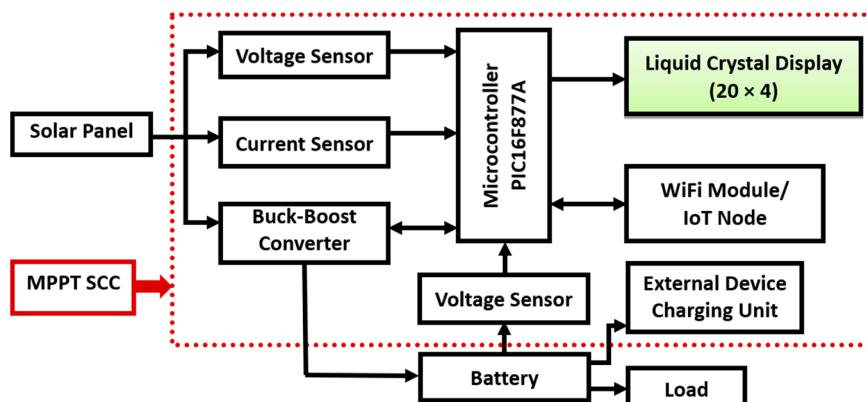


Figure 3. Proposed block diagram of the MPPT solar charge controller (SCC).

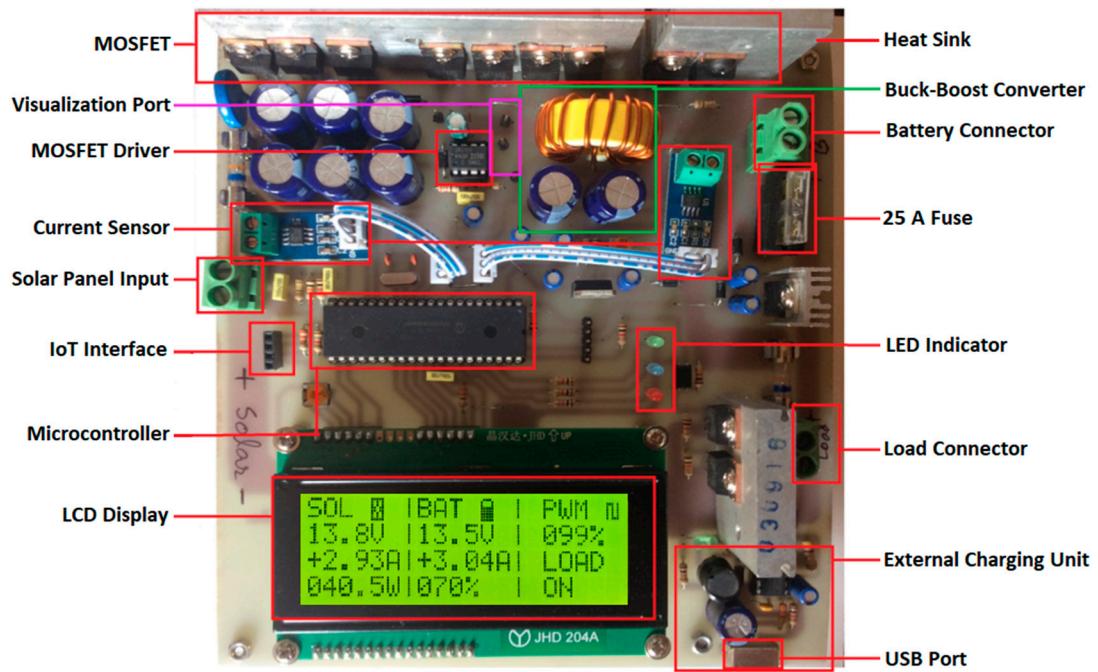


Figure 4. The complete prototype of the proposed charge controller.

The proposed buck-boost converter is selected and found from different configurations of the DC–DC converter reviewed to date [41]. A boost converter is a converter in which output must be equivalent to or larger than the input voltage.

According to Figure 5, when the switch is ON, the input voltage passes through the inductor. Therefore, the inductor voltage in this stage is $V_{in} = V_L$. When the switch is OFF, the diode becomes forward biased and the output voltage will be $V_{out} = V_{in} + V_L$. In steady-state conditions, the total energy stored in the inductor will be equal to the released energy when the switch is closed. The boost converter output voltage, value of an inductor, and the capacitor can be measured by the following equations:

$$V_{out} = \frac{V_{in}}{1 - D} \quad (3)$$

$$L = \frac{V_{in} \times D}{\Delta I_L \times f} \quad (4)$$

$$C = \frac{I_{out} \times D}{\Delta V_{out} \times f} \quad (5)$$

A buck converter is a DC–DC converter where the voltage of output is always smaller than the voltage of input. The output of the buck converter, V_{0ut} , the value of an inductor, L , and value of the capacitor, C , can be measured by the following equations:

$$V_{0ut} = V_{in} \times D \quad (6)$$

$$L = \frac{V_{0ut} \times (1 - D)}{\Delta i_L \times f} \quad (7)$$

$$C = \frac{(1 - D)}{8L \left(\frac{\Delta V_{out}}{V_{out}} \right) \times f^2} \quad (8)$$

Here, the duty cycle ratio is denoted by D , f is the frequency, ΔI_L is the inductor current, and ΔV_{out} is the peak to peak ripple voltage of the output.

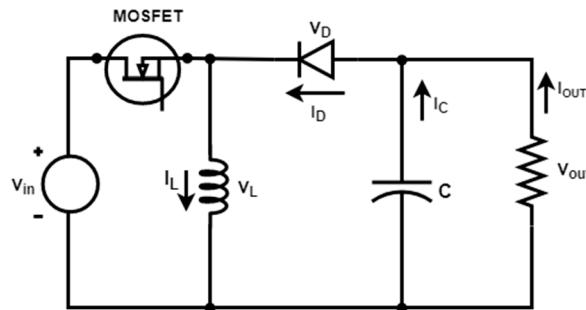


Figure 5. Proposed buck–boost converter.

In this work, a modified buck–boost converter is proposed, which is shown in Figure 5. A metal-oxide semiconductor field-effect transistor (MOSFET) is replaced instead of a traditional switch. MOSFET is a switching device that facilitated the reduction in the measurable amount of voltage drop in diodes. When the MOSFET is in ON mode, then, the current flows through the circuit and inductor stores the energy. When the MOSFET is in OFF mode, then, the diode is ON and the inductor releases the stored energy [42].

5. Simulation Setup and Results

Function block parameters are shown in Table 1 to develop the subsystem mask of the SM-85KSM PV module. The ideal factor (I_F) of 1.3, open circuit voltage (V_{OC}) of 19.7 V, short circuit current (I_{SC}) of 5.9 A, short circuit current temperature coefficient (TC) of 0.003, 36 cells in series, 1 cell in parallel and the reference temperature of 298 K are used.

Table 1. Functional block parameters of the SM-85KSM PV module.

I_F (uL)	V_{OC} (V)	I_{SC} (A)	TC of I_{SC} (uL)	N_S (uL)	N_P (uL)	T (K)
1.3	19.7 V	5.9 A	0.003	36	1	298 K

unitless (uL).

Figure 6a,b present the I–V and the P–V characteristics curve of the proposed PV module model, respectively, in different solar irradiances at 25 °C constant temperature. The lowest irradiance is 200 W/m², and in this state, the PV panel produces the lowest power. The highest irradiance is 1000 W/m², and in this state, PV panel generates the highest power.

Figure 7 shows the proposed mathematical model for the buck–boost converter, which is simulated in MATLAB/SIMULINK. Repeating the sequence and duty cycle generates pulses and connected to the MOSFETs, gain as a switching signal.

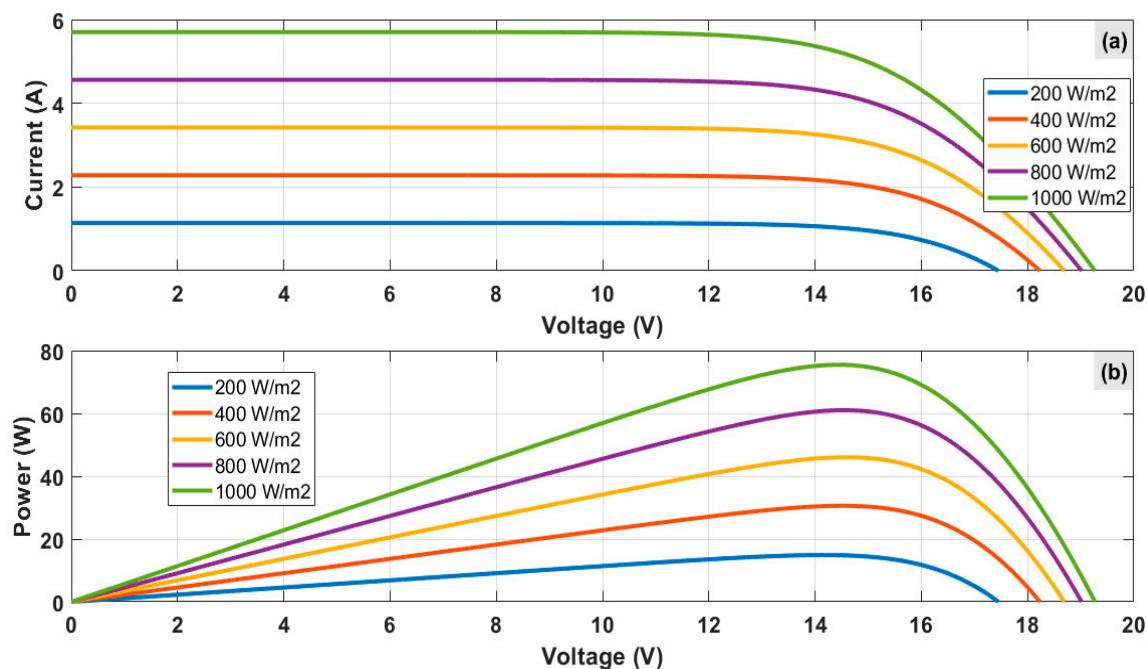


Figure 6. Characteristics curve of the proposed SM-85KSM PV module for different solar irradiance at 25 °C. (a) I-V (current–voltage) curve (b) P-V (power–voltage) curve.

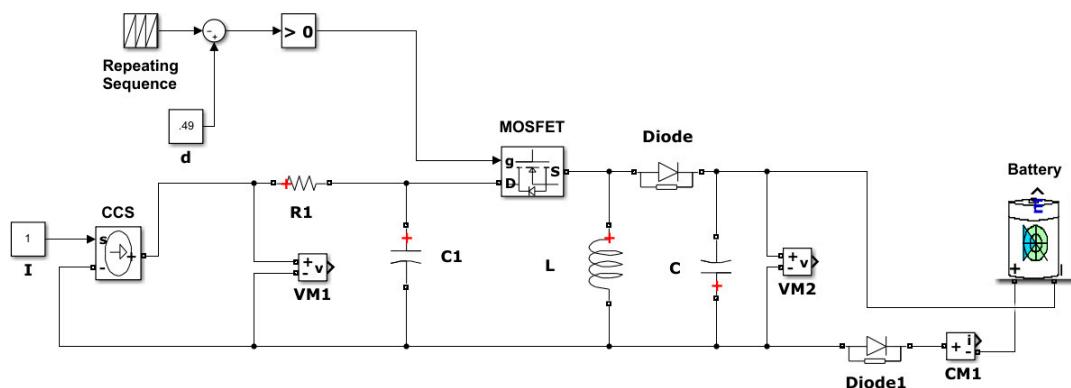


Figure 7. Simulation diagram of buck–boost converter.

The output of the buck–boost converter is shown in Figure 8 in three individual plots. The first plot shows the output voltage of the converter. The output voltage is unstable in the time of 0 to 0.1 s and the maximum voltage in this time range is 17.1 V. The output starts to stabilize from 0.1 s and is immediately stable with the voltage of 16 V. The second plot shows the output current of the converter where the maximum current is higher than 3.5 A in the 0 to 0.1 s. Later, from 0.1 s, the current stabilizes with the constant current of 2.20 A. The third plot is the battery charging state at 13.5 V.

The proposed SIMULINK model of the MPPT solar charge controller is shown in Figure 9. A PV module of SM-85KSM, the buck–boost converter, which is sub-masked of a 12 V, 100 Ah lead-acid battery, MPPT block, makes the complete system operable standalone PV system.

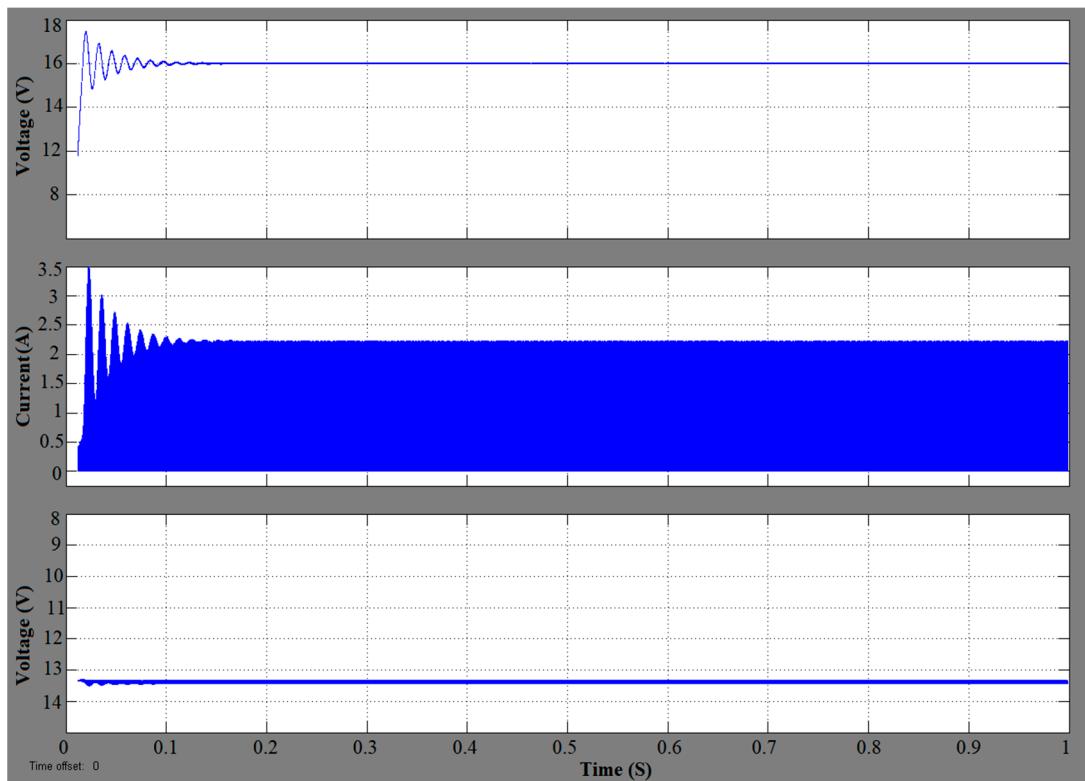


Figure 8. Simulation output of the buck-boost converter.

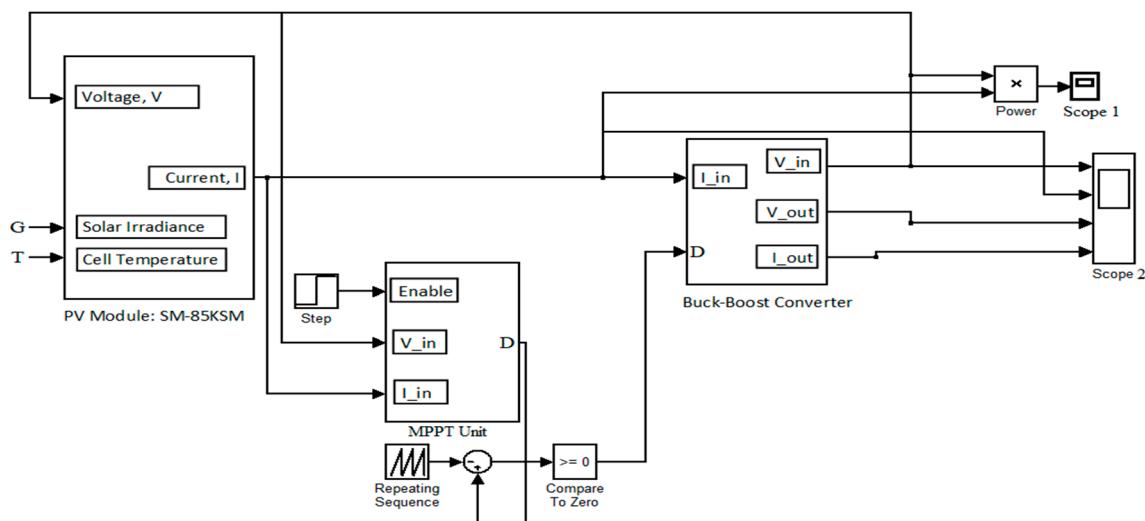


Figure 9. Proposed MPPT solar charge controller in MATLAB/SIMULINK.

The maximum solar irradiance (G) of 1000 W/m^2 and temperature (T) of 298 K are used. Figure 10 presents the simulation results, where four scope blocks are connected to the output of them. The scope shows the converter input voltage (V_{Input}) in the first plot, input current (I_{Input}) in the second plot, output power (P_{Output}) in the third plot, and the output current (I_{Output}) in the fourth plot.

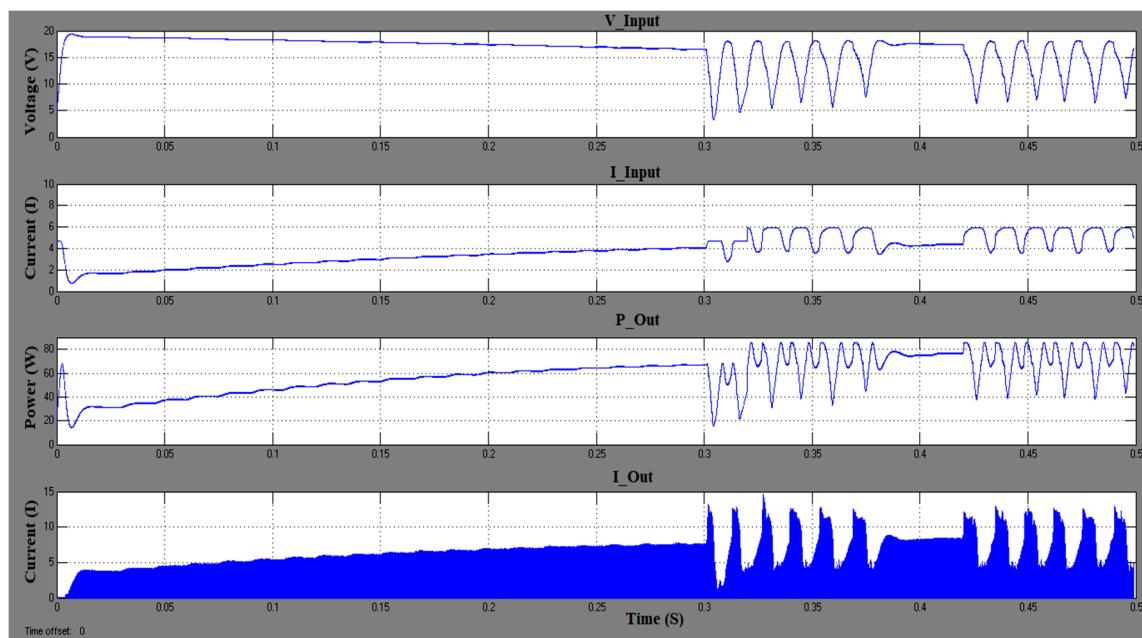


Figure 10. Simulation results of the proposed charge controller.

6. Experimental Setup and Results

A real-time experiment is carried out to validate the simulation results. The experimental setup for the validation of the designed solar charge controller is shown in Figure 11a,b. Figure 11a shows the PV panel on the rooftop, model number SM-85KSM from KYOCERA, Japan. Figure 11b shows the complete laboratory setup with the battery and solar testbed. A 12 V, 100 Ah lead-acid battery from HAMKO is used for energy storage. The output power of the PV module is stored in the battery through the solar charge controller; the controller operation is tested by the digital oscilloscope—the brand name is GWINSTEK and the model number is GDS-2204A. The incoming voltage, current as well as the battery condition are directly displayed by the analog meter board.

Figure 12a shows the PV output voltage (Channel 1, red color) and the converted voltage (Channel 2, blue color) of the buck-boost converter from the oscilloscope in a single plot with respect to $10\ \mu s$ time. The PV voltage is almost 16 V, which is over the range to charge the battery, so the converter reduces the voltage to 13 V, as the highest required voltage to charge a lead-acid battery is 14.4 V without damaging the battery. The converter output voltage, duty cycle and the battery charging state is shown in Figure 12b, as the channel 1 (blue color), channel 2 (red color) and channel 3 (green color), respectively, in a single plot. The plot is taken in $10\ \mu s$ timeframes and the zoomed portion observed at $2\ \mu s$ timeframes. The converter voltage in blue color is shown in the first plot, the duty cycle is presented in the second plot in red color, and the third plot is the battery charging state in green color. The on-time of the duty cycle is 98% and the rest 2% of the duty cycle is shown on the right side of the second plot in the zoomed version. The effect of the rest 2% duty cycle on the battery charging state is also shown on the right side of the third plot as a zoomed version. Both the zoomed signal is in $2\ \mu s$ time range.

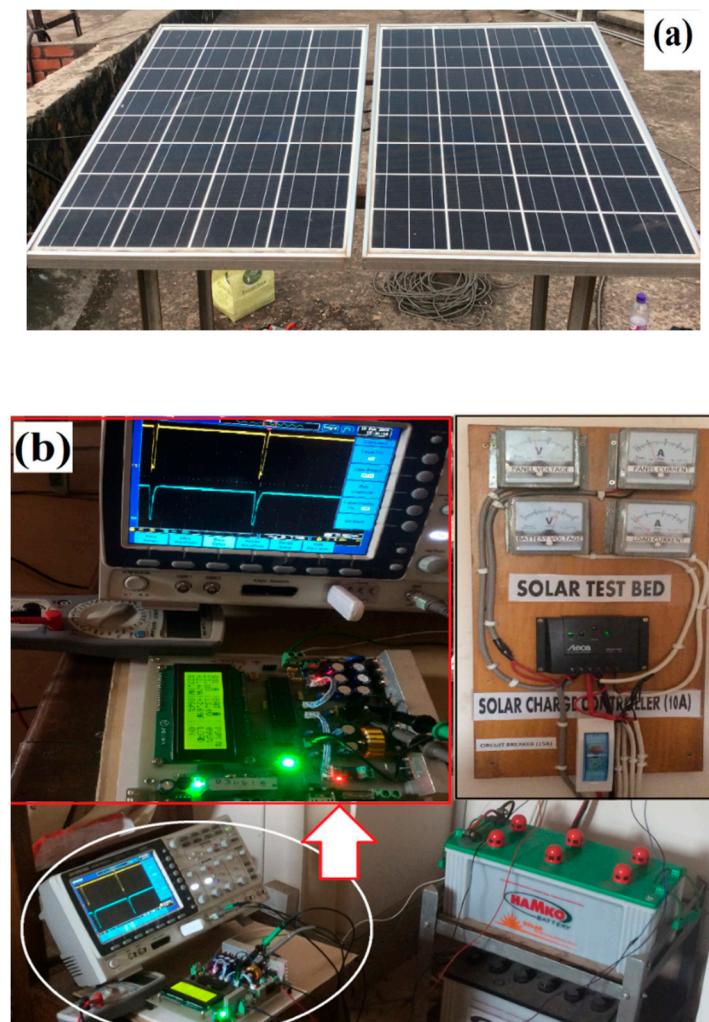


Figure 11. Experimental setup of the complete system: (a) PV module on the rooftop, and (b) laboratory setup (inset) with battery (bottom-right corner) and metering board (top-right corner).

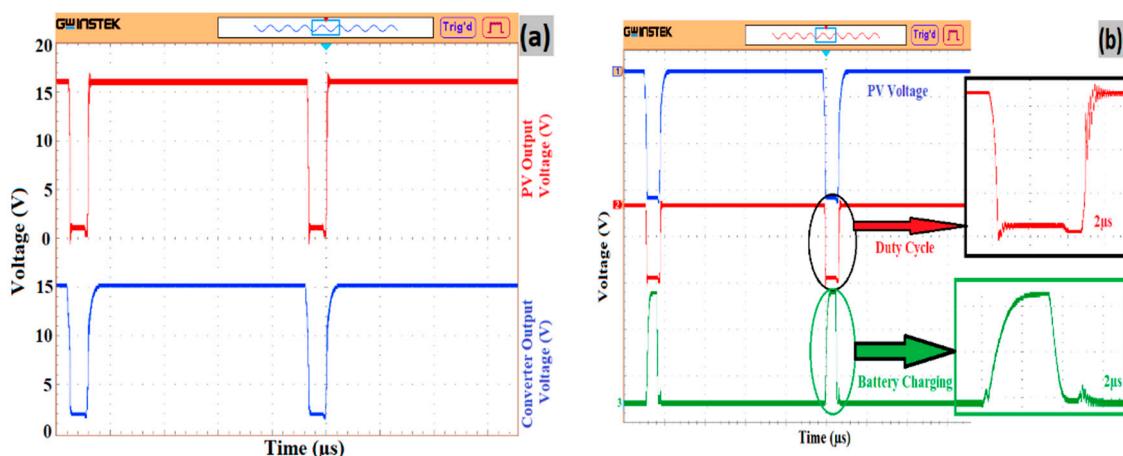


Figure 12. (a) The output waveform of the buck-boost converter from the oscilloscope, (b) output plot from the oscilloscope.

The crucial data, such as related PV panel and batteries system voltages, currents, temperatures, input and output power of the charge controller, state of charge of batteries, etc., are collected through IoT-enabled sensors of the charge controller and transferred to the webserver or other resources using the IoT concept. These data then will be available from a smartphone or webpage, as shown in Figure 13a. In this project, the logged data are transferred to an online service named “Byte stream mode”. This enables the users to monitor the charge controller from the remote area. This device is also compatible with the GSM and Bluetooth modules to directly send warning messages during abnormal situations such as the high temperature of the batteries, etc., to the cellphone. Figure 13b shows the function of the external device charging unit through the universal serial bus (USB) port. A smartphone is charging through the USB port, while the charge state of the battery is 45%. Incoming PV voltage is 20.7 V, manually measured by the digital multimeter. This USB port is enabled to charge any electronic device without any charger.

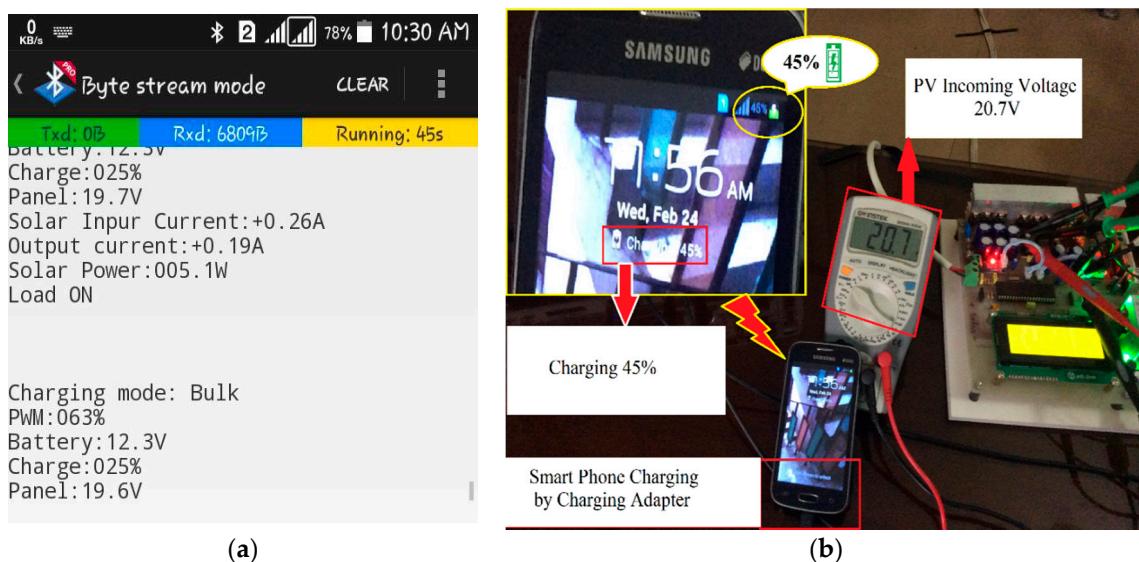


Figure 13. (a) System monitoring by smartphone through IoT, (b) external device charging unit.

The experimental results of the proposed MPPT solar charge controller are shown in Table 2. The experimental values are taken at the times of 8.30 a.m. to 5.00 p.m. After 30 min average interval, the results are recorded manually as well as compared with the value of LCD. The highest efficiency, 99.73924381~99.74, is recorded at 1.30 p.m., where the PV power is 25.311 W and the extracted power by the system to the load is 25.245 W. This proves that the MPPT technique to extract the maximum power from the PV panel is working efficiently. Figure 14a–d depicts the value of (a) PV and load voltage, (b) PV and load current, (c) PV and load power, and (e) efficiency graphically. Equation (9) is used to determine the charge controller efficiency (η).

$$\eta = \frac{P_{out}}{P_{in}} \times 100\% \quad (9)$$

where, P_{out} = output power and P_{in} = input power.

From the obtained results, the comparative analysis of different MPPT techniques efficiency is shown in Table 3.

Table 2. Experimental results achieved from the proposed charge controller.

Sl. No.	Time	Panel			Load			Efficiency (%)
		Voltage (V)	Current (A)	Power (W)	Voltage (V)	Current (A)	Power (W)	
1	08.30 AM	14.4	1.58	22.752	12.6	1.76	22.176	97.46835443
2	09.00 AM	13.9	2.89	40.171	13.4	2.83	37.922	94.40143387
3	09.30 AM	14.2	1.99	28.258	13.0	1.74	22.62	80.04812796
4	10.00 AM	13.6	1.89	25.704	13.3	1.92	25.536	99.34640523
5	10.30 AM	14.0	2.45	34.3	13.6	2.51	34.136	99.52186589
6	11.00 AM	14.1	2.58	36.378	13.9	2.61	36.279	99.72785750
7	11.30 AM	14.2	0.26	3.692	12.2	0.25	3.05	82.61105092
8	12.00 AM	14.2	2.78	39.476	13.9	2.82	39.198	99.29577465
9	12.30 PM	13.8	1.92	26.496	13.5	1.95	26.325	99.35461957
10	01.00 PM	14.0	2.59	36.26	14.1	2.53	35.673	98.38113624
11	01.30 PM	14.3	1.77	25.311	13.5	1.87	25.245	99.73924381
12	02.00 PM	13.9	0.47	6.533	12.8	0.47	6.016	92.08633094
13	02.30 PM	14.0	1.79	25.06	13.5	1.80	24.3	96.96727853
14	03.00 PM	14.5	2.64	38.28	14.1	2.68	37.788	98.71473354
15	03.30 PM	13.4	0.51	6.834	12.9	0.52	6.708	98.15627744
16	04.00 PM	13.4	0.47	6.298	12.9	0.47	6.063	96.26865672
17	04.30 PM	13.3	0.45	5.985	12.9	0.46	5.934	99.14786967
18	05.00 PM	13.3	0.55	7.315	12.9	0.55	7.095	96.99248120

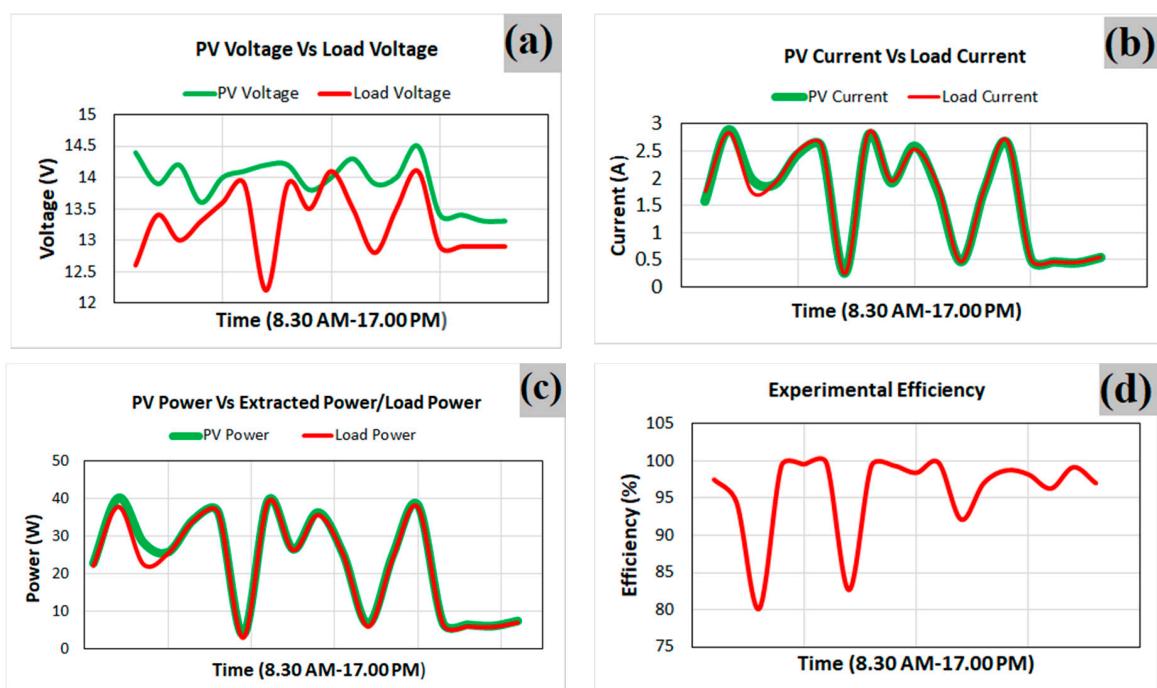
**Figure 14.** (a–d) Graphical representation of experimental results and efficiency.

Table 3. Comparative analysis of different MPPT technique efficiency.

References	Author's Name	Year	Tech.	Efficiency	RM
[10]	Jubaer Ahmed et al.	2015	P&O MPPT	99.20%	SI
[11]	Anil. S. Hiwale et al.	2014	P&O MPPT	87%	HI
[12]	Ankur Bhatt. et al.	2018	P&O MPPT	94.5%	SSHI
[13]	John Macaulay et al.	2018	FLC P&O	0.38%	SSHI
[36]	Tawfik Radjai et al.	2015	P&O MPPT	98%	SSHI
[38]	Dubey et al.	2014	ANN	99%	SI
[37]	Unal Yilmaz et al.	2018	FLC MPPT	94.8–99.4%	SI
*	Proposed design	2020	P&O MPPT	99.74%	SSHI

* SSHI—Software Simulation (SI) and Hardware Implementation (HI), Tech.—Technique, RM—Research Mode.

7. Conclusions

An IoT-equipped MPPT-SCC is designed, implemented, and tested in this paper. The proposed MPPT-SCC consists of a common P&O algorithm with a modified buck–boost converter. To validate the results, the proposed hardware was first simulated in the MATLAB/SIMULINK platform and then, a prototype device was made and tested for one month. Then, the proposed design was validated through simulation and experimental results. The experimental results show that the proposed SCC has an acceptable performance and efficiency of around 99.74%. The proposed charge controller is equipped with an IoT platform that enables us to easily monitor the condition of the SCC remotely. To improve the performance further, thorough investigation and optimization are necessary. The collected data through the IoT platform can be used in smart home applications as training data for machine learning (ML) techniques. ML besides P&O can be incorporated in the future to increase the speed, reduce the fluctuation around the maximum power point, and increase the efficiency further of the device.

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