



- All of classical control can be summerized in "exploit the knowledge of the loop gain L(s) to figure out the properties of the closed-loop transfer furtion T(s) and S(s) with the least effort possible"
 - * Classical methods for foodback control
 - 1 Root Locus
 - -> Quick assessment of Control design feasibility. The insights are Correct and clear!
 - -> Can only be used from finite-dimentional Systems'
- > Difficult to do sophisicated design.
 - -> Hand to oneposed uncentainty.
- 2 Nyquist plot
 - >The most authoritative closed-loop Stability test:
 - -> at can always be used (finite on Infinite dimensional systems)



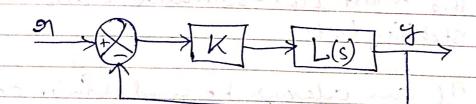
- > Easy to orapresent uncertainty.
- Sophisticated design.

3 Bode plots

- -> Potentially misleading onesults unless the System is open-loop stable and minimum-phase.
- > Easy to supresent uncertainty.
- -> Easy to clear, this is the tool of choice for sophisticated design.

* Even's Root Locus method

- => Invented in the late yo's by Walter R. Evans
- => Useful to study how the oxob of a polynomial change as a function of a scalar parameter e.g. the gain.



Loop gain - $K L(s) = K \frac{N(s)}{O(s)} = K \frac{(s-Z_1)(s-Z_2)\cdots(s-Z_m)}{(s-P_1)(s-P_2)-(s-P_n)}$



=> The sensitivity function is

$$S(s) = \frac{1}{1+kL(s)} - \frac{D(s)}{D(s)+kN(s)}$$

=> The closed-loop poles are the Solutions of the characteristic equation

$$D(s) + K(V(s) = 0)$$

* The groot locus orules

=> Since the degree of D(s) + KN(s) is the same on the degree of D(s), the number of closed-loop poles is the same as the number of open-loop poles.

=> For K -> O D(s) + K(N(s) => D(s)

the closed-loop poles approaches

 \Rightarrow For $K \rightarrow \infty$ D(s) + KN(s) = KN(s)

-> The closed-toup poles approaches
the open-loop zeros.

> If the degree of N(s) is smaller, then
the "excess" closed-loop poles goes to
infinity.



* The angle and magnitude onle > Let us onewrite the closed-loop characteristic equation as: $\frac{N(s)}{D(s)} = \frac{-1}{k}$ · The engle onle => Take the engument on both sides! L(S-Z1) + L(S-Z2) + --+ L(S-Zm) -L(S-P1) - L(S-P2) ---- L(S-Pn) = · The magnitude orule => Take the argument on both sides: |S-Z11.|S-Z21, --- |S-Zm| 15-P1-15-R1....|S-Pn1 * Comphical Interpretation L(5-P2) A5-2)

1(s-P1)



All points on the complex plane that could potentially be a closed-loop pole have to salisfy the agle condition.

=> All points on the need axis are on the

Some corresponds to negative K sculoces and some corresponds to positive K prootlocus.

* Asymptotos

Jules than zeros, form the magnitude condition, the excess doord-loop poles will have to go to infinity.

=> Since this is the complex plane we need to identify"in which direction" they go toward impirity".

=> If we "zoom out" sufficiently for the contributions from all the finite open loof poles and zeros will all be approximately egned to LS:

> So agle side (a be appreximated a: (m-m) LS = -EK ± 9360°

= L-K ± 9/360°

