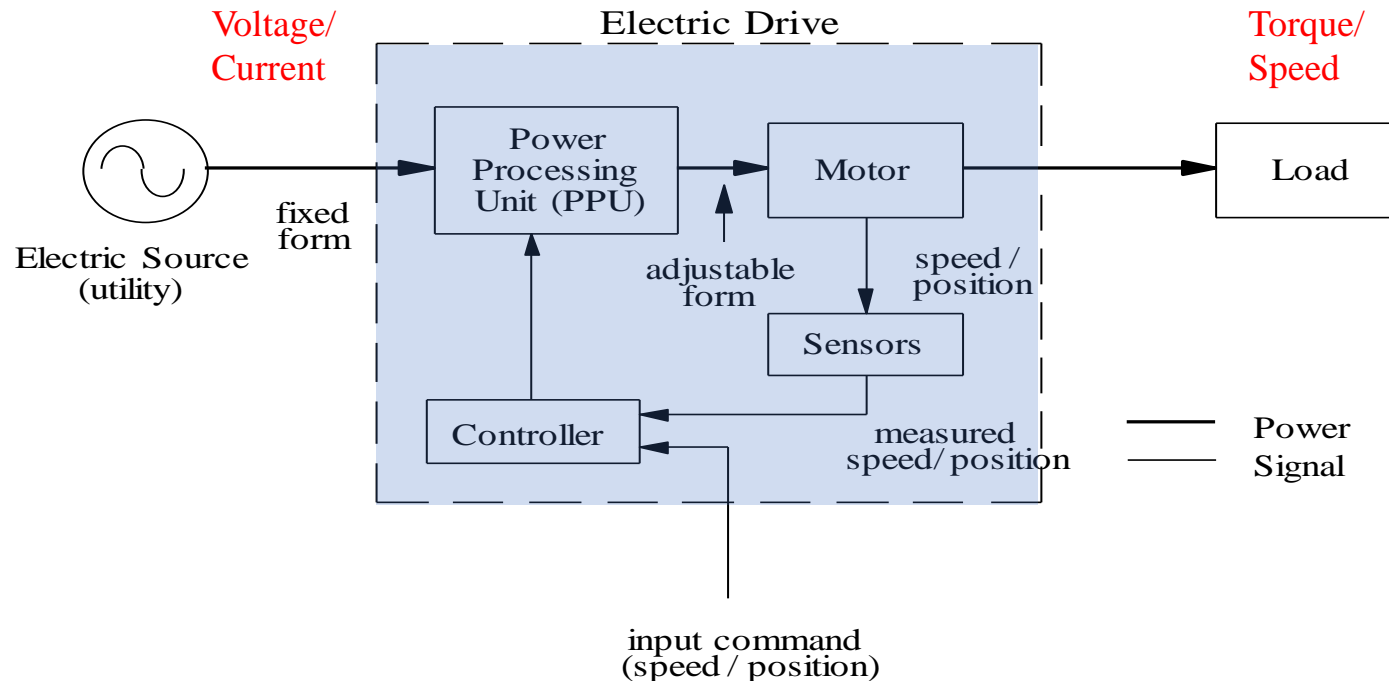


# Understanding Mechanical System Requirements

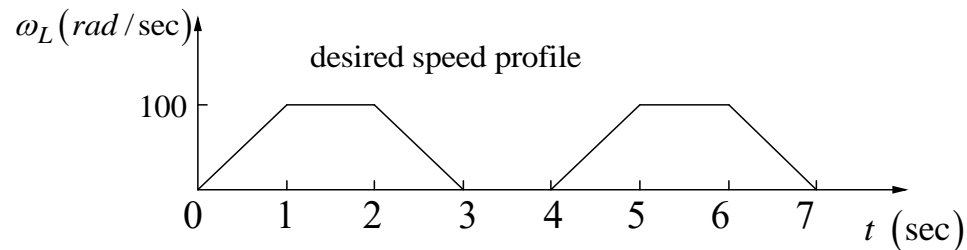
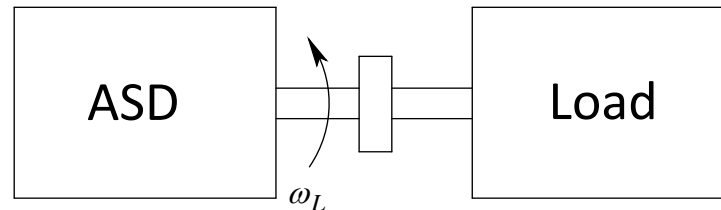
ASD

# Block diagram of adjustable speed drives



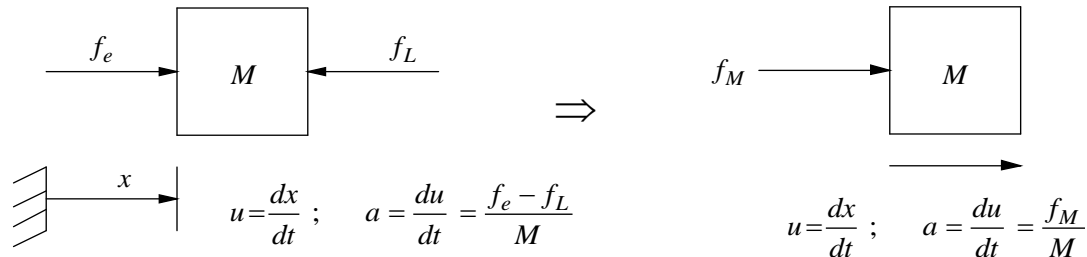
- *Electric drives* are an interface between an *electrical system* and a *mechanical system*.

# How can the ASD accelerate and decelerate the load to give desired speed profile?



- *Electric drive* must satisfy the requirements of *torque and speed* imposed by *mechanical loads* connected to them.
- The load in this figure may require a trapezoidal profile for the angular speed.
- Understanding *the requirements* from *mechanical system* is *necessary* for selecting an *appropriate electric drive* for a given application

# Systems With Linear Motion

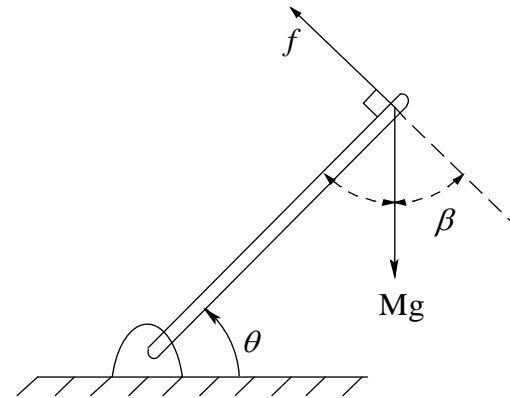
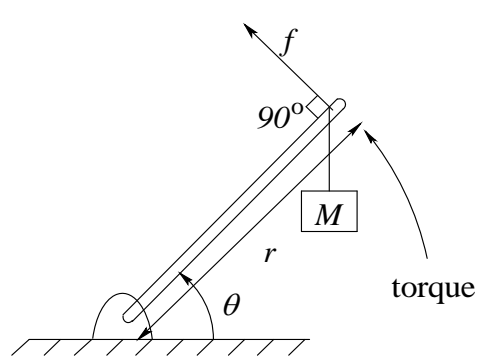


- ❑ Figure on left includes load force,  $f_L$ , that must be overcome
- ❑ Figure on right shows only the force,  $f_M$ , available to accelerate the mass,  $M$

Acceleration	Power Input	Kinetic energy
$a = \frac{f_e - f_L}{M} = \frac{f_M}{M}$	$P_e(t) = f_e \cdot u = \underbrace{f_M \cdot u}_{\text{Power for accelerating the mass}} + \underbrace{f_L \cdot u}_{\text{Power for load (work or friction loss)}}$	$W_M = \frac{1}{2} M u^2$
		$\underbrace{\hspace{10em}}_{\text{Stored energy in the moving mass}}$

# Rotating Systems

- Most electric motors are of a *rotating* type.



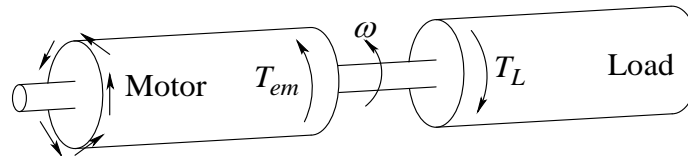
$$f = Mg \cos \theta$$

$$\tau = Mgr \cos \theta$$

☐ Torque = force    radius  
 $[Nm]$              $[N]$              $[m]$

- ☐ Example: what torque is needed to hold  $M$  motionless

# Torque in an electric drive

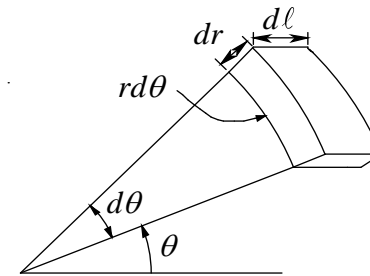
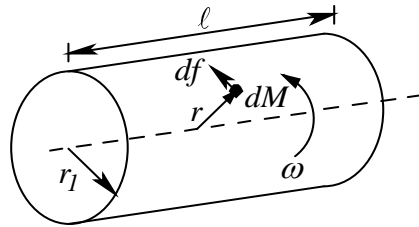


- ❑  $T_{em}$  electromagnetic torque produced by motor
- ❑  $T_{em}$  is opposed by load torque,  $T_L$
- ❑ The difference,  $T_{em} - T_L = T_J$ , will accelerate the system
- ❑ 
$$\frac{d\omega}{dt} = \frac{T_{em} - T_L}{J} = \frac{T_J}{J}$$

where  $J$  is the moment of inertia

- In a rotational system, the *angular acceleration*, due to the net torque acting on it, is determined by its *moment-of-inertia  $J$* .

# Calculation of Moment of Inertia $J$ of a Uniform Cylinder



$$d f = dM \frac{d}{dt} v$$

$$dM = \rho \underbrace{r d\theta}_{\text{arc}} \underbrace{dr}_{\text{height}} \underbrace{d\ell}_{\text{length}}$$

$$\Rightarrow dT = r^2 dM \frac{d}{dt} \omega = \rho (r^3 dr d\theta d\ell) \frac{d}{dt} \omega$$

$$T = \rho \left( \int_0^{r_l} r^3 dr \int_0^{2\pi} d\theta \int_0^{\ell} d\ell \right) \frac{d}{dt} \omega = \underbrace{\left( \frac{\pi}{2} \rho \ell r_l^4 \right)}_J \frac{d}{dt} \omega$$

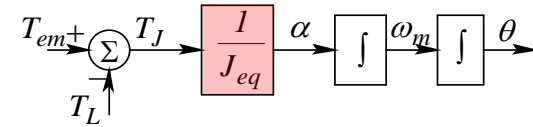
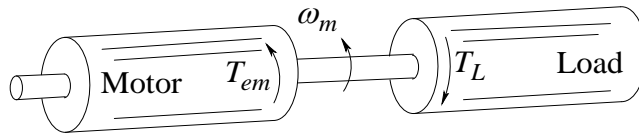
$$J_{\text{solid}} = \frac{\pi}{2} \rho \ell r_l^4 = \frac{1}{2} M r_l^2$$

$$\because M = \rho (\pi r_l^2) \ell$$

$\rho$  : material density in  $\text{kg/m}^3$

$\hookrightarrow r \downarrow \Rightarrow J \downarrow$

# Acceleration, Speed and Position, Power and Energy



*Motor and load torque interaction with a rigid coupling*

$$\text{acceleration, } \alpha = \frac{d\omega_m}{dt} = \frac{1}{(J_m + J_L)} (T_{em} - T_L) = \frac{T_J}{J_{eq}}$$

$$\Rightarrow \text{speed, } \omega_m(t) = \omega_m(0) + \int_0^t \alpha(\tau) d\tau$$

$$\Rightarrow \text{position, } \theta(t) = \theta(0) + \int_0^t \omega(\tau) d\tau$$

*Torque is the fundamental variable for controlling speed and position.*

*Dynamic model of mechanical system*

Power Input

$$P_{em}(t) = T_{em} \cdot \omega = \underbrace{T_J \cdot \omega}_{\text{Power for accelerating the rotating mass}} + \underbrace{T_L \cdot \omega}_{\text{Power for load (work or friction loss)}}$$

Kinetic energy

$$W = \frac{1}{2} J \omega^2$$

*Regenerative Braking.*

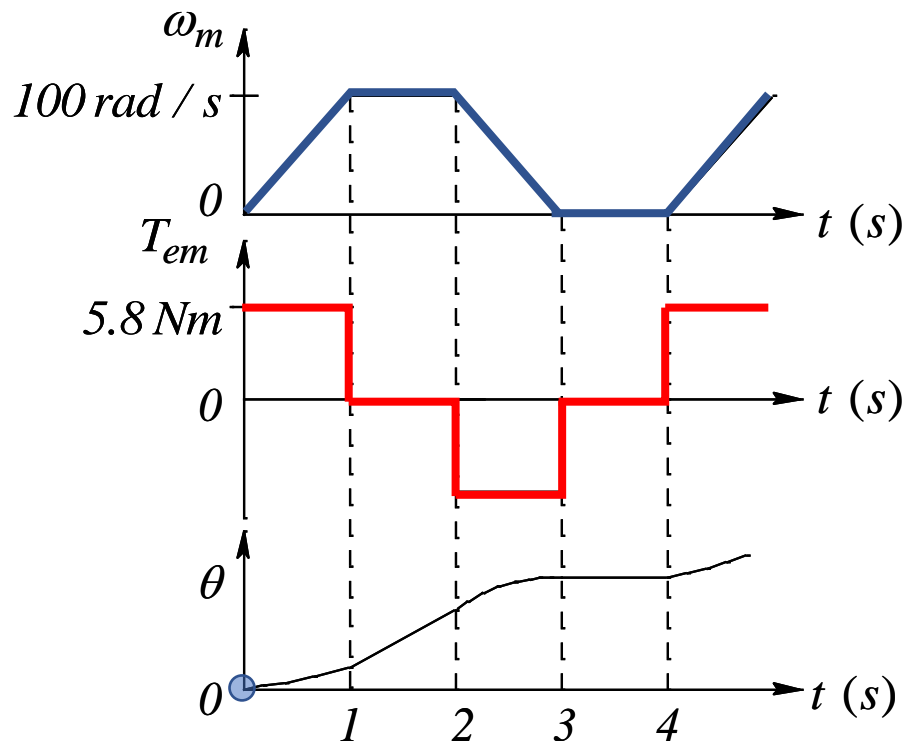
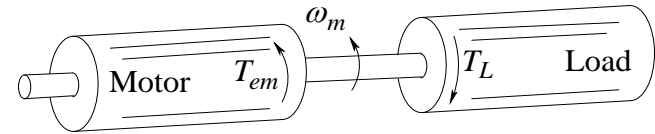
Power for accelerating the rotating mass

Power for load (work or friction loss)

Stored energy in the rotating mass of inertia  $J$



# Speed, torque, and angle variations with time



Consider that the above rotating system has the combined inertia  $J_{eq} = 0.058 \text{ kg.m}^2$  and is required to have a trapezoidal profile of angular speed profile shown on the left. The load torque is zero.

Calculate and plot the electromagnetic torque  $T_{em}$  required from the motor, and the change in position.

From the given waveform of angular speed, the magnitude of acceleration and the deceleration is  $100 \text{ rad/s}^2$ .

During the intervals of acceleration and deceleration, since  $T_L = 0$ ,

$$T_{em} = T_J = J_{eq} \frac{d\omega_m}{dt} = \pm 5.8 \text{ Nm}$$

During intervals with a constant speed, no torque is required

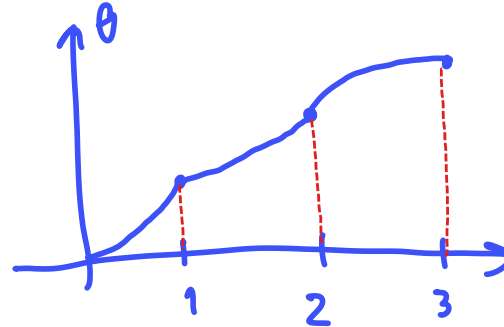
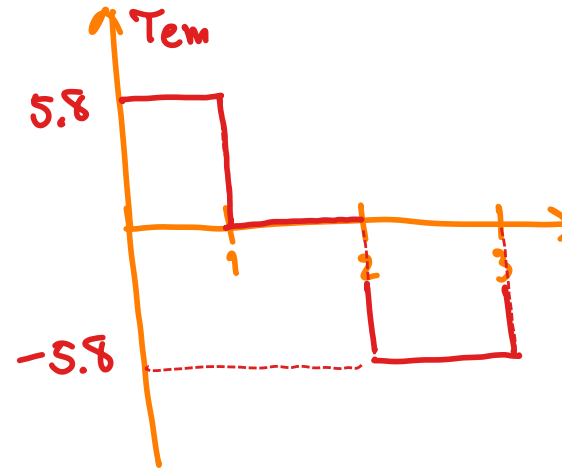
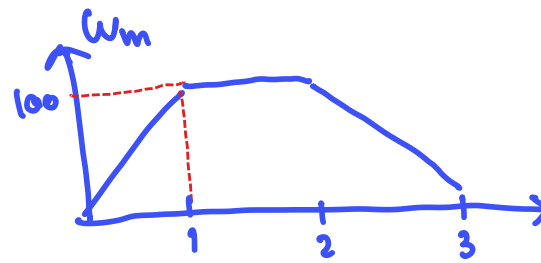
The position is the time-integral of speed :

$$\theta = \theta(0) + \int_0^t \omega_m d\tau \quad ; \quad \text{assume } \theta(0) = 0$$

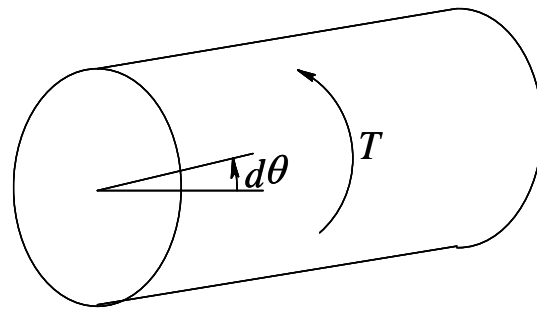
$$T_{em} - \overset{0}{T_L} = J_{eq} \frac{d\omega_m}{dt}$$

$$= 0.058 \times 100$$

$$T_{em} = 5.8 \text{ Nm}$$



# Torque, work, and power



Rotational system

- If a net torque  $T$  causes the cylinder to rotate by a differential angle  $d\theta$ , the differential work done is

$$dW = T d\theta$$

- The power can be expressed as:

$$p = \frac{dW}{dt} = T \frac{d\theta}{dt} = T \omega_m$$

- Substitute for torque  $T$ :

$$p = \underbrace{J \frac{d\omega_m}{dt}}_T \omega_m$$

- The *kinetic energy* stored in the rotating mass of inertia  $J$  is :

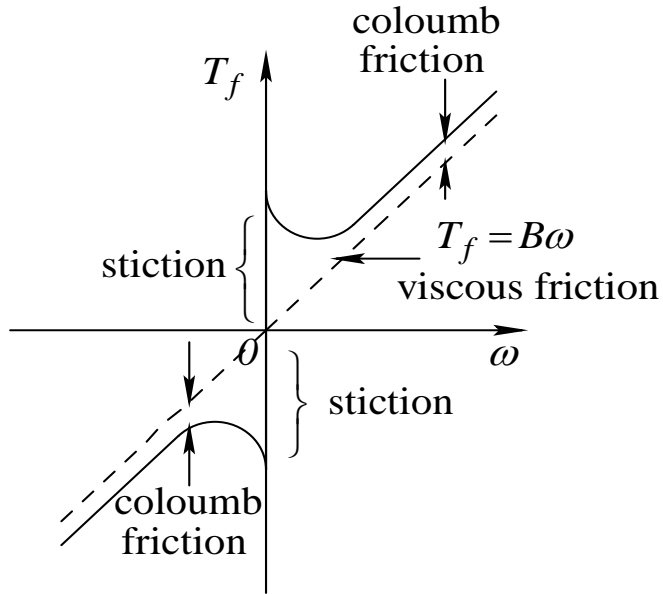
- *This stored kinetic energy can be recovered by making the power  $p(t)$  reverse direction ( $p(t) < 0$ ) !!*

$$W = \int_0^t p(\tau) d\tau = J \int_0^t \omega_m \frac{d\omega_m}{d\tau} d\tau = J \int_0^{\omega_m} \omega_m d\omega_m = \frac{1}{2} J \omega_m^2$$

## Friction in Machine

- Bearing
- Fan

# Frictional Torque



- ☐ Stiction: static component
- ☐ Coulomb friction: dynamic component (constant magnitude)
- ☐ Viscous friction: speed dependent
- ☐ In general, friction is non-linear

- *Friction* within the motor and the load acts to *oppose rotation*.
- *Friction* occurs in the *bearings* that support rotating structure and moving objects in air encounter *windage or drag*.
- In *vehicles*, this *drag* is a major force that must be overcome.
- The *friction characteristic* may be linearized for an *approximate* analysis by means of the *dotted line*.
- With this approximation, the characteristic is similar to viscous friction in which

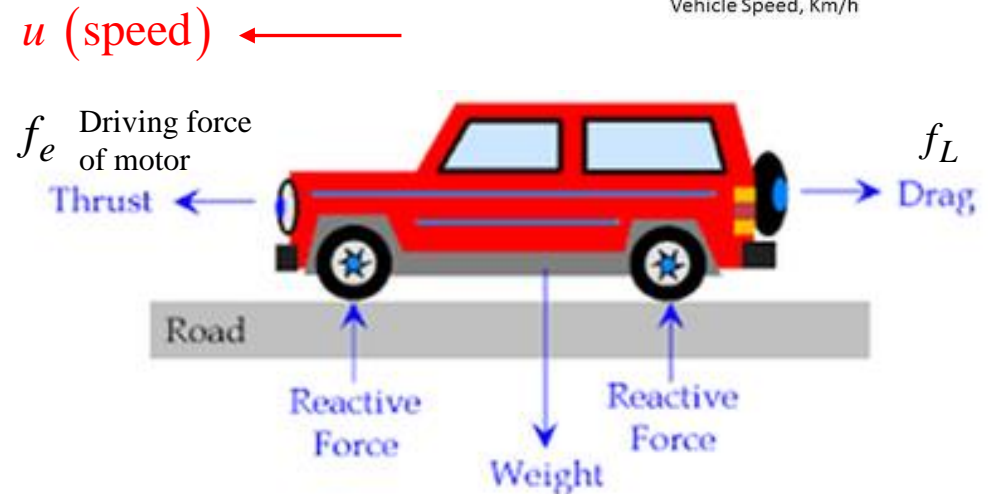
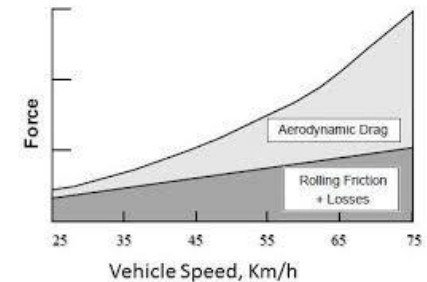
$$T_f = B\omega_m$$

Where  $B$  is the coefficient of viscous friction or viscous damping.

# Example: Aerodynamic drag

- The aerodynamic *drag force* in automobiles is a kind of *resistance force*.
- It is dependent on the velocity  $u$  of the vehicles.



$$f_L = 0.046 C_w A u^2$$



Drag power at different speeds

$$p = f_L \cdot u$$

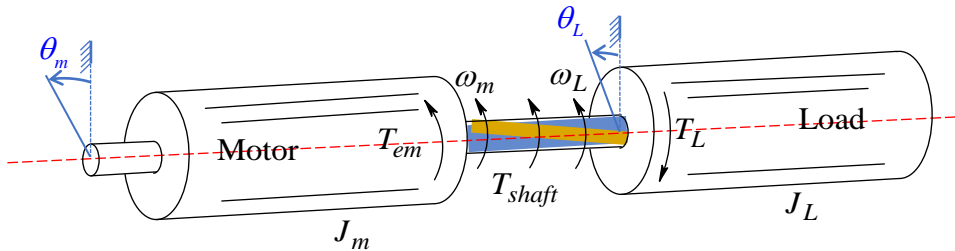
$\therefore$  power  $\propto$  speed<sup>3</sup>

Speed (km/h)	Power (w)	
	 $C_w = 0.3$	 $C_w = 0.5$
50	0.86 kW	1.44 kW
100	6.9 kW	11.5 kW
150	23.3 kW	38.8 kW

$C_w$ : drag coefficient (a unit-less quantity)

A: the vehicle cross-sectional area in m<sup>2</sup>

# Flexible Coupling /Torsional Resonances



At motor end  $T_{shaft} = T_{em} - J_m \frac{d\omega_m}{dt}$

At load end  $T_{shaft} = T_L + J_L \frac{d\omega_L}{dt}$

$$(\theta_m - \theta_L) = \frac{T_{shaft}}{K}$$

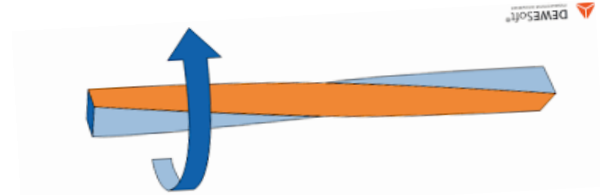
**$K$  : shaft torsional or the compliance coefficient**

$\theta_m$  and  $\theta_L$  : angular rotation at the two ends of the shaft

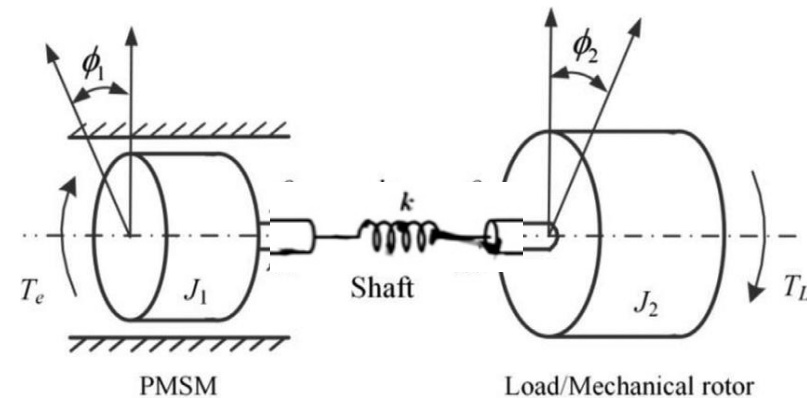
□ For rigid coupling:  $K \rightarrow \infty$ ,  $\theta_m = \theta_L$ ,  $\omega_m = \omega_L$

(  $J_M$  and  $J_L$  can be treated as one inertial mass:  $J_{eq} = J_M + J_L$  )

□ Finite  $K$  may lead to resonances



*In reality, any shaft will twist (flex) as it transmits torque from one end to the other.*



- The shaft of finite compliance will act as a spring.
- This compliance in the presence of energy storage in the masses, and inertias of the system, can lead to resonance at certain frequencies.

# Mechanical - Electrical Analogy

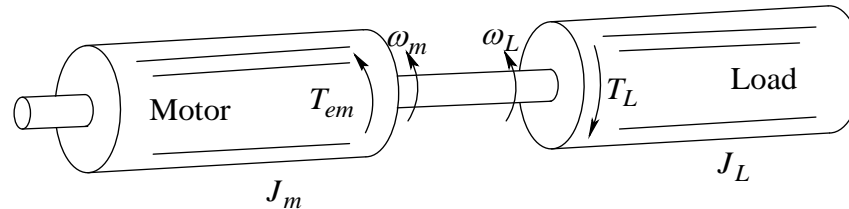
- Analogy with electrical circuits can be very useful when analyzing mechanical system.
- A commonly used analogy is to relate mechanical and electrical quantities, as show in Table 2-2.

**TABLE 2-2** Torque–Current Analogy

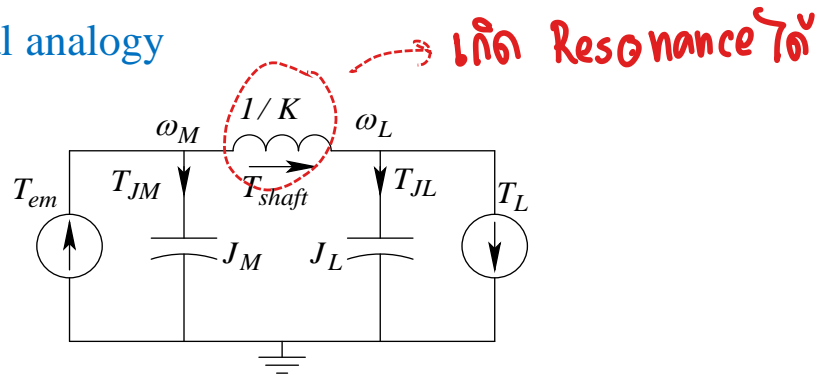
Mechanical system	Electrical system
Torque ( $T$ )	Current ( $i$ )
Angular speed ( $\omega_m$ )	Voltage ( $v$ )
Angular displacement ( $\theta$ )	Flux linkage ( $\psi$ )
Moment of inertia ( $J$ )	Capacitance ( $C$ )
Spring constant ( $K$ )	1/Inductance ( $1/L$ )
Damping coefficient ( $B$ )	1/Resistance ( $1/R$ )
Coupling ratio ( $n_M/n_L$ )	Transformer ratio ( $n_L/n_M$ )

# Electrical Analogy of Motor & Load

## Mechanical system

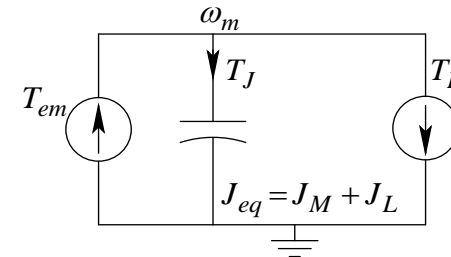


## Electrical analogy



Finite shaft stiffness

- Each *inertia* is represented by a *capacitor* from its node to a reference (ground) node.
- In this circuit, the *similar differential equations* can be written.



Infinite shaft stiffness

- If the shaft is of infinite *stiffness* ( $K \rightarrow \infty$ ), the *inductance* representing it becomes zero.
- In the resulting circuit,  $\omega_m = \omega_L$ , the two capacitors representing the two inertias can now be combined to result in a single equation.



# Coupling Mechanisms

- It is preferable to couple the load directly to the motor, to avoid:
  - *Additional cost and power loss*
  - *Nonlinearity due to backlash*
  - *Wear and tear*

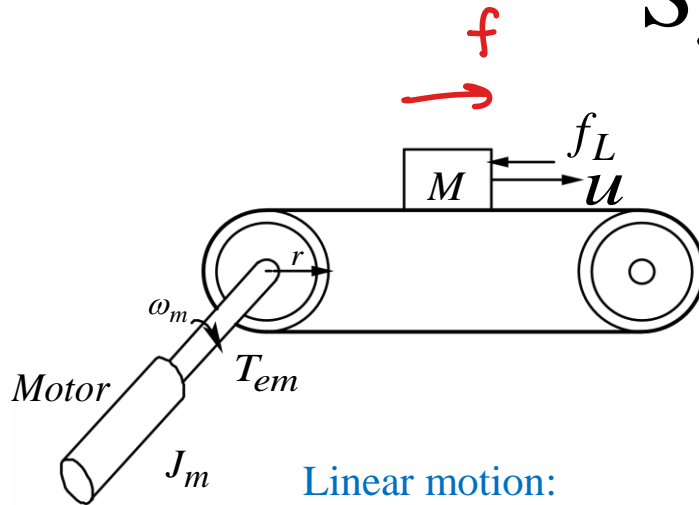
## □ Required when

- a (rotary) motor is driving a load which requires linear (translational) motion
- motors prefer higher rotational speed than that required by the load
- the axis of rotation needs to be changed

## □ Types

- Conveyor belts (belt and pulley)
- Rack and pinion or a lead-screw type of arrangement
- Gear mechanisms

# Conversion between Linear and Rotary Systems



Linear motion:

$J_m$  = motor inertia  
 $M$  = mass of load  
 $r$  = pulley radius

$$f = M \frac{du}{dt} + f_L$$

$$u = r \omega_m$$

Angular and linear speeds are related by the radius  $r$ :

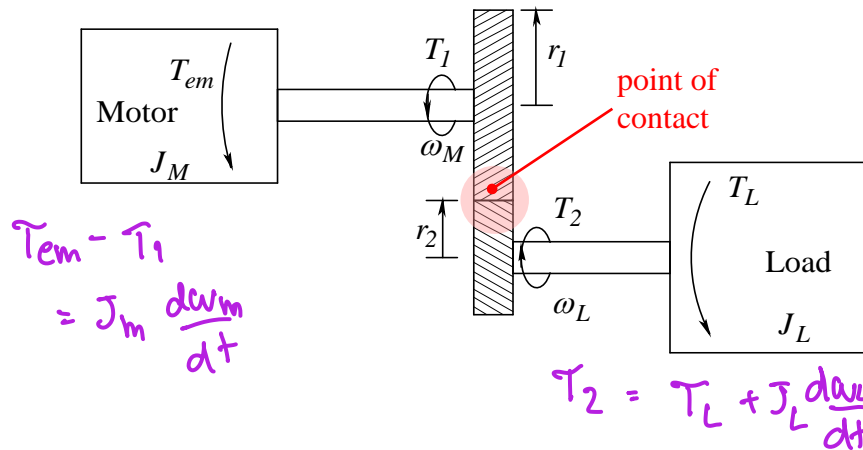
Force  $f$  is delivered by the motor in the form of a torque  $T$ :

$$T = r f = r^2 M \frac{d\omega_m}{dt} + r f_L$$

Electromagnetic torque required from the motor is:

$$T_{em} = \underbrace{J_m \frac{d\omega_m}{dt}}_{\text{required to accelerate motor}} + \underbrace{r^2 M \frac{d\omega}{dt} + r f_L}_{\text{due to load}}$$

# Gears



Purpose:

- Gears are used for matching speeds.

Assumption:

- Shafts are assumed to be of infinite stiffness (rigid)
- Masses of gears are ignored.
- No power loss in the gears.

Principle:

- Both gears must have the same linear speed at the point of contact.

□ Basic relationships: radius, speed, torque

Equal speeds at gear surfaces  $\Rightarrow r_1 \omega_M = r_2 \omega_L$

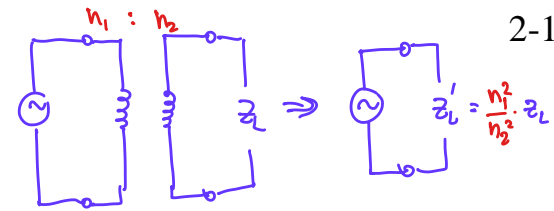
Power transferred across gears  $\Rightarrow \omega_M T_1 = \omega_L T_2$ , (... Assuming no power loss)

$$\Rightarrow \frac{r_1}{r_2} = \frac{\omega_L}{\omega_M} = \frac{T_1}{T_2} \quad \& \quad \underbrace{\left( T_{em} - J_M \frac{d\omega_M}{dt} \right)}_{T_1} \omega_M = \underbrace{\left( T_L + J_L \frac{d\omega_L}{dt} \right)}_{T_2} \omega_L$$

□ Geared up: speed increased, torque decreased  $\omega_L > \omega_M$ ;  $T_2 < T_1$ ;  $r_2 < r_1$

□ Geared down: speed decreased, torque increased  $\omega_L < \omega_M$ ;  $T_2 > T_1$ ;  $r_2 > r_1$

# Gears (cont'd)



## □ Equivalent Inertia

$$T_{em} = \underbrace{\left[ J_m + J_L \left( \frac{\omega_L}{\omega_m} \right)^2 \right]}_{J_{eq}} \frac{d\omega_m}{dt} + \left( \frac{\omega_L}{\omega_m} \right) T_L$$

$$\Rightarrow J_{eq} = J_m + J_L \left( \frac{\omega_L}{\omega_m} \right)^2 = J_m + J_L \left( \frac{r_1}{r_2} \right)^2$$

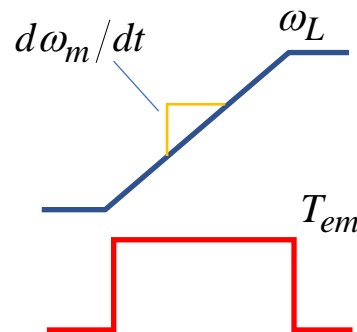
## □ Optimum gear ratio (to minimize $T_{em}$ )

$$T_{em} = \underbrace{\left[ J_m + J_L \left( \frac{r_1}{r_2} \right)^2 \right]}_{J_{eq}} \frac{d\omega_m}{dt}$$

- The electromagnetic torque  $T_{em}$  required from motor to accelerate a motor-load combination depends on the gear ratio.

(For inertial load, TL can be assumed to be negligible.)

$$\left. \frac{dT_{em}}{d(r_1/r_2)} \right|_{d\omega_L/dt} = 0$$



- For a given load-acceleration  $d\omega_m/dt$ ,  $T_{em}$  can be minimized by selecting an optimum gear ratio  $(r_1/r_2)_{opt}$
- The derivative of the optimum gear ratio shows that the load inertia “seen” by the motor should equal the motor inertia.

$$J_m = \left( \frac{r_1}{r_2} \right)_{opt.}^2 \cdot J_L \quad \Rightarrow \quad \left( \frac{r_1}{r_2} \right)_{opt.} = \sqrt{\frac{J_m}{J_L}}$$

$$\text{and } (T_{em})_{opt.} = 2 J_m \frac{d\omega_m}{dt} = 2 J_m \left( \frac{r_2}{r_1} \right)_{opt.} \frac{d\omega_L}{dt}$$

# Types of Loads

- Load torques normally act to oppose rotation.
- Loads can be classified into the following categories:
  - 1) Centrifugal (Squared) Torque
  - 2) Constant Torque
  - 3) Squared Power
  - 4) Constant Power

# Centrifugal loads

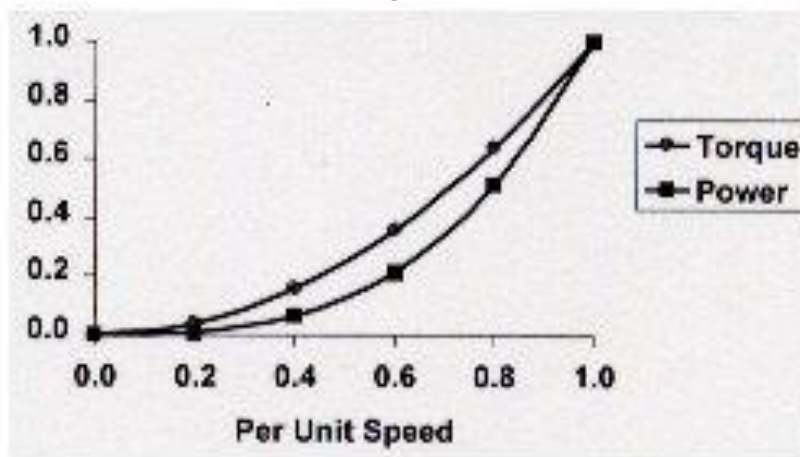
- Centrifugal loads, such as fans and blowers, require torque that varied with speed<sup>2</sup>

$$T_L = k \omega_L^2$$

- And load power that varies with speed<sup>3</sup>

$$P_L = T_L \omega_L = k \omega_L^3$$

Centrifugal Load



Blower



© 2000 d

# Constant-Torque Loads

- In constant-torque loads, such as conveyors, hoists, cranes and elevators, torque remains constant with speed

$$T_L = \text{const}$$

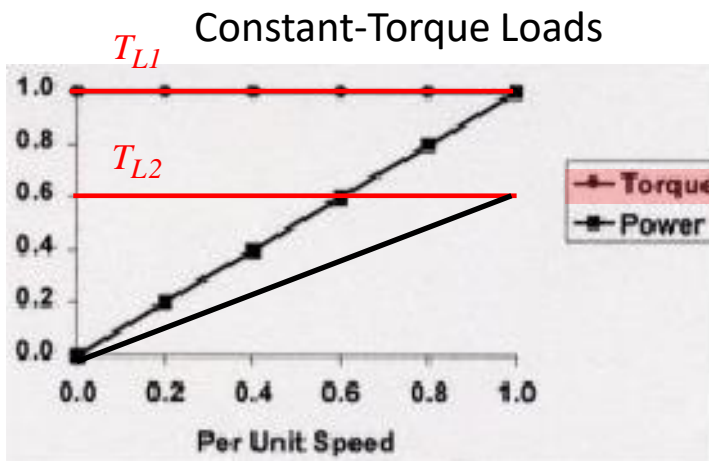
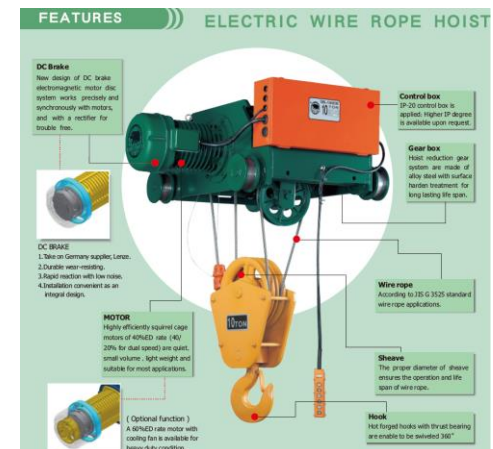
- And load power varies linearly with speed

$$P_L = T_L \omega_L \propto \omega_L$$

Elevator



Hoist



# Squared-Power Loads

- In squared-power loads, such as compressors and rollers, torque vary linearly with speed

$$T_L = k \omega_L$$

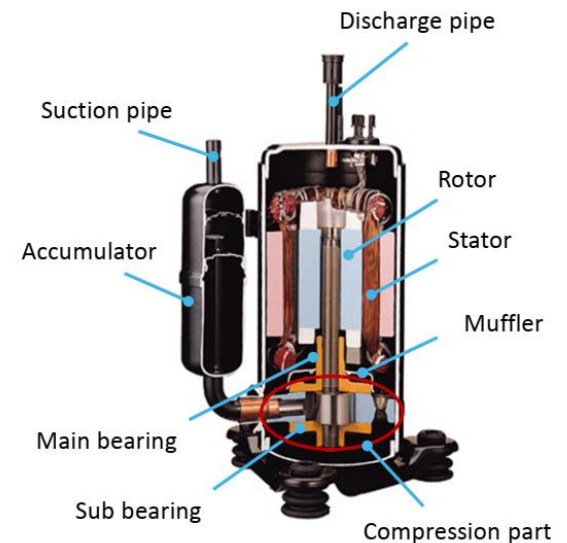
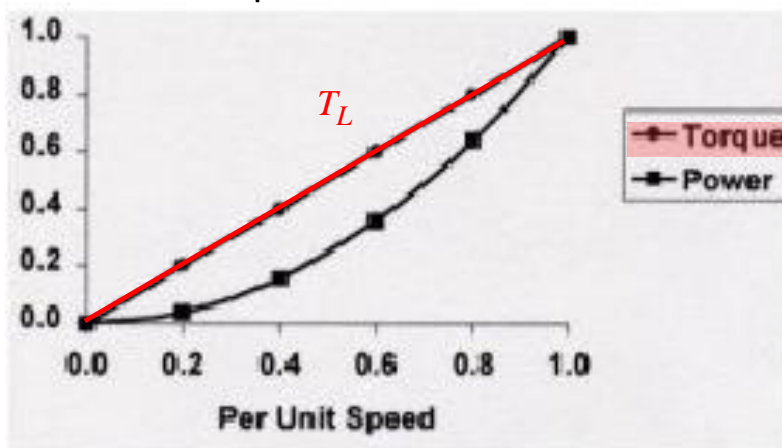
- And load power varies with speed<sup>2</sup>

$$P_L = T_L \omega_L \propto k \omega_L^2$$

Compressor for Air Conditioner



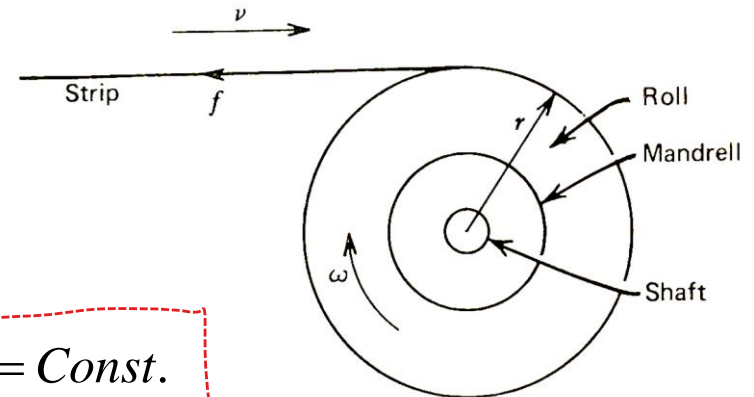
Squared-Power Load





# Constant-Power Loads

- Typical applications of constant-power load over a range of speed are the take-up roll (or winder and unwinder) in a steel strip, plastic or paper mill.
- Basic operation of take-up roll:
  - If *a satisfactory roll is to be formed*, the strip tension or the force  $f$  must be constant :
  - The strip will emerge from the mill rolls at constant speed  $v$ :



$$f = \text{Const.}$$

$$v = \text{Const.}$$

- Torque and angular speed are:
- The power is therefore constant :
- The relationship between torque and angular speed is hyperbola:
- The radius of the roll is varied; for the winder, the radius  $r$  will build up. On the other hand, for the unwinder, the radius  $r$  will fall off.

$$T_L = f \cdot r \quad ; \quad \omega_L = \frac{v}{r}$$

$$\begin{matrix} \downarrow r & \uparrow \\ \Rightarrow T_L \uparrow \end{matrix}$$

$$P_L = f \cdot v = T_L \cdot \omega_L = \text{Const.}$$

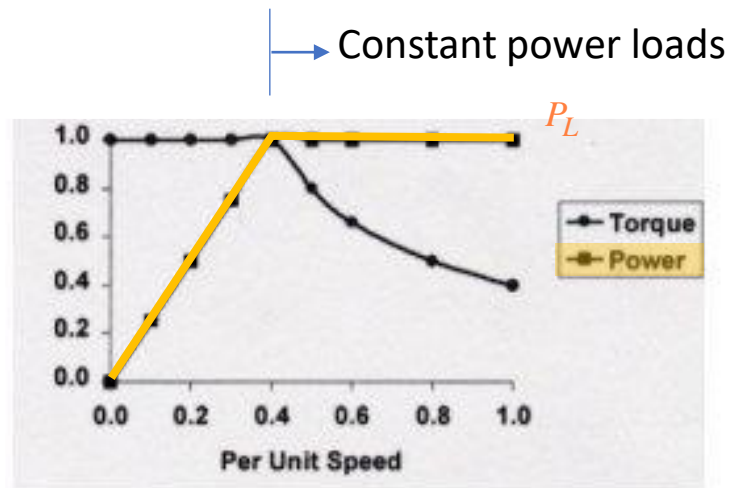
# Constant-Power Loads (Cont.)

- In constant-power loads, such as winder and unwinder and rollers, the torque beyond a certain speed range varies inversely with speed

$$T_L = \frac{k}{\omega_L}$$

- And load power remains constant with speed

$$P_L = T_L \omega_L = k \quad (Const.)$$

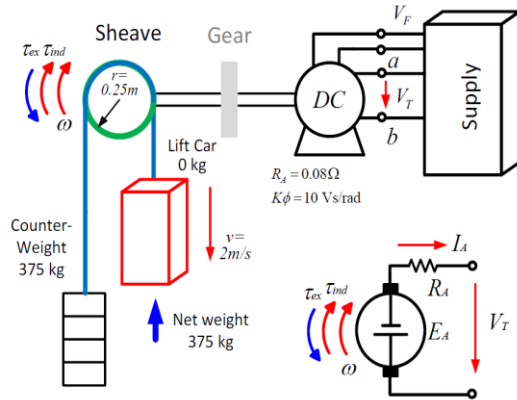


Winder and Unwinder

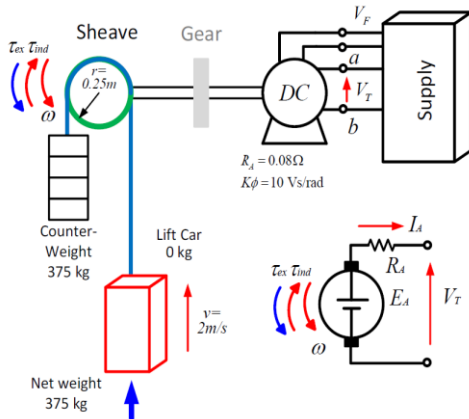


# Four-Quadrant Operation

## Elevator drive



Operation in quadrant 3

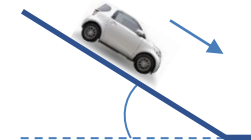


Operation in quadrant 4

## Electric-Vehicle drive

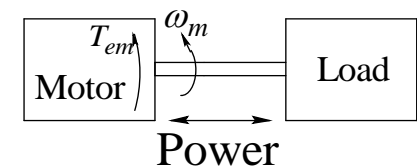
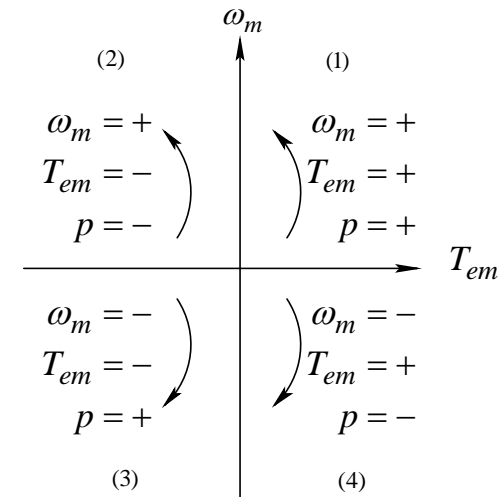


Operation in quadrant 1



Operation in quadrant 2

- In many high-performance systems, drives are required to operate in all four quadrants of the torque-speed plane.
- The motor drives the load in forward direction in quadrant 1, and in the reverse direction in quadrant 3. And the average power is positive ( $p = +$ ) and flows from the motor to mechanical load.
- To control the load speed rapidly, it may be necessary to operate the system in the regenerative braking mode, where the power flows from the load into the motor.
- In quadrant 2, the speed is positive, but the torque produce by the motor is negative. In quadrant 4, the speed is negative, and the motor torque is positive.



# Required Drive Characteristics

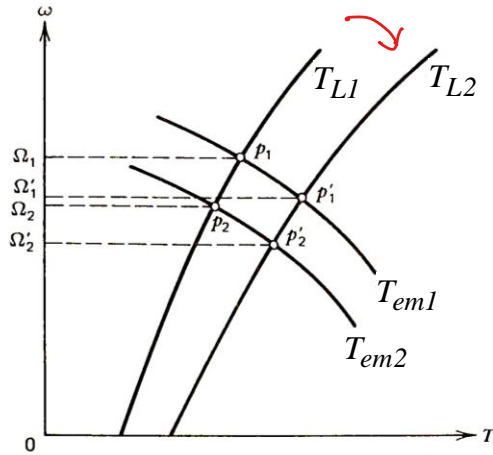
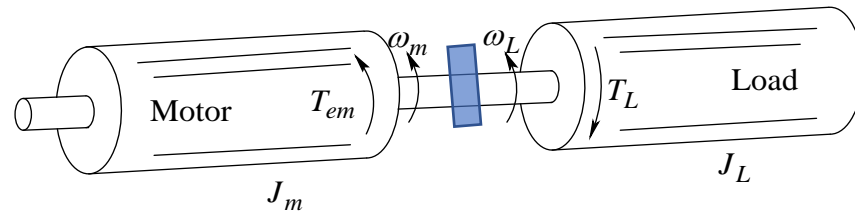
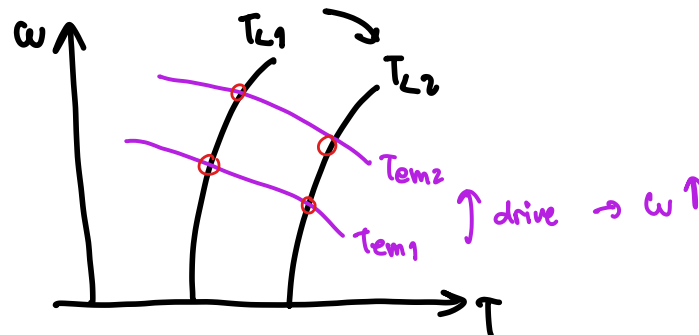


Fig. 1.18. Steady-state operating points.

- There are 2 torque-speed characteristics : one from electric machine ( $T_{em}-\omega$ ), the other from load ( $T_L-\omega$ ).
- The crossing among these 2 characteristics indicates each steady-state operating point  $p$ .



Electromagnetic torque generated from electric machine	• Inertia ( $J_m, J_L$ ) • Shaft torsional ( $K$ )	Mechanical Coupling (for mech. Translation)	Friction Torque	Load Torque, 1) Squared Torque 2) Constant Torque 3) Squared Power 4) Constant Power
$T_{em}$	$J \frac{d\omega_m}{dt}$ $K(\theta_m - \theta_L)$	$\tilde{T}_L = \frac{r_1}{r_2} T_L$	$T_f$	$T_L$



# Dynamic Operation

- ❑ How the operating point changes with time
- ❑ Important for High Performance Drives
- ❑ Speed change: rapid and without any oscillations
- ❑ Requires good controller design, as discussed in chapter 5

# Summary

- ❑ What are the MKS units for force, torque, linear velocity, angular velocity, speed, and power?
- ❑ What is the relationship between force, torque, and power?
- ❑ Show that torque is the fundamental variable in controlling speed and position.
- ❑ What is the kinetic energy stored in a moving mass and a rotating inertia?

# Summary

- ❑ What is the mechanism for torsional resonances?
- ❑ What are the various types of coupling mechanisms?
- ❑ What is the optimum gear ratio to minimize the torque  
required from the drive to accelerate a load?
- ❑ What are the torque-speed and the power-speed profiles  
for various types of loads?