



CALC SHEET
CONCRETE PROJECT
BUILDING 18

CONCRETE PROJECT

BUILDING 18

SUPERVISORS:

DR. MOHAMED NABIL .

DR. AMR ZAHER .

DESIGBNED BY :

MOHAMED FARID .

1601254

USING ETABS 20

DEFINE MATERIAL :

E Material Property Data

General Data

Material Name	fou 35
Material Type	Concrete
Directional Symmetry Type	Isotropic
Material Display Color	 Change...
Material Notes	Modify/Show Notes...

Material Weight and Mass

<input checked="" type="radio"/> Specify Weight Density	<input type="radio"/> Specify Mass Density
Weight per Unit Volume	2.5 tonf/m ³
Mass per Unit Volume	0.254929 tonf-s ² /m ⁴

Mechanical Property Data

Modulus of Elasticity, E	2619160.17074176 tonf/m ²
Poisson's Ratio, U	0.2
Coefficient of Thermal Expansion, A	0.0000099 1/C
Shear Modulus, G	1091316.74 tonf/m ²

Design Property Data

Modify/Show Material Property Design Data...
--

Advanced Material Property Data

Nonlinear Material Data...	Material Damping Properties...
Time Dependent Properties...	

Modulus of Rupture for Cracked Deflections

<input checked="" type="radio"/> Program Default (Based on Concrete Slab Design Code)
<input type="radio"/> User Specified

Buttons

OK **Cancel**



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E Material Property Data X

General Data

Material Name	st 24
Material Type	Rebar
Directional Symmetry Type	Uniaxial
Material Display Color	 Change...
Material Notes	Modify/Show Notes...

Material Weight and Mass

Specify Weight Density Specify Mass Density

Weight per Unit Volume	7.85 tonf/m ³
Mass per Unit Volume	0.800477 tonf·s ² /m ⁴

Mechanical Property Data

Modulus of Elasticity, E	20000000 tonf/m ²
Coefficient of Thermal Expansion, A	0.0000117 1/C

Design Property Data

[Modify/Show Material Property Design Data...](#)

Advanced Material Property Data

[Nonlinear Material Data...](#) [Material Damping Properties...](#)

[Time Dependent Properties...](#)

[OK](#) [Cancel](#)



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E Material Property Data

General Data

Material Name	st 400
Material Type	Rebar
Directional Symmetry Type	Uniaxial
Material Display Color	 Change...
Material Notes	Modify/Show Notes...

Material Weight and Mass

<input checked="" type="radio"/> Specify Weight Density	<input type="radio"/> Specify Mass Density
Weight per Unit Volume	7.85 tonf/m ³
Mass per Unit Volume	0.800477 tonf·s ² /m ⁴

Mechanical Property Data

Modulus of Elasticity, E	20000000 tonf/m ²
Coefficient of Thermal Expansion, A	0.0000117 1/C

Design Property Data

Modify/Show Material Property Design Data...
--

Advanced Material Property Data

Nonlinear Material Data...	Material Damping Properties...
Time Dependent Properties...	

Buttons

[OK](#) [Cancel](#)

LOAD PATEREN :

E Define Load Patterns

Load	Type	Self Weight Multiplier	Auto Lateral Load
Dead	Dead	1	
Dead	Dead	1	
Live	Live	0	
fc	Super Dead	0	
dead stair	Super Dead	0	
wall	Super Dead	0	
live stair	Live	0	
EQ X	Seismic	0	
EQ Y	Seismic	0	

Click To:

- Add New Load
- Modify Load
- Modify Lateral Load...
- Delete Load

OK Cancel

E Seismic Load Pattern - Eurocode8 2004

Direction and Eccentricity		Parameters	
<input checked="" type="checkbox"/> X Dir	<input type="checkbox"/> Y Dir	Country	CEN Default
<input checked="" type="checkbox"/> X Dir + Eccentricity	<input type="checkbox"/> Y Dir + Eccentricity	Ground Acceleration, ag/g	0.3
<input checked="" type="checkbox"/> X Dir - Eccentricity	<input type="checkbox"/> Y Dir - Eccentricity	Spectrum Type	2
Ecc. Ratio (All Diaph.)	0.05	Ground Type	B
Overwrite Eccentricities	<input type="button" value="Overwrite..."/>	Soil Factor, S	1.35
		Spectrum Period, Tb	0.05 sec
		Spectrum Period, Tc	0.25 sec
		Spectrum Period, Td	1.2 sec
		Lower Bound Factor, Beta	0.2
		Behavior Factor, q	5
		Correction Factor, Lambda	1
Time Period		OK	Cancel
<input type="radio"/> Approximate	Ct (m) = <input type="text"/>		
<input type="radio"/> Program Calculated			
<input checked="" type="radio"/> User Defined	T = 0.84 sec		
Story Range			
Top Story	Story9		
Bottom Story	Base		

E Seismic Load Pattern - Eurocode8 2004

Direction and Eccentricity		Parameters	
<input type="checkbox"/> X Dir	<input checked="" type="checkbox"/> Y Dir	Country	CEN Default
<input type="checkbox"/> X Dir + Eccentricity	<input checked="" type="checkbox"/> Y Dir + Eccentricity	Ground Acceleration, ag/g	0.3
<input type="checkbox"/> X Dir - Eccentricity	<input checked="" type="checkbox"/> Y Dir - Eccentricity	Spectrum Type	2
Ecc. Ratio (All Diaph.) <input type="text" value="0.05"/>		Ground Type	B
Overwrite Eccentricities <input type="button" value="Overwrite..."/>		Soil Factor, S	1.35
		Spectrum Period, Tb	0.05 sec
		Spectrum Period, Tc	0.25 sec
		Spectrum Period, Td	1.2 sec
		Lower Bound Factor, Beta	0.2
		Behavior Factor, q	5
		Correction Factor, Lambda	1
Time Period			
<input type="radio"/> Approximate	Ct (m) = <input type="text"/>		
<input type="radio"/> Program Calculated			
<input checked="" type="radio"/> User Defined	T = <input type="text" value="0.84"/> sec		
Story Range			
Top Story	Story9		
Bottom Story	Base		
		<input type="button" value="OK"/>	<input type="button" value="Cancel"/>

E Load Combination Data

General Data											
Load Combination Name	<input type="text" value="dead combo"/>										
Combination Type	<input type="button" value="Linear Add"/>										
Notes	<input type="button" value="Modify/Show Notes..."/>										
Auto Combination	<input type="text" value="No"/>										
Define Combination of Load Case/Combo Results											
<table border="1"> <thead> <tr> <th>Load Name</th> <th>Scale Factor</th> </tr> </thead> <tbody> <tr> <td>Dead</td> <td>1</td> </tr> <tr> <td>fc</td> <td>1</td> </tr> <tr> <td>dead stair</td> <td>1</td> </tr> <tr> <td>wall</td> <td>1</td> </tr> </tbody> </table>		Load Name	Scale Factor	Dead	1	fc	1	dead stair	1	wall	1
Load Name	Scale Factor										
Dead	1										
fc	1										
dead stair	1										
wall	1										
<input type="button" value="Add"/> <input type="button" value="Delete"/>											
<input type="button" value="OK"/> <input type="button" value="Cancel"/>											



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E Load Combination Data

General Data	
Load Combination Name	live combo
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No
Define Combination of Load Case/Combo Results	
Load Name	Scale Factor
Live	1
live stair	1

OK **Cancel**

E Load Combination Data

General Data	
Load Combination Name	working
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No
Define Combination of Load Case/Combo Results	
Load Name	Scale Factor
dead combo	1
live combo	1

OK **Cancel**



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E Load Combination Data

X

General Data

Load Combination Name	ultimate
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	1.4
live combo	1.6

Add Delete

OK Cancel

FOR EARTHQUAKS :

E Load Combination Data

X

General Data

Load Combination Name	S1
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	1.12
live combo	0.5
SPEC X	1
SPEC Y	0.3
SPEC Z	0.3

Add Delete

OK Cancel

E Load Combination Data

General Data

Load Combination Name	S2
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	1.12
live combo	0.5
SPEC X	0.3
SPEC Y	1
SPEC Z	0.3

Buttons: Add, Delete

OK **Cancel**

E Load Combination Data

General Data

Load Combination Name	S3
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	1.12
live combo	0.5
SPEC X	0.3
SPEC Y	0.3
SPEC Z	1

Buttons: Add, Delete

OK **Cancel**

E Load Combination Data

General Data

Load Combination Name	S4
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	0.9
live combo	0.5
SPEC X	1
SPEC Y	0.3
SPEC Z	0.3

Buttons: Add, Delete

OK **Cancel**

E Load Combination Data

General Data

Load Combination Name	S5
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	0.9
live combo	0.5
SPEC X	0.3
SPEC Y	1
SPEC Z	0.3

Buttons: Add, Delete

OK **Cancel**



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E Load Combination Data

X

General Data

Load Combination Name	S6
Combination Type	Linear Add
Notes	Modify/Show Notes...
Auto Combination	No

Define Combination of Load Case/Combo Results

Load Name	Scale Factor
dead combo	0.9
live combo	0.5
SPEC X	0.3
SPEC Y	0.3
SPEC Z	1

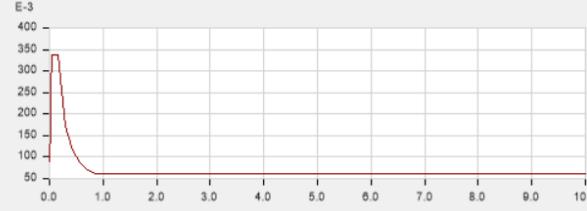
Add

Delete

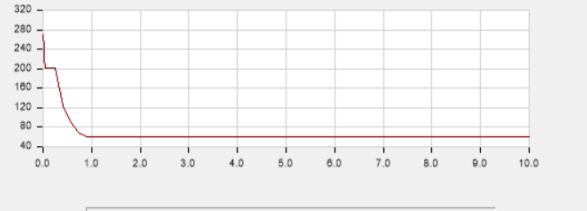
OK Cancel

DEFINE FUNCTION :

E EuroCode 8 - 2004 Function Definition

Function Name	RS VE	Function Damping Ratio	Damping Ratio	0.05
Parameters		Function Graph		
Country	CEN Default			
Direction	Vertical			
Ground Acceleration, ag/g	0.3			
Spectrum Type	2			
Ground Type				
Soil Factor, S				
Acceleration Ratio, Avg/Ag	0.45			
Spectrum Period, Tb	0.05 sec			
Spectrum Period, Tc	0.15 sec			
Spectrum Period, Td	1 sec			
Lower Bound Factor, Beta	0.2			
Behavior Factor, q	1			
<input type="button" value="Convert to User Defined"/> <input type="button" value="OK"/> <input type="button" value="Cancel"/>				

E EuroCode 8 - 2004 Function Definition

Function Name	RS H2	Function Damping Ratio	Damping Ratio	0.05
Parameters		Function Graph		
Country	CEN Default			
Direction	Horizontal			
Ground Acceleration, ag/g	0.3			
Spectrum Type	2			
Ground Type	B			
Soil Factor, S	1.35			
Acceleration Ratio, Avg/Ag				
Spectrum Period, Tb	0.05 sec			
Spectrum Period, Tc	0.25 sec			
Spectrum Period, Td	1.2 sec			
Lower Bound Factor, Beta	0.2			
Behavior Factor, q	5			
<input type="button" value="Convert to User Defined"/> <input type="button" value="OK"/> <input type="button" value="Cancel"/>				

LOAD CASES :

E Load Case Data

General			
Load Case Name	SPEC X		
Load Case Type	Response Spectrum		
Mass Source	Previous (MsSrc1)		
Analysis Model	Default		

Loads Applied			
Load Type	Load Name	Function	Scale Factor
Acceleration	U1	RS HZ	11.8

Advanced

Other Parameters			
Modal Load Case	Modal		
Modal Combination Method	CQC		
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1		
	Rigid Frequency, f2		
	Periodic + Rigid Type		
Earthquake Duration, td			
Directional Combination Type	SRSS		
Absolute Directional Combination Scale Factor			
Modal Damping	Constant at 0.05	<input type="button" value="Modify>Show..."/>	
Diaphragm Eccentricity	0.05 for All Diaphragms	<input type="button" value="Modify>Show..."/>	



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E Load Case Data

General

Load Case Name	SPEC Y	Design...
Load Case Type	Response Spectrum	Notes...
Mass Source	Previous (MsSrc1)	
Analysis Model	Default	

Loads Applied

Load Type	Load Name	Function	Scale Factor
Acceleration	U2	RS HZ	10.5

Other Parameters

Modal Load Case	Modal	
Modal Combination Method	CQC	
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1	
	Rigid Frequency, f2	
	Periodic + Rigid Type	
Earthquake Duration, td		
Directional Combination Type	SRSS	
Absolute Directional Combination Scale Factor		
Modal Damping	Constant at 0.05	Modify/Show...
Diaphragm Eccentricity	0.05 for All Diaphragms	Modify/Show...

DEFINE P DELTA :

E Preset P-Delta Options

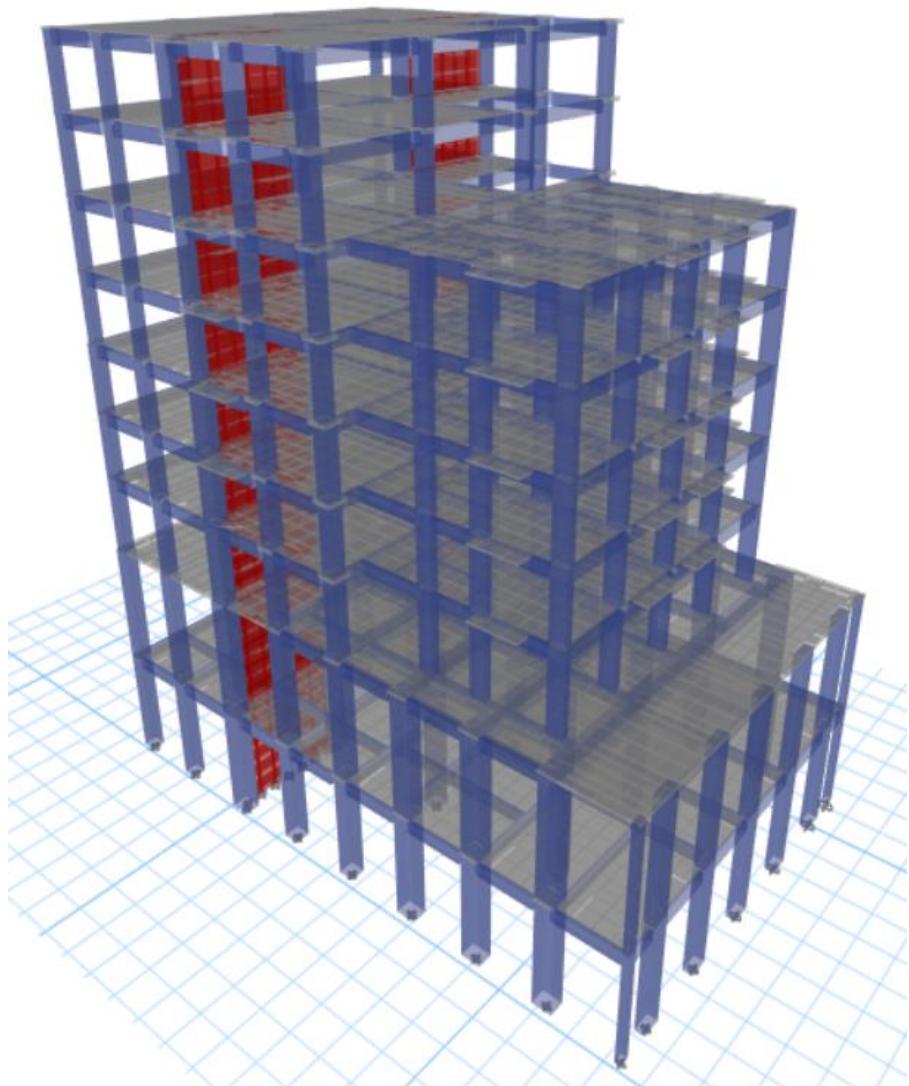
Automation Method	
<input type="radio"/> None	
<input type="radio"/> Non-iterative - Based on Mass	
<input checked="" type="radio"/> Iterative - Based on Loads	
Iterative P-Delta Load Case	
Load Pattern	Scale Factor
Dead	1
Dead	1
dead stair	1
fc	1
Live	0.5
live stair	0.5
wall	1
Relative Convergence Tolerance 0.0001	
OK Cancel	

DEFINE MASS SOURCE :

E Mass Source Data

Mass Source Name	MsSrc1
Mass Source	
<input type="checkbox"/> Element Self Mass	
<input type="checkbox"/> Additional Mass	
<input checked="" type="checkbox"/> Specified Load Patterns	
<input type="checkbox"/> Adjust Diaphragm Lateral Mass to Move Mass Centroid by:	
This Ratio of Diaphragm Width in X Direction	<input type="text"/>
This Ratio of Diaphragm Width in Y Direction	<input type="text"/>
Mass Multipliers for Load Patterns	
Load Pattern	Multiplier
Dead	1
Dead	1
fc	1
dead stair	1
wall	1
Live	0.5
live stair	0.5
Mass Options	
<input checked="" type="checkbox"/> Include Lateral Mass	
<input checked="" type="checkbox"/> Include Vertical Mass	
<input checked="" type="checkbox"/> Lump Lateral Mass at Story Levels	
OK Cancel	

MODEL 1



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E Modal Participating Mass Ratios

File Edit Format-Filter-Sort Select Options

Units: As Noted Hidden Columns: No Sort: None

Modal Participating Mass Ratios

Filter: None

	Case	Mode	Period sec	UX	UY	UZ	SumUX	SumUY	SumUZ	RX
▶	Modal	1	1.604	0.0001	0.8055	2.45E-05	0.0001	0.8055	2.45E-05	0.137
	Modal	2	1.251	0.2496	0.0008	0	0.2497	0.8062	2.494E-05	3.121E-05
	Modal	3	0.942	0.4623	0.0001	1.305E-05	0.712	0.8063	3.799E-05	2.43E-06
	Modal	4	0.514	0.0002	0.0948	1.226E-05	0.7122	0.9011	0.0001	0.3152
	Modal	5	0.448	0.0509	0.0005	8.279E-07	0.7631	0.9017	0.0001	0.002
	Modal	6	0.292	0.0014	0.0281	0.0004	0.7645	0.9298	0.0005	0.0255
	Modal	7	0.281	0.0147	0.0024	4.648E-05	0.7792	0.9322	0.0005	0.0019
	Modal	8	0.242	0.1228	1.592E-06	0.0005	0.902	0.9322	0.001	1.826E-05
	Modal	9	0.223	3.097E-05	0.0001	0.1832	0.902	0.9323	0.1843	0.0736
	Modal	10	0.198	0.0012	0.0325	0.0012	0.9032	0.9648	0.1855	0.0565
	Modal	11	0.194	0.0075	0.0043	0.0082	0.9107	0.9691	0.1937	0.0139
	Modal	12	0.186	0.0017	1.748E-05	0.1181	0.9124	0.9691	0.3118	0.0253
	Modal	13	0.16	0.0007	0.0005	0.1104	0.9131	0.9696	0.4222	0.0016
	Modal	14	0.146	1.044E-05	0.0259	0.0087	0.9131	0.9955	0.4309	0.0392
	Modal	15	0.13	0.0007	0.0023	0.0879	0.9138	0.9978	0.5188	0.0126

Record: << < 1 > >> of 20 Add Tables... Done

E Base Reactions

File Edit Format-Filter-Sort Select Options

Units: As Noted Hidden Columns: No Sort: None

Base Reactions

Filter: None

	Output Case	Case Type	Step Type	Step Number	FX tonf	FY tonf	FZ tonf	MX tonf-m	MY tonf-m	MZ tonf-m
▶	EQ X	LinStatic	Step By Step	1	-362.9318	0	0.0001	0.3548	-8964.5684	-4664.1216
	EQ X	LinStatic	Step By Step	2	-362.9318	-6.071E-07	0.0001	0.6276	-8968.1587	-4297.0738
	EQ X	LinStatic	Step By Step	3	-362.9318	0	0.0001	0.082	-8960.9782	-5031.1693
	EQ Y	LinStatic	Step By Step	1	0	-362.9317	3.42E-05	9102.1645	-0.503	16420.7363
	EQ Y	LinStatic	Step By Step	2	0	-362.9317	3.642E-05	9101.9152	2.6522	16112.0924
	EQ Y	LinStatic	Step By Step	3	0	-362.9317	3.197E-05	9102.4139	-3.6583	16729.3801
	SPEC X	LinRespSpec	Max		324.4052	10.8687	48.7657	650.1581	6678.6101	5609.0127
	SPEC Y	LinRespSpec	Max		9.4573	326.9782	32.0008	7833.8389	1458.012	15106.2879

Record: << < 1 > >> of 8 Add Tables... Done

DRIFT

K4 =0.7*5*F4*0.5

	A	B	F	K
1	TABLE: Story Drifts		DRV	
4	Story9	SPEC X	0.000896	0.001568
5	Story9	SPEC X	0.000447	0.000782
7	Story8	SPEC X	0.001035	0.001811
8	Story8	SPEC X	0.000632	0.001106
10	Story7	SPEC X	0.001142	0.001999
11	Story7	SPEC X	0.000606	0.001061
13	Story6	SPEC X	0.001369	0.002396
14	Story6	SPEC X	0.000708	0.001239
16	Story5	SPEC X	0.001569	0.002746
17	Story5	SPEC X	0.000797	0.001395
20	Story4	SPEC X	0.001815	0.003176
21	Story4	SPEC X	0.00093	0.001628
24	Story3	SPEC X	0.002098	0.003672
25	Story3	SPEC X	0.001125	0.001969
27	Story2	SPEC X	0.001456	0.002548
28	Story2	SPEC X	0.000673	0.001178
30	Story1	SPEC X	0.000759	0.001328
31	Story1	SPEC X	0.000354	0.00062
33			MAX	0.003672

K9 =0.7*5*0.5*F9

	A	B	F	K
1	TABLE: Story Drifts		DRV	
6	Story9	SPEC Y	0.000818	0.001432
9	Story8	SPEC Y	0.001174	0.002055
12	Story7	SPEC Y	0.0014	0.00245
15	Story6	SPEC Y	0.001629	0.002851
18	Story5	SPEC Y	0.000315	0.000551
19	Story5	SPEC Y	0.001775	0.003106
22	Story4	SPEC Y	0.000363	0.000635
23	Story4	SPEC Y	0.002037	0.003565
26	Story3	SPEC Y	0.002396	0.004193
29	Story2	SPEC Y	0.002424	0.004242
32	Story1	SPEC Y	0.001266	0.002216
33			MAX Y	0.004242

COLUMNS

A	B	H	L	M	N	O		
Story	Label	FZ	AC	B	T	CHOOSE		
		tonf						
5	Base	61	11.2746	74.35288	30	2.478429	30	
7	Base	66	11.5224	75.98705	30	2.532902	30	
3	Base	71	43.4225	286.3594	30	9.545314	30	
9	Base	76	73.3757	483.8925	30	16.12975	30	
0	Base	81	79.4006	523.6251	30	17.45417	30	
1	Base	86	76.4202	503.9701	30	16.799	30	
2	Base	91	43.4891	286.7986	30	9.559954	30	
3	Base	96	551.0013	3633.702	40	90.84254	100	
4	Base	101	537.2757	3543.185	40	88.57963	100	
5	Base	106	675.6525	4455.742	40	111.3935	110	
5	Base	111	606.8526	4002.026	40	100.0506	100	
7	Base	116	175.0244	1154.238	30	38.47459	40	
3	Base	121	154.5737	1019.371	30	33.97903	50	
9	Base	126	153.592	1012.897	30	33.76323	50	
0	Base	131	171.2828	1129.563	30	37.65209	60	
1	Base	136	179.2029	1181.794	30	39.39312	60	
2	Base	141	199.2687	1314.122	30	43.80407	60	
3	Base	146	335.4066	2211.914	30	73.73047	80	
4	Base	151	354.6235	2338.644	30	77.95481	80	
5	Base	156	374.6752	2470.88	30	82.36265	80	
5	Base	161	328.283	2164.936	30	72.16453	70	

DESIGN COMINATION :

E Design Load Combinations Selection - Concrete Frame Design

Strength

Choose Combinations

List of Combinations

- DConS1
- DConS2
- DConS3
- DConS4
- DConS5
- DConS6
- DConS7
- DConS8
- DConS9
- DConS10
- DConS11
- DConS12
- DConS13
- DConS14

Design Combinations

- S1
- S2
- S3
- S4
- S5
- S6
- ultimate

OK Cancel

E Concrete Frame Design Preferences for BS 8110-97

Item	Value	
01 Design Code	BS 8110-97	
02 Multi-Response Case Design	Step-by-Step - All	
03 Number of Interaction Curves	24	
04 Number of Interaction Points	11	
05 Consider Minimum Eccentricity?	Yes	
06 Ignore Beneficial P_u for Beam Design?	No	
07 Gamma (Steel)	1.15	
08 Gamma (Concrete)	1.5	
09 Gamma (Concrete Shear)	1.5	
10 User Defined Allowable PT Stresses?	No	
11 Concrete Strength Ratio at Transfer f'_{ci} / f'_{cu}	0.8	
12 Transfer: Top Fiber Tensile Stress / $f'_{ci}^{(1/2)}$	3	
13 Transfer: Bottom Fiber Tensile Stress / $f'_{ci}^{(1/2)}$	3	
14 Transfer: Extreme Fiber Compressive Stress / f'_{ci}	0.6	
15 Final: Top Fiber Tensile Stress / $f'_{cu}^{(1/2)}$	6	
16 Final: Bottom Fiber Tensile Stress / $f'_{cu}^{(1/2)}$	6	
17 Final: Extreme Fiber Compressive Stress / f'_{cu}	0.6	
18 Sustained: Extreme Fiber Compressive Stress / ...	0.45	

Set To Default Values

All Items
Selected Items

Reset To Previous Values

All Items
Selected Items

OK
Cancel

Item Description

The selected design code. Subsequent design is based on this selected code.

Explanation of Color Coding for Values

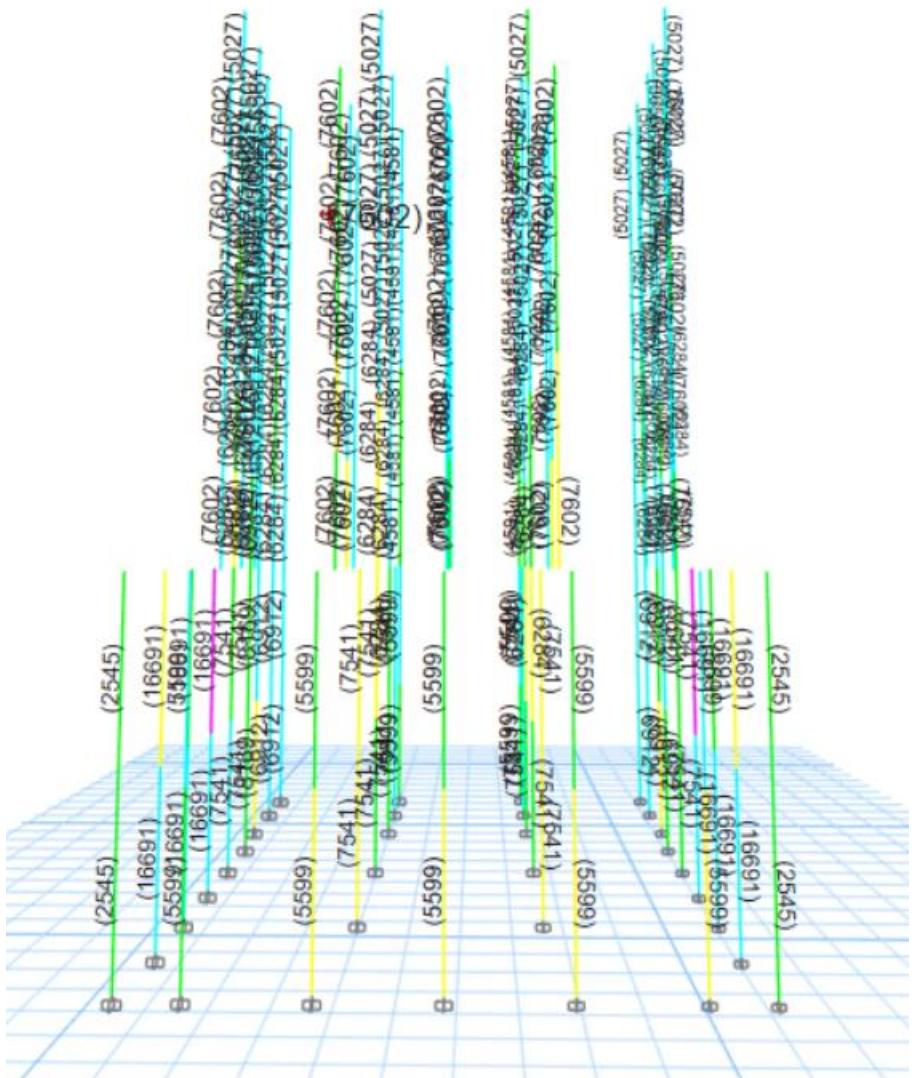
Blue: Default Value

Black: Not a Default Value

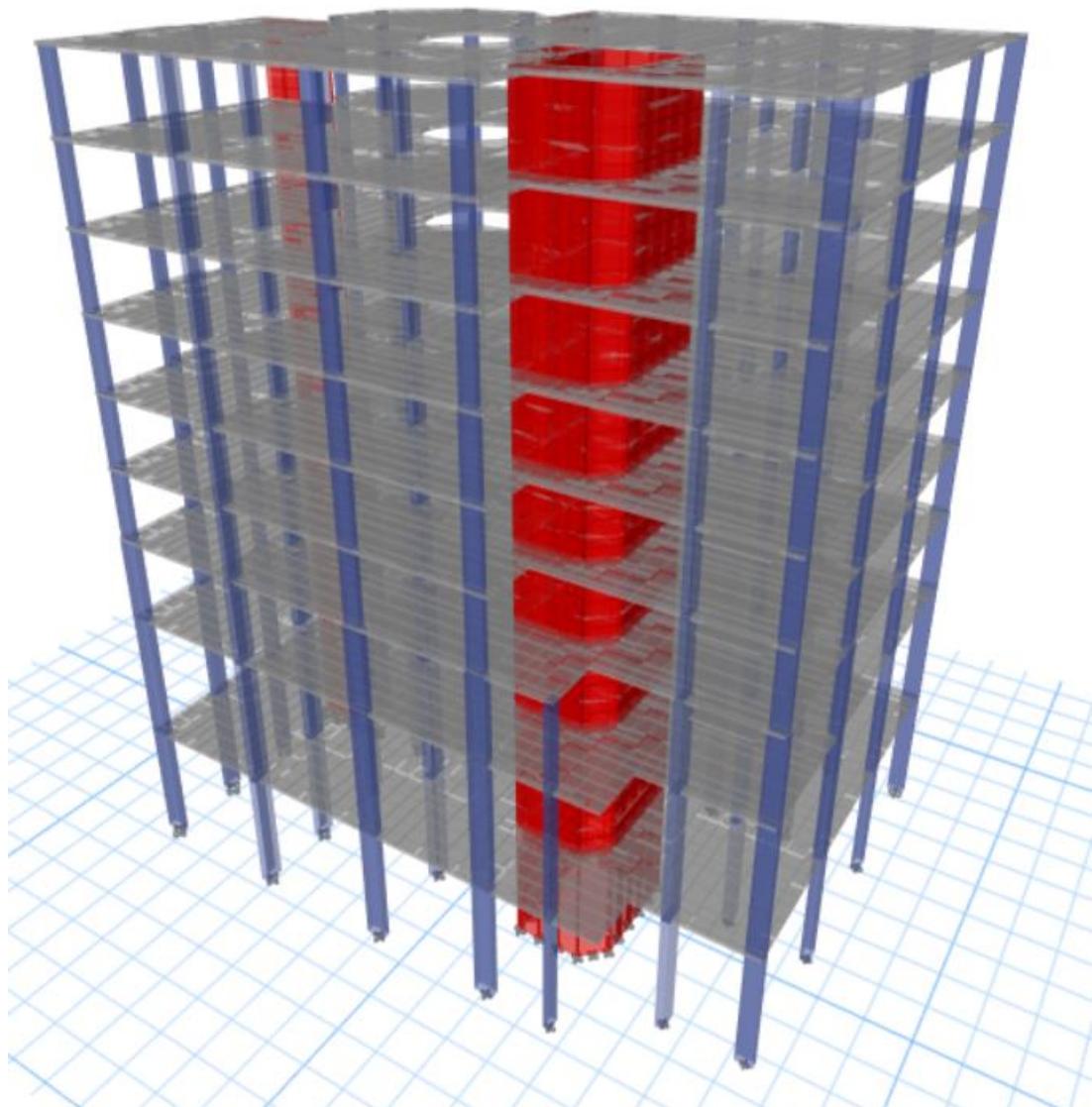
Red: Value that has changed during the current session



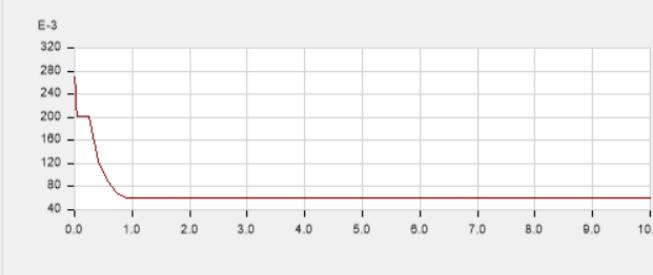
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MODEL 2



E EuroCode 8 - 2004 Function Definition

Function Name	RS	Function Damping Ratio
Damping Ratio	0.05	
Parameters		
Country	CEN Default	Function Graph
Direction	Horizontal	
Ground Acceleration, ag/g	0.3	
Spectrum Type	2	
Ground Type	B	
Soil Factor, S	1.35	
Acceleration Ratio, Avg/Ag		
Spectrum Period, Tb	0.05 sec	
Spectrum Period, Tc	0.25 sec	
Spectrum Period, Td	1.2 sec	
Lower Bound Factor, Beta	0.2	
Behavior Factor, q	5	
Function Points		
Period	Acceleration	
0	0.27	
0.0167	0.2475	
0.0333	0.225	
0.05	0.2025	
0.25	0.2025	
0.4083	0.124	
0.5667	0.0893	
0.725	0.0698	
0.8833	0.06	
1.0417	0.06	
Plot Options		
<input checked="" type="radio"/> Linear X - Linear Y <input type="radio"/> Linear X - Log Y <input type="radio"/> Log X - Linear Y <input type="radio"/> Log X - Log Y		
OK		Cancel
Convert to User Defined		



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E Load Case Data X

Load Case Name	SPEC X	Design...
Load Case Type	Response Spectrum	Notes...
Mass Source	Previous (MsSrc1)	
Analysis Model	Default	

Loads Applied

Load Type	Load Name	Function	Scale Factor
Acceleration	U1	RS	13

Advanced

Other Parameters

Modal Load Case	Modal
Modal Combination Method	CQC
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1
	Rigid Frequency, f2
	Periodic + Rigid Type
Earthquake Duration, td	
Directional Combination Type	SRSS
Absolute Directional Combination Scale Factor	
Modal Damping	Constant at 0.05
Diaphragm Eccentricity	0.05 for All Diaphragms



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E Load Case Data X

General			
Load Case Name	SPEC Y		
Load Case Type	Response Spectrum		
Mass Source	Previous (MsSrc1)		
Analysis Model	Default		
Loads Applied			
Load Type	Load Name	Function	Scale Factor
Acceleration	U2	RS	10
<input type="checkbox"/> Advanced			
Other Parameters			
Modal Load Case	Modal		
Modal Combination Method	CQC		
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1		
	Rigid Frequency, f2		
	Periodic + Rigid Type		
Earthquake Duration, td			
Directional Combination Type	SRSS		
Absolute Directional Combination Scale Factor			
Modal Damping	Constant at 0.05	<input style="width: 100px; height: 25px;" type="button" value="Modify>Show..."/>	
Diaphragm Eccentricity	0.05 for All Diaphragms	<input style="width: 100px; height: 25px;" type="button" value="Modify>Show..."/>	
<input style="width: 80px; height: 30px;" type="button" value="OK"/>		<input style="width: 80px; height: 30px;" type="button" value="Cancel"/>	



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Modal Participating Mass Ratios

File Edit Format-Filter-Sort Select Options

Units: As Noted Hidden Columns: No Sort: None

Modal Participating Mass Ratios

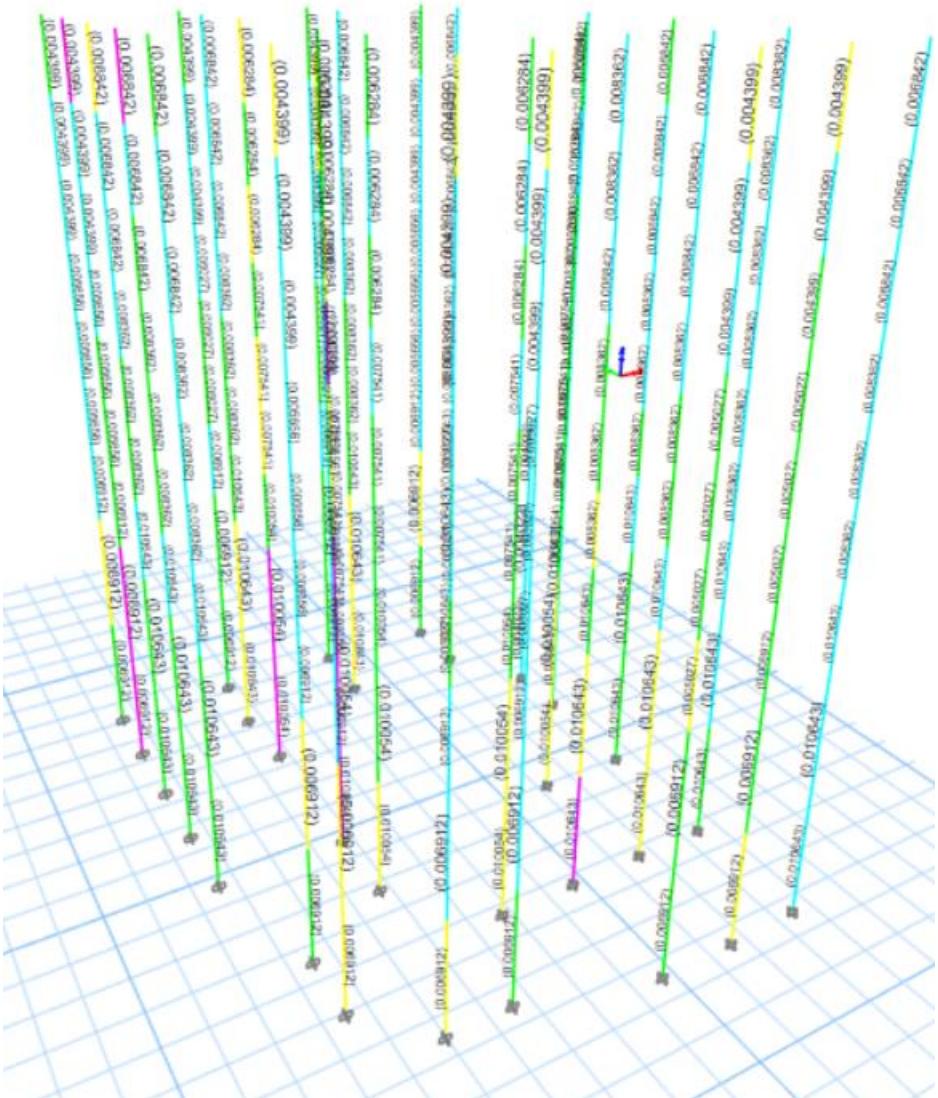
	Case	Mode	Period sec	UX	UY	UZ	SumUX	SumUY	SumUZ	RX
▶	Modal	1	2.385	0.5197	0.0102	0	0.5197	0.0102	0	0.0043
	Modal	2	1.95	0.0014	0.7114	0	0.521	0.7216	0	0.3
	Modal	3	1.457	0.2142	0.0082	0	0.7352	0.7299	0	0.0028
	Modal	4	0.583	0.0768	0.0009	0	0.812	0.7308	0	0.0038
	Modal	5	0.381	0.001	0.1762	0	0.813	0.907	0	0.3874
	Modal	6	0.313	0.0714	8.389E-06	0	0.8844	0.907	0	0.0001
	Modal	7	0.27	0.0376	0.0004	0	0.922	0.9074	0	0.001
	Modal	8	0.162	0.0057	0.0021	0	0.9277	0.9095	0	0.0073
	Modal	9	0.15	0.0033	0.0431	0	0.931	0.9526	0	0.1262
	Modal	10	0.126	0.0293	0.0029	0	0.9603	0.9556	0	0.0079
	Modal	11	0.113	0.0051	0.0007	0	0.9653	0.9562	0	0.0025
	Modal	12	0.089	0.0047	0.0223	0	0.97	0.9785	0	0.0783
	Modal	13	0.085	0.0014	0.0001	0	0.9714	0.9786	0	0.0003
	Modal	14	0.074	0.0157	0.0052	0	0.9871	0.9838	0	0.0177
	Modal	15	0.065	0.0033	0.0105	0	0.9904	0.9942	0	0.0388

Record: << < 1 > >> of 20 Add Tables... Done

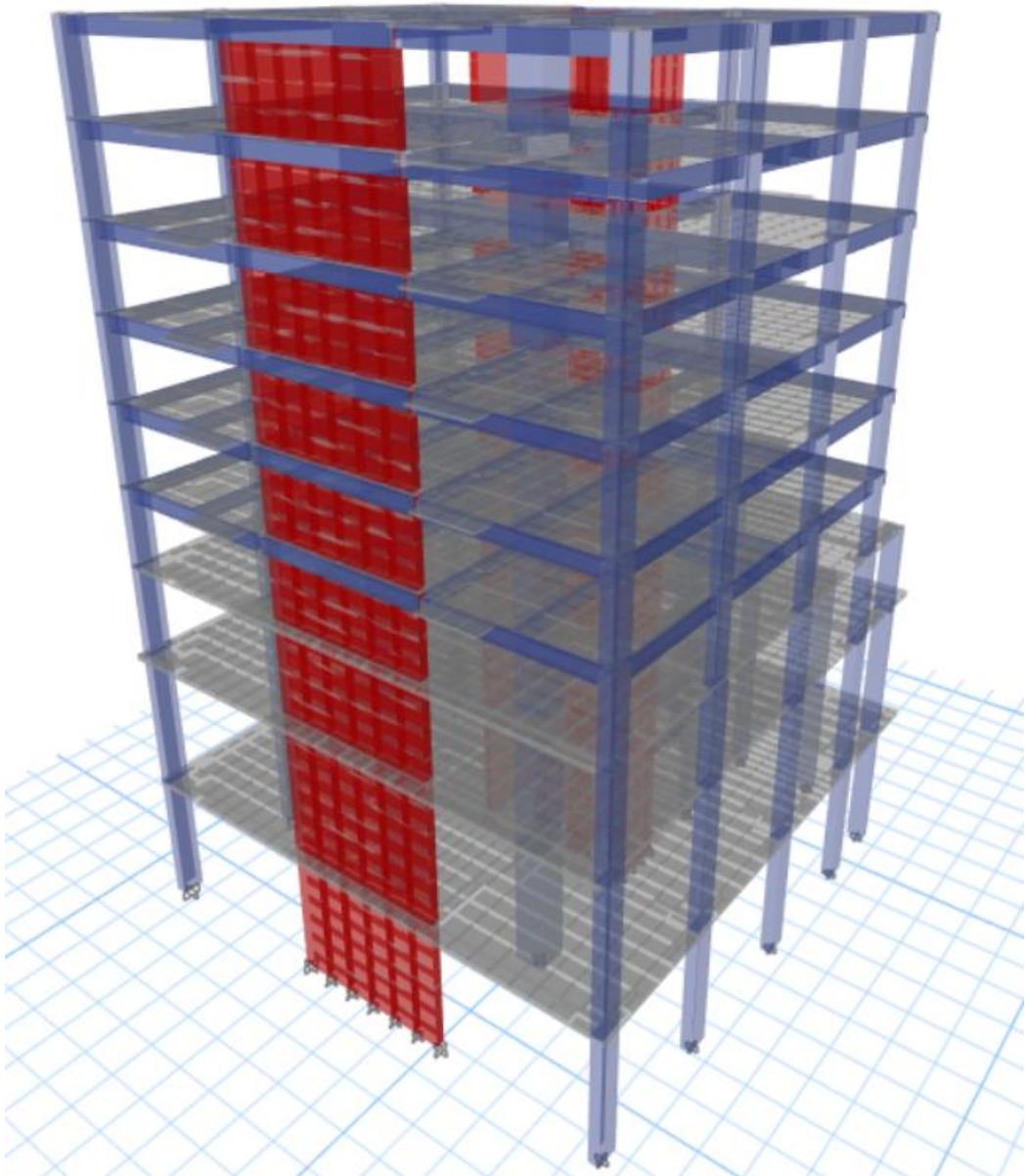
Story	Label	FZ	ac	b	t	t chosen
Base	1	46.5944	307.2772	30	10.24257	
Base	~19590	128.8699	849.8615	30	28.32872	
Base	86	130.6082	861.3251	30	28.71084	
Base	131	131.8441	869.4755	30	28.98252	
Base	~19601	135.1909	891.5467	30	29.71822	
Base	~19607	145.0096	956.2983	30	31.87661	
Base	36	147.6161	973.4875	30	32.44958	
Base	6	158.9777	1048.414	30	34.94714	
Base	91	160.5364	1058.693	30	35.28978	60
Base	136	160.8965	1061.068	30	35.36893	
Base	96	163.9022	1080.89	30	36.02966	
Base	126	179.6439	1184.702	30	39.49007	
Base	116	212.0397	1398.343	30	46.61144	
Base	76	214.1789	1412.451	30	47.08169	
Base	21	221.2357	1458.988	30	48.63295	
Base	11	228.852	1509.216	30	50.30719	
Base	121	244.1076	1609.822	30	53.66074	
Base	26	267.4835	1763.98	30	58.79933	
Base	106	275.0424	1813.829	30	60.46096	
Base	41	281.593	1857.028	30	61.90094	
Base	51	281.7236	1857.889	30	61.92965	
Base	101	287.3813	1895.2	30	63.17335	
Base	81	287.9648	1899.048	30	63.30161	80
Base	16	347.4724	2291.485	30	76.38282	
Base	66	395.1558	2605.944	30	86.86478	
Base	111	396.6911	2616.068	30	87.20228	
Base	46	428.1783	2823.718	30	94.12393	
Base	56	442.8351	2920.375	30	97.34585	
Base	141	446.3869	2943.799	30	98.12662	
Base	61	456.6804	3011.681	30	100.3894	120
Base	71	544.8286	3592.994	30	119.7665	
Base	31	557.8373	3678.783	30	122.6261	



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MODEL 3





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E Load Case Data

General

Load Case Name	SPEC X	Design...
Load Case Type	Response Spectrum	Notes...
Mass Source	Previous (MsSrc1)	
Analysis Model	Default	

Loads Applied

Load Type	Load Name	Function	Scale Factor
Acceleration	U1	RS HZ	13.9

Other Parameters

Modal Load Case	Modal	
Modal Combination Method	CQC	
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1	
	Rigid Frequency, f2	
	Periodic + Rigid Type	
Earthquake Duration, td		
Directional Combination Type	SRSS	
Absolute Directional Combination Scale Factor		
Modal Damping	Constant at 0.05	Modify/Show...
Diaphragm Eccentricity	0.05 for All Diaphragms	Modify/Show...



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E Load Case Data X

General

Load Case Name	SPEC YI	Design...
Load Case Type	Response Spectrum	Notes...
Mass Source	Previous (MsSrc1)	
Analysis Model	Default	

Loads Applied

Load Type	Load Name	Function	Scale Factor
Acceleration	U2	RS HZ	10.2

1 Add Delete Advanced

Other Parameters

Modal Load Case	Modal	
Modal Combination Method	CQC	
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1	
	Rigid Frequency, f2	
	Periodic + Rigid Type	
Earthquake Duration, td		
Directional Combination Type	SRSS	
Absolute Directional Combination Scale Factor		
Modal Damping	Constant at 0.05	Modify/Show...
Diaphragm Eccentricity	0.05 for All Diaphragms	Modify/Show...

OK Cancel



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E Base Reactions

Base Reactions										
	Output Case	Case Type	Step Type	Step Number	FX tonf	FY tonf	FZ tonf	MX tonf-m	MY tonf-m	MZ tonf-m
▶	EQ X	LinStatic	Step By Step	1	-649.2055	1.425E-06	0.0021	-24.8848	-17397.6559	-29412.4342
	EQ X	LinStatic	Step By Step	2	-649.2055	1.708E-06	0.0024	-30.5092	-17407.629	-28770.2464
	EQ X	LinStatic	Step By Step	3	-649.2055	1.142E-06	0.0019	-19.2604	-17387.6827	-30054.622
	EQ Y	LinStatic	Step By Step	1	6.268E-06	-649.2055	0.0066	17408.0226	24.8543	13655.9546
	EQ Y	LinStatic	Step By Step	2	9.44E-06	-649.2055	0.0063	17414.0442	35.5408	12977.3884
	EQ Y	LinStatic	Step By Step	3	3.097E-06	-649.2055	0.0069	17402.001	14.1678	14334.5208
	SPEC X	LinRespSpec	Max		495.1581	305.9264	53.778	6633.1744	9493.6536	25195.5524
	SPEC Y	LinRespSpec	Max		223.4529	400.3314	23.8735	8305.3142	4564.7918	9154.0659

Record: << < 1 > >> of 8

Add Tables...

Done



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E Modal Participating Mass Ratios

File Edit Format-Filter-Sort Select Options

Units: As Noted Hidden Columns: No Sort: None

Modal Participating Mass Ratios

Filter: None

	Case	Mode	Period sec	UX	UY	UZ	SumUX	SumUY	SumUZ	RX
▶	Modal	1	1.761	0.3665	0.2066	4.328E-05	0.3665	0.2066	4.328E-05	0.0573
	Modal	2	1.558	0.2187	0.5041	2.168E-05	0.5853	0.7106	0.0001	0.1484
	Modal	3	1.175	0.128	0.026	0	0.7132	0.7367	0.0001	0.0097
	Modal	4	0.415	0.0783	0.0323	0.0003	0.7916	0.769	0.0004	0.0568
	Modal	5	0.319	0.0393	0.1244	0.0005	0.8309	0.8934	0.0009	0.2027
	Modal	6	0.294	0	0.0001	0.1091	0.8309	0.8935	0.11	0.0194
	Modal	7	0.29	5.719E-06	0.0003	0.0229	0.8309	0.8938	0.1328	0.0052
	Modal	8	0.27	0.0001	1.485E-05	0.0483	0.8311	0.8938	0.1812	0.0117
	Modal	9	0.253	0.0042	0.0002	1.363E-05	0.8353	0.894	0.1812	0
	Modal	10	0.239	0.001	0.0006	0.0136	0.8363	0.8946	0.1947	0.0057
	Modal	11	0.229	0.0084	0.0011	0.1501	0.8447	0.8956	0.3449	0.0045
	Modal	12	0.224	0.0551	0.0031	0.025	0.8998	0.8987	0.3699	0.0019
	Modal	13	0.19	0.0005	0.0002	0.1144	0.9003	0.8989	0.4843	0.0002
	Modal	14	0.173	0.016	0.0105	0.0009	0.9164	0.9094	0.4851	0.0236
	Modal	15	0.145	0.012	2.206E-05	9.361E-07	0.9283	0.9095	0.4851	0.0001

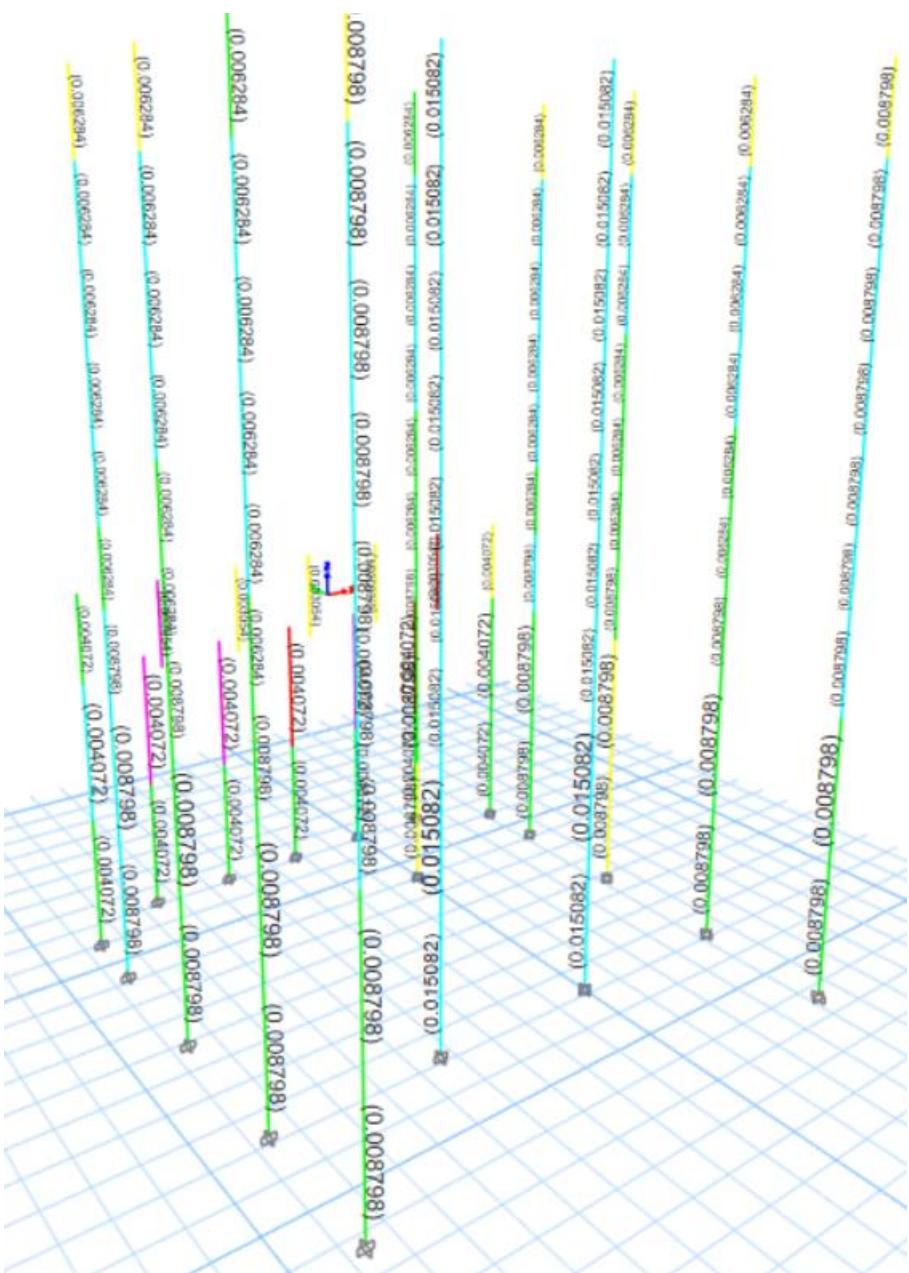
Record: << < 1 > >> of 20

Add Tables...

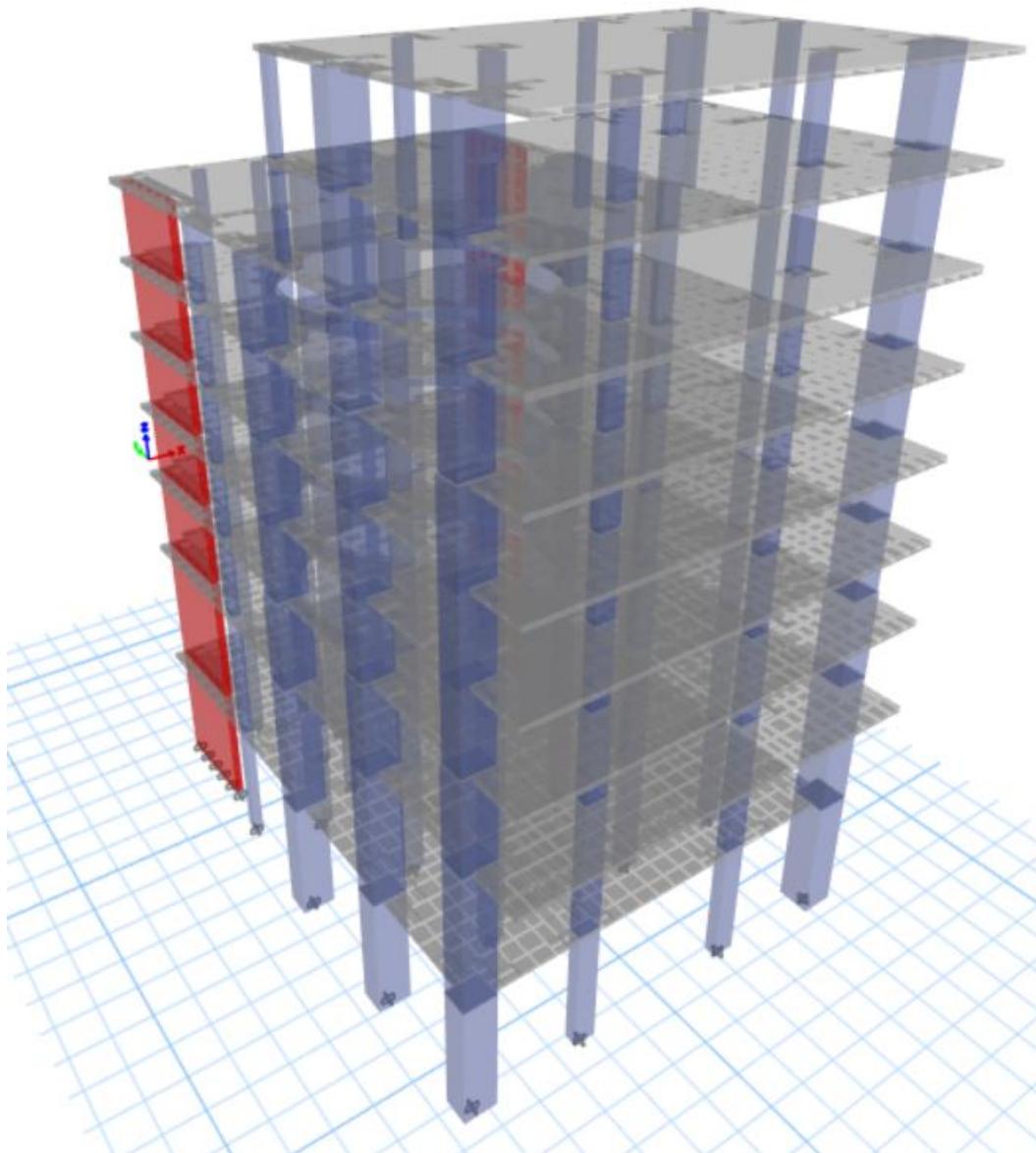
Done



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MODEL 4



E Load Case Data X

General

Load Case Name	SPEC X	Design...
Load Case Type	Response Spectrum	Notes...
Mass Source	Previous (MsSrc1)	
Analysis Model	Default	

Loads Applied

Load Type	Load Name	Function	Scale Factor	
Acceleration	U1	RS	12.6	Add
				Delete

Advanced

Other Parameters

Modal Load Case	Modal	CQC
Modal Combination Method	CQC	
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1	<input type="text"/>
	Rigid Frequency, f2	<input type="text"/>
	Periodic + Rigid Type	<input type="text"/>
Earthquake Duration, td	<input type="text"/>	
Directional Combination Type	SRSS	
Absolute Directional Combination Scale Factor	<input type="text"/>	
Modal Damping	Constant at 0.05	Modify/Show...
Diaphragm Eccentricity	0.05 for All Diaphragms	Modify/Show...

OK
Cancel



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E Load Case Data X

General

Load Case Name	SPEC Y	<input type="button" value="Design..."/>
Load Case Type	Response Spectrum	<input type="button" value="Notes..."/>
Mass Source	Previous (MsSrc1)	
Analysis Model	Default	

Loads Applied

Load Type	Load Name	Function	Scale Factor
Acceleration	U2	RS	9.8067

Other Parameters

Modal Load Case	Modal	
Modal Combination Method	CQC	
<input type="checkbox"/> Include Rigid Response	Rigid Frequency, f1	
	Rigid Frequency, f2	
	Periodic + Rigid Type	
Earthquake Duration, td		
Directional Combination Type	SRSS	
Absolute Directional Combination Scale Factor		
Modal Damping	Constant at 0.05	<input type="button" value="Modify>Show..."/>
Diaphragm Eccentricity	0.05 for All Diaphragms	<input type="button" value="Modify>Show..."/>

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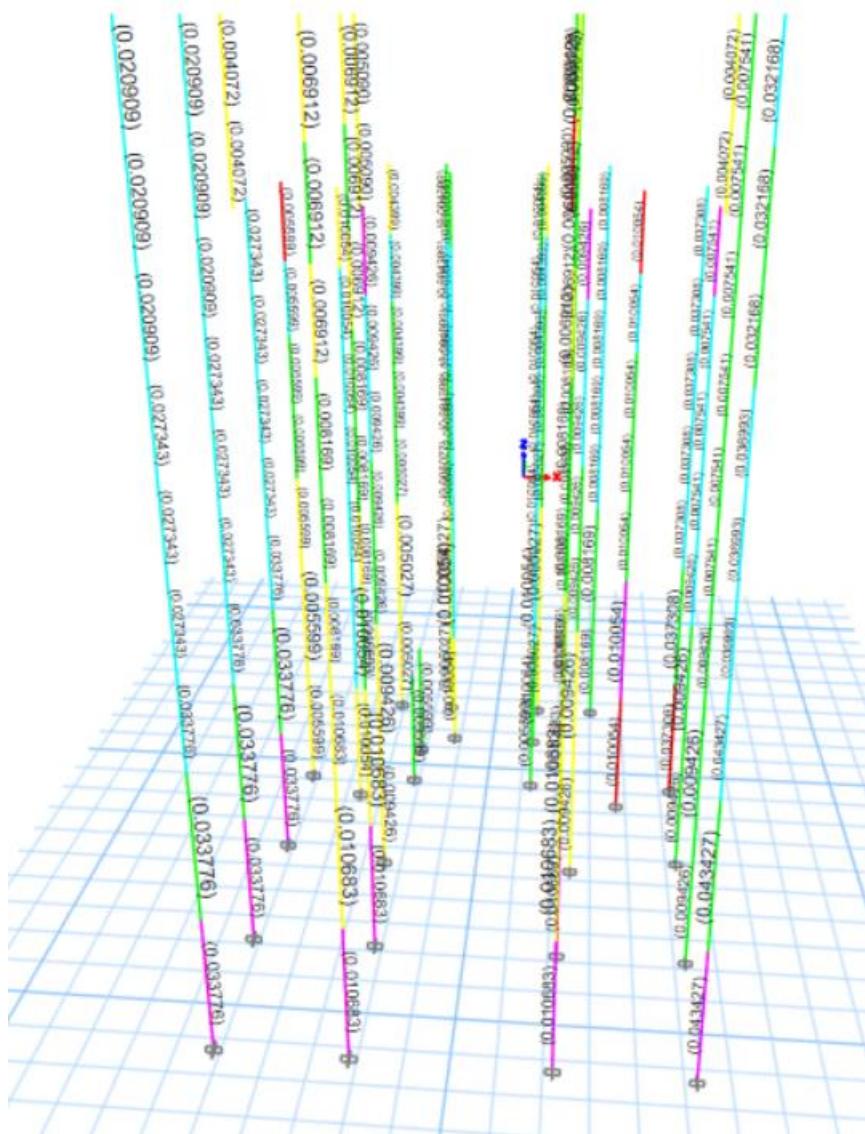
E Modal Participating Mass Ratios

Case	Mode	Period sec	UX	UY	UZ	SumUX	SumUY	SumUZ	RX	
►	Modal	1	2.379	0.7521	0.0005	1.591E-06	0.7521	0.0005	1.591E-06	0.0001
	Modal	2	1.57	0.0024	0.7254	0.0001	0.7546	0.726	0.0001	0.166
	Modal	3	1.374	0.0487	0.0097	0	0.8032	0.7357	0.0001	0.0023
	Modal	4	0.618	0.0834	1.293E-05	3.917E-06	0.8866	0.7357	0.0001	1.733E-05
	Modal	5	0.462	5.624E-06	0.0836	0.001	0.8866	0.8193	0.0011	0.1063
	Modal	6	0.368	0.0082	6.775E-07	0.0002	0.8948	0.8193	0.0013	0.0003
	Modal	7	0.362	0.0003	0.005	0.0089	0.8951	0.8242	0.0102	0.0001
	Modal	8	0.342	4.995E-05	0.0012	0.0088	0.8951	0.8254	0.019	0.0001
	Modal	9	0.328	0.0296	0.0002	4.43E-05	0.9247	0.8256	0.0191	0.0004
	Modal	10	0.312	7.45E-07	0.0003	0.0393	0.9247	0.8258	0.0584	0.0042
	Modal	11	0.285	2.388E-05	0.0012	0.0717	0.9247	0.827	0.1301	0.0171
	Modal	12	0.246	0.0005	0.0367	0.0324	0.9252	0.8637	0.1625	0.0344
	Modal	13	0.236	2.499E-05	0.042	0.0668	0.9252	0.9057	0.2293	0.1194
	Modal	14	0.22	0.0009	0.0112	0.0598	0.9261	0.917	0.2891	0.002
	Modal	15	0.183	0.0315	0.0006	1.069E-05	0.9576	0.9175	0.2891	0.0001

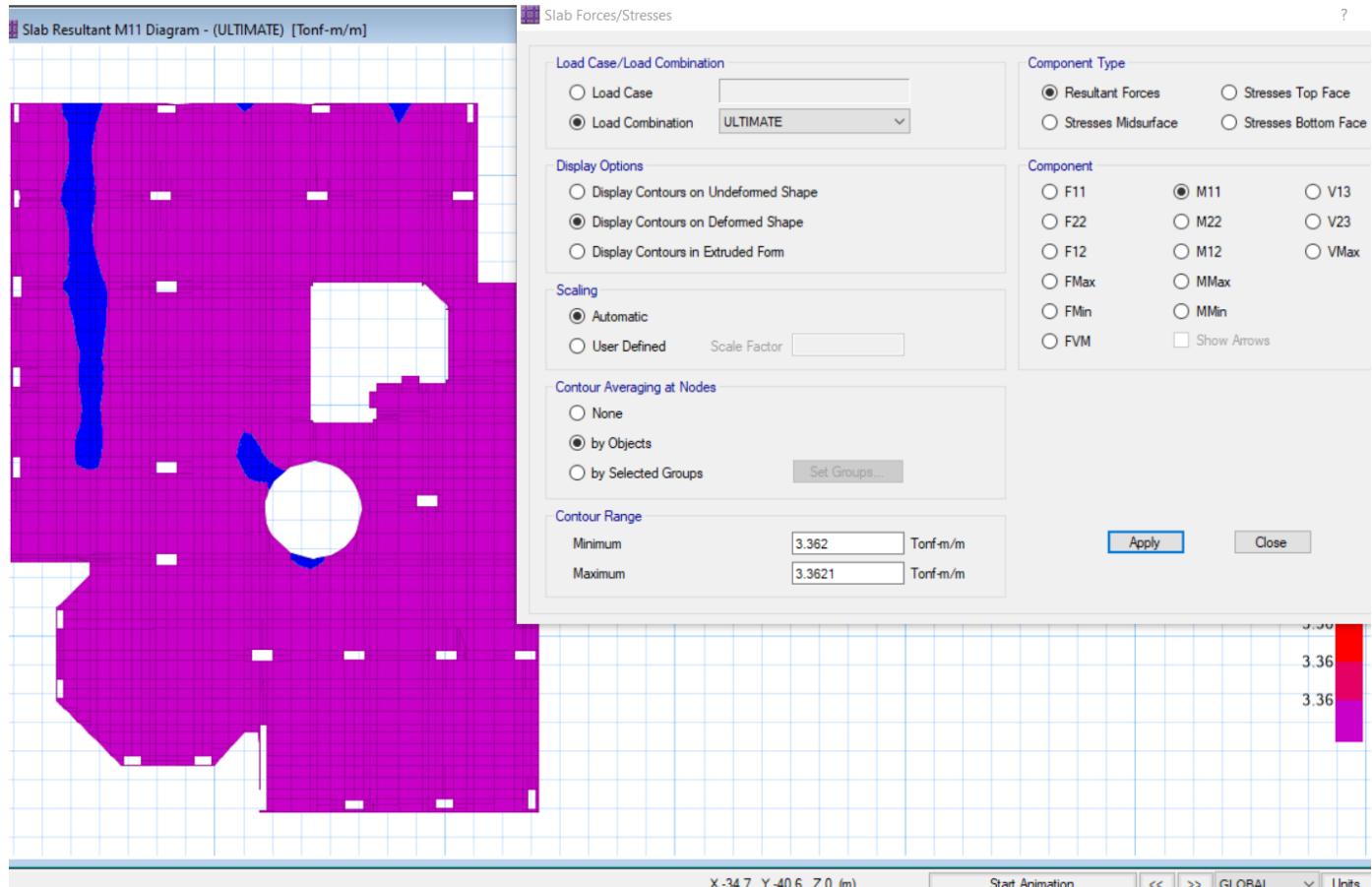
Record: << < 1 > >> of 20 Add Tables... Done



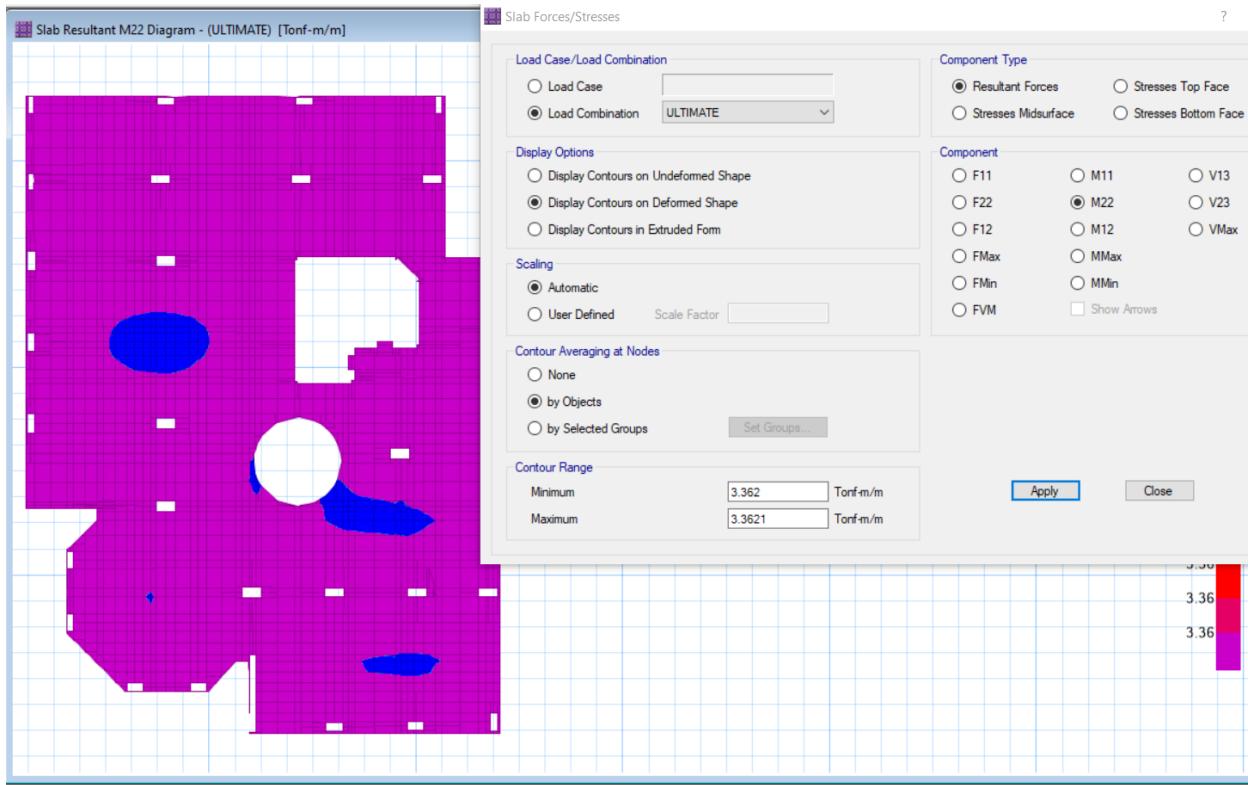
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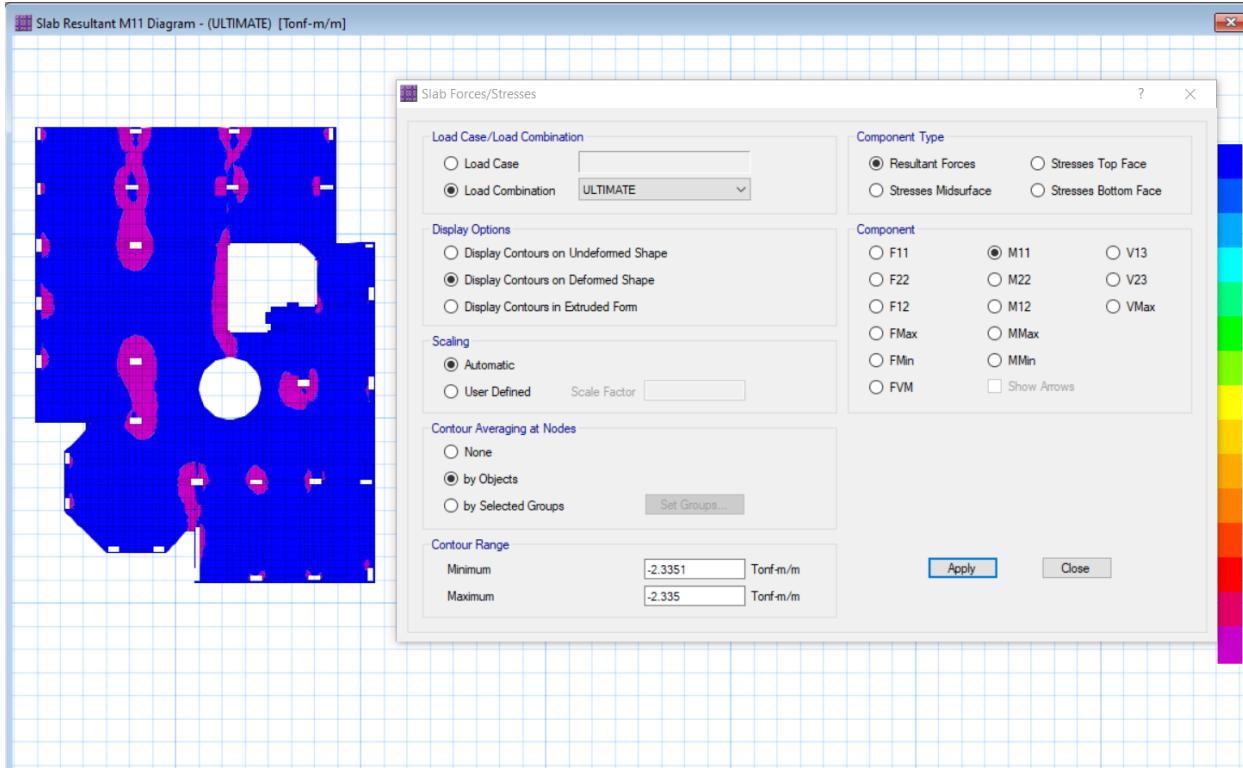
USING SAFE



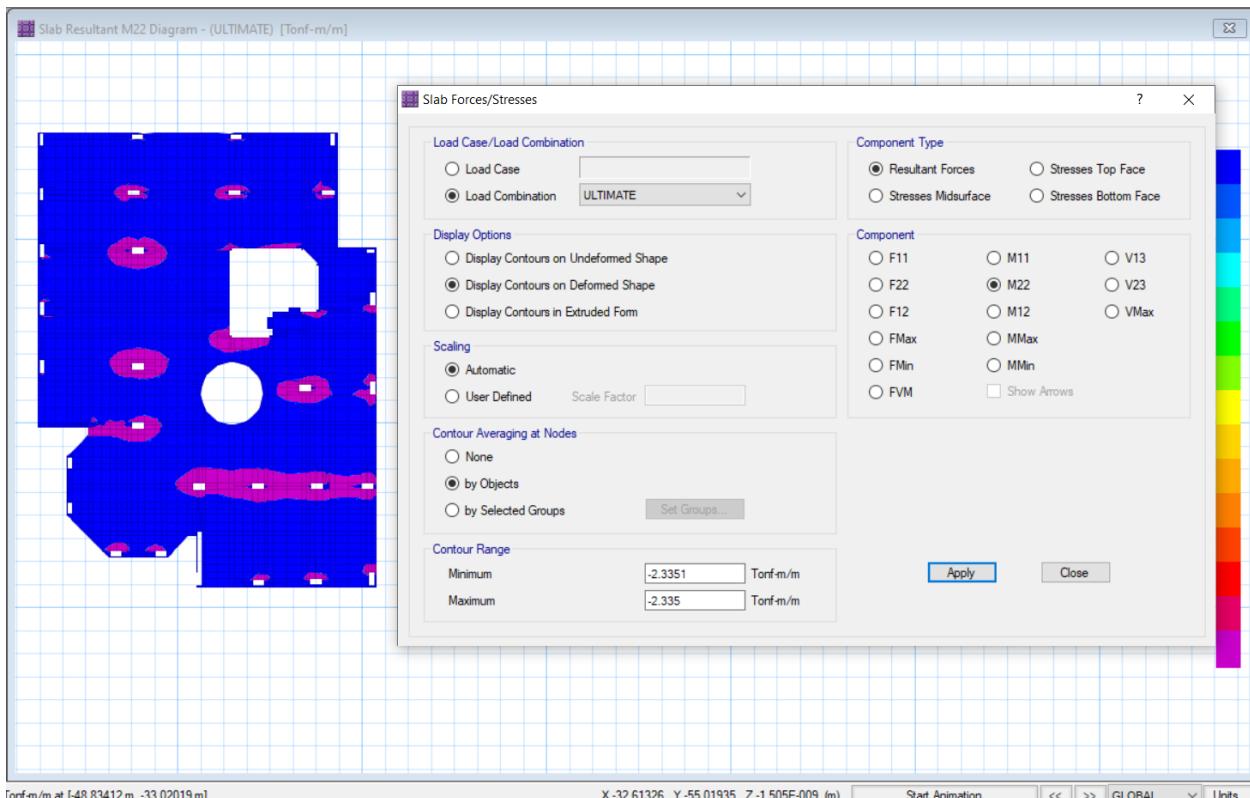
**CALC SHEET
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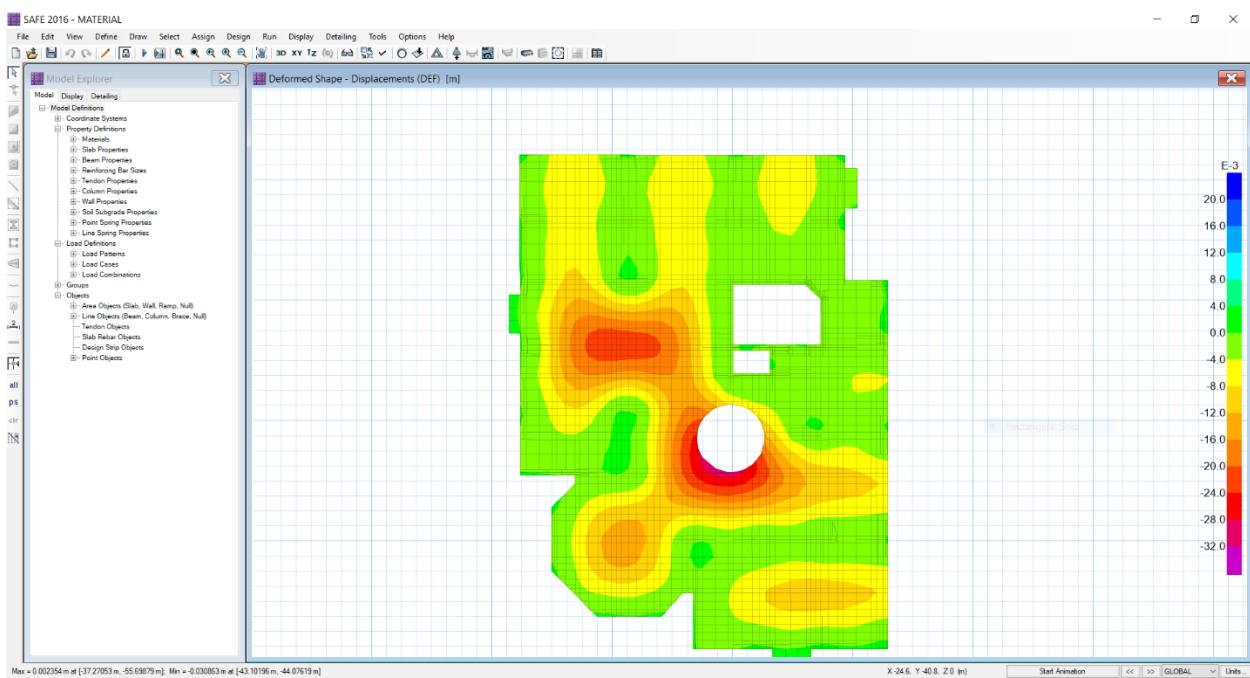
**CALC SHEET
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Tonf-m/m at [-48.83412 m, -33.02019 m] X-32.61326, Y-55.01935, Z-1.505E-009 (m) Start Animation << >> GLOBAL Units...



B28 v : X ✓ f_x 60

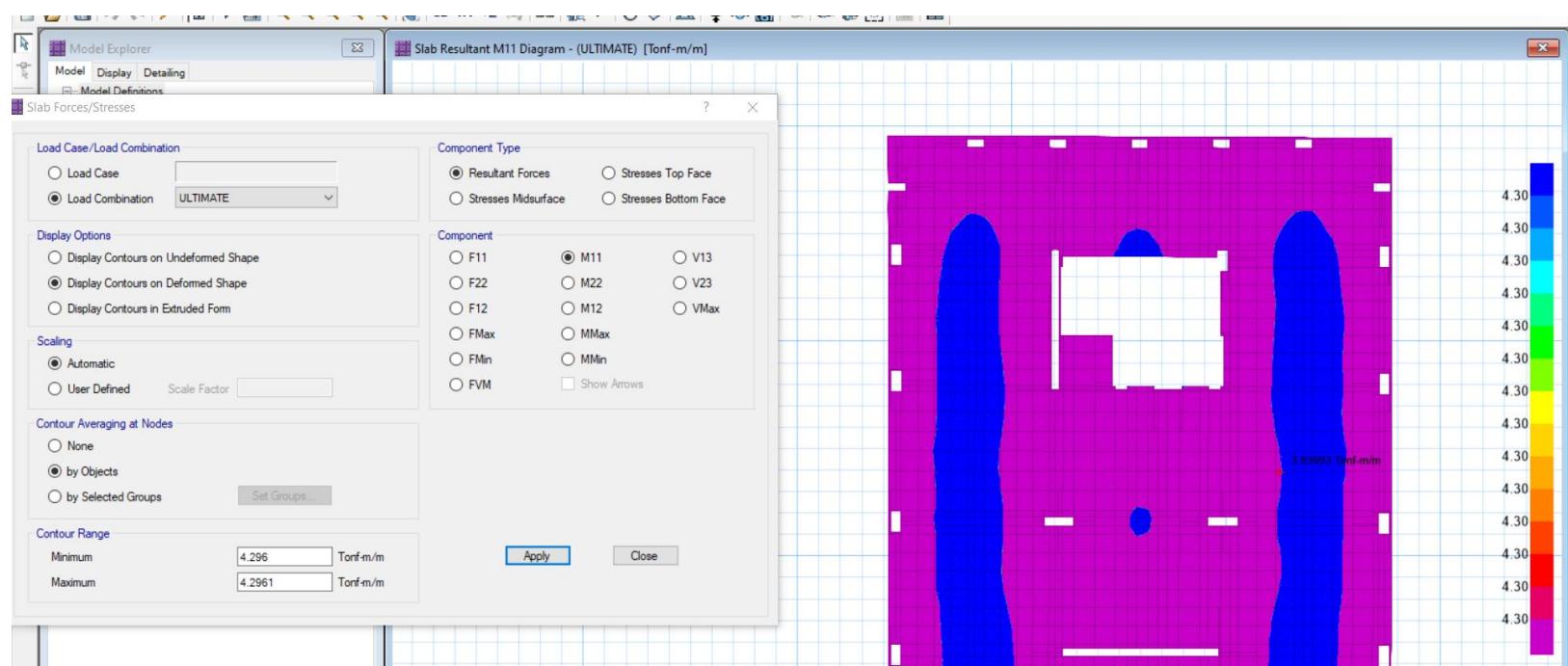
A	B	C	D	E	F	G	H	I	J			
14												
15												
16												
17												
18												
19												
20												
21												
22												
23												
24	Col.	Ult. Load N_u (ton)	Col. Dims.		Slab Thick (cm)	Critical Perimeter	b_o (cm)	q_{cpu} (kg/cm ²)	q_{pu} (kg/cm ²)	Notes		
25			b (cm)	t (cm)								
26	1	82	50	90	20	Auto	348	16.32	15.94	Safe		
27	2	60	40	90	20	Auto	328	15.41	12.37	Safe		
28	3	60	30	60	25	Auto	268	16.32	11.70	Safe		
29	4	60	30	60	25	Auto	268	16.32	11.70	Safe		
30	5	60	30	60	25	Auto	268	16.32	11.70	Safe		
31	6	60	30	60	25	Auto	268	16.32	11.70	Safe		
32	7	60	30	60	25	Auto	268	16.32	11.70	Safe		
33	8	60	30	60	25	Auto	268	16.32	11.70	Safe		
34	9	60	30	60	25	Auto	268	16.32	11.70	Safe		
35												
36												
	◀ ▶ ...	Slab ana	Slabs	Flat slab	Punching	Punching-RFT	Beams	Beams-As`	M,N	Shear	Torsion	Rec

B28 v : X ✓ f_x 60

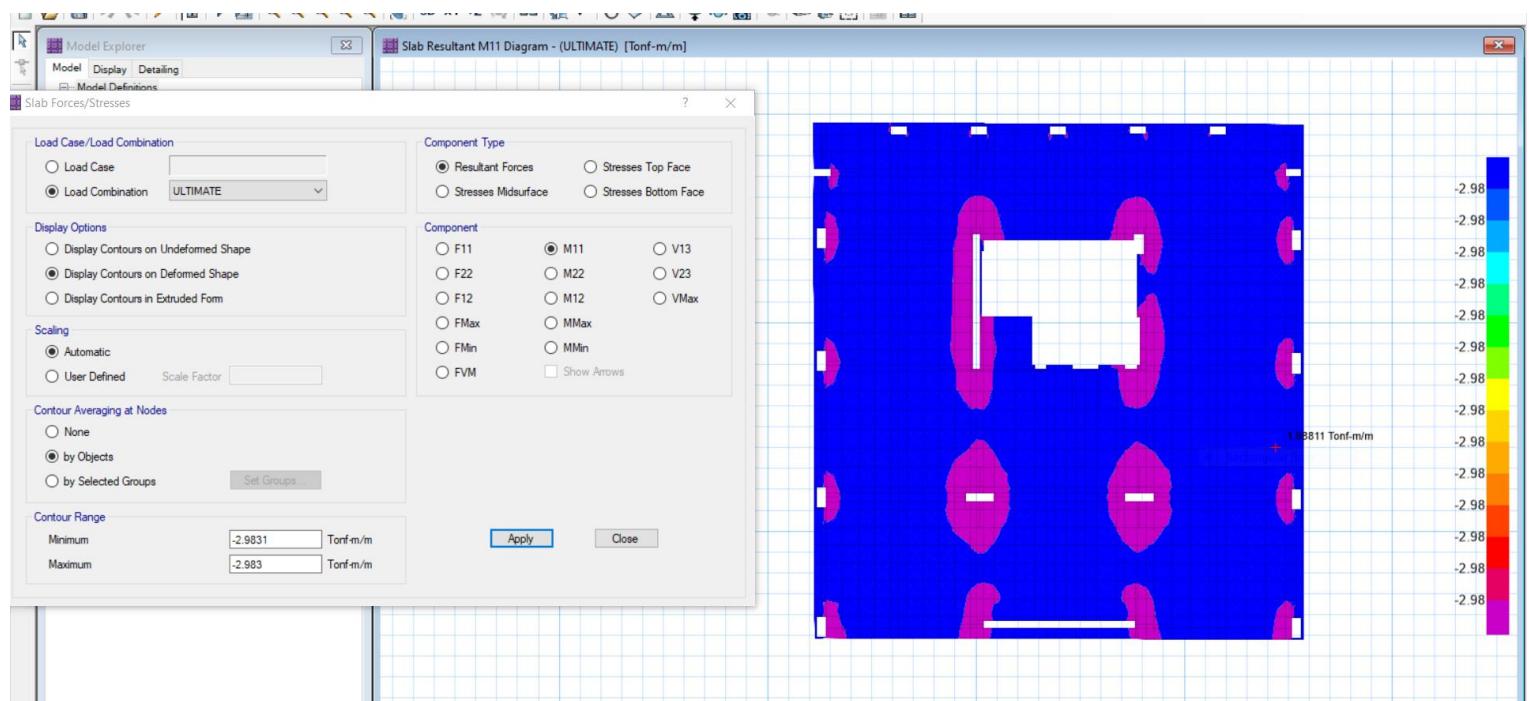
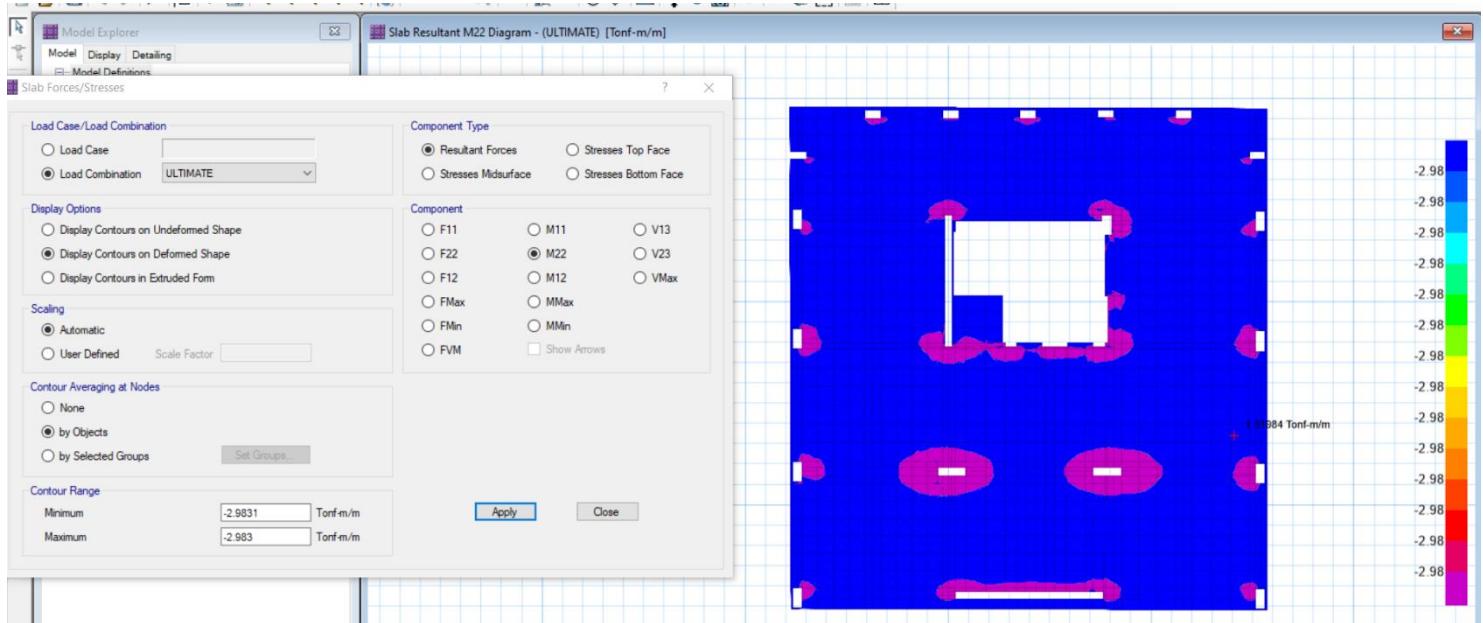
Edge columns:

A	B	C	D	E	F	G	H	I	J	V
53										
54										
55										
56										
57										
58										
59										
60										
61										
62										
63										
64	Col.	Ult. Load N_u (ton)	Col. Dims.		Slab Thick (cm)	Critical Perimeter	b_o (cm)	q_{cpu} (kg/cm ²)	q_{pu} (kg/cm ²)	Notes
65			b (cm)	t (cm)						
66	1	25	30	80	20	Auto	174	14.28	10.99	Safe
67	2	27.9	40	80	20	Auto	194	16.32	11.00	Safe
68	3	35	40	90	20	Auto	204	15.41	13.12	Safe
69	4	32	40	90	20	Auto	204	15.41	12.00	Safe

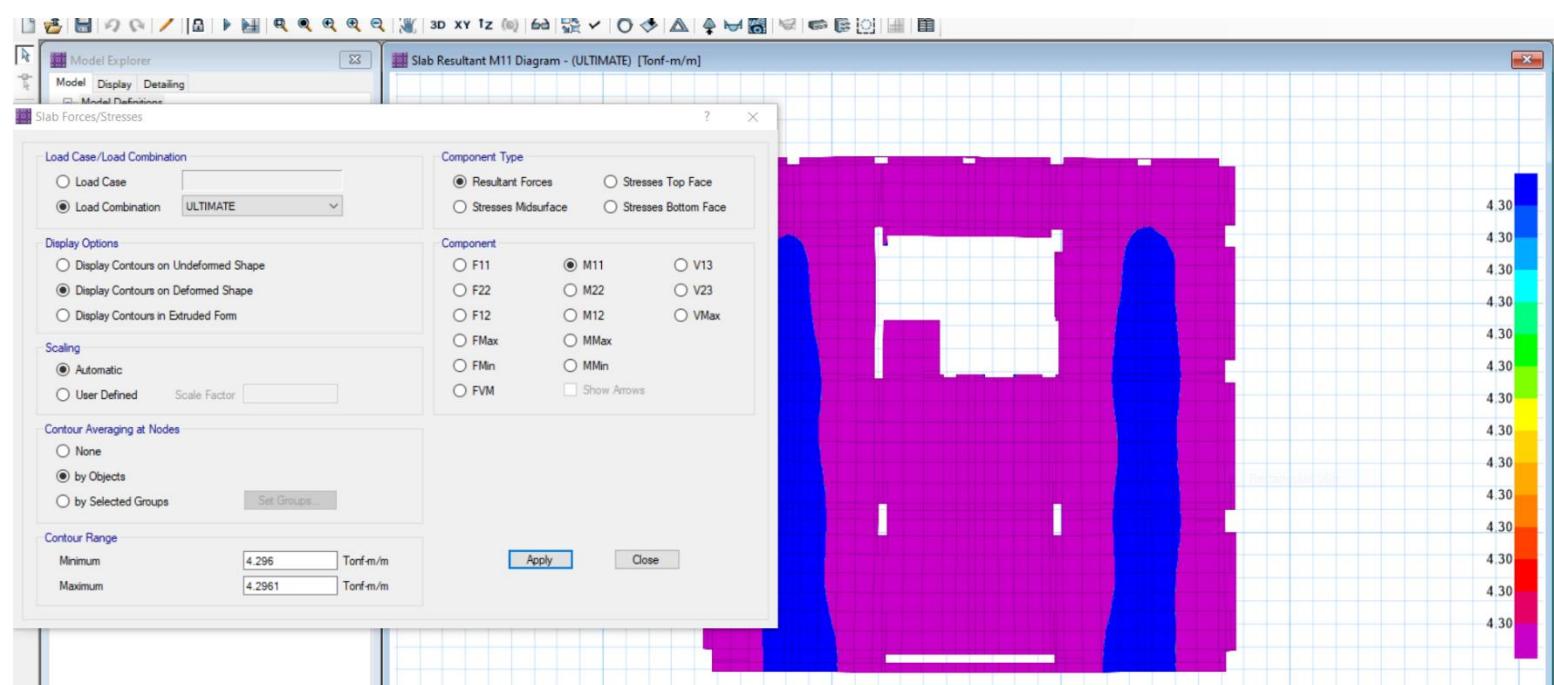
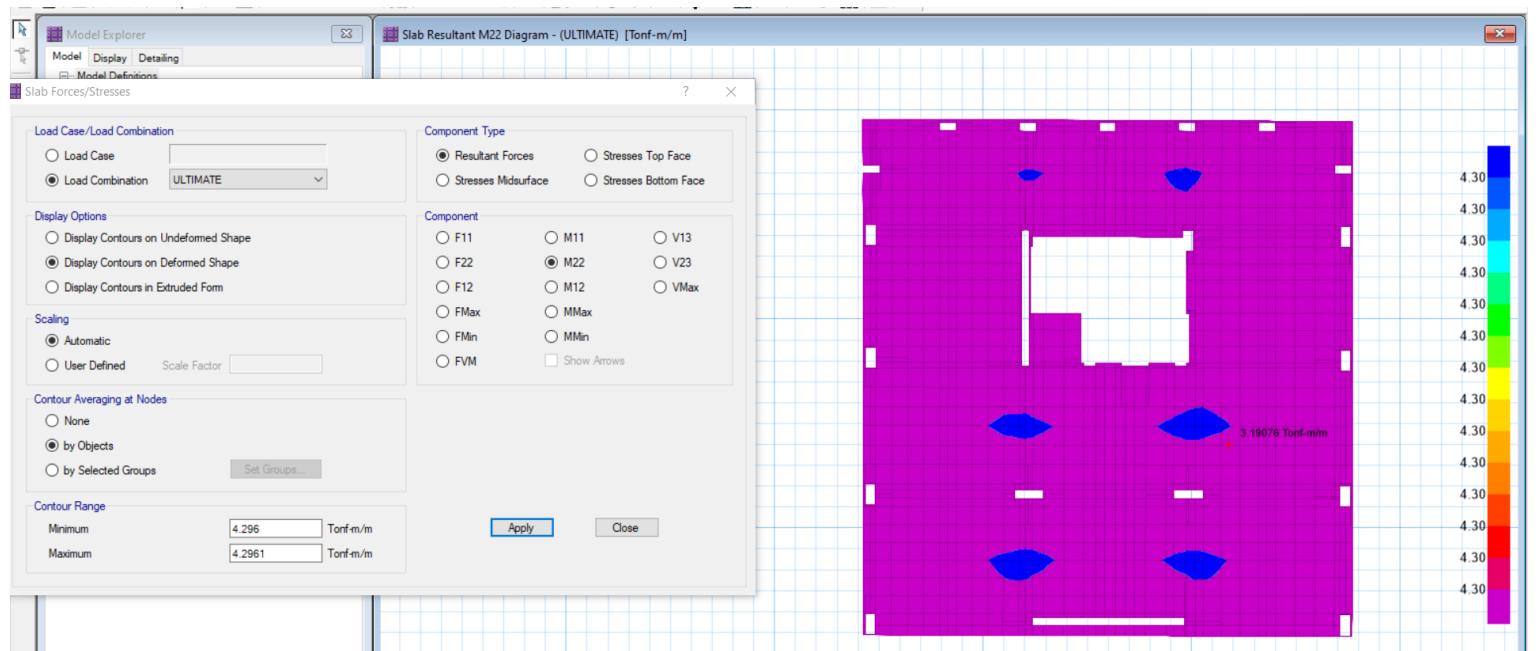
MODEL 3 :



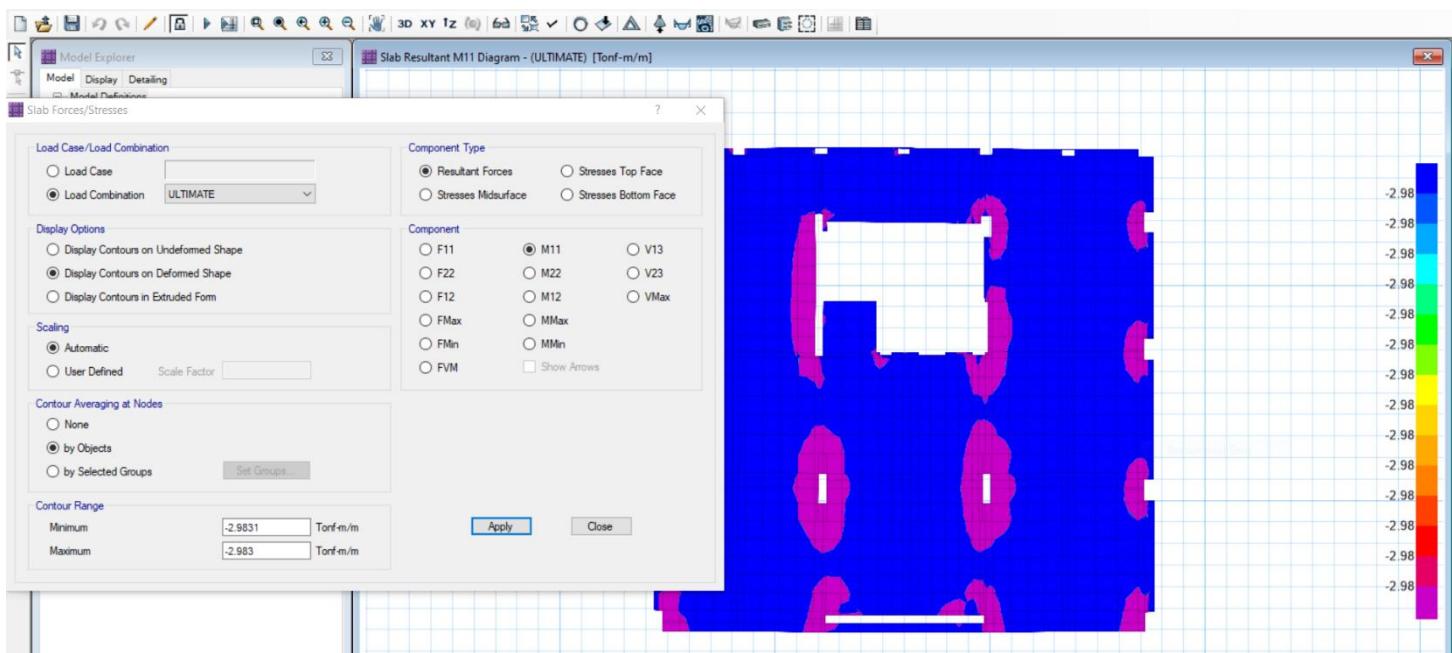
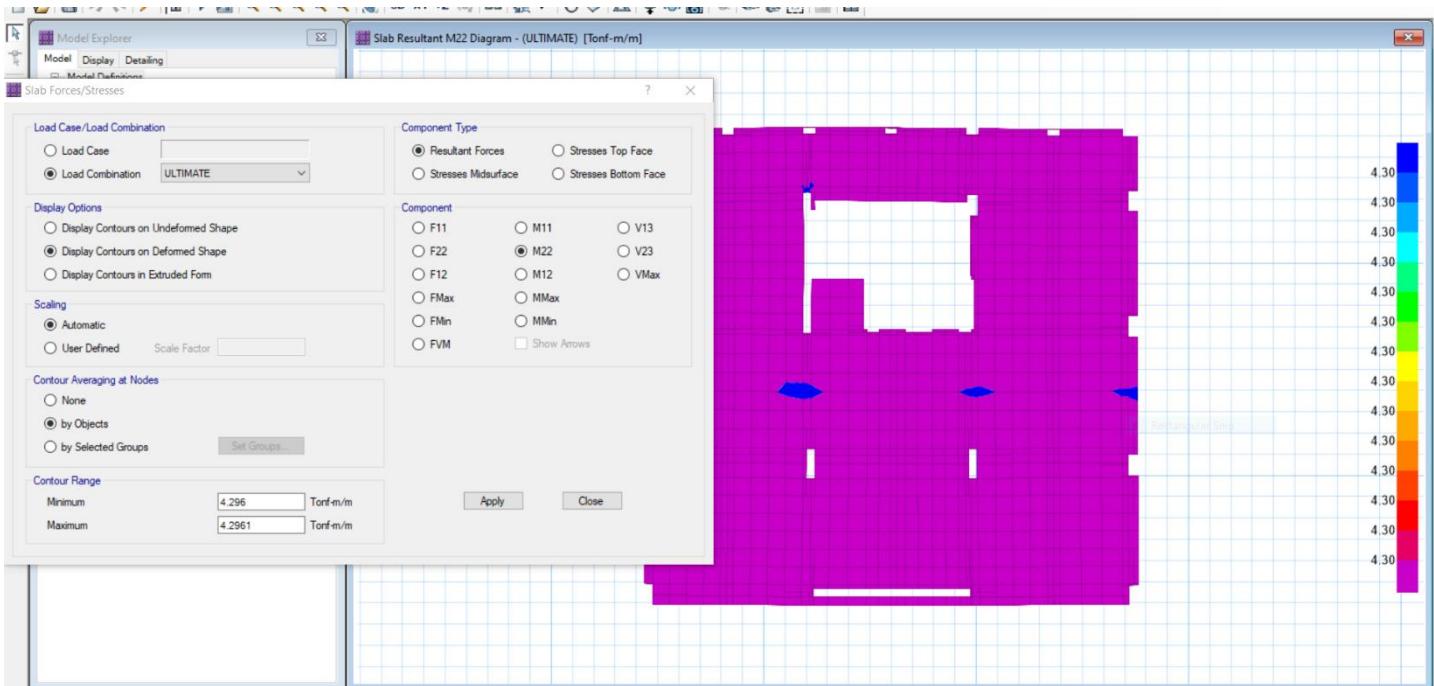
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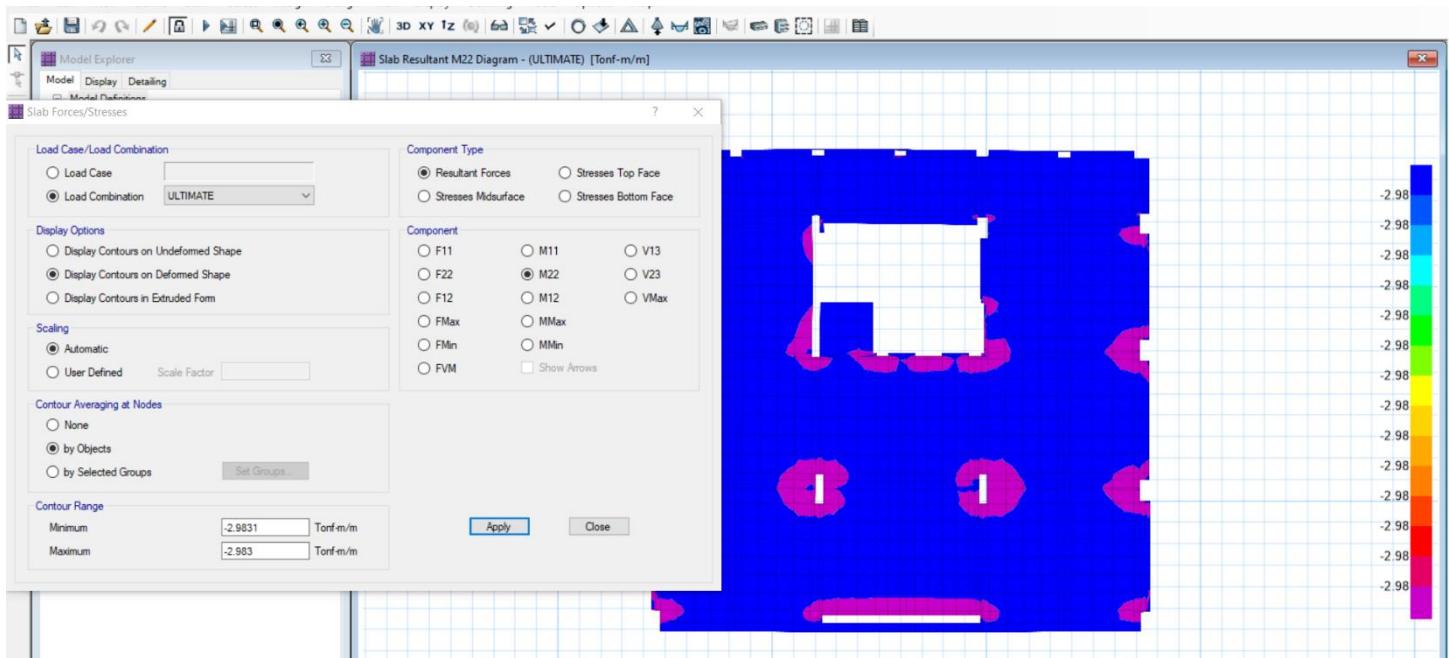
CALC SHEET
CONCRETE PROJECT
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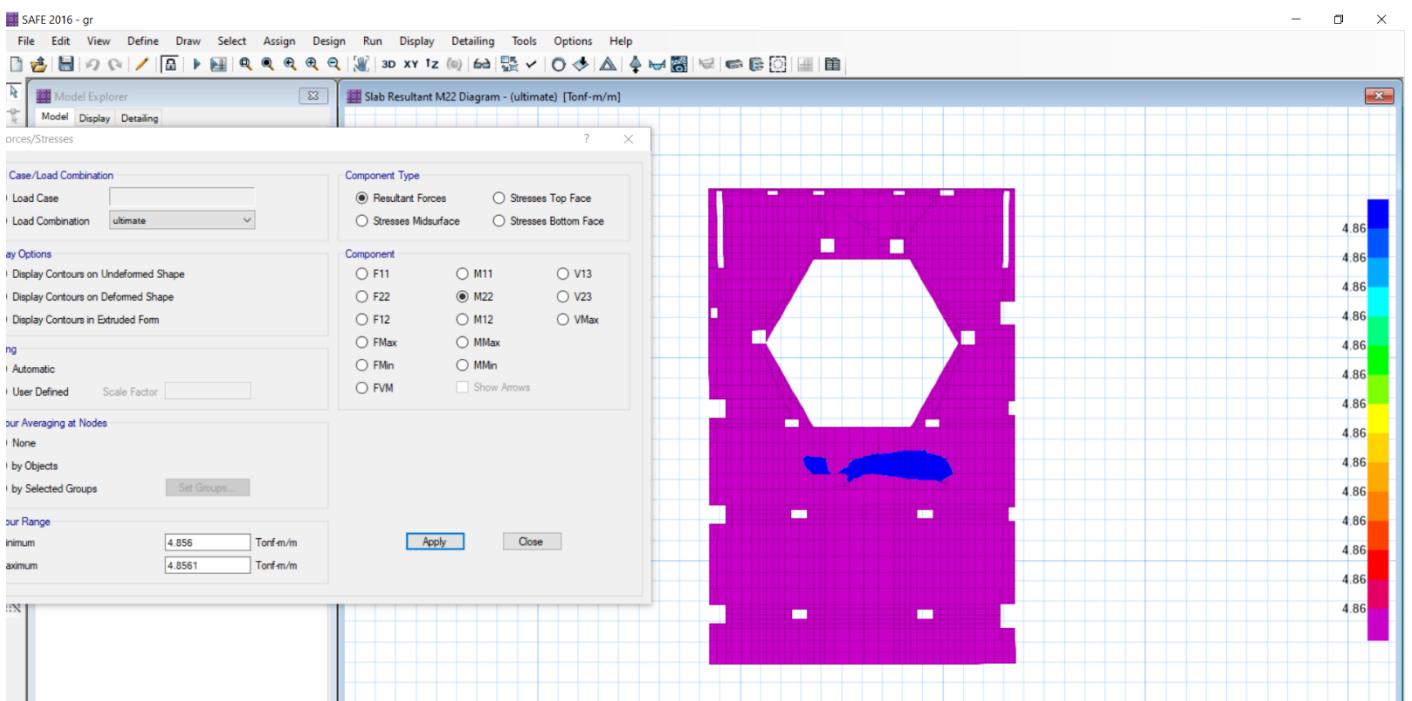
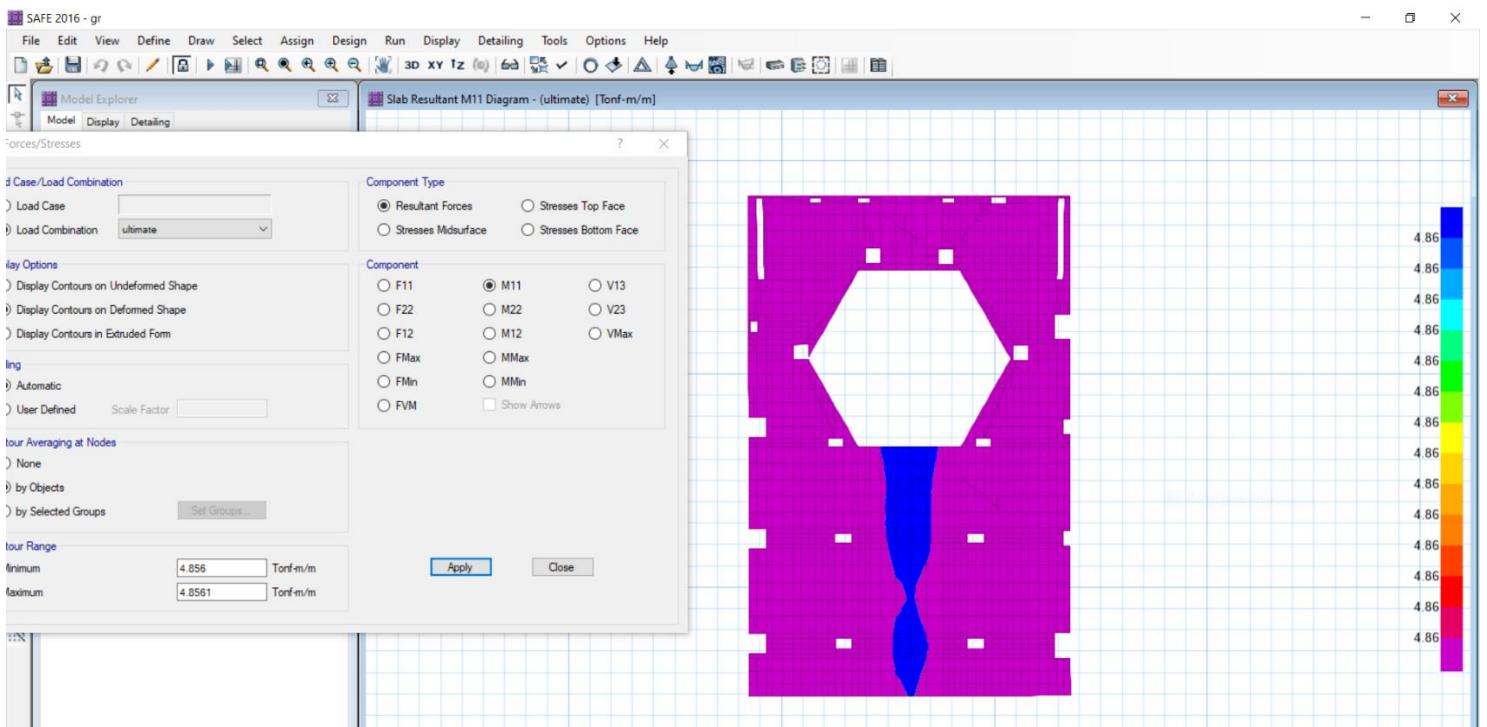
CALC SHEET
CONCRETE PROJECT
BUILDING 18



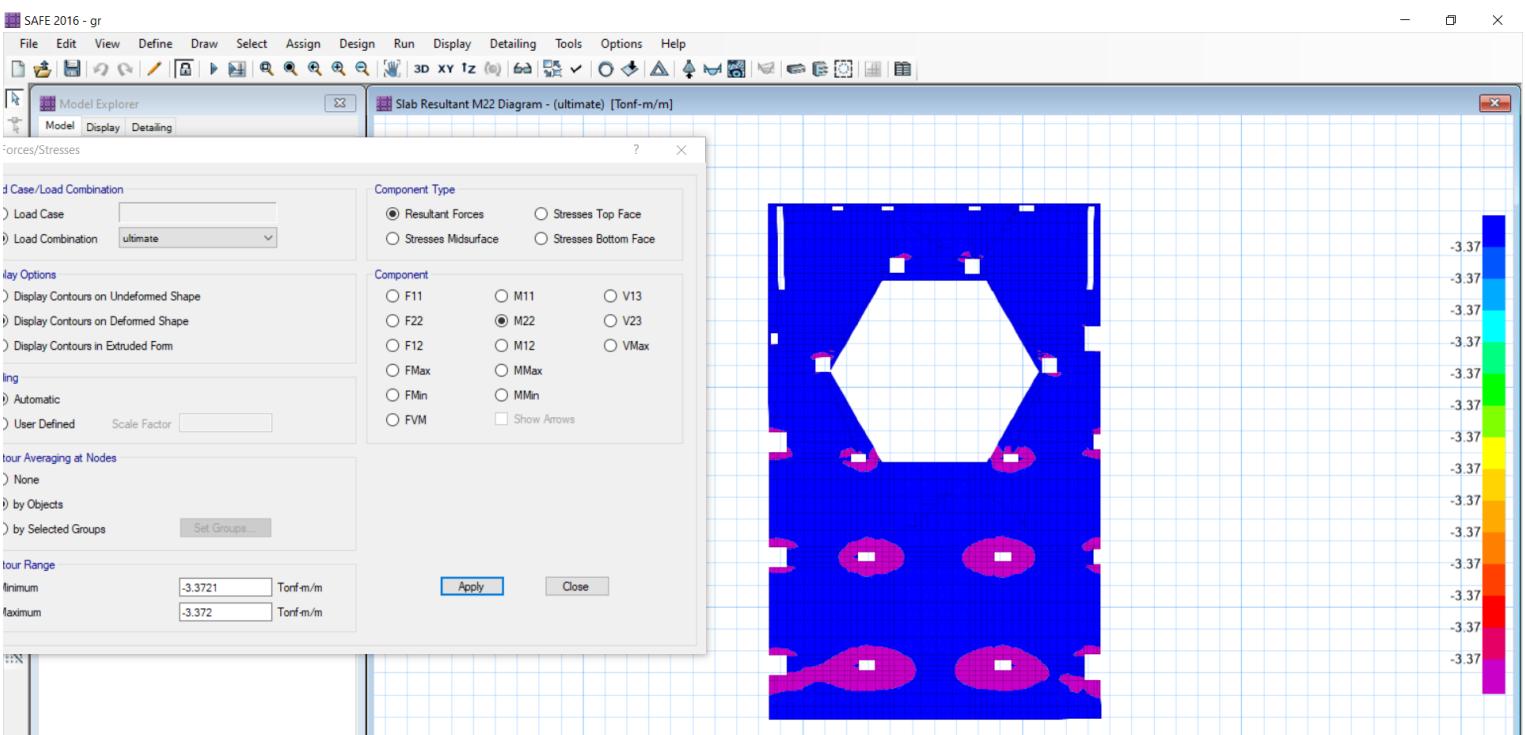
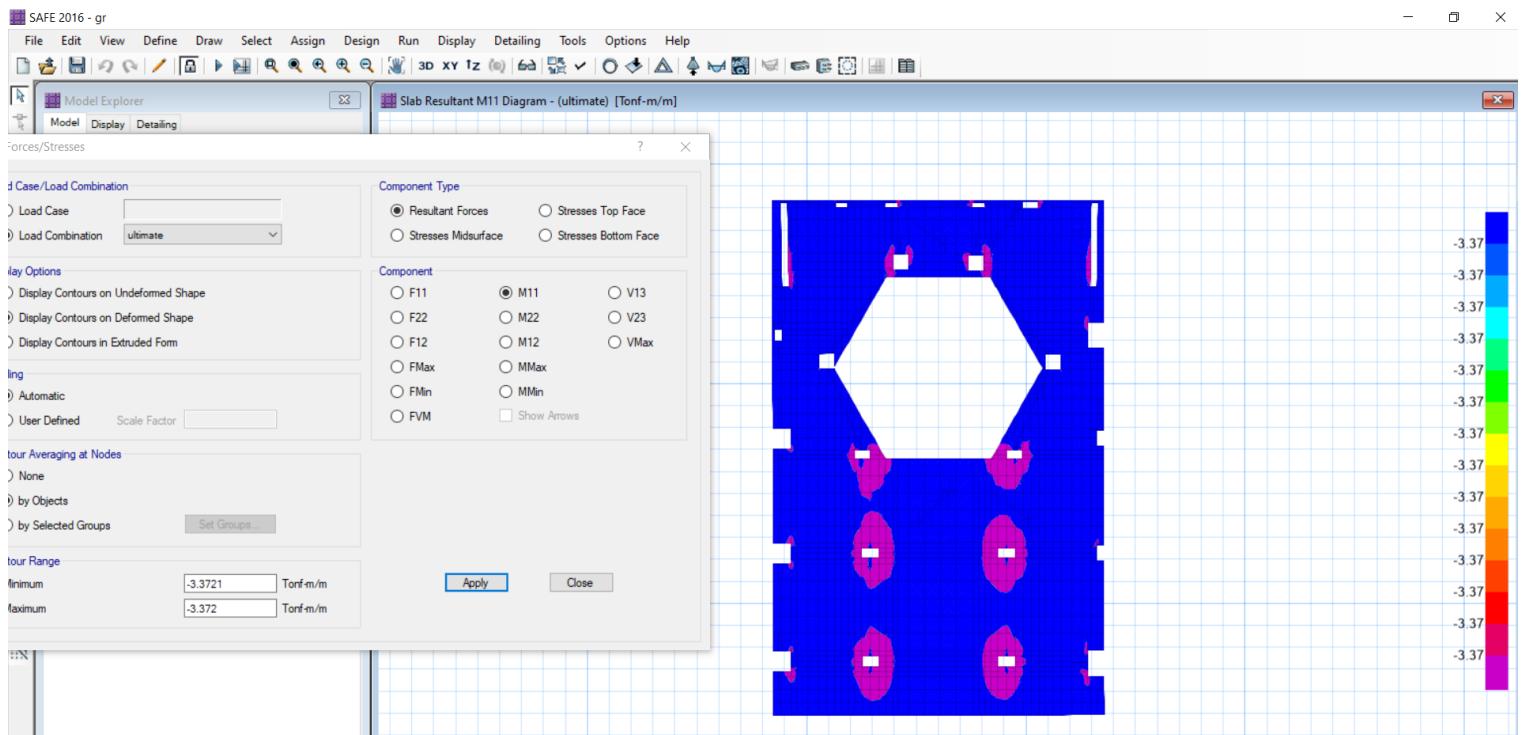
**CALC SHEET
CONCRETE PROJECT
BUILDING 18**



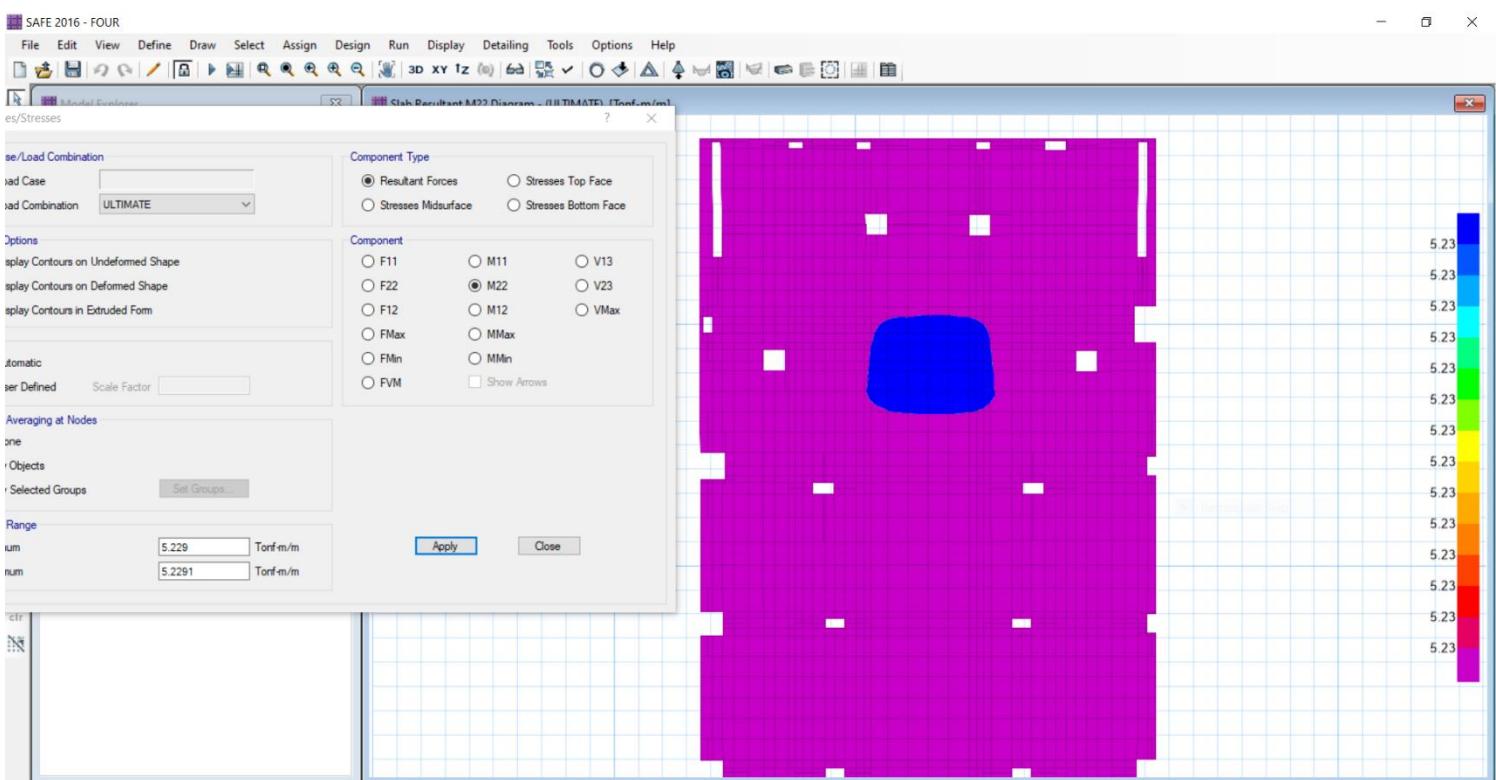
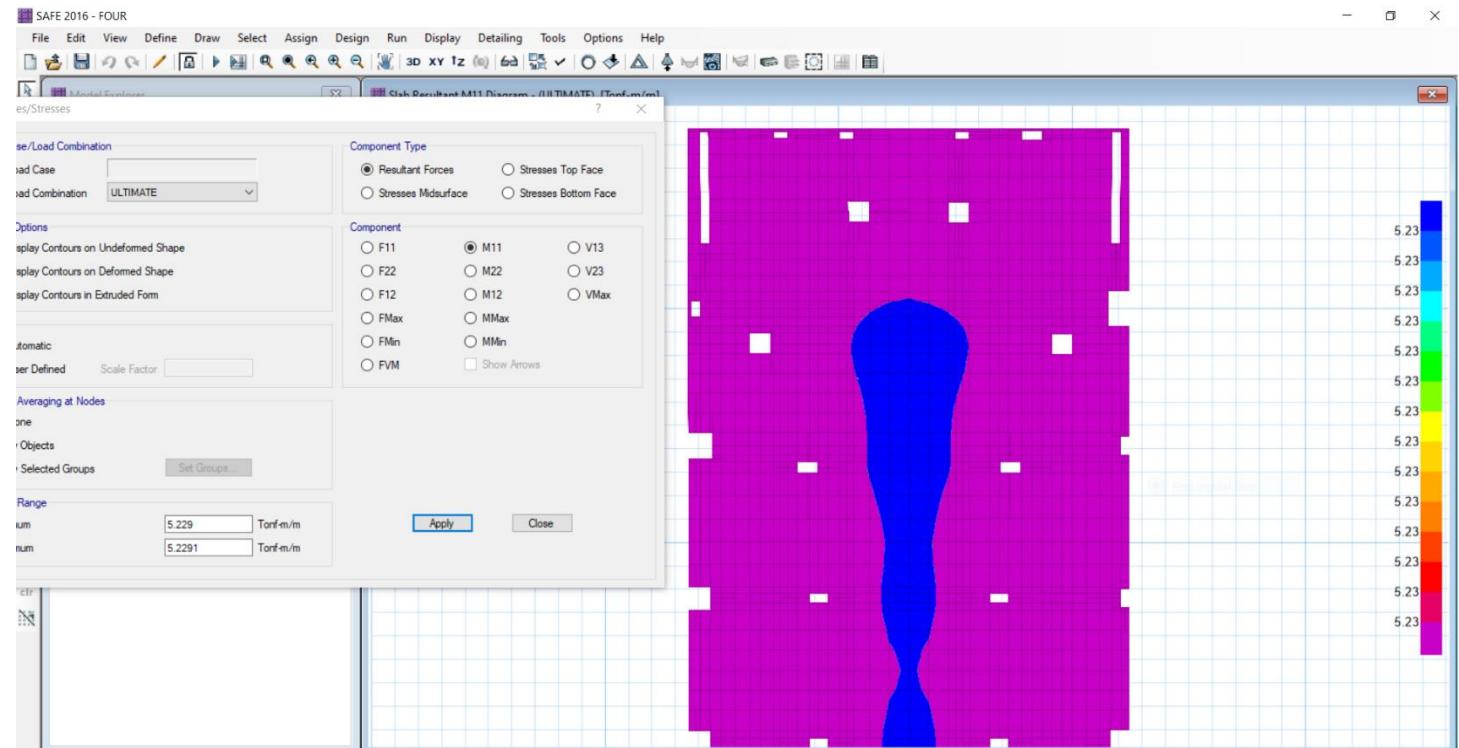
MODEL 4 :



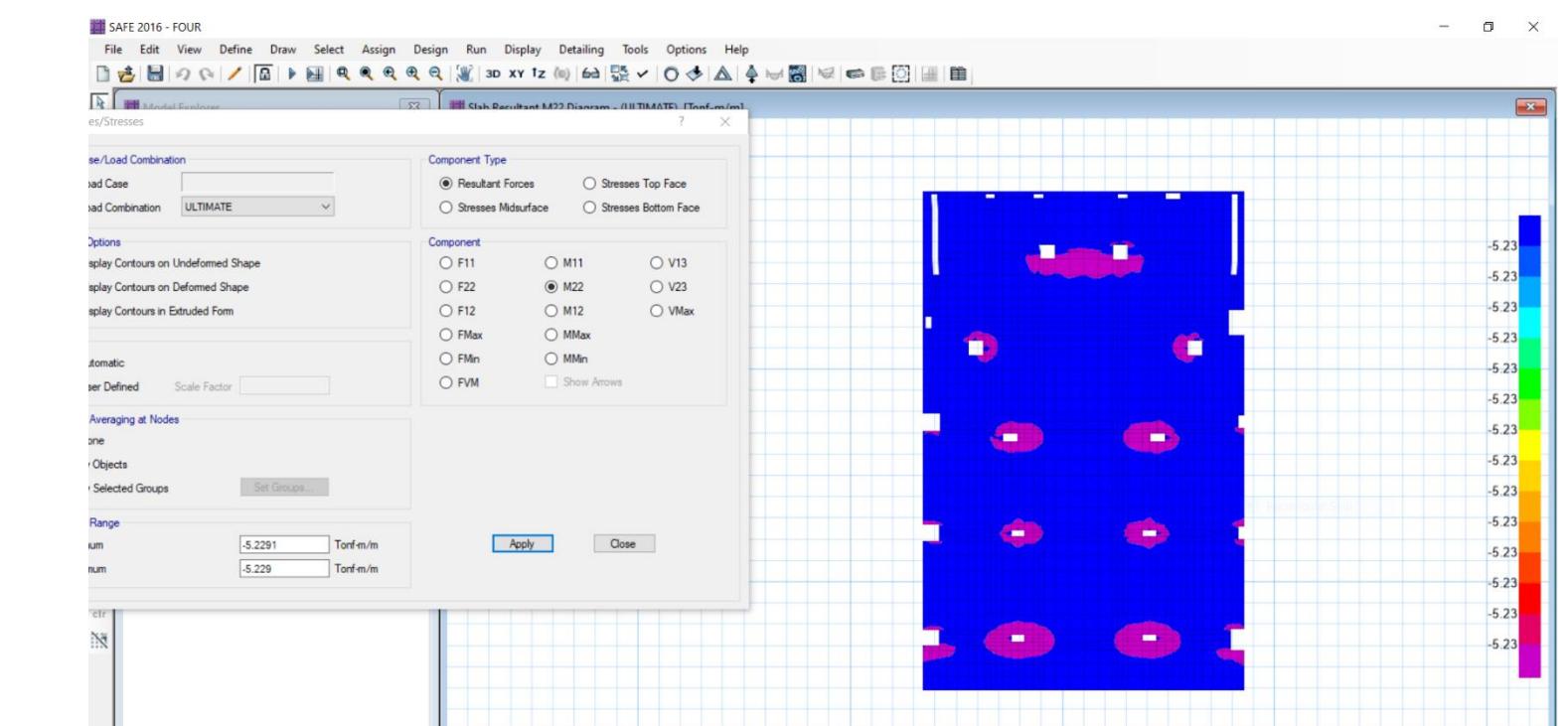
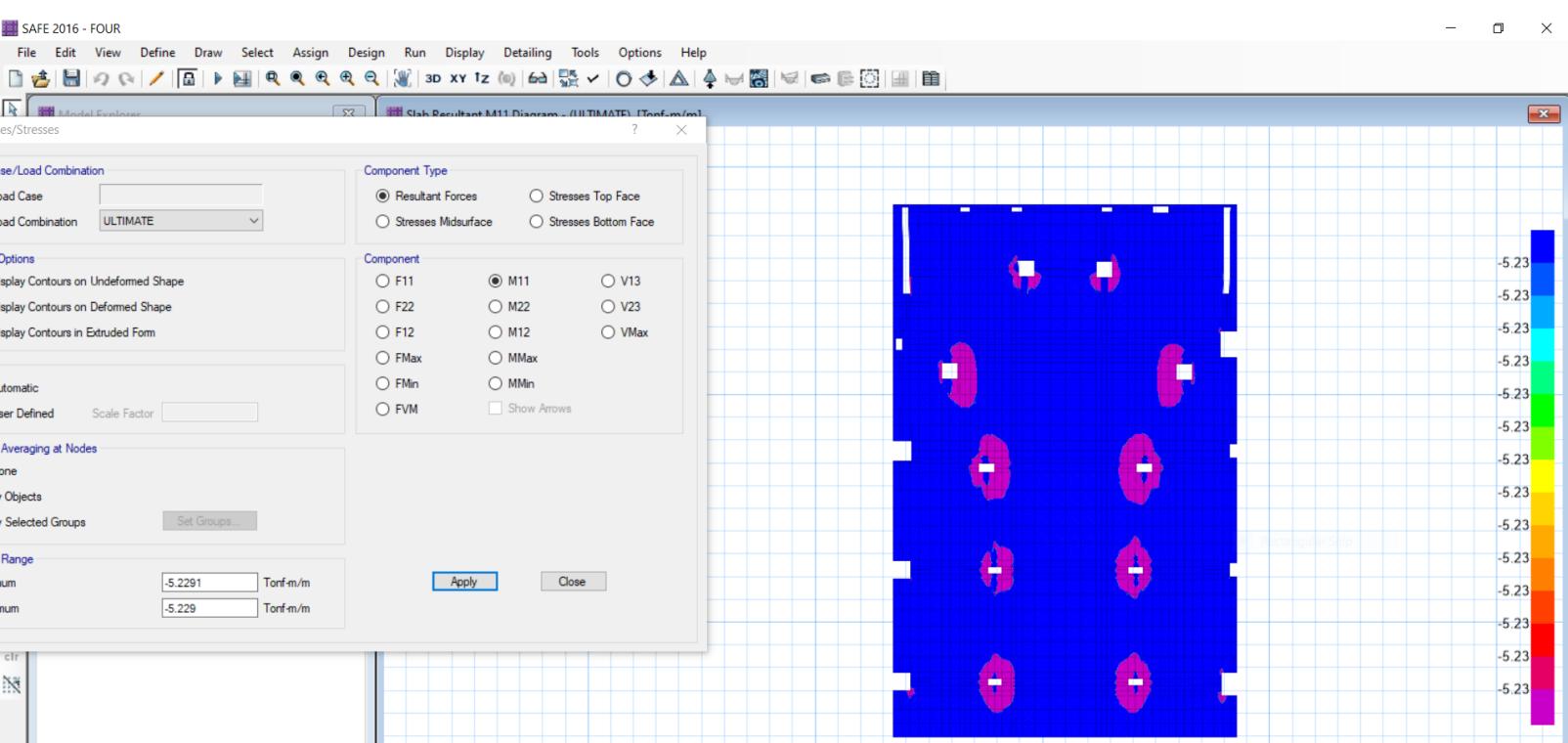
**CALC SHEET
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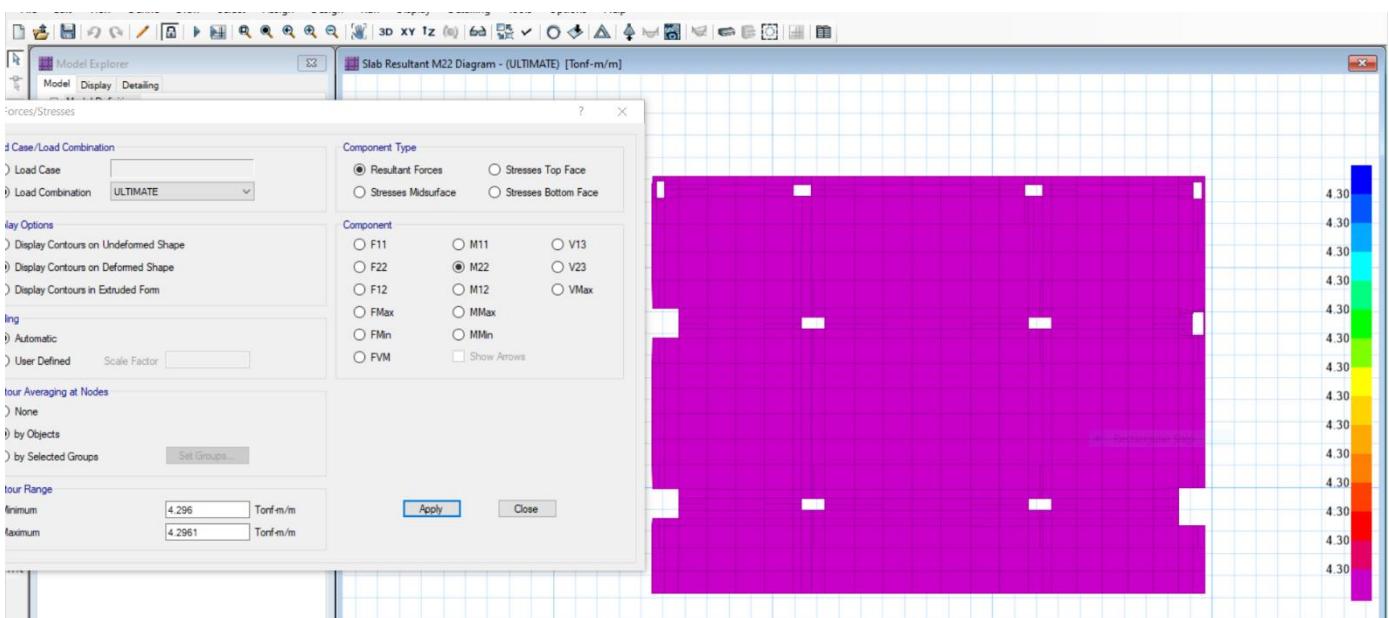
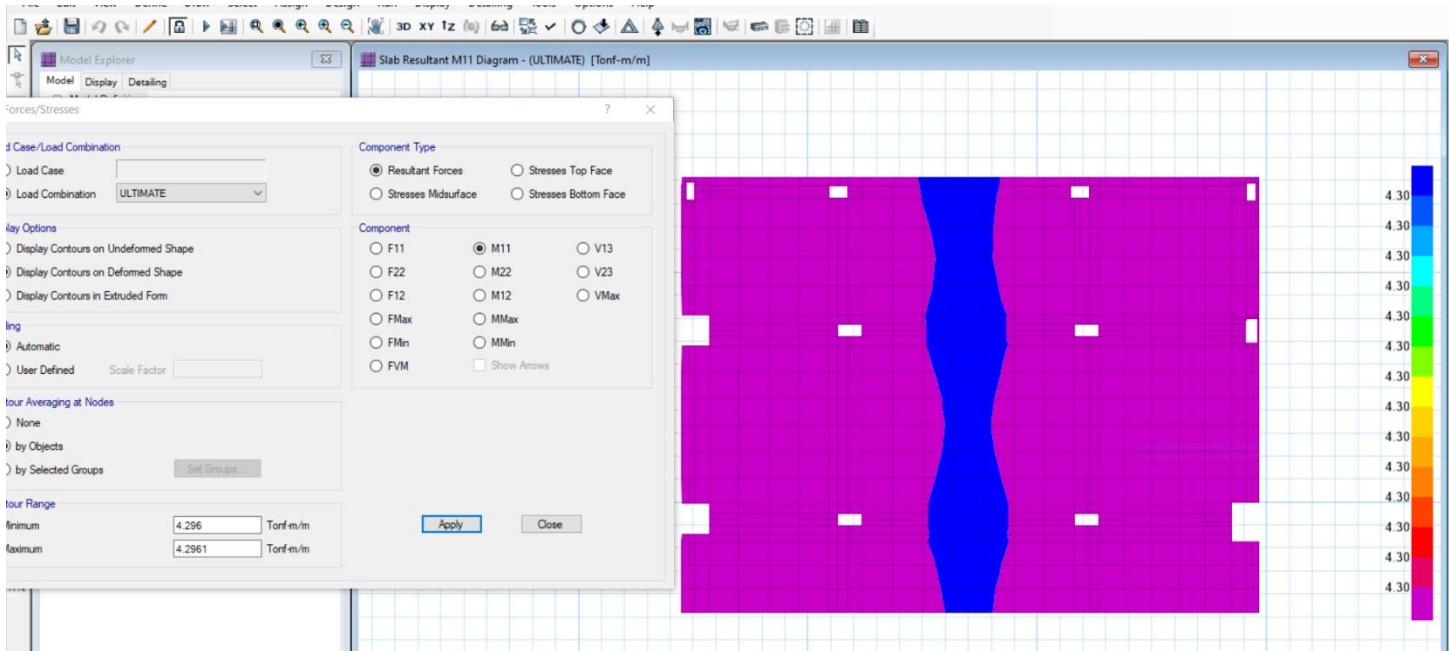
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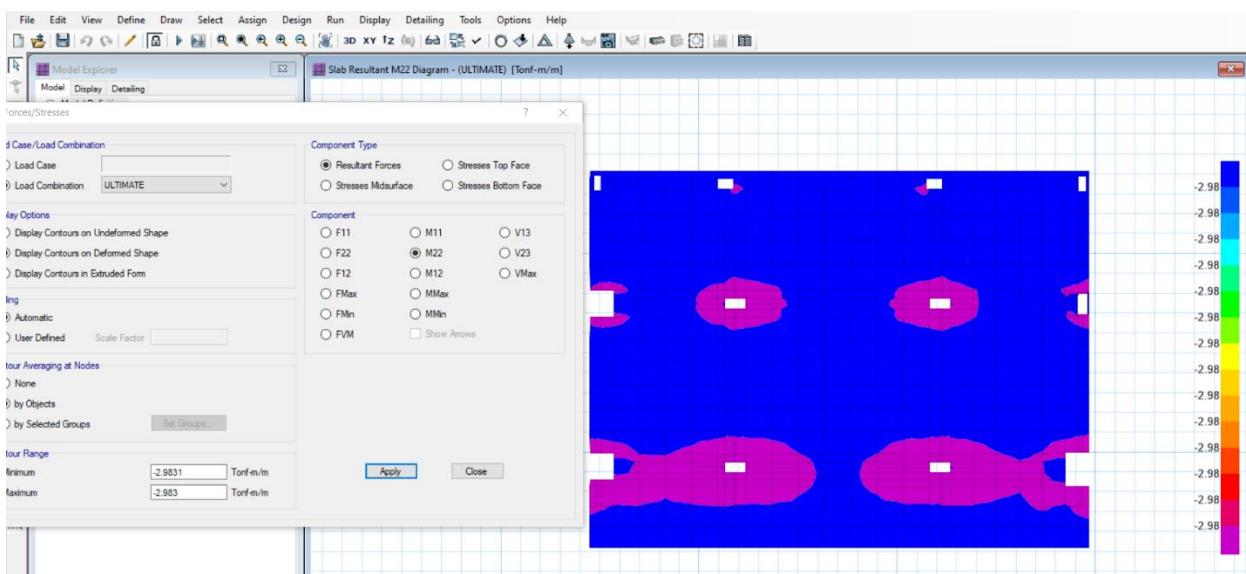
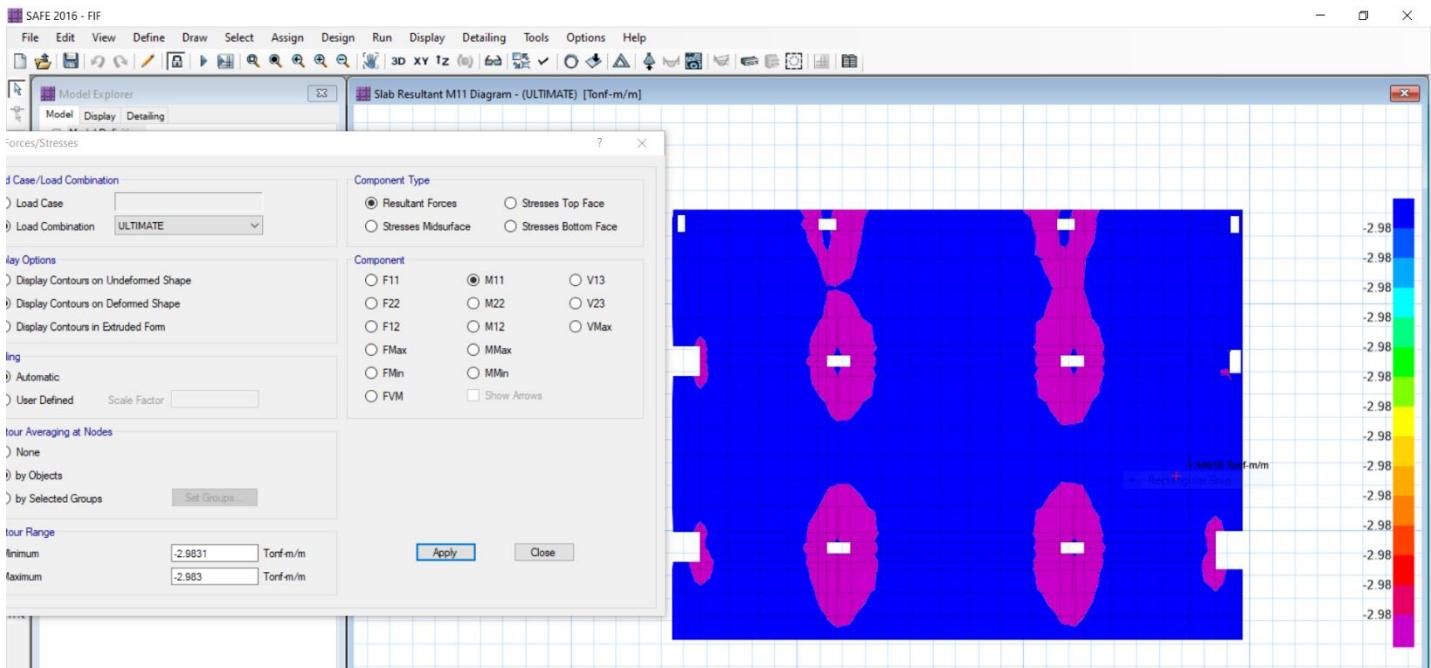
CALC SHEET
CONCRETE PROJECT
BUILDING 18



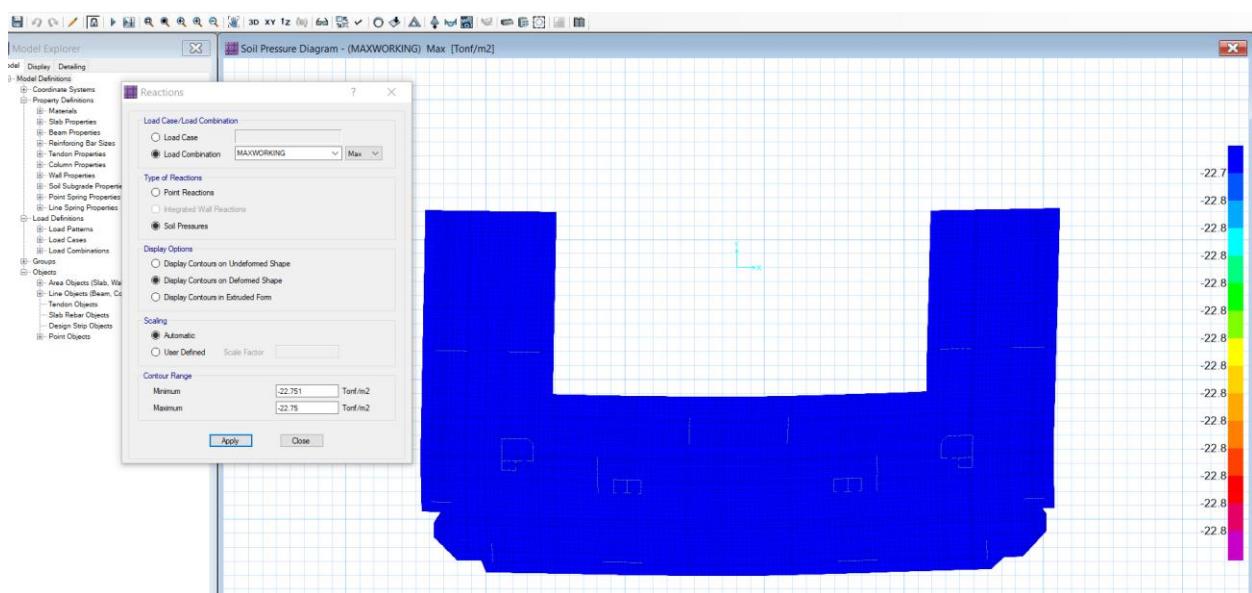
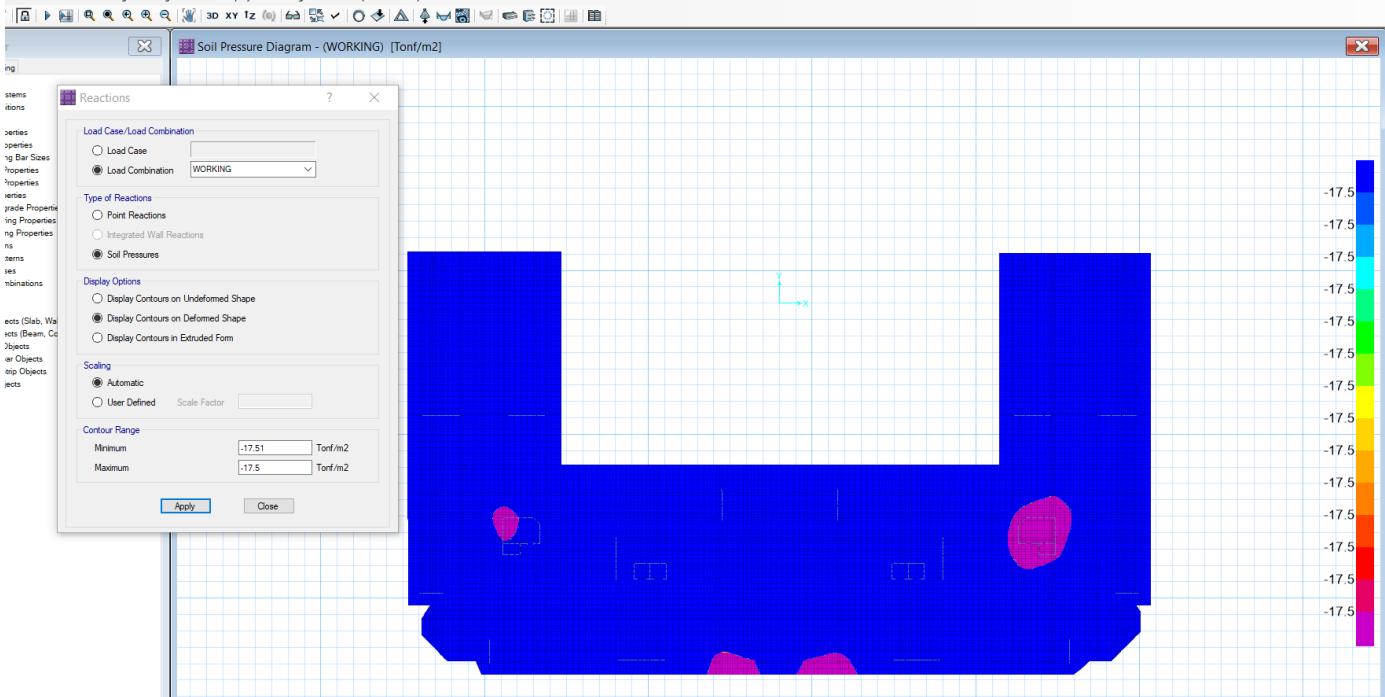
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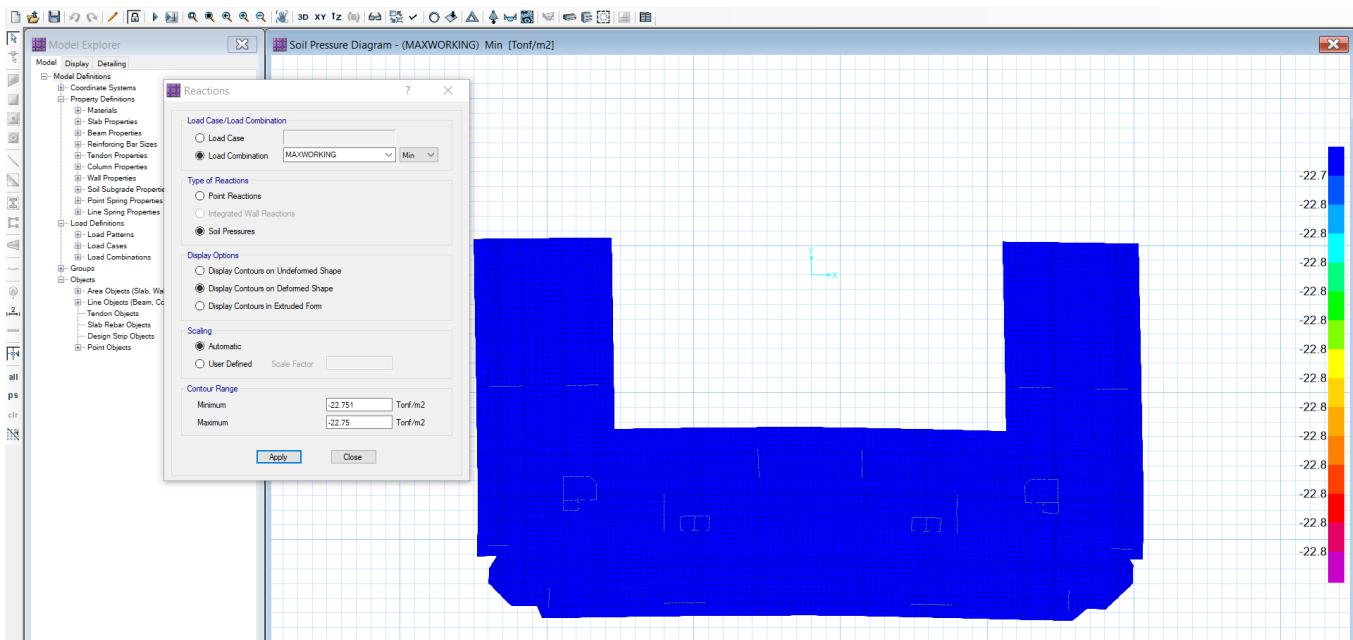
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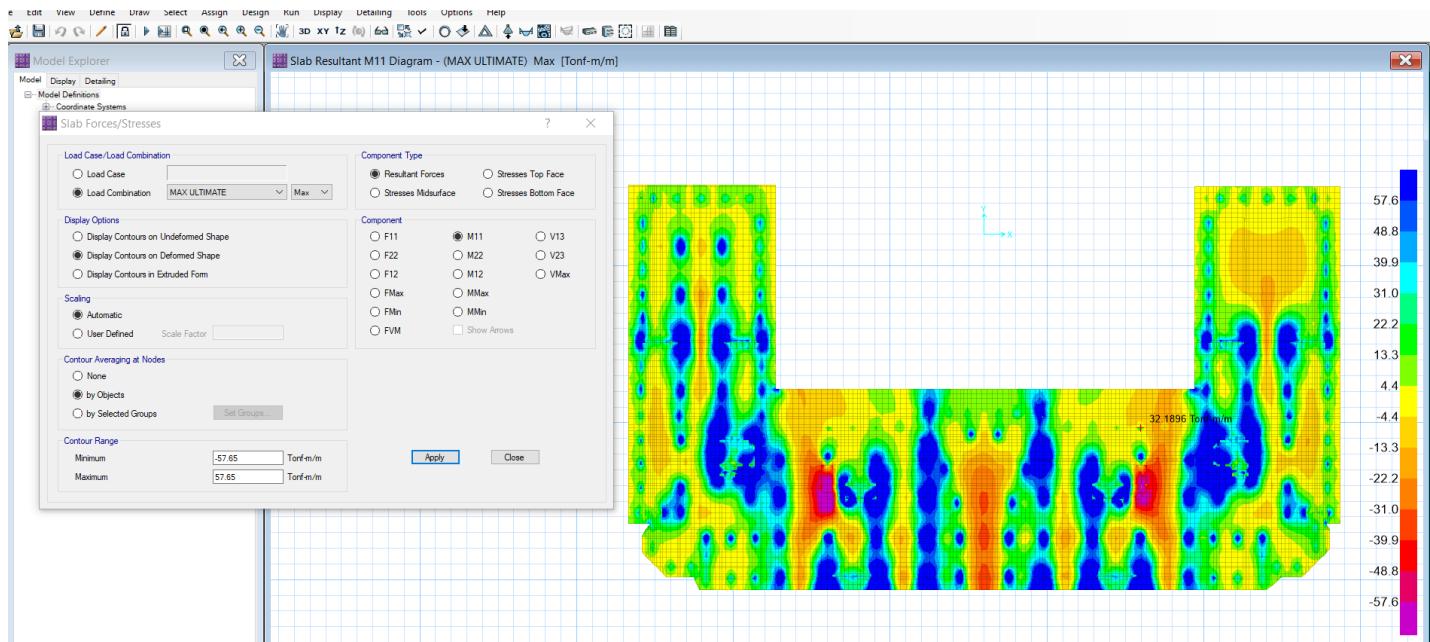
FOR RAFT



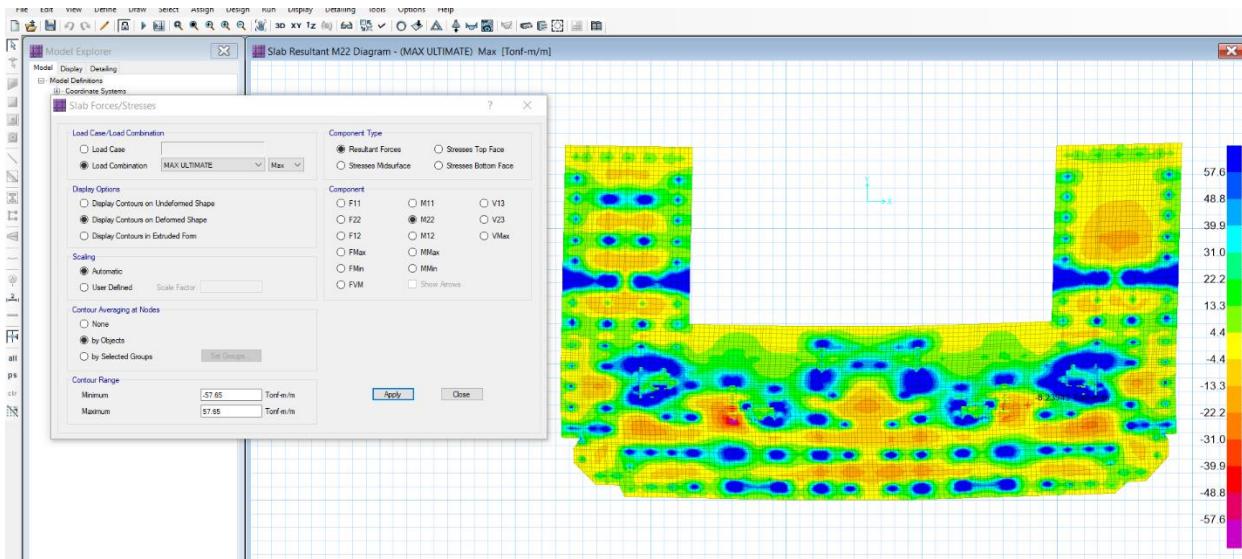
**CALC SHEET
CONCRETE PROJECT
BUILDING 18**



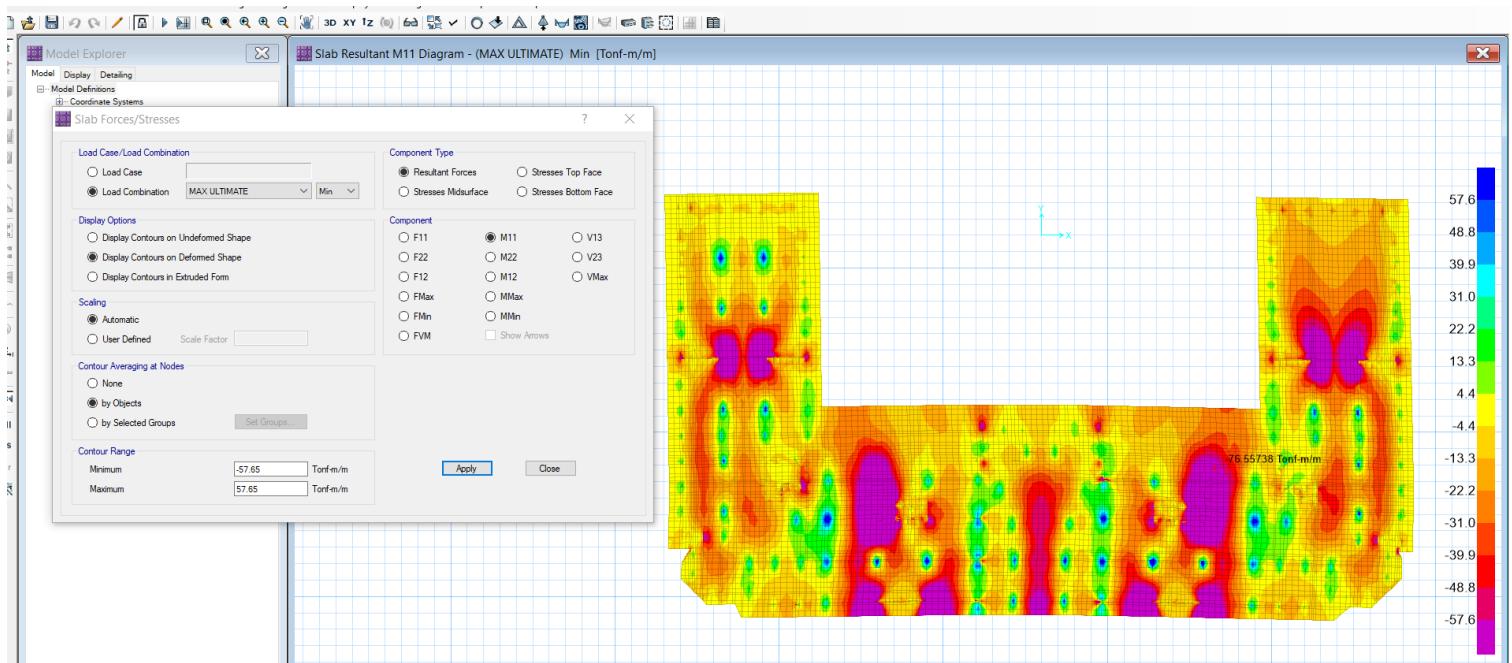
M11 BLUE BOTTOM



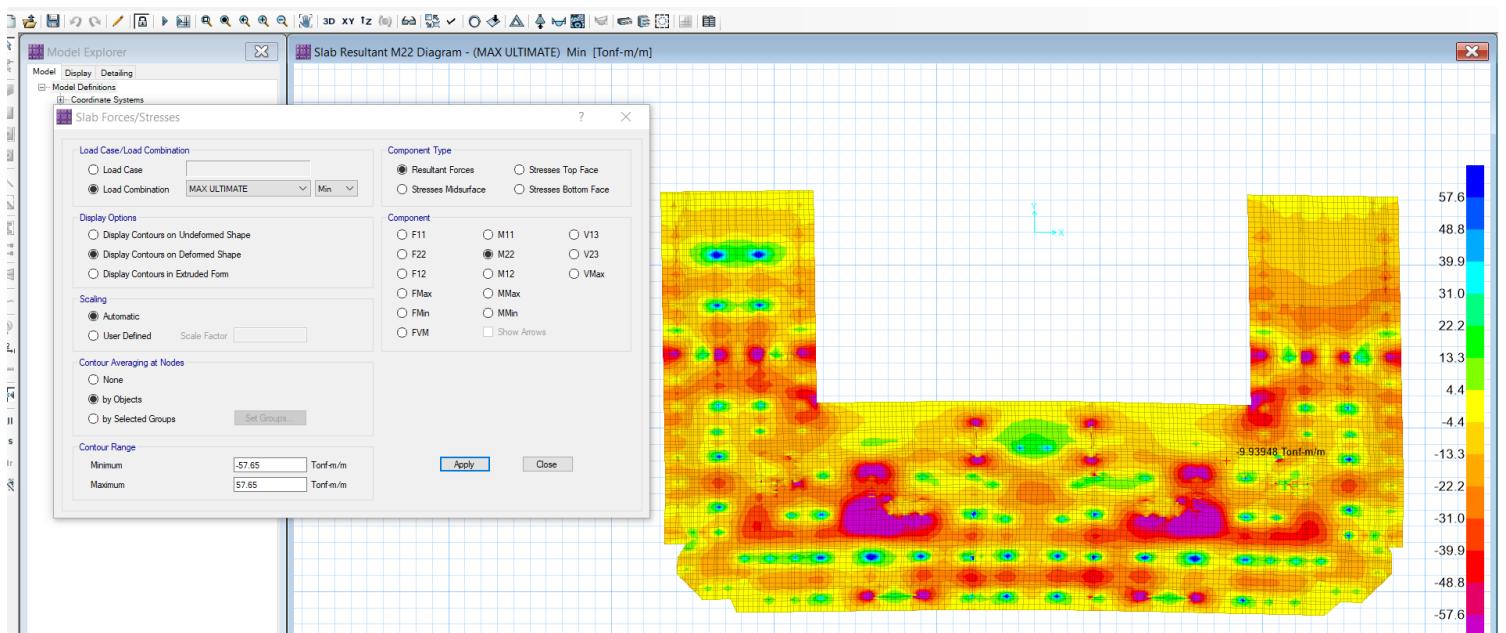
M22 BLUE BOTTOM



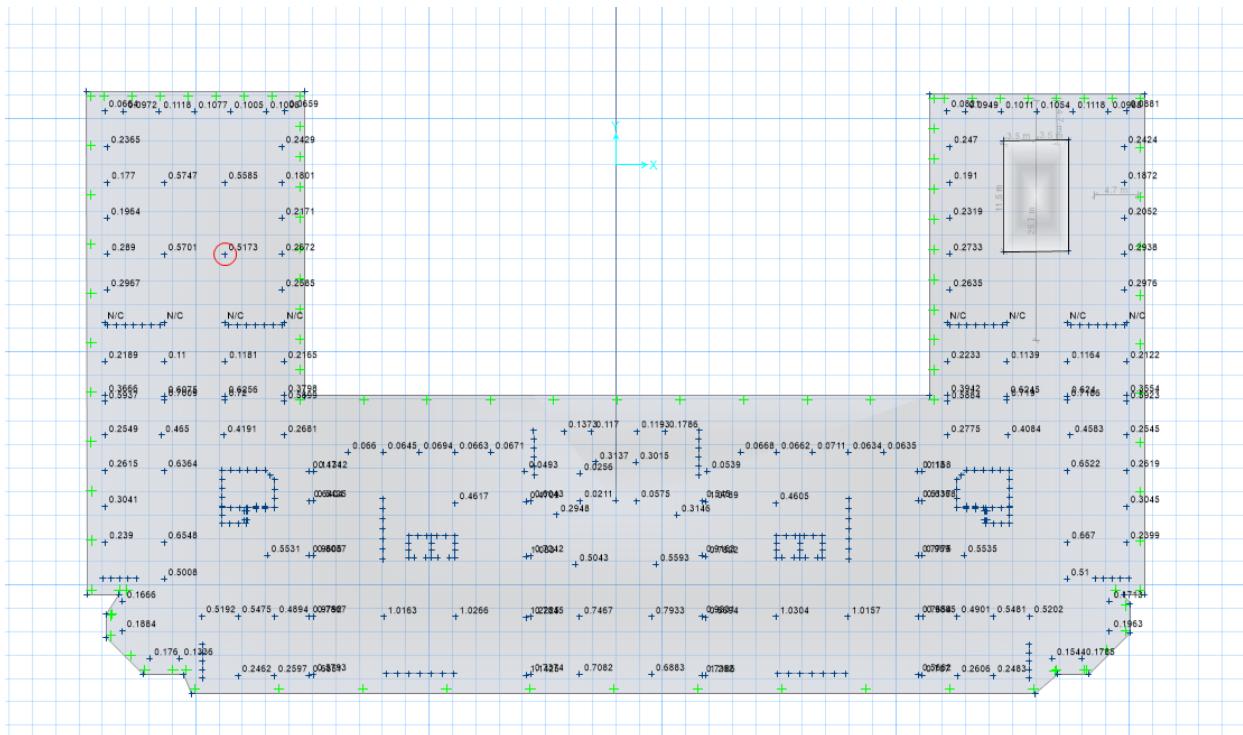
M11 PURPLE TOP



M22 PURPLE TOP



PUNCHING





CALC SHEET
CONCRETE PROJECT
BUILDING 18

$$R^2 = (3,6)^2 + (R-3)^2$$

$$R = 3,6 \text{ m}$$

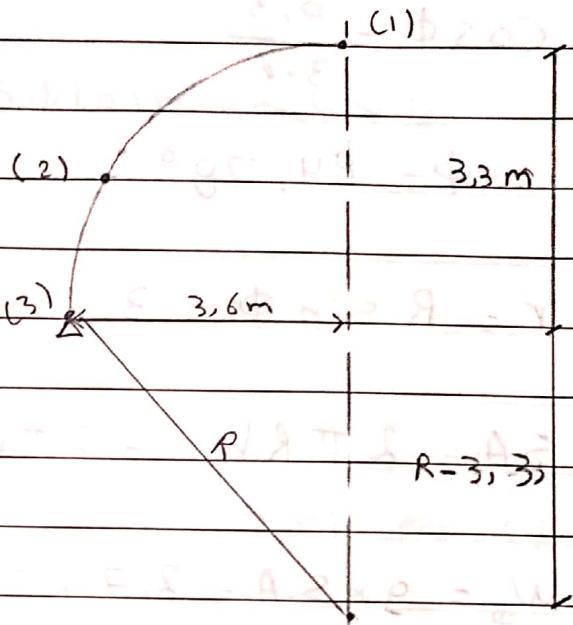
* For Sec (1)

$$\phi = 0^\circ$$

$$Z = g \cos \phi$$

$$g = t_s \gamma_c + F.c \\ = 0,1 * 25 + 0,2 = 2,7 \text{ KN/m}^2$$

$$\therefore Z = 2,7 \text{ KN/m}^2$$



* For Sec (2)

$$\cos \phi = \frac{1,95}{3,6} \quad \therefore \phi = 57,2^\circ$$

$$r = R \sin \phi$$

$$= 3,6 \sin 57,2$$

$$= 3,02 \text{ m}$$

$$SA = 2\pi R h$$

$$= 2\pi * 3,6 * 1,65 = 37,32 \text{ m}^2$$

$$W_\phi = g * S.A = 2,7 * 37,32 = 100,76 \text{ KN}$$

$$T_1 = \frac{100,76}{2\pi * 3,02 * \sin 57,2} = 6,3 \text{ KN/m} \quad \text{"comp"}$$

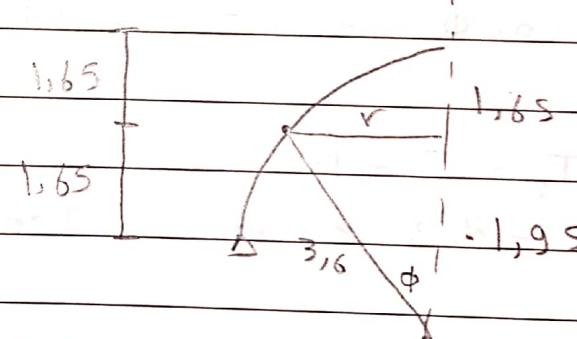
$$R_1 = R_2 = R = 3,6 \text{ m}$$

$$Z = g \cos \phi = 2,7 \cos 57,2 = 1,46$$

$$T_1 + T_2 = Z * R$$

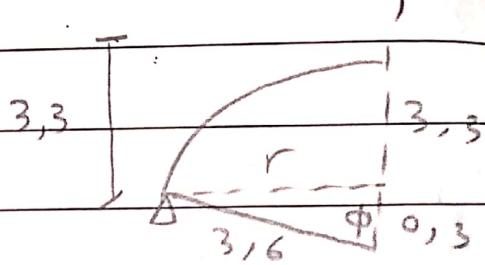
$$T_2 = -1,04$$

(1)



For Sec (3)

$$\cos \phi = \frac{0,3}{3,6}$$



$$\therefore \phi = 84,78^\circ$$

$$r = R \sin \phi = 3,6 \sin 84,78 = 3,5 \text{ m}$$

$$SA = 2\pi r h = 2\pi \cdot 3,6 \cdot 3,3 = 74,64 \text{ m}^2$$

$$W_\phi = g \cdot S.A = 2,7 \cdot 74,64 = 201,528$$

$$T_1 = \frac{201,528}{2\pi \cdot 3,5 \cdot \sin 84,78} = 9,2 \text{ kN/m} \quad \text{"comp"}$$

$$Z = g \cos \phi = 2,7 \cos 84,78 = 0,24 \text{ kN/m}^2$$

$$T_1 + T_2 = Z \cdot R$$

$$T_2 = -8,33 \text{ kN/m} \quad \text{"Tens"}$$

* FoR Design:

$$T_{max} = 9,2 \text{ kN/m} \quad \text{"comp"}$$

$$\text{Actual Stress} = \frac{T_{max}}{A_c} = \frac{9,2 \cdot 10^3}{1000 \cdot 100} = 0,092 \text{ N/mm}^2$$

$$\therefore F_{cu} = 35$$

$$\therefore F_{co} = 8 \text{ N/mm}^2$$

$$\text{Allowable Stress} = \frac{F_{co}}{2} = \frac{8}{2} = 4 > \text{Actual}$$

(2)

$\therefore t_s = 100 \text{ mm}$ is OK

$T_1 \rightarrow$ No tens \Rightarrow use $5 \phi 10 \text{ mm}^2$ each side.

$$T_2 \text{ "max Tens"} = 8,33 \text{ kN/m}$$

$$\therefore A_s = \frac{1,5 * 8,33 * 10^3}{400/1,15} = 35,9 \text{ mm}^2/\text{m}$$

$$\therefore \frac{35,9}{2} = 17,96 \text{ mm}^2/\text{m} \rightarrow \text{use min } 5 \phi 10 \text{ each side}$$

► Loads on Beam

$$\frac{V}{g,2} = \sin 84,78$$

$$V = 9,16 \text{ kN/m}$$

$$\frac{H}{g,2} = \cos 84,78$$

$$H = 0,83 \text{ kN/m}$$

$$L = \frac{2\pi r}{n} = \frac{2\pi * 3,6}{12} = 1,88 \text{ m}$$

$$t = \frac{L}{12} + 0,2 = \frac{1,88}{12} + 0,2 = 0,35 \text{ m}$$

\therefore Take B (250 * 400)

(3)

$$o.w_{(Beam)} = b \times t \times d_c$$

$$= 0,25 \times 0,40 \times 25 = 2,5 \text{ kN/m}$$

$$w = o.w + v = 2,5 + 9,16 = 11,66 \text{ kN/m}$$

$$\text{Normal Force} = H \times r = 0,83 \times 3,6 = 3 \text{ kN}$$

$$P = w \times 2\pi \times r$$

$$= 11,66 \times 2\pi \times 3,6$$

$$= 264 \text{ kN}$$

$$\therefore n = 12$$

$$\max M_{-ve} = \frac{w_1^2}{12} = \frac{11,66 \times (1,88)^2}{12} = 3,43 \text{ kNm}$$

$$\max M_{+ve} = \frac{w_1^2}{24} = \frac{11,66 \times (1,88)^2}{24} = 1,7 \text{ kNm}$$

$$\max Q = \frac{wl}{2} = \frac{11,66 \times 1,88}{2} = 11 \text{ kN}$$

(4)

design of B :-

"sec -v moment"

$$T - H \cdot r = 0,83 \cdot 3,6 = 3$$

$$M = 3,43 \cdot 1,5 = 5,145 \text{ kNm}$$

$$T = 1,5 \cdot 3 = 4,5 \text{ kN}$$

$$e = \frac{M}{T} = \frac{5,145}{4,5} = 1,14 > 0,5 \xrightarrow{\text{use } e_s}$$

$$e_s = e - \frac{t}{2} + c = 1,14 - \frac{0,4}{2} + 0,05 = 0,99 \approx 1$$

$$M_s = T \cdot e_s = 4,5 \text{ kN}$$

$$d = c_1 \sqrt{\frac{M_s}{f_{cu} b}}$$

$$350 = c_1 \sqrt{\frac{4,5 \cdot 10^6}{350 \cdot 250}} = 19 \quad J=0,826$$

$$A_s = \frac{4,5 \cdot 10^6}{0,826 \cdot 400 \cdot 350} + \frac{4,5 \cdot 10^3}{(400/115)}$$

$$= 51,85 \text{ mm}^2$$

check $(A_s)_{\min}$

$$M_{\min} b d = \left(0,225 + \frac{\sqrt{3s}}{400} \right) * 250 * 350 = 291 \text{ mm}^2$$

$$1,3 A_{s,\text{req}} = 1,3 * 51,85 = 67,405 \quad (5)$$

$$\frac{0,15}{100} \times 250 + 350 = 131,25$$

∴ use it $3\phi 12$

* For Sec of +ve moment $\rightarrow H - S \rightarrow I - T$

$$\text{use } A_s - A_s^{\min} = 3\phi 12$$

* check shear

$$q_{v_{cu \text{ un}}} = 0,16 \sqrt{\frac{f_{cu}}{\gamma_c}} = 0,16 \sqrt{\frac{35}{1,5}} = 0,77 \text{ N/mm}^2$$

$$q_{v_{cu \text{ cr}}} = 0,12 \sqrt{\frac{f_{cu}}{\gamma_c}} = 0,12 \sqrt{\frac{35}{1,5}} = 0,97 \text{ N/mm}^2$$

$$q_{v_{um \text{ un}}} = 0,7 \sqrt{\frac{f_{cu}}{\gamma_c}} = 0,7 \sqrt{\frac{35}{1,5}} = 3,38 \text{ N/mm}^2$$

Actual Shear

$$q_{v_u} = \frac{Q_{max}}{bd} = \frac{1,5 \times 11 \times 10^3}{250 \times 350} = 0,18 \text{ N/mm}^2$$

$$q_{v_u} < q_{v_{cu \text{ unc}}} \therefore \text{use } 5\phi 8$$

(6)

* Dome above Roof *

$$R^2 = (5)^2 + (R - 4,6)^2$$

$$R = 5 \text{ m}$$

* For sec (1)

$$\phi = \text{zero}$$

$$Z = g \cos \phi$$

$$g = t_s \gamma_c + f.c$$

$$= 0,1 * 25 + 0,2 = 2,7 \text{ kN/m}^2$$

$$Z = g \cos \phi = 2,7 \text{ kN/m}^2$$

* For sec (2)

$$\cos \phi = \frac{2,7}{5} \quad \therefore \phi = 57,31^\circ$$

$$r = R \sin \phi$$

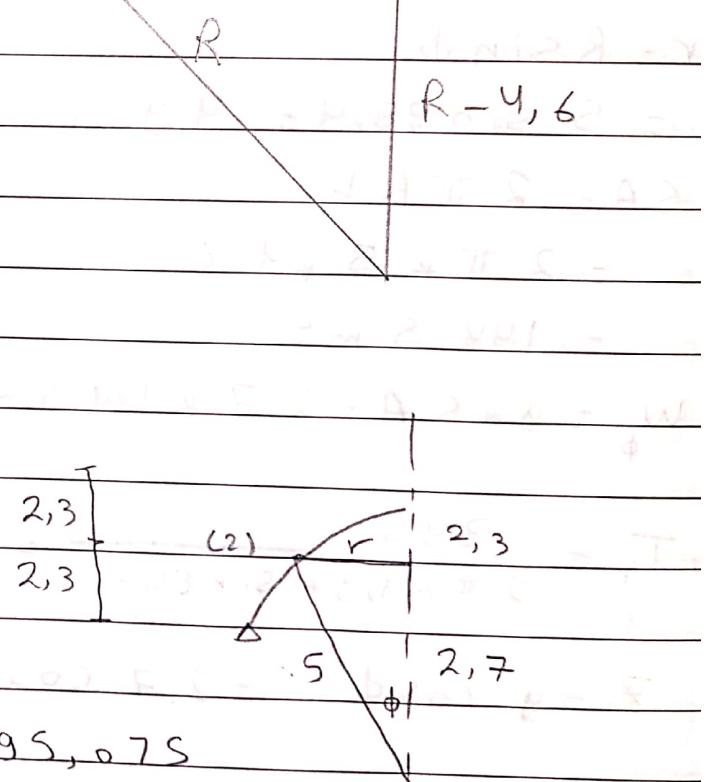
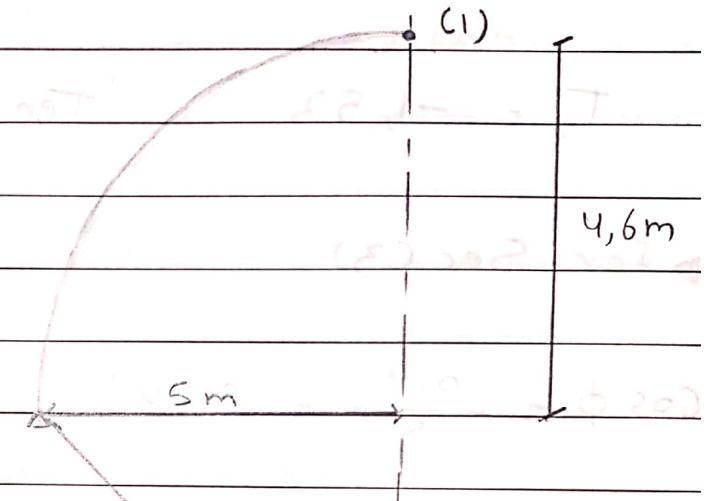
$$= 5 \sin 57,31 = 4,2 \text{ m}$$

$$S.A = 2\pi R h$$

$$= 2\pi * 5 * 2,3$$

$$= 72,25 \text{ m}^2$$

$$W_\phi = g * S.A = 2,7 * 72,25 = 195,075$$



$$\therefore T_1 = \frac{195,075}{2\pi * 4,2 * \sin 57,31} = 8,78 \quad \text{"comp"}$$

$$R_1 = R_2 = R = 5 \text{ m}$$

$$Z = g \cos \phi = 2,7 \cos 57,31 = 1,45$$

(1) (5)

$$T_1 + T_2 = Z * R$$

$$8,78 + T_2 = 1,45 * 5$$

$$T_2 = -1,53 \quad \text{"Tens"}$$

► For Sec (3)

$$\cos \phi = \frac{0,4}{5} = 85,4^\circ$$

$$r = R \sin \phi$$

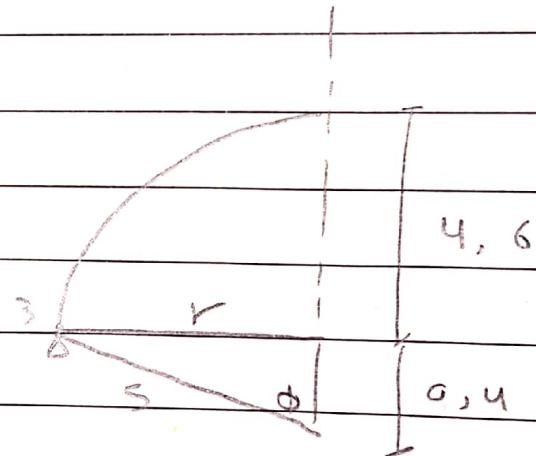
$$= 5 \sin 85,4 = 4,9$$

$$SA = 2\pi R h$$

$$= 2\pi * 5 * 4,6$$

$$= 144,5 \text{ m}^2$$

$$W_\phi = g * S.A = 2,7 * 144,5 = 390 \text{ N}$$



$$T_1 = \frac{390}{2\pi * 4,9 * \sin 85,4} = 12,7 \quad \text{"comp"}$$

$$Z = g \cos \phi = 2,7 \cos 85,4^\circ = 0,216 \text{ kN/m}^2$$

$$T_1 + T_2 = Z * R$$

$$T_2 = -11,62 \text{ kN/m}^2 \quad \text{"Tens"}$$

(2)

* For Design

$$T_{max} = 12,7 \text{ "comp"}$$

$$\text{Actual Stress} = \frac{T_{max}}{A_c} = \frac{12,7 \times 10^3}{1000 \times 100} = 0,127 \text{ N/mm}^2$$

$$F_{c0} = 35$$

$$F_{c0} = 8 \text{ N/mm}^2$$

$$\text{Allowable stresses : } \frac{F_{c0}}{2} = \frac{8}{2} = 4 > \text{Actual stress}$$

\therefore Safe for $t_s = 100 \text{ mm}$

$T_1 \rightarrow$ No tens

use $S\phi 10 \text{ /m}$ each side

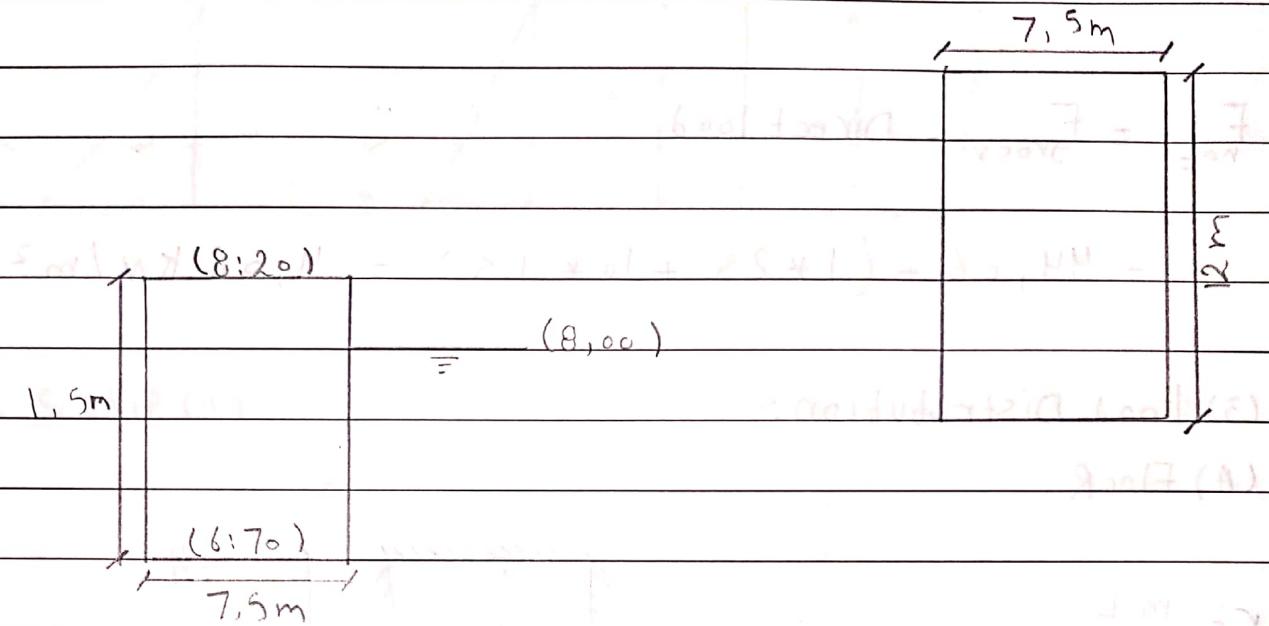
$$T_2 \text{ "max tens" } = -11,62 \text{ KN/m}$$

$$\therefore A_s = \frac{1,5 \times 11,62 \times 10^3}{400 / 1,15} = 50,11 \text{ mm}^2/\text{m}$$

$$\therefore \frac{50,11}{2} = 25,05 \text{ mm}^2/\text{m} \rightarrow \text{use min } S\phi 10 \text{ each side}$$

(3)

* Design of Pool *



(1) Concrete Dimension.

$$t_w = \frac{h}{16} = \frac{1500}{16} = 93\text{mm} \leq 250\text{mm}$$

$\therefore \text{take } t_w = 250\text{mm}$

$$t_f = 1\text{m} = 1000\text{mm}$$

(2) Check Soil Stress

$\Sigma w = \text{own weight of elements} + \text{weight of water in tank}$

$$\Sigma w = (7,5 \times 12 \times 1) \times 25 + (1,5 \times 12 \times 0,25) \times 25 \times 2$$

Number of walls

$$+ (1,5 \times 7,5 \times 0,25) \times 25 \times 2 + (7,5 \times 1,5 \times 12) \times 10$$

Number of walls

$$\Sigma w = 2250 + 225 + 140,625 + 1350 = 3965,625 \text{ KN}$$

(3.1 (F))

$$F_{\text{gross}} = \frac{\sum w}{A} = \frac{3965,625}{7,5 \times 12} = 44,06 \text{ kN/m}^2$$

$$F_{\text{net}} = F_{\text{gross}} \quad \text{Direct load}$$

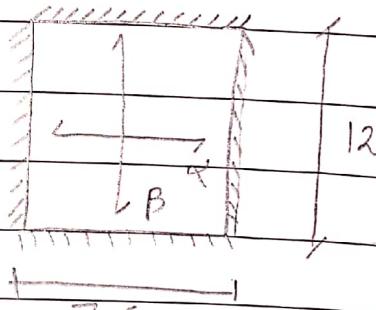
$$= 44,06 - (1 + 2,5 + 1,0 + 1,5) = 4,06 \text{ kN/m}^2$$

(3) Load Distribution:-

(A) Floor

$$r = \frac{m L}{m' L_s}$$

$$\therefore \frac{12}{7,5} = 1,6$$



$$\alpha = \frac{r^4}{1+r^4} = \frac{(1,6)^4}{1+(1,6)^4} = 0,86$$

$$B = 1 - \alpha = 0,14$$

(B) WALL (1)

One Way in V.L direction

$$e_1 = \text{zero}$$

$$e_2 = e_1 + K_a + \gamma_{\text{soil}} * h$$

$$= \frac{1}{3} * 18 * 1,5 = 9 \text{ kN/m}^2 \quad e_2 = 9$$

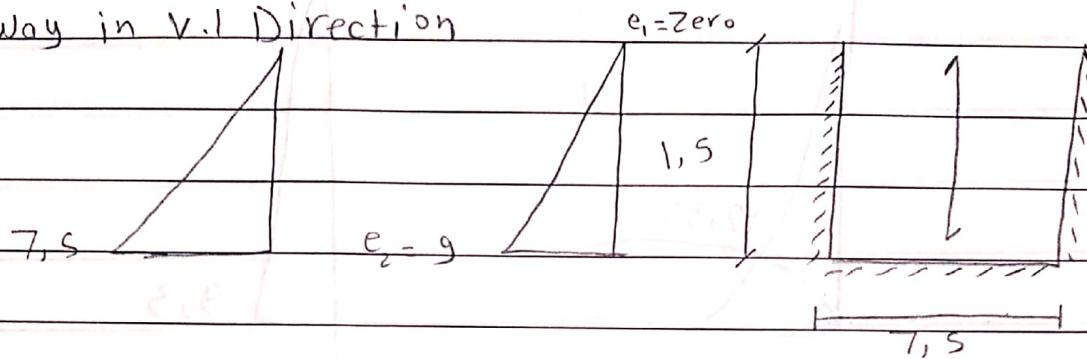
$$\therefore h_w > \frac{h}{2}$$

$$\therefore e = \frac{1,3(1 - \frac{1}{3}) * 10 + 1,3}{1,5} = 7,5 \text{ kN/m}^2$$

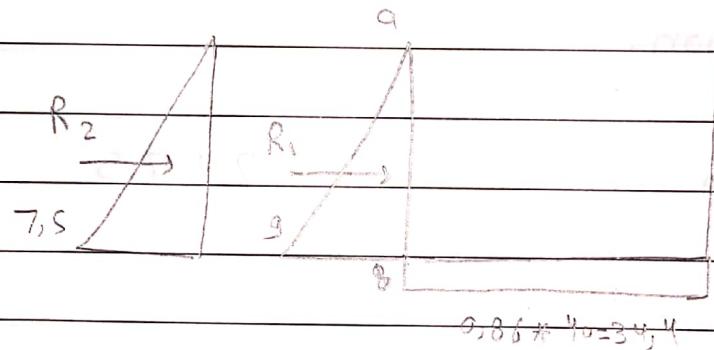
(2)

(c) Wall (2)

one way in V.L Direction



* For V.L STRIP (1)

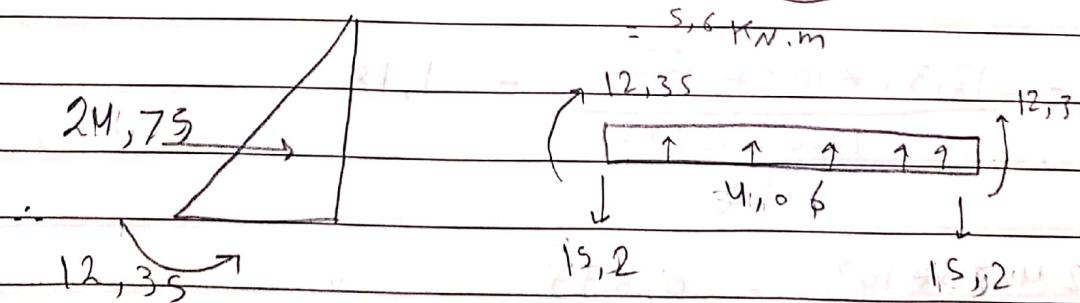


$$R_1 = \frac{9 \times 3}{2} = 13.5 \text{ KN}$$

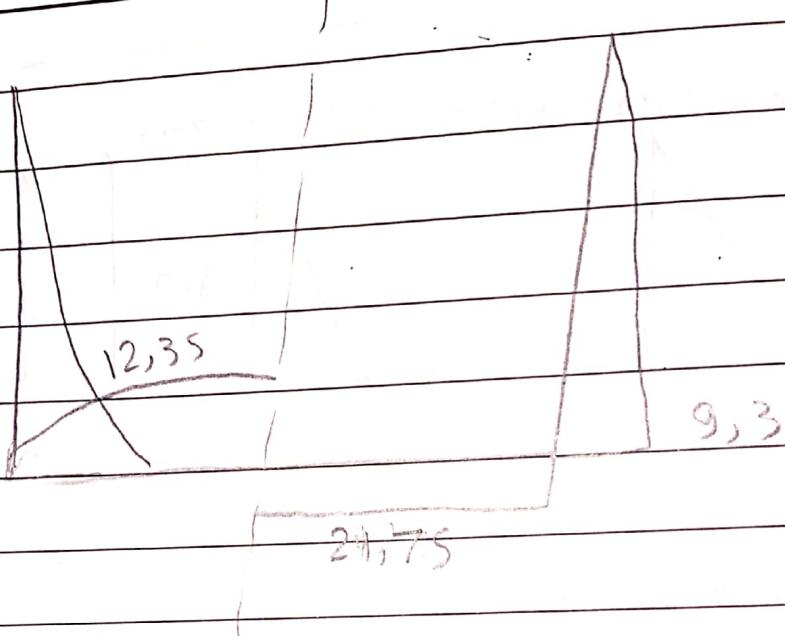
$$13.5 \times 0.86 = 11.67 \text{ KN.m}$$

$$R_2 = \frac{7.5 \times 3}{2} = 11.25 \text{ KN}$$

$$11.25 \times 0.86 = 9.675 \text{ KN.m}$$



(3)(n)



* Design of Section.

$$M = 12,35 \text{ kN.m}$$

$$T = 24,75$$

$$t = \sqrt{\frac{M * 10^3}{\sigma_s}} + 3_0$$

$$\sqrt{\frac{12,35 * 10^3}{\sigma_s}} + 3_0 = 232 \text{ mm}$$

Take $t = 250 \text{ mm}$

$$F_m = \frac{M * y}{I} = \frac{12,35 * 10^6 * \frac{250}{2}}{1000 * (250)^3} = 1,18$$

$$F_N = \frac{N}{A} = \frac{24,75 * 10^3}{1000 * 250} = 0,099$$

$$\therefore f_{tot} = 0,099 + 1,18 = 1,2$$

$$F_{ult} = \frac{0,6 \sqrt{3s}}{1,7} = 2,08 > f_{tot} = \text{Safe}$$

(4) (E)

* For Design

$$M_u = 1,5 * 12,35 = 20 \text{ kNm}$$

$$T_u = 1,5 * 24,75 = 40 \text{ kN}$$

$$e - \frac{M}{E} = \frac{20}{40} = 0,5 > \frac{t}{2} - \text{cover}$$

$$\therefore e_s = e - \frac{t}{2} + \text{cover}$$

$$= 0,5 - \frac{0,25}{2} + 0,4 = 0,415$$

$$M_s = T_u * e_s = 0,415 * 40 = 16,6$$

$$d = c_1 \sqrt{\frac{M_u * 10^6}{f_{cu} * 1000}}$$

$$210 = c_1 \sqrt{\frac{16,6 * 10^6}{35 * 1000}} \quad c_1 = 9,6 \quad J = 0,826$$

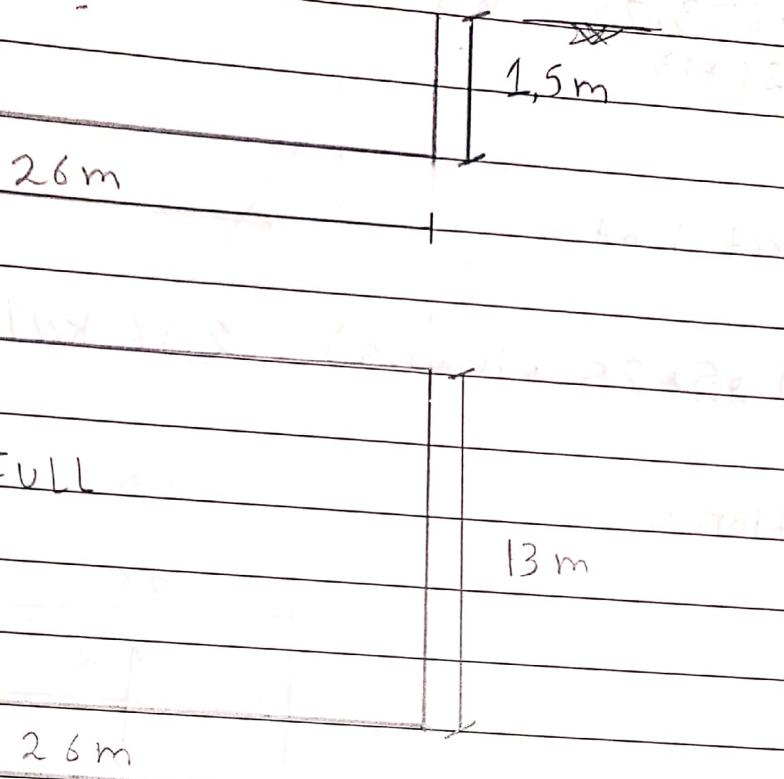
$$A_s = \frac{1}{\beta_{cr}} \left(\frac{M * 10^6}{f_y * J_k d} + \frac{N * 10^3}{f_y / \gamma_s} \right)$$

$$= \frac{1}{0,75} \left(\frac{16,6 * 10^6}{400 * 0,826 * 210} + \frac{40 * 10^3}{400 / 1,15} \right)$$

$$= 510 \text{ mm}^2 \rightarrow 5 \phi 16 / \text{m}^1$$

(5)

* Design of Pool 2 **



(1) Concrete Dimension:

$$* t_w = \frac{h}{16} = \frac{1500}{16} = 93\text{mm} < 250\text{mm}$$

$t_w = 250\text{mm}$

$$* t_f = \frac{L}{12} = \frac{1300}{12} = 1033\text{mm}$$

Take $t_f = 1050\text{mm}$

(2) Check Soil stresses

$\Sigma w = \text{own weight of elements} + \text{weight of water in tank}$

$$\Sigma w = (26 \times 13 \times 1,05) \times 25 + (1,5 \times 13 \times 0,25) \times 25 \times 2$$

$$+ (1,5 \times 26 \times 0,25) \times 25 \times 2 + (26 \times 13 \times 1,5) \times 10$$

$$\Sigma w = 8872,5 + 243,75 + 487,5 + 5070 = 14673,75\text{KN}$$

(E6)

$$F_{gross} = \frac{\sum w}{A} = \frac{14673,75}{26 \times 13} = 43,41 \text{ KN/m}^2$$

$$F_{net} = F_{gross} - \text{Direct load}$$

$$= 43,41 - (1,05 + 2,5 + 1,0 + 1,5) = 2,16 \text{ KN/m}^2$$

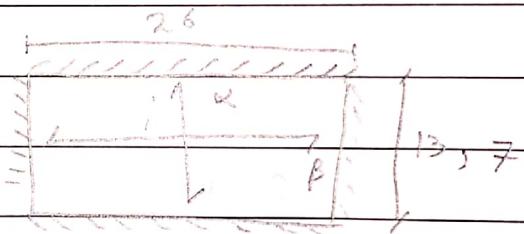
(3) Load Distribution:

(A) Floor

$$\frac{26}{13,7} = 1,8$$

$$\alpha = 0,9$$

$$\beta = 0,1$$

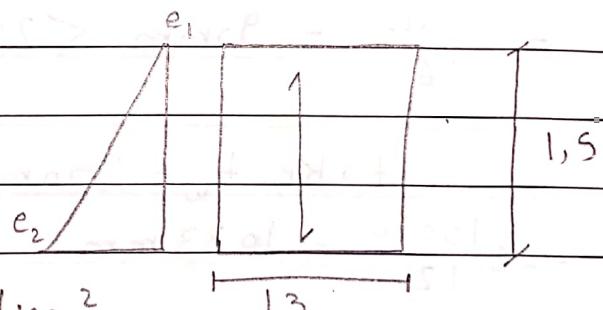


(B) Wall (1)

one way in V.I direction.

$$e_1 = \text{zero}$$

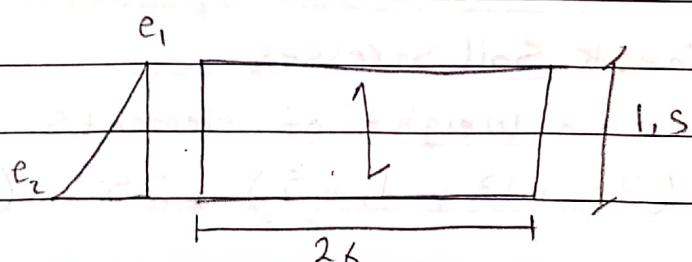
$$e_2 = K_a \times \gamma_{soil} \times h \\ = \frac{1}{3} \times 18 \times 1,5 = 9 \text{ KN/m}^2$$



(C) Wall (2)

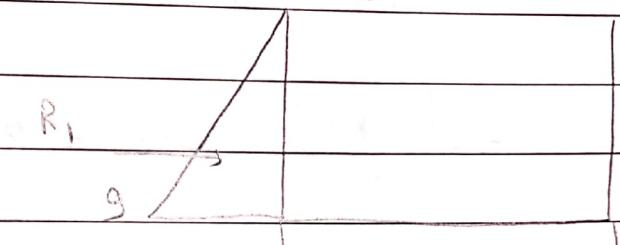
$$e_1 = \text{zero}$$

$$e_2 = \frac{1}{3} \times 18 \times 1,5 = 9 \text{ KN/m}^2$$



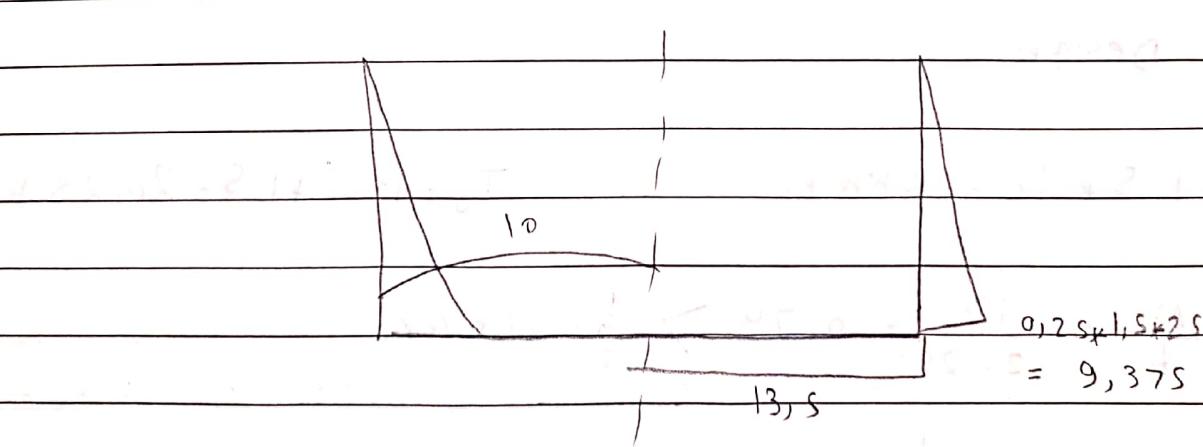
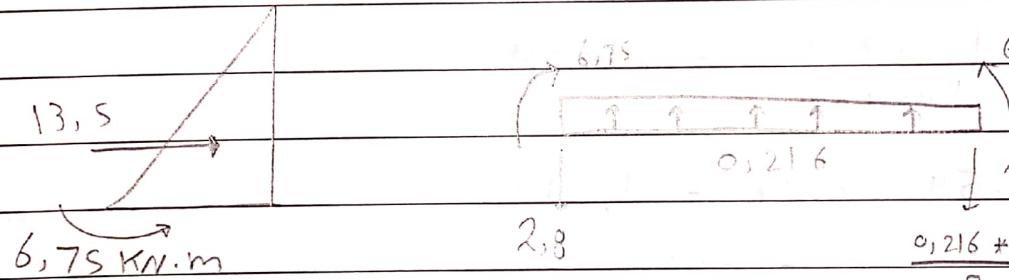
(7)

for v.l Strip



$$0,1 * 2,16 = 0,216 \text{ kN/m}$$

$$R_1 = \frac{9 * 3}{2} = 13,5 \text{ kN}$$



(8)

* Design of Section

$$M = 10 \text{ kN.m}$$

$$T = 13, S$$

$$E = \sqrt{\frac{M * 10^3}{0,3}} + 30 = \sqrt{\frac{10 * 10^3}{0,3}} + 30 = 212 \text{ mm}$$

take $t = 250 \text{ mm}$

$$\frac{F_m}{m} = \frac{M * y}{I} = \frac{10 * 10^6 * \frac{250}{2}}{1000 * (250)^3} = 0,96$$

12

$$\frac{F_N}{N} = \frac{A}{A} = \frac{13,5 * 10^3}{1000 * 250} = 0,54$$

$$\frac{F_{tot}}{f_{tot}} = 0,54 + 0,96 = 1,50$$

$$\frac{F_{all}}{f_{tot}} = \frac{0,6 \sqrt{35}}{1,7} = 2,08 > f_{tot} \therefore \text{Safe.}$$

* For Design

$$M_0 = 1,5 * 10 = 15 \text{ kN.m}$$

$$T_0 = 13,5 * 1,5 = 20,25 \text{ kN}$$

$$e = \frac{M}{E} = \frac{15}{20,25} = 0,74 > \frac{t}{2} \text{ - cover}$$

$$\therefore e_s = e - \frac{t}{2} + \text{cover}$$

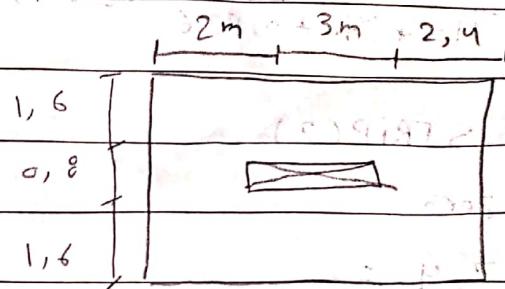
$$= 0,5 - \frac{0,25}{2} + 0,04 = 0,415$$

(g)

MeZanine Left Stair

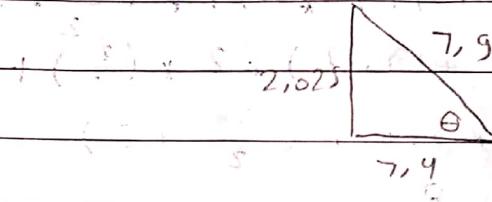
$$W_{sh} = 1,4 (t_s \gamma_c + F.c) + 1,6 L.L$$

$$= 1,4 (0,3 \times 25 + 2) + 1,6 \times 4 \\ = 19,7 \text{ kN/m}^2$$



$$W_{si} = 1,4 (t_{avg} \gamma_c + F.c) + 1,6 L.L (\cos \theta \cdot P.S) + P.S \cdot (F.c - t_{avg} \gamma_c)$$

$$= 1,4 (0,38 \times 25 + 2) + 1,6 \times 4 \times \frac{7,4}{7,9} \\ = 22,3 \text{ kN/m}^2$$



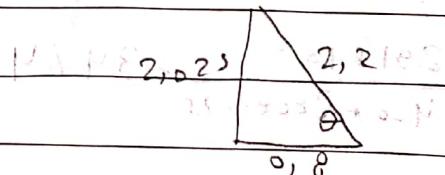
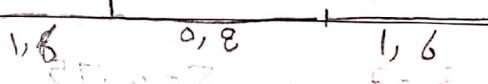
$\sum M @ A = \text{Zero}$

$$22,3 \times 2,2 \times \left(\frac{0,8}{2} + \frac{1,6}{2} \right)$$

$$= R \times \left(\frac{1,6}{2} + \frac{1,6}{2} + 0,8 \right)$$

$$\therefore R = 24,5$$

$$w = \frac{R}{x} = \frac{24,5}{1,6} = 15,3$$



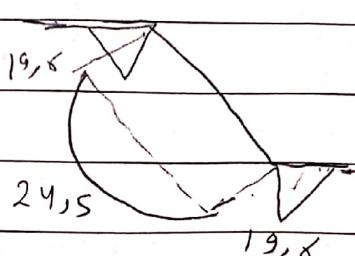
* For Design

$$\therefore 280 = C \times \sqrt{\frac{24,5 \times 10^6}{35 \times 1000}}$$

$$C = 10,5$$

$$J = 0,826$$

(ii)



$$A_s = \frac{24,5 \times 10^6}{400 \times 280 \times 0,826} = 264,8 \rightarrow \text{use } S \phi 10$$

* For STRIP(2)

$\sum M @ zero$

$$R_1 \times 7,4 =$$

$$(15,3 + 19,7) \times 2,4 + (\frac{2,4}{2} + 3+2)$$

$$+ (15,3 + 19,7) \times 2 \times (\frac{2}{2}) +$$

$$22,3 \times 3,6 + (\frac{3,6}{2} + 2)$$

$$R_1 = 117,8$$

$\sum M @ B - zero$

$$R_2 \times 7,4 = (15,3 + 19,7) + (\frac{2}{2} + 3 + 7,4)$$

$$+ 2 + 22,3 \times 3,6 + (\frac{3,6}{2} + 2,4)$$

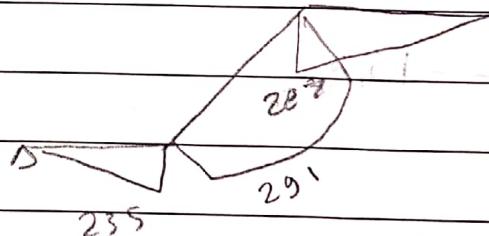
$$+ (15,3 + 19,7) \times 2,4 + \frac{2,4}{2}$$

$$R_2 = 119,7$$

$$280 = c + \sqrt{\frac{291 \times 10^6}{35 \times 1000}}$$

$$c = 3,07$$

$$s = 0,75$$



$$A_s = \frac{291 \times 10^6}{400 \times 280 \times 0,75} = 3464$$

10 φ 22

(2)

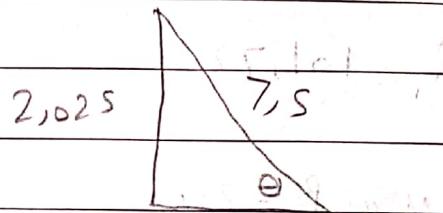
TyP.stair 2,4 3,5 1,4

$$w_{sh} = 1,4 (0,32 * 2s + 2) + 1,6 * 4 \quad 1,4$$

$$\approx 20,9 \text{ KN/m}^2 \quad (0,5 + 0,8 * 2,5) + (1,5 + 1,8 * 2,5) \quad 1,4$$

$$w_{si} = 1,4 (0,4 * 2s + 2) + 1,6 * 4 * \frac{7,3}{7,5}$$

$$\approx 23,03$$

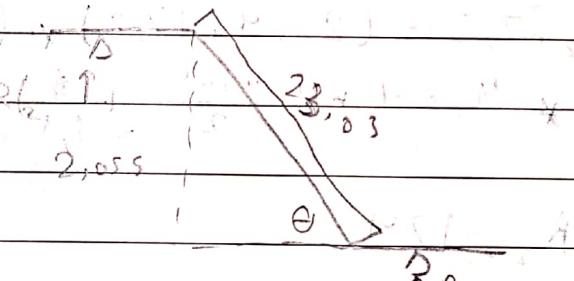


$$23,03 + 2,1 * \left(\frac{0,5}{2} + \frac{2,5}{2} \right) \quad 1,9$$

$$= R * (0,5 + 1,9)$$

$$R = 24,2$$

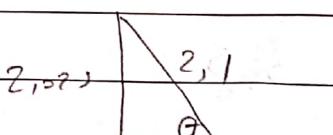
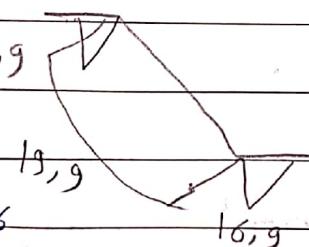
$$w = \frac{R}{x} = 17,2$$



* For Design

$$300 = c * \sqrt{\frac{19,9 * 10^6}{35 * 100c}} \quad 16,9$$

$$c = 12,5 \quad I = 0,826$$



$$A_s = \frac{19,9 * 10^6}{400 * 300 * 0,826} = 200,7 \rightarrow 5 \# 10 / \text{m}^2 \text{ (1A-1)}$$

(1)

For Strip(2)

$\sum M @ A = \text{zero}$

$$R_1 \times 7,3 = (20,4 + 17,2) \times \left(\frac{1,9}{2} + 3,5 + 2,4\right) + (20,4 + 17,2) \times 2,4 \times \frac{2,4}{2} + 23,03 \times 4,04 \times \left(\frac{3,5}{2} + 2,4\right)$$

$$R_1 = 101,72$$

$\sum M @ B = \text{zero}$

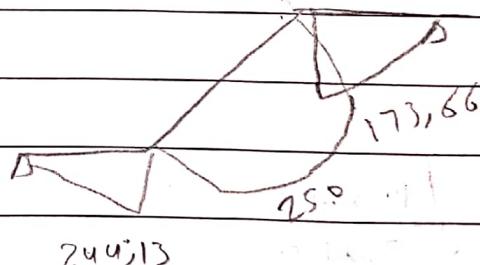
$$R_2 \times 7,3 = (20,4 + 17,2) \times \left(\frac{2,4}{2} + 3,5 + 2\right) \times 2,9 + 23,03 \times 4,04 \times \left(\frac{4,04}{2} + 1,9\right) + (20,4 + 17,2) \times 1,9 \times \frac{3,19}{2}$$

$$R_2 = 124$$

$$300 = c \sqrt{\frac{290 \times 10^6}{35 + 100c}}$$

$$c = 3,5$$

$$J = 0,78$$



$$A_s = \frac{250 \times 10^6}{400 \times 300 \times 0,78} = 2670 \text{ mm}^2$$

$$= 10 \phi 18$$