Voids

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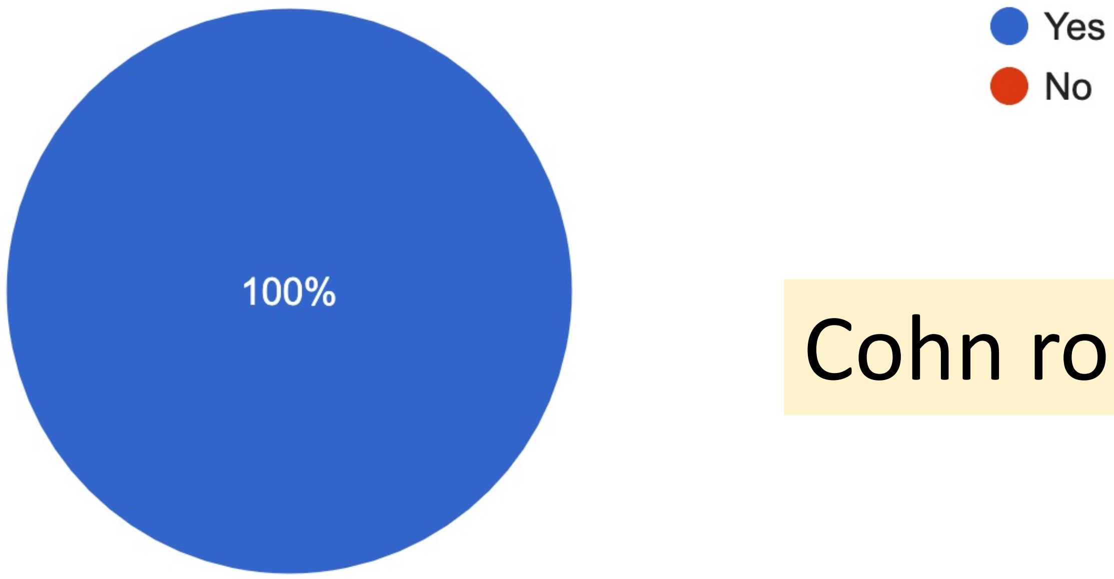
House Keeping

I would like to move the final to December 14th at 10 am - 11:30 am. Room TBD.

5 responses



Cohn room or CSRB?

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A simple though experiment

If we placed a sphere and a disc into a finite volume of material, what aspects of those features would help define the change in energy for the total system?

Now let's consider vacancy condensation

- Vacancy condensation is different than interstitial clustering:

- The energy of a small, spherical cluster of vacancies is:

$$E_s = 4\pi r^2 \sigma$$

- As n_v increases, the lowest energy configuration is a planar loop, but it first must pass through a disc shaped cavity geometry:

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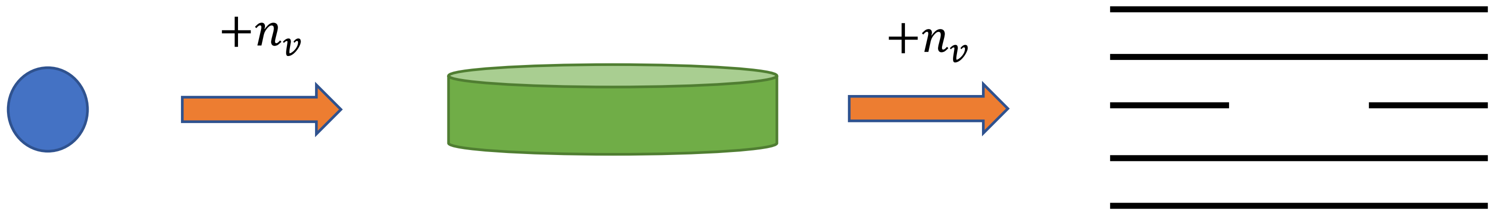
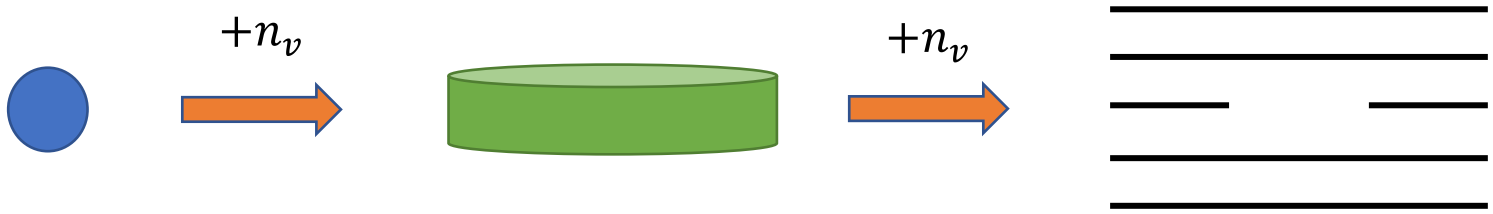
Now let's consider vacancy condensation



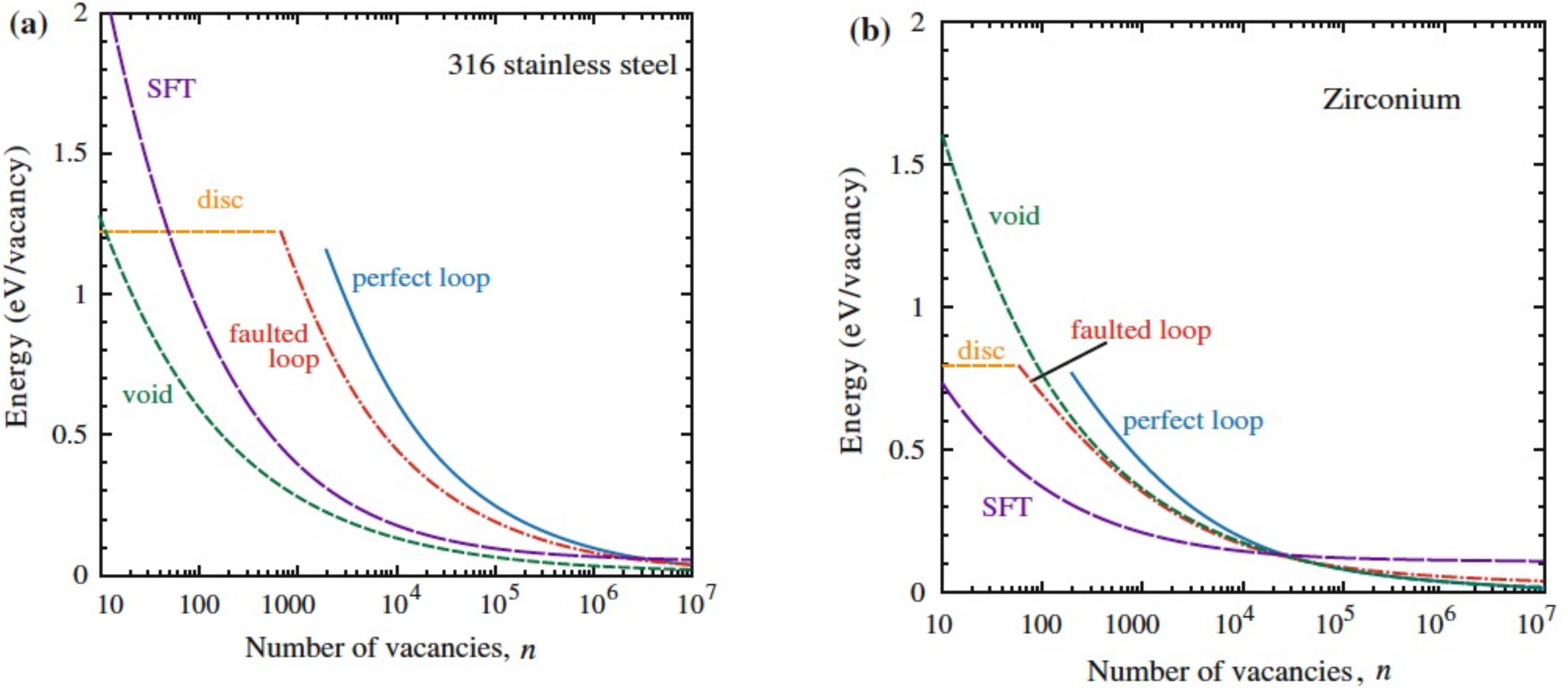
$$\therefore \quad E_s = 4\pi r^2\sigma \rightarrow E_c = 2\pi r^2\sigma$$

- For the same nv, $E_C > E_s$ meaning an activation energy is required to generate loops

Now let's consider vacancy condensation



Visualizing the energetics (again)



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Voids formed in metals

- Voids form by vacancy condensation. Vacancies are supersaturated in irradiated metals.
- Void formation requires "bias" or preferential absorption of self-interstitials at dislocations or other sinks, relative to vacancies
  - V - I recombination is an "unbiased" process since it removes vacancies and interstitials at the same rate
  - Cavities are unbiased sinks for point defects
  - Because of dislocation bias, slightly more interstitials (~20%) are absorbed by dislocations, leaving a slight excess of vacancies to first *nucleate* and then *grow* voids.
- These processes are very sensitive to gas pressure in the cavity
  - A void has no gas (in practice, could have very low levels of gas atoms)
  - Impurity atoms within the metal (e.g., O, N) and He produced by (n,a) reactions or by direct implantation are the principal radiation-produced gases that can be trapped by cavities.

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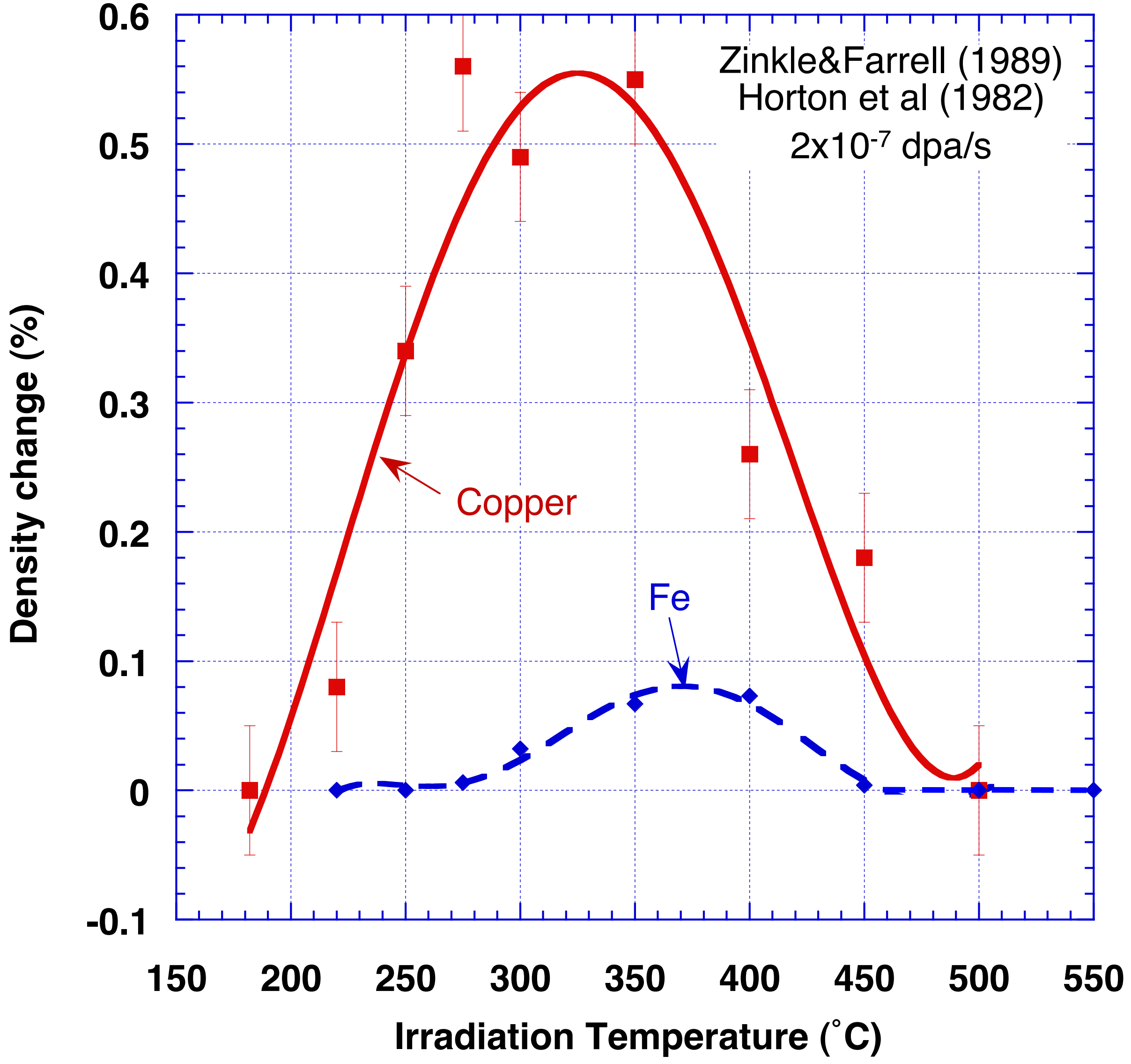
Comparison of Temperature-Dependent Void Swelling in Neutron Irradiated Cu and Fe at 1 dpa



Void swelling is typically of concern for irradiation temperatures between ~0.3 and ~0.6 T_M

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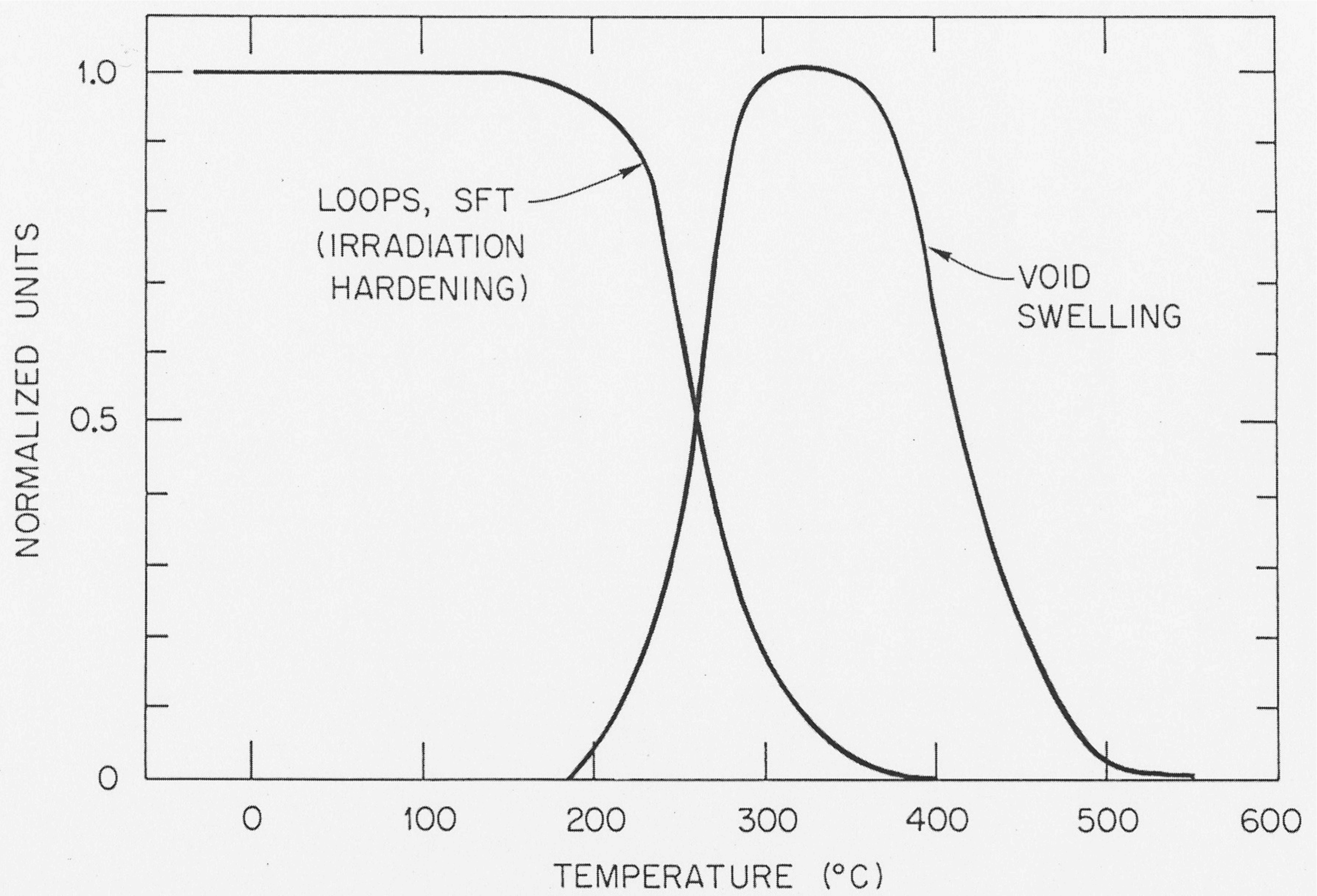
Temperature dependence for void swelling involves balance between recombination and vacancy emission



Zinkle, ASTM STP 1125 (1992) p. 813

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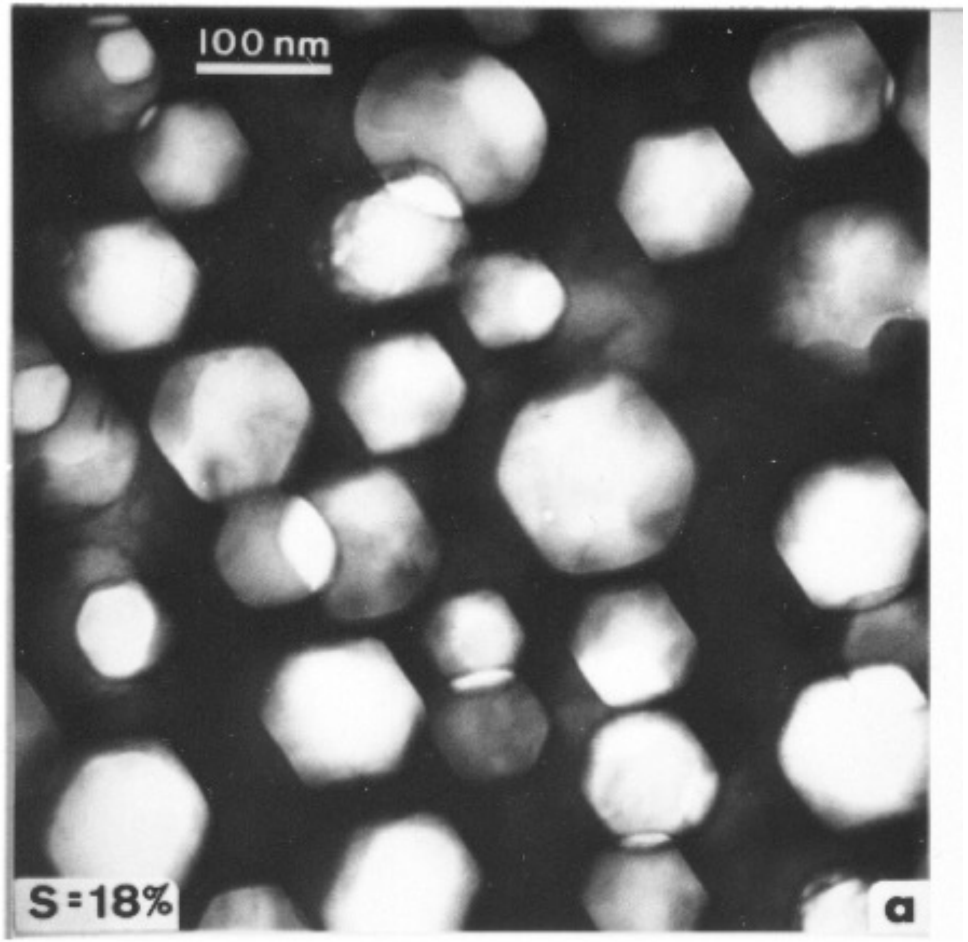
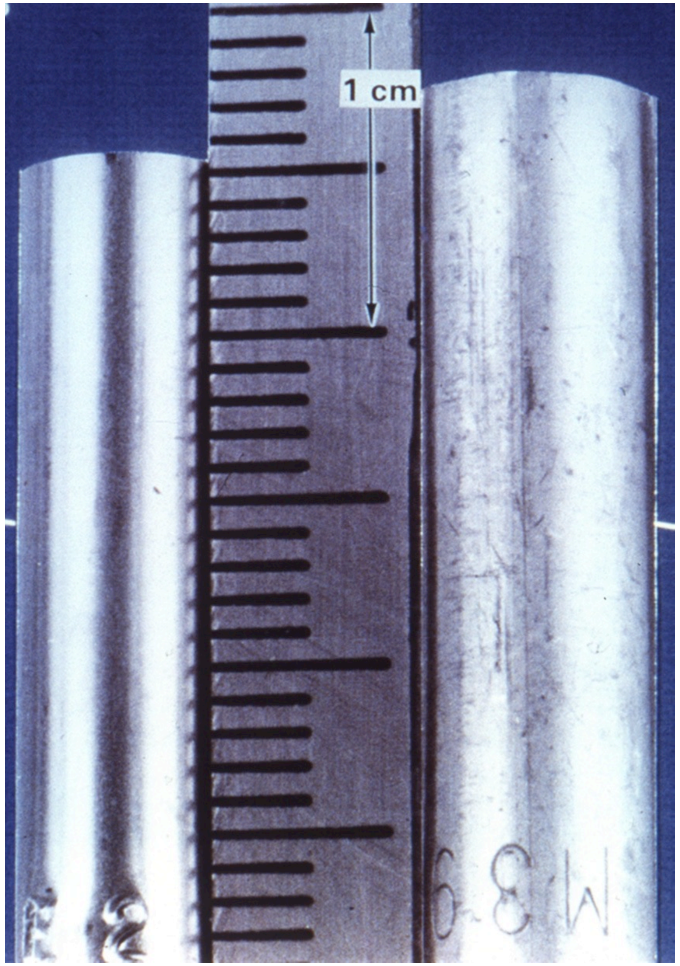
Physical effect of void formation in a material

ion-irradiated austenitic stainless steel (625˚C, 70 dpa)



N. Packan & K. Farrell, J. Nucl. Mater. *<u>85&86</u>* *(1979) 677*

neutron irradiated 20%CW 316 steel at $T=523^0C$, $1.5x10^{23}n/cm^2$



J.L. Straalsund et al., J. Nucl. Mater. *<u>108&109</u>* *(1982) 299*

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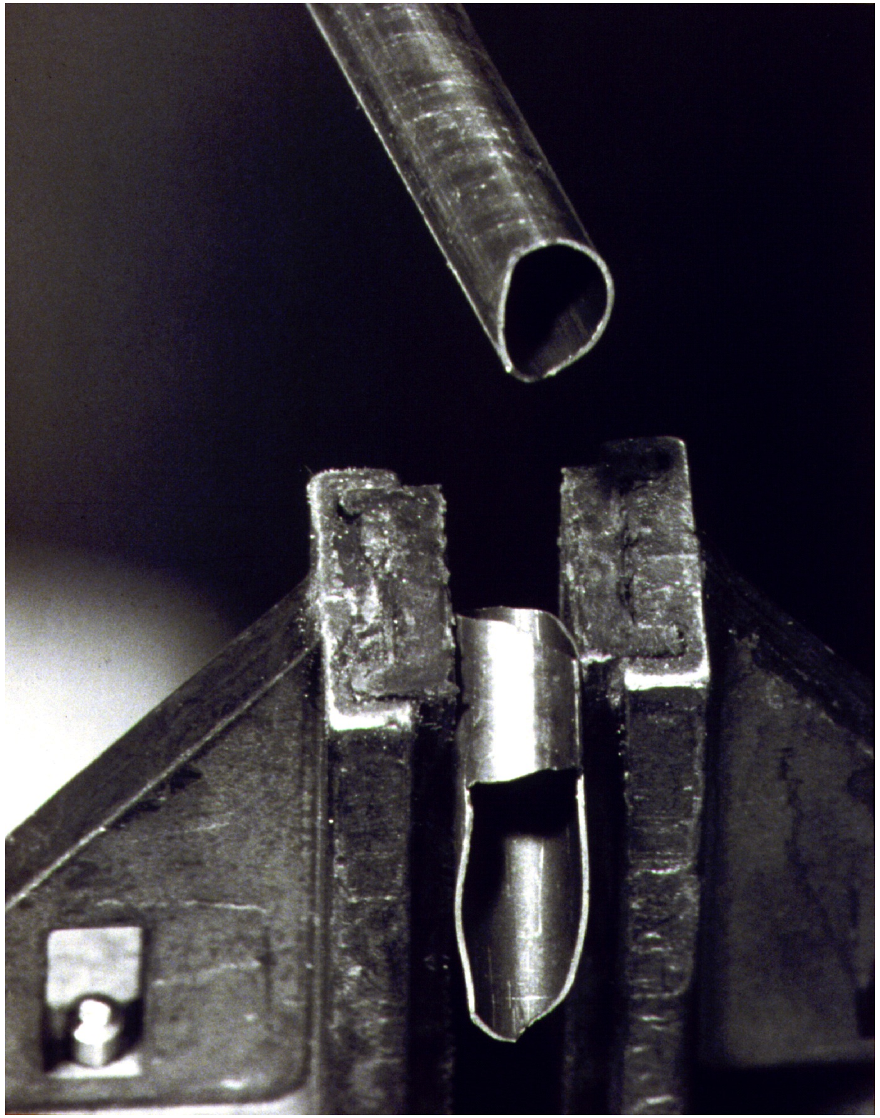
Physical effect of void formation in a material



Porter and Garner, 1988

- 14% swelling
- 316 stainless steel irradiated at ~400°C
- Failure occurred during clamping in a vise at room temperature.
- Tearing modulus has fallen to zero, with no resistance to crack propagation.

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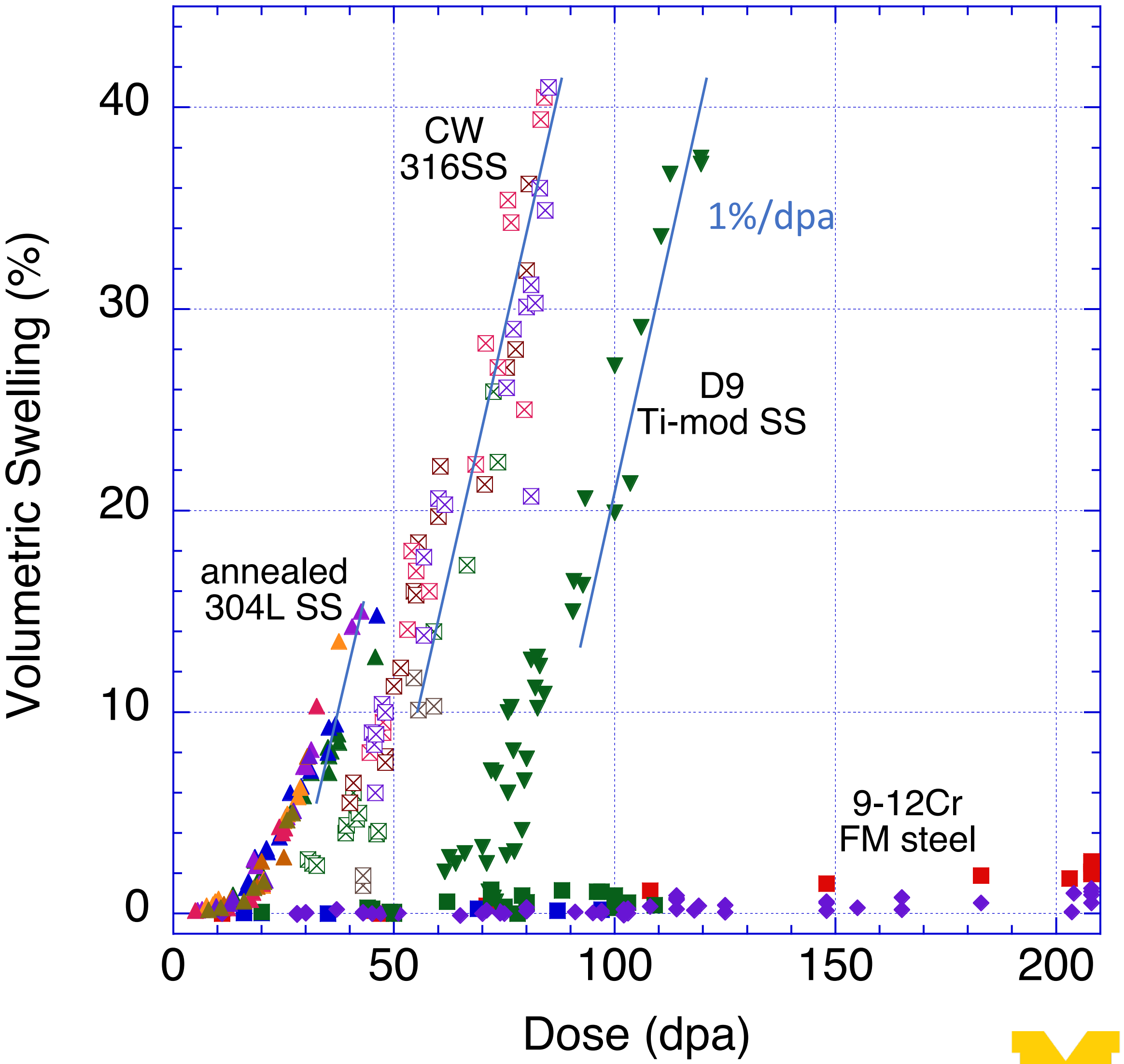
Physical effect of void formation in a material

Dimensional changes >5-10 vol.% are unacceptable for typical engineering designs

E.g., linear dimensional change due thermal expansion in 316SS between room temperature and 500°C is:

$Dl = a\Delta T = 18 \times 10^{6}/^{\circ}C * 480^{\circ}C = 0.86\%$



Zinkle & Was, Acta Mater. 61 (2013)

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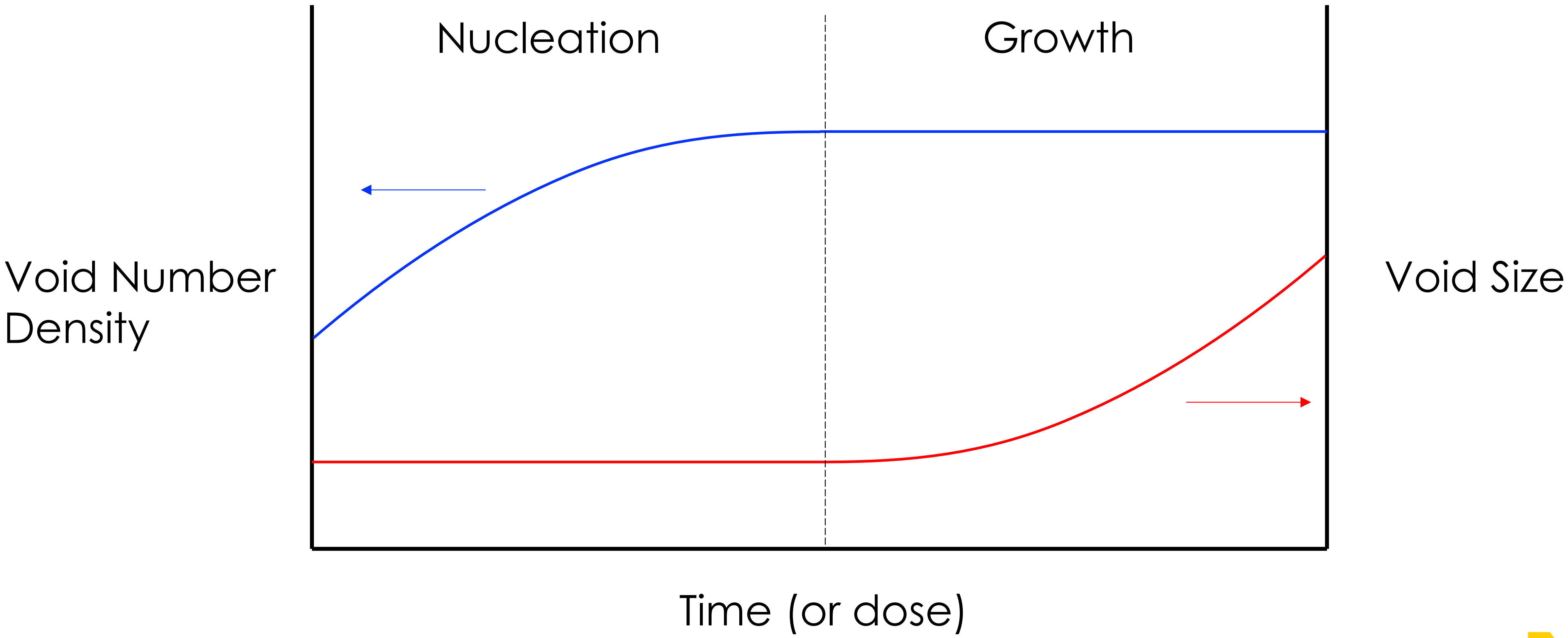
Nucleation vs. Growth



Void Nucleation Theory: Gibbs free energy

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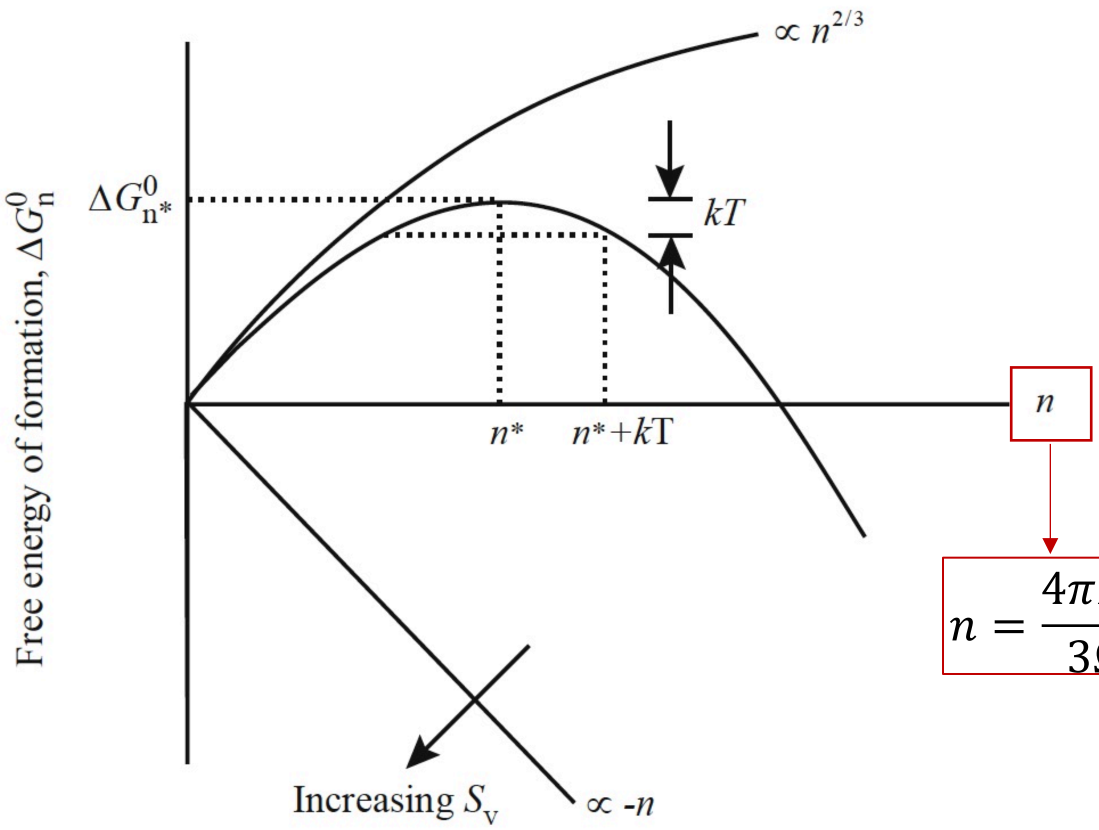
Void Nucleation Theory: Graphical depiction

$$\Delta G_n^0 = -nkT \cdot \ln(S_v) + (36\pi\Omega^2)^{1/3}\gamma n^{2/3}$$

Fig. 8.2 Schematic illustration of ΔG_n^0, the free energy of formation of a spherical void consisting of n vacancies and the effect of thermal fluctuations on the critical size void embryo

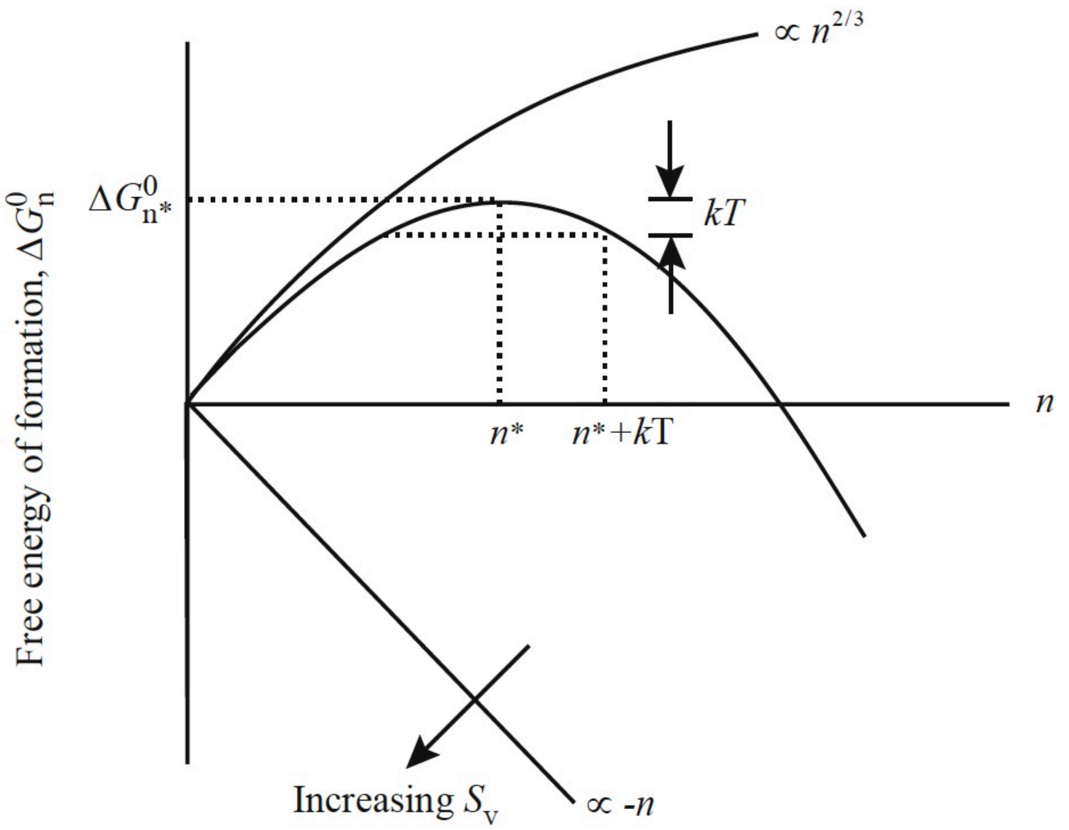


$$n = \frac{4\pi R_v^3}{3\Omega}$$

Derivations and discussion in Was 8.1

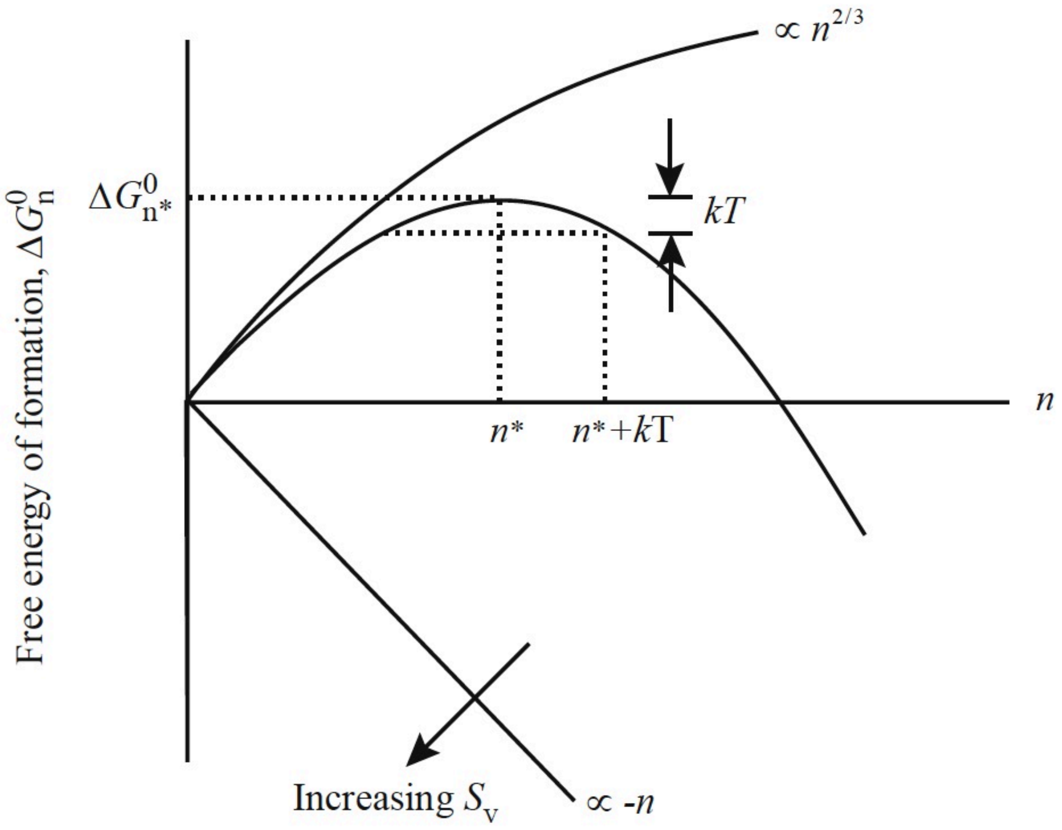
Void Nucleation Theory: Graphical depiction

We can solve for n* by:



Derivations and discussion in Was 8.1

Void Nucleation Theory: Graphical depiction



- Homogeneous nucleation:

When supercritical particles are formed due to thermal fluctuations

- Heterogeneous nucleation:

When external objects (surfaces, interfaces, impurities, defects, seeds) lower the barrier for nucleation

What happens to the graph with heterogeneous nucleation?

Derivations and discussion in Was 8.1

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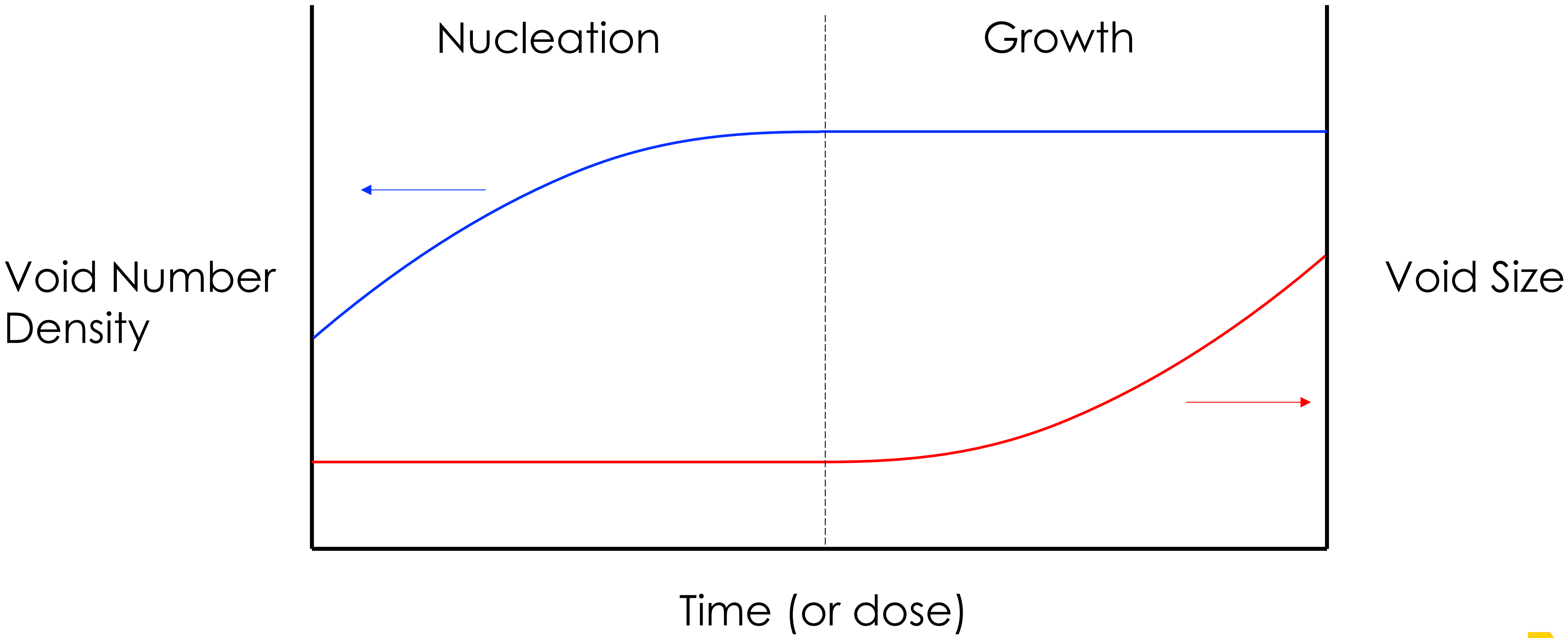
Nucleation vs. Growth



Void Nucleation Rate

- Nucleation of v_j on one particular kind of attractive sites (e.g. compressive stress field around a dislocation). The following assumptions are made:
  1. The lattice is in thermal and dynamic equilibrium, which are minimally affected by displacement and thermal spikes
  2. Mono-vacancies and solvent mono-interstitials are the only mobile point defects present (gas atoms are neglected)
  3. The defects obey dilute solution thermodynamics
  4. A steady state concentration of vacancies and interstitials exist
  5. Void growth rate is diffusion limited

Void Nucleation Rate

- Voids are three-dimensional clusters of vacancies formed by the following reactions
  1. **Cluster growth** by v absorption: $v + v_j \rightarrow v_{j+1}$
  2. More generally, we consider **small cluster mobility**: $v_j + v_k \rightarrow v_{j+k}$
  3. **Cluster shrinkage** by v emission: $v_j \rightarrow v_{j-1} + v$
     - Depends on equilibrium v concentration at void surface - C_v^0 from the rate of absorption of v by cavities and also depends on the binding energy between the v and the cluster
  4. **Cluster shrinkage** by *i* absorption: $v_j + i_k \rightarrow v_{j-k}$
     - Depends on *i* and i_k concentrations
  5. Growth by *i* emission is neglected, e.g. $C_i^0 \sim 0$

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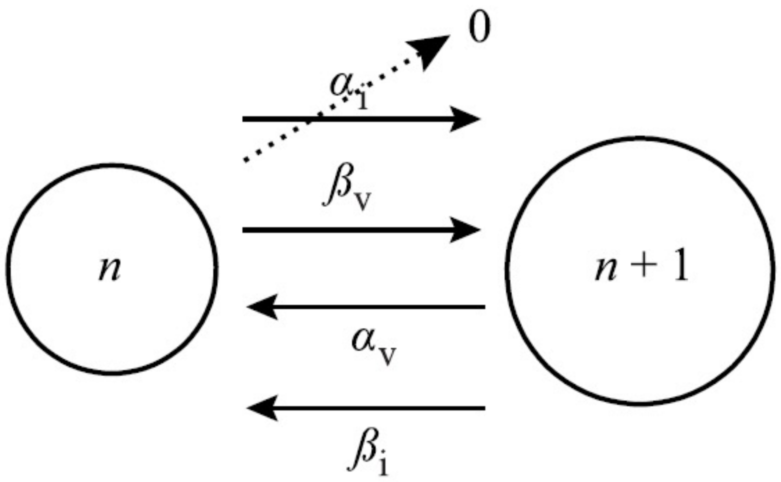
Void Nucleation Rate

- The flux between any two sized voids, say n and $n+1$:

$$J_n = \beta_v(n)\rho(n) - p(n+1)(\alpha_v(n+1) + \beta_i(n+1))$$



- $\beta_v(n)\rho(n)$ = rate of v absorption by clusters of size n
- $\alpha_v(n+1)\ p(n+1)$ = rate of v emission by clusters of size $n+1$
- $\beta_i(n+1)p(n+1)$ = rate of *i* absorption by clusters of size $n+1$

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Void Nucleation Rate

- Lengthy derivation covered in Was 8.1.2
- For sake of simplicity, the # of void embryos can be written as:

$$\frac{\rho^0(n)}{C_v} = e^{\sum_{k=1}^{n-1} \ln\left(\frac{\sqrt[3]{\frac{k}{k+1}}}{\left(\frac{C_v^{\mathrm{eq}}}{C_v} e^{\left(\frac{8\pi\gamma}{\xi \sqrt[3]{k+1}} - p \right) \frac{\Omega}{kT}} + \frac{D_i C_i}{D_v C_v} \right)} \right)}$$

- C_v^{eq}/C_v is the inverse of vacancy supersaturation S_v^{-1}
- $(D_i C_i)/(D_v C_v)$ is the arrival rate ratio between v and *i*
- γ is the surface energy of the cavity
- *p* is the gas pressure in the cavity (p=0 for voids!)

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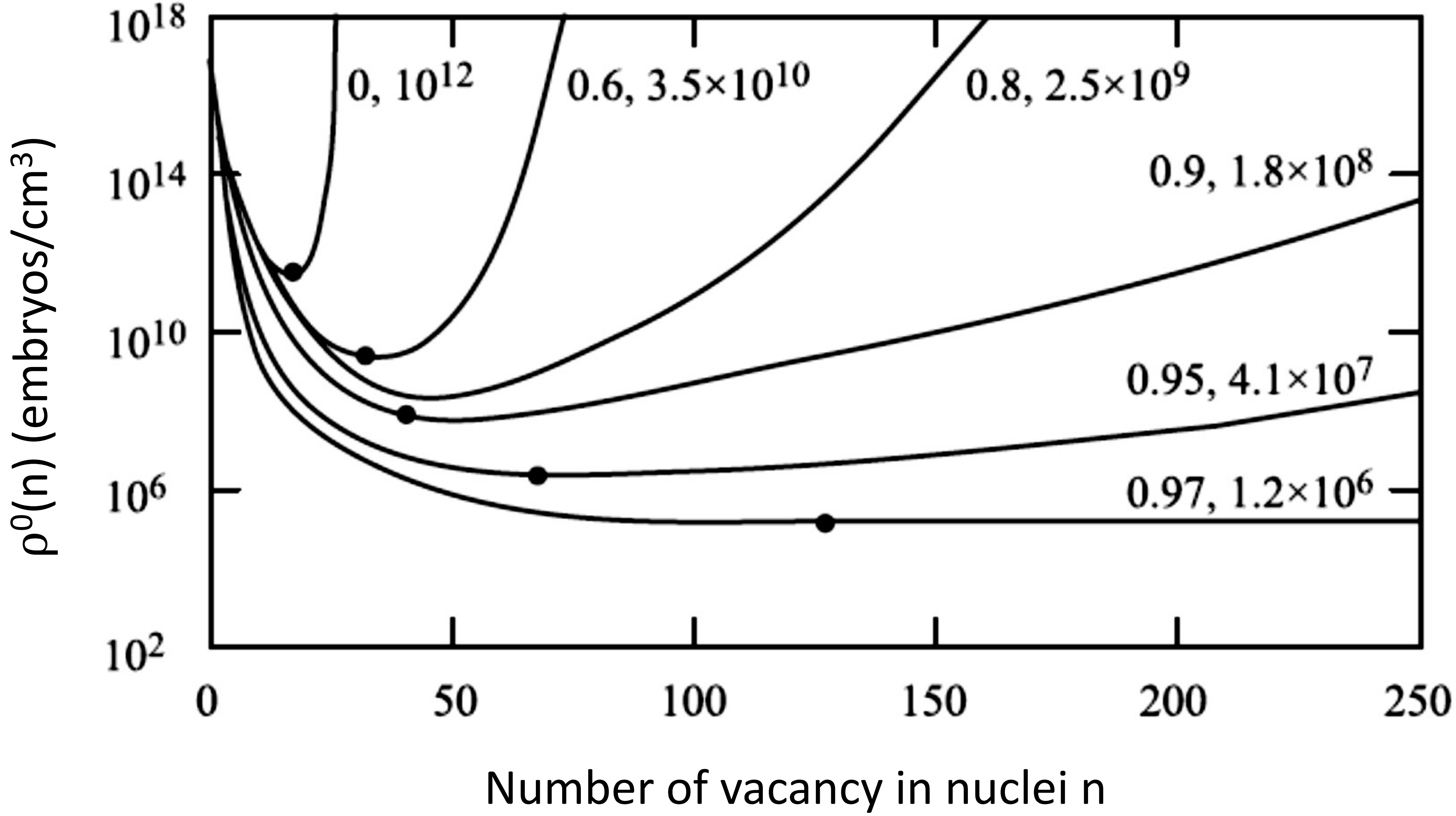
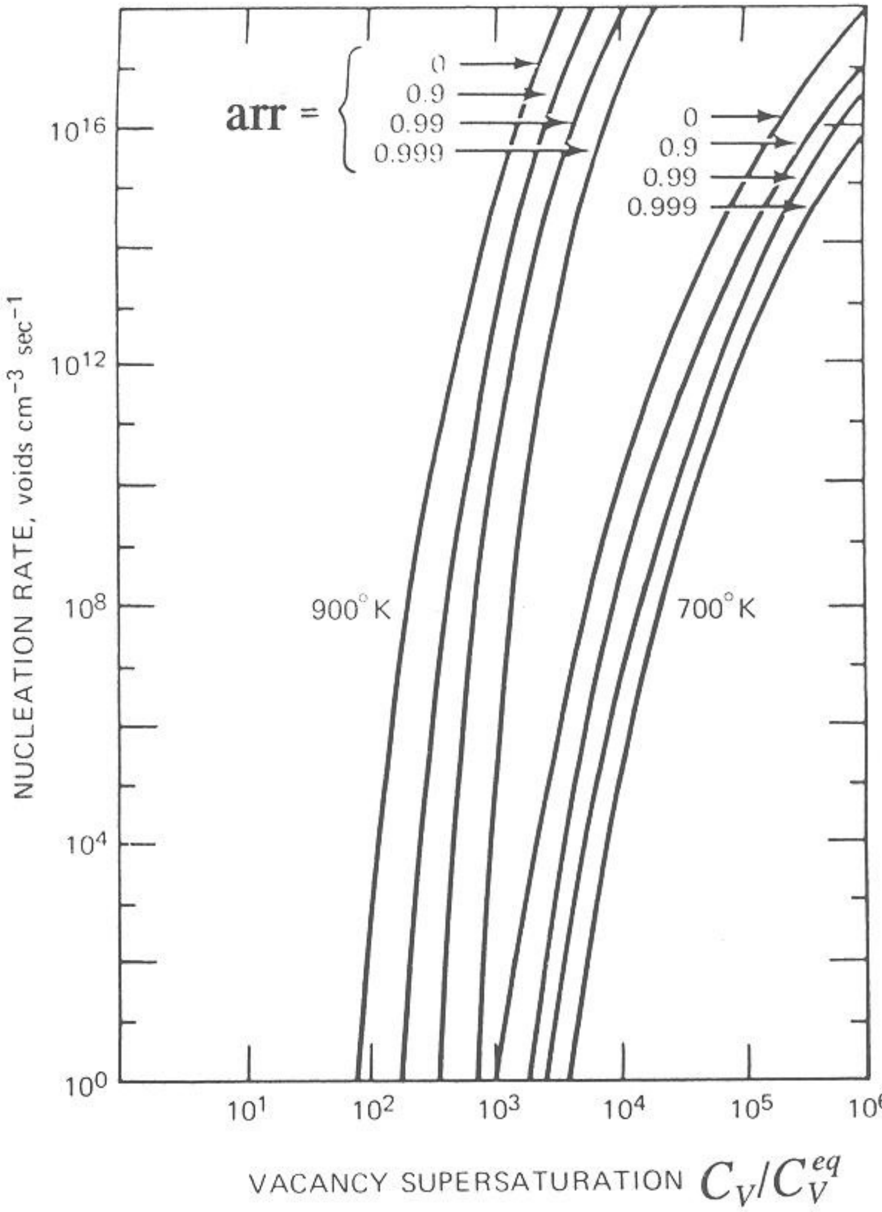


10^{18}
10^{14}
10^{10}
10^{6}
10^{2}
0
50
100
150
200
250
0, 10^{12}
0.6, 3.5×10^{10}
0.8, 2.5×10^{9}
0.9, 1.8×10^{8}
0.95, 4.1×10^{7}
0.97, 1.2×10^{6}
$\rho^0(n)$ (embryos/cm^3)
Number of vacancy in nuclei n

Void Nucleation Rate

- To obtain void nucleation as $(D_iC_i)/(D_vC_v)$ approaches 1 requires higher vacancy supersaturation
- Strong dependence of nucleation on vacancy supersaturation



<u>Typical results:</u>

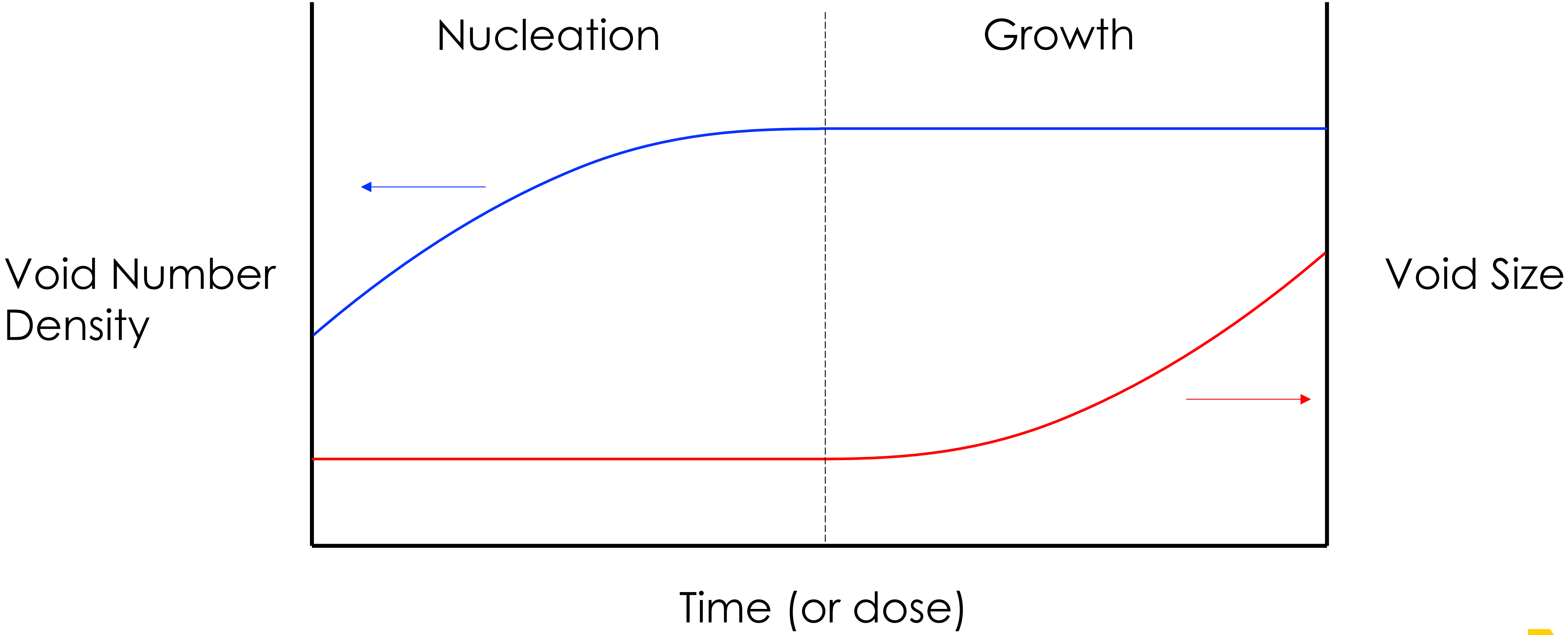
$T = 700$ K; $C_v/C_v^{eq} = 10^4$

arr = $(D_IC_I)/(D_vC_v) = 0.99$

$J \sim 10^8$ voids nucleated/cm^3/s

- After 1 year, $3\text{x}10^{15}$ voids/cm^3
- The voids are small, about the critical size

Nucleation vs. Growth



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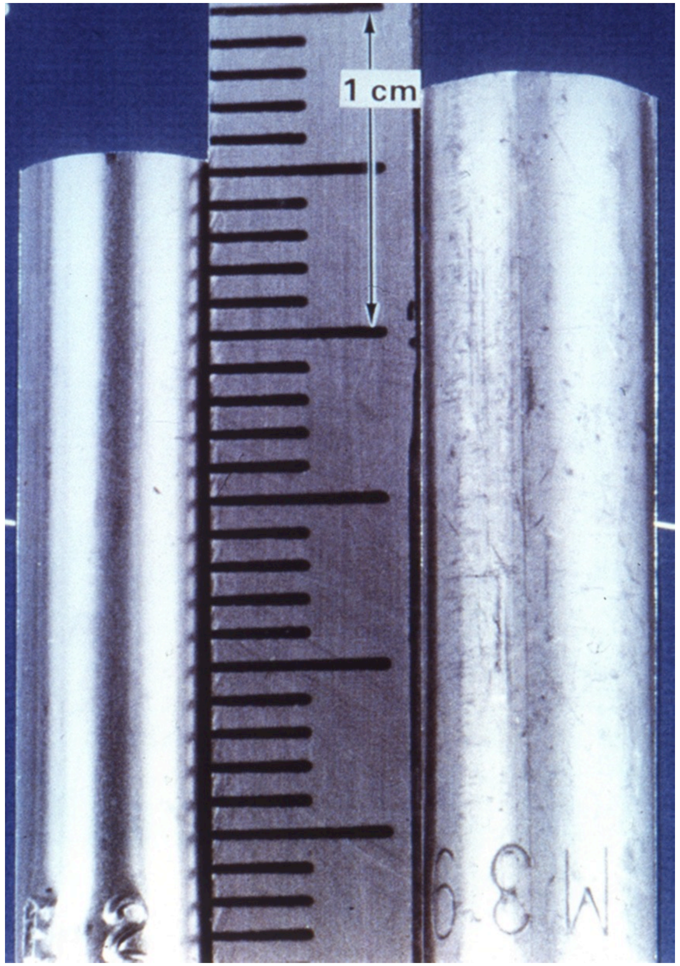
Void Growth

- During the ***nucleation*** period, the number density of cavities increases with time, but the sizes remain small
- During the ***growth*** period that follows, the number density stabilizes at a value of N cm^{-3} and the cavity size increases with time R(t)
- In most cases, we're interested in quantifying ***swelling*** either in the growth or nucleation stage:



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Void Growth

- For void growth, we need to know the net flux of vacancies to a void embryo. The net rate is thus a combination of the fluxes of interstitials and vacancies to a void, where:

Void swelling in neutron irradiated austenitic steel

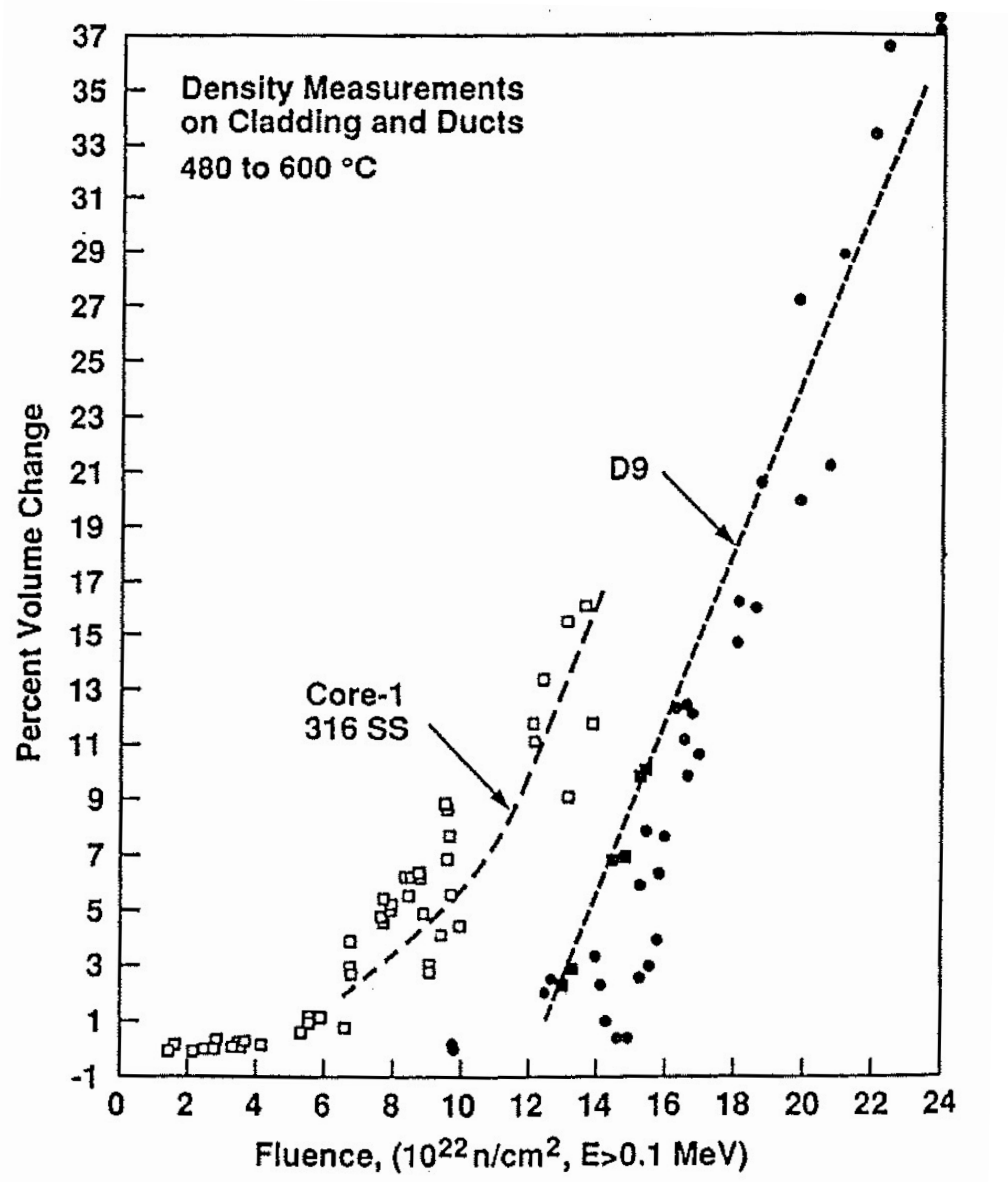

Fig. 3. Swelling observed in two cold-worked austenitic alloys after serving as fuel cladding in the open core of FFTF [23].

Linear swelling vs. dose after transition dose

Typical post-transient volumetric swelling rates are:
~0.5-1%/dpa (FCC)
~0.1-0.2%/dpa (BCC)

F.A. Garner et al., J. Nucl. Mater. 276 (2000) 123

Void Growth

$$dV/_{dt} = 4\pi R\Omega(D_v C_v - D_i C_i)$$

Void Growth

$$K_0 - K_{iv}C_iC_v - K_{vs}C_vC_s = 0$$

$$K_0 - K_{iv}C_iC_v - K_{is}C_iC_s = 0$$

Solving for C_i and C_v, we get the familiar solution of:

$$C_v = \frac{-K_{is}C_s}{2K_{iv}} + \left[\frac{K_0K_{is}}{K_{iv}K_{vs}} + \frac{K_{is}^2C_s^2}{4K_{iv}}\right]^{1/2}$$

$$C_i = \frac{-K_{vs}C_s}{2K_{iv}} + \left[\frac{K_0K_{vs}}{K_{iv}K_{is}} + \frac{K_{vs}^2C_s^2}{4K_{iv}}\right]^{1/2}$$

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Void Growth

Void Growth

Remember:

$$C_v = \frac{-K_{is}C_s}{2K_{iv}} + \left[\frac{K_0 K_{is}}{K_{iv}K_{vs}} + \frac{K_{is}^2 C_s^2}{4K_{iv}}\right]^{1/2}$$

$$C_i = \frac{-K_{vs}C_s}{2K_{iv}} + \left[\frac{K_0 K_{vs}}{K_{iv}K_{is}} + \frac{K_{vs}^2 C_s^2}{4K_{iv}}\right]^{1/2}$$

and

$$k_{jx}^2 = \frac{K_{jx}C_x}{D_j}$$

Void Growth

- With everything defined,

$$C_v = \frac{D_v(4\pi R\rho_v + z_v p_d)}{2K_{iv}}\left(\sqrt{1+\eta} - 1\right)$$

$$C_i = \frac{D_i(4\pi R\rho_v + z_i p_d)}{2K_{iv}}\left(\sqrt{1+\eta} - 1\right)$$

$$\eta = \frac{4K_0 K_{iv}}{D_i D_v (4\pi R\rho_v + z_v p_d)^2}$$

$$dR/_{dt} = \dot{R} = \frac{\Omega}{R}\left(D_v(C_v - C_v^V) - D_i C_i\right)$$

- We can now rewrite the growth law as:

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Void Growth

$$R\dot{R} = K_o\Omega\left(\frac{z_i - z_v}{z_v}\right)\frac{z_v\rho_d}{(4\pi R\rho_v + z_v\rho_d)(4\pi R\rho_v + z_i\rho_d)}F(\eta)$$

- The first term is the main dpa-rate effect on void growth
- The second term is the "bias" term: if $Z_I = Z_V$, *void growth is impossible*
- The third term is the sink-strength balance term. Void growth is eliminated if there are too many or too few dislocations. Optimum growth occurs when the void sink term $(4\pi R\rho_v)$ and the dislocation sink term $(z_v\rho_d)$ are equal.
- The fourth term contains the effect of point defect recombination:

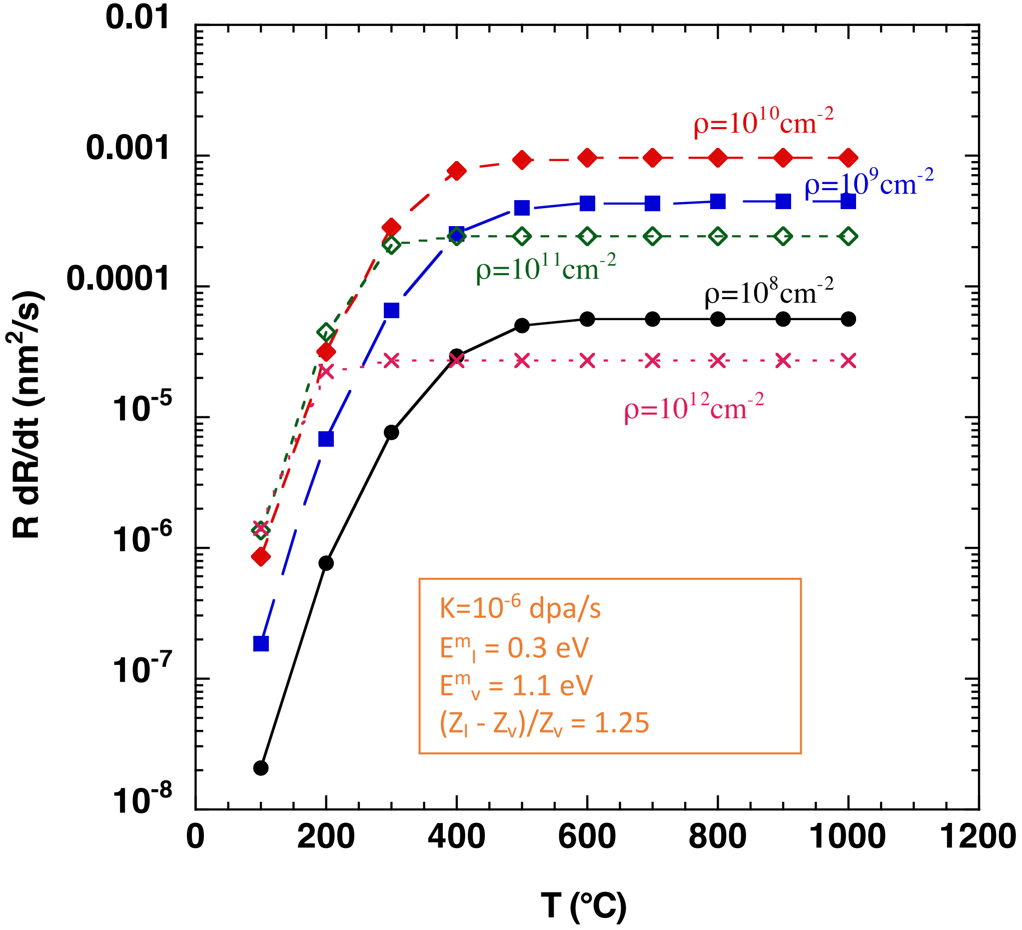
$$F(\eta) = 2\left(\sqrt{1+\eta} - 1\right)/\eta$$

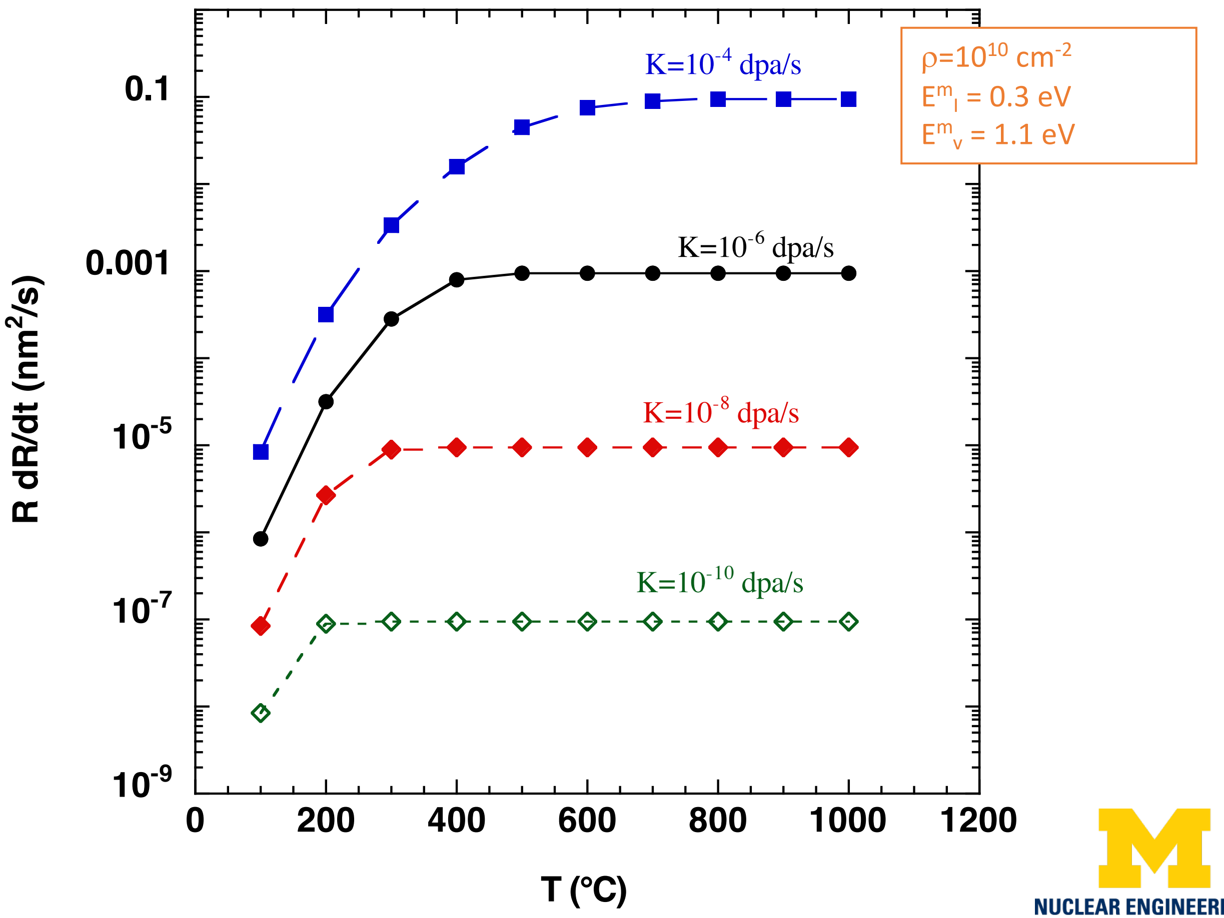
Since h decreases with increasing temperature and F decreases with increasing η:

- At high temperature, F $\rightarrow$ 1 and recombination does not effect void growth
- At low temperature, F $\rightarrow$ 0 and recombination prevents void growth.

Void Growth

$$R\dot{R} = K_o\Omega\left(\frac{z_i - z_v}{z_v}\right)\frac{z_v\rho_d}{(4\pi R\rho_v + z_v\rho_d)(4\pi R\rho_v + z_i\rho_d)}F(\eta)$$





Vacancy Thermal Emission

- The four factor formula does not account for C_v^0, but at high temperatures this assumption is not valid. At very high temperatures, void growth ceases due to vacancies "boiling off", e.g. vacancy emission. If we repeat taking into account C_v^0, we get:

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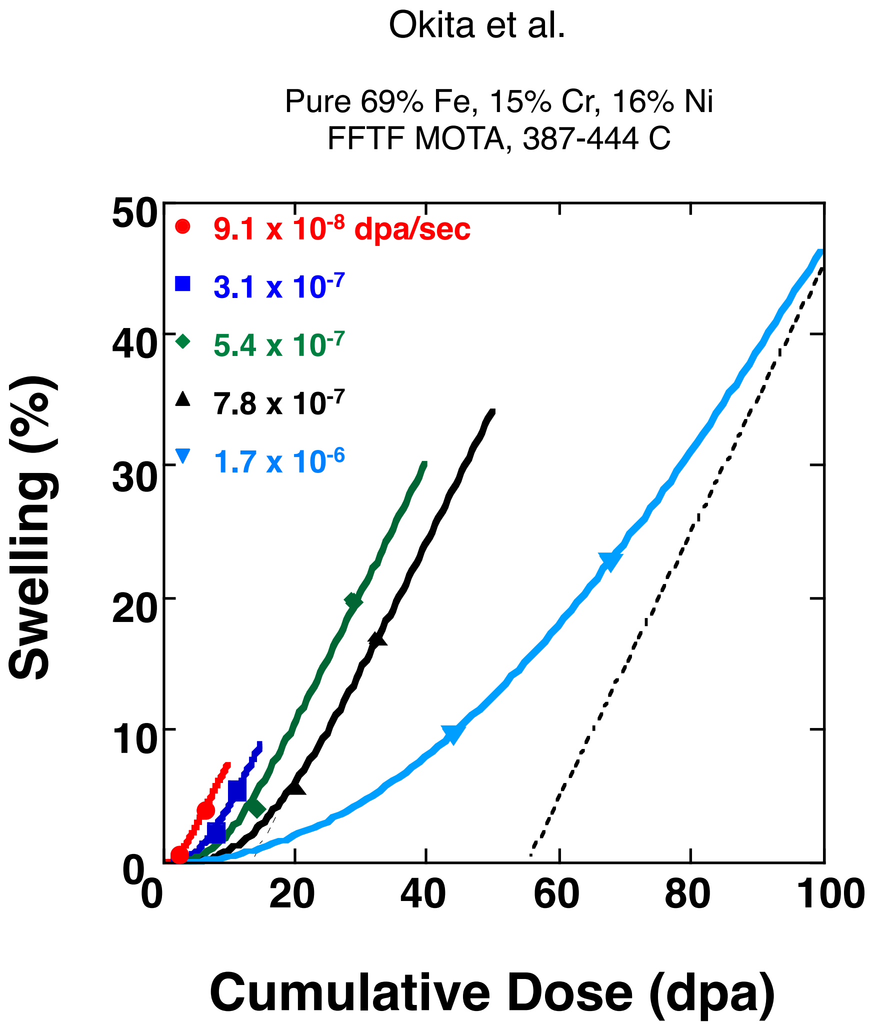
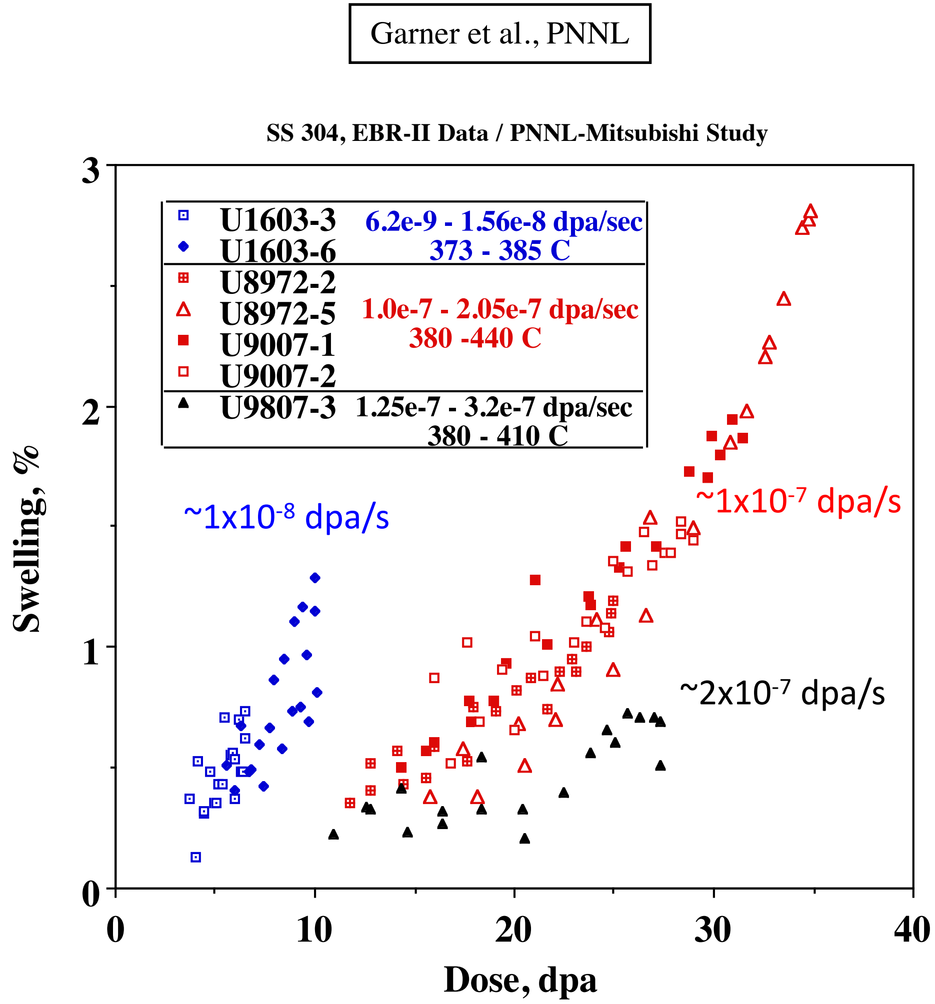
Dose, dose rate & temperature effects on swelling

- Theory predicts that void selling rate passes through a maximum with temperature. The maximum is ~1/3 the melting temperature of the metal (T_m K)
- The void growth model also includes the effect of dose rate and accumulated dose
- The dose rate effect means that void swelling at the same dose is different for ion or electron irradiation (high dose rates) compared to neutrons (low dose rate)
- The steady state swelling is roughly correlated to the damage:
- Or

The onset of void swelling can be a strong function of the dose rate





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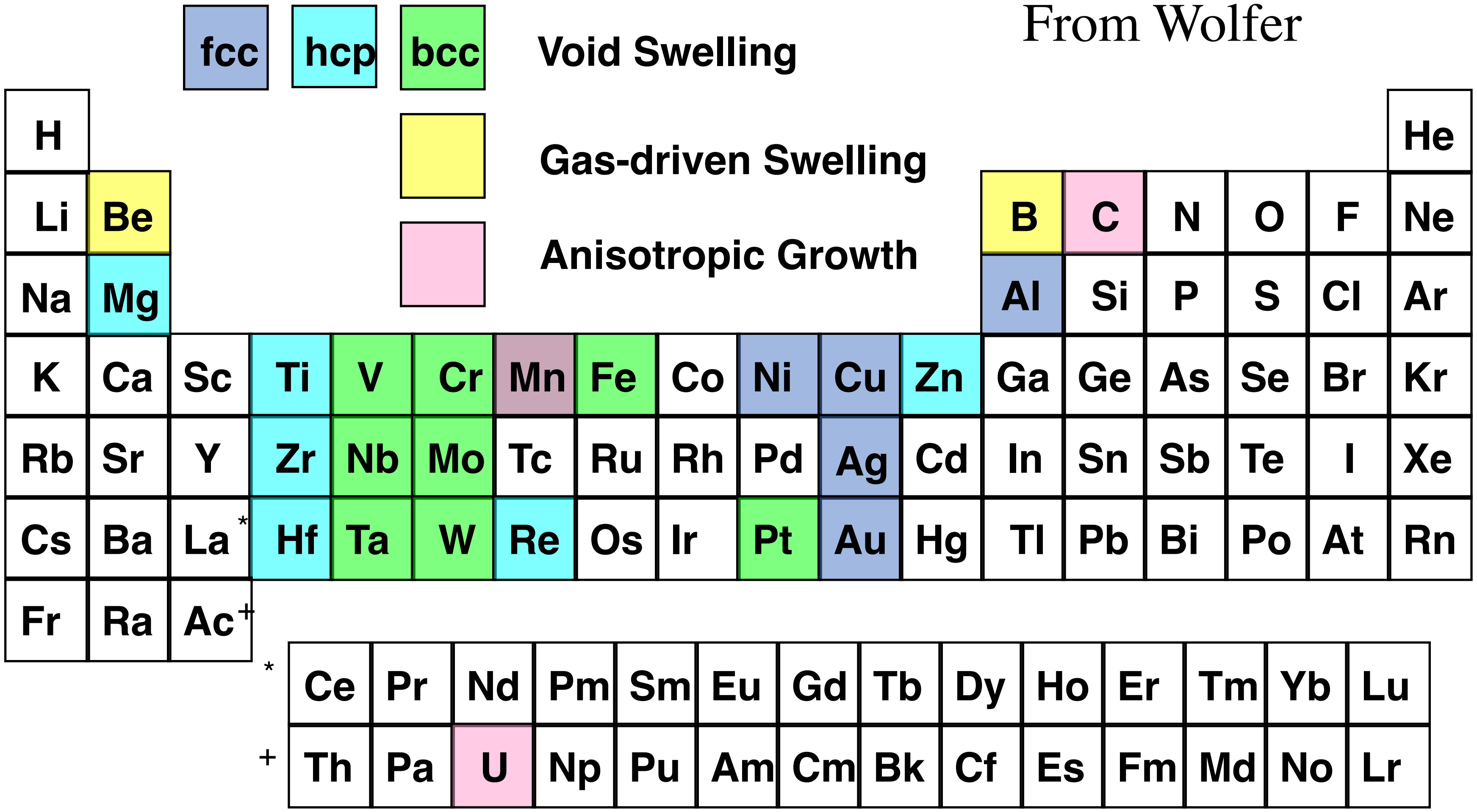
Effect of materials variables on void growth

From Wolfer



No Element Tested Has Ever Failed to Swell

Questions?