

Consider an object that is attached to a wall by a spring and forced to oscillate to and fro by a periodic driving function  $f(t) = F_0 \cos(\omega t)$ . Let  $x(t)$  be the object's displacement from equilibrium at time  $t$ . Under the assumption of small displacements, the system is governed by the following second order, constant-coefficient, differential equation.

$$mx'' + bx' + kx = F_0 \cos(\omega t) \quad (1)$$

The letter  $m$  denotes the mass of the object,  $k$  is the spring constant, and the letter  $b$  denotes the damping constant. All three of these constants, and the constants  $F_0$  and  $\omega$ , are assumed to be positive;  $\omega$  is called the *forcing frequency*. Recall that the *natural frequency* of the system is  $\omega_0 = \sqrt{k/m}$ . This is the frequency of the oscillations when the system is undamped and unforced:  $mx'' + kx = 0$ .

## Steady-State Solutions

The general solution to Equation (1) is  $x(t) = x_h(t) + x_p(t)$  where  $x_h(t)$  is the general solution to the associated *homogeneous* equation and  $x_p(t)$  is a *particular* solution to the forced equation. When the system is damped,  $x_h(t)$  contains decaying exponentials and it approaches zero as  $t \rightarrow \infty$ . After sufficient time has passed, the motion will be governed by  $x_p(t)$  and the system is said to have reached *steady-state*. The *steady-state solution*, also denoted  $x_{ss}(t)$ , is periodic with the same frequency as the driver. This is the motion that interests us here.

The steady-state solution for the simple driver  $F_0 \cos(\omega t)$  in Equation (1) can be found by substituting  $x = A \cos(\omega t) + B \sin(\omega t)$  into (1) and solving for  $A$  and  $B$ . When the driver is a general periodic function of frequency  $\omega$  the steady-state solution can be found by a similar method involving the complex Fourier series for the driver.

## Steady-State Solution for Any Periodic Driver

We wish to obtain the steady-state solution to

$$mx'' + bx' + kx = f(t) \quad (2)$$

where  $f$  is periodic of period  $P$  and (circular) frequency  $\omega = 2\pi/P$ . Here is how.

1. Obtain the complex Fourier series representation for the driver.<sup>1</sup>

$$f(t) = \sum_{n=-\infty}^{\infty} c_n e^{in\omega t}$$

2. Substitute  $x(t) = a_n e^{in\omega t}$  into the left side of (2) and solve for  $a_n$ , assuming that the driver is  $c_n e^{in\omega t}$ . That is, let  $x = a_n e^{in\omega t}$  in

$$mx'' + bx' + kx = c_n e^{in\omega t} \quad (3)$$

and solve for  $a_n$ . This turns out to be easy because all of the exponential terms cancel. For the  $n = 0$  case substitute  $x = a_0$  and the constant  $a_0$  will simply be  $c_0/k$ . However, for  $n \geq 1$ ,  $a_n$  will be a complex number.

3. Once  $a_n$  is found, let  $a_{-n} = \overline{a_n}$ , and the steady-state solution to (2) is

$$x_{ss}(t) = \frac{c_0}{k} + \sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} a_n e^{in\omega t} = \frac{c_0}{k} + \sum_{n=1}^{\infty} 2 \Re(a_n e^{in\omega t}). \quad (4)$$

Here is an example.

Example 1. Obtain the steady-state solution to the mass-spring system  $x'' + x' + 4x = f(t)$  where  $f$  is periodic of period  $P = \pi$  defined on the interval  $0 < t < \pi$  as follows.

$$f(t) = \begin{cases} 1 & , \quad 0 < t < \pi/2 \\ -1 & , \quad \pi/2 < t < \pi \end{cases}$$

---

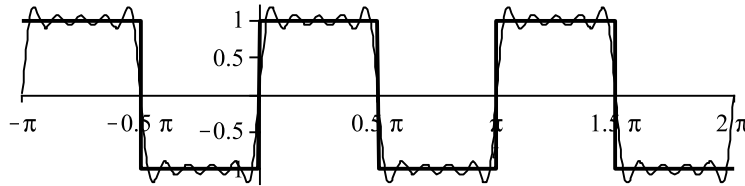
<sup>1</sup>Note the switch from  $k$  to  $n$  for the summation index in the Fourier series. This is to avoid confusion with the spring constant.

Plot the steady-state solution and the driver, suitably scaled to the dimensions of position vs time.

Solution. The driver is odd. See its graph below. Therefore,  $c_0 = 0$ . Since  $P = \pi$ ,  $\omega = 2\pi/P = 2$ , so the Fourier series for the driver has the form  $f(t) = \sum_{n=-\infty}^{\infty} c_n e^{2int}$  where

$$\begin{aligned} c_n &= \frac{1}{\pi} \int_0^\pi f(t) e^{-2int} dt = \frac{1}{\pi} \left( \int_0^{\pi/2} e^{-2int} dt + \int_{\pi/2}^\pi (-1) e^{-2int} dt \right) \\ &= \frac{1}{\pi} \left( \left. \frac{e^{-2int}}{-2in} \right|_{t=0}^{t=\pi/2} + \left. \frac{e^{-2int}}{2in} \right|_{t=\pi/2}^{t=\pi} \right) \\ &= \frac{1}{2\pi in} ((1 - e^{-\pi in}) + (e^{-2\pi in} - e^{-\pi in})) \\ &= \frac{1}{2\pi in} (2 - 2(-1)^n) \\ &= \frac{(-1)^n - 1}{\pi n} i. \end{aligned}$$

The coefficient  $c_n$  is pure imaginary. This is always the case when the waveform is odd. Observe also that when  $n$  is even,  $c_n = 0$ . The following plot confirms that these are the correct coefficients.



The driver  $f$  and its Fourier approximation  $S_9(t)$ .

Because there is no constant in the Fourier series for  $f$ , there is no constant in the steady-state solution. Therefore,

$$x_{ss}(t) = \sum_{n=1}^{\infty} 2 \Re(a_n e^{2int})$$

where  $a_n$  is found by substituting  $x = a_n e^{2int}$  into the differential equation

$$x'' + x' + 4x = c_n e^{2int}.$$

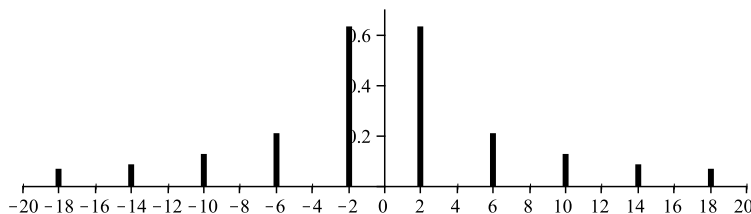
Doing so yields the following equation

$$-4n^2 a_n e^{2int} + 2ina_n e^{2int} + 4a_n e^{2int} = c_n e^{2int},$$

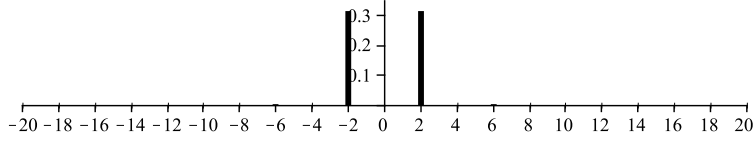
which simplifies to

$$(4 - 4n^2 + 2in)a_n = c_n.$$

Consequently, the  $n^{\text{th}}$  complex Fourier series coefficient for the steady-state solution is  $a_n = c_n / (4 - 4n^2 + 2in)$ . Observe that these coefficients approach 0 very quickly, implying that the oscillations in the steady-state solution will be completely determined by the first few non-zero harmonics. The amplitude spectrum for the driver is sketched below. The amplitude spectrum for the steady-state solution follows.

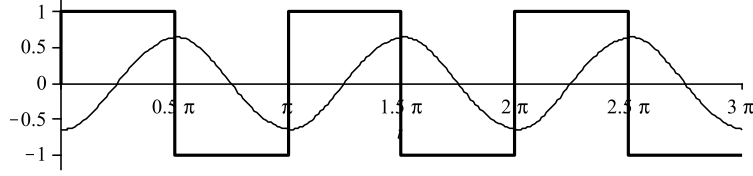


The amplitude spectrum for the periodic driver  $f$ .



The amplitude spectrum for the steady-state solution  $x_{ss}$ .

The following picture shows the driver and the steady-state solution. Five harmonics were used to plot  $x_{ss}$ . The picture obtained using just the *first* harmonic in the solution looks essentially the same.



The driver  $f$  and the steady-state solution  $x_{ss}$ .

A formula for the first harmonic in  $x_{ss}$

First observe that  $c_n$  is zero when  $n$  is even. For odd  $n$ ,  $c_n = -2i/n\pi$ . Therefore,

$$a_n = \frac{c_n}{4 - 4n^2 + 2in} = \frac{-2i}{n\pi(4 - 4n^2 + 2in)}, \quad n \text{ odd}.$$

In particular, when  $n = 1$ ,  $a_1 = -1/\pi$ . Therefore, using just the first harmonic,

$$x_{ss}(t) \approx 2 \Re(a_1 e^{2it}) = -\frac{2}{\pi} \cos(2t).$$

The amplitude of the first harmonic is 0.637. The next non-zero harmonic is  $-\frac{2}{3\pi\sqrt{9+16^2}} \cos(6t - \delta_3)$  where  $\delta_3 = \arctan(16^2/9)$ . Its amplitude is 0.013.

## A General Formula

The method illustrated in Example 1 is completely general, applying to any piecewise smooth driver of period  $P$ . In summary, it proceeds as follows. Begin by expressing the system in the form

$$mx'' + bx' + kx = \sum_{n=-\infty}^{\infty} c_n e^{in\omega t}, \quad \omega = 2\pi/P. \quad (5)$$

The steady-state solution will then have the form

$$x_{ss}(t) = \sum_{n=-\infty}^{\infty} a_n e^{in\omega t}$$

where  $x = a_n e^{in\omega t}$  is a particular solution to

$$mx'' + bx' + kx = c_n e^{in\omega t}.$$

To find  $a_n$  simply substitute  $x = a_n e^{in\omega t}$  into the last equation to obtain

$$-mn^2\omega^2 a_n e^{in\omega t} + ibn\omega a_n e^{in\omega t} + ka_n e^{in\omega t} = c_n e^{in\omega t}$$

which implies that

$$a_n = \frac{c_n}{k - mn^2\omega^2 + ibn\omega}.$$

Consequently,

$$x_{ss}(t) = \sum_{n=-\infty}^{\infty} \frac{c_n}{k - mn^2\omega^2 + ibn\omega} e^{in\omega t}. \quad (6)$$

Three comments:

1. The form of the  $n^{\text{th}}$  complex Fourier coefficient in Equation (6) makes it clear that the higher-order harmonics have almost no effect on the steady-state solution.
2. If information about a particular harmonic is needed, say the  $n^{\text{th}}$  one, its amplitude is  $2|a_n|$  (why?). Therefore,

$$n^{\text{th}} \text{ Amplitude} = A_n = \frac{2|c_n|}{\sqrt{(k - mn^2\omega^2)^2 + b^2n^2\omega^2}}.$$

3. An explicit formula for the  $n^{\text{th}}$  steady-state harmonic is given by

$$n^{\text{th}} \text{ Harmonic} = A_n \cos(n\omega t - (\delta_n - \gamma_n))$$

where  $\delta_n$  is the argument of  $k - mn^2\omega^2 + ibn\omega$  and  $\gamma_n$  is the argument of  $c_n$ .

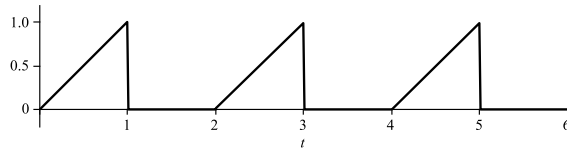
The following example illustrates these observations.

Example 2. Consider the mass-spring system

$$x'' + 0.1x' + 24x = f(t)$$

where  $f$  is the period 2 driver defined in Example 1 of the Complex Fourier Series, Part I handout.

$$f(t) = \begin{cases} t & , \quad 0 < t < 1 \\ 0 & , \quad 1 < t < 2 \end{cases}$$



The driver  $f$  has period 2.

Since  $P = 2$ ,  $\omega = 2\pi/P = \pi$ , and  $f(t) = \sum_{n=-\infty}^{\infty} c_n e^{in\pi t}$  where

$$c_0 = \frac{1}{4} \quad \text{and} \quad c_n = \frac{1}{2} \left( \frac{(-1)^n}{n\pi} i + \frac{(-1)^n - 1}{n^2\pi^2} \right).$$

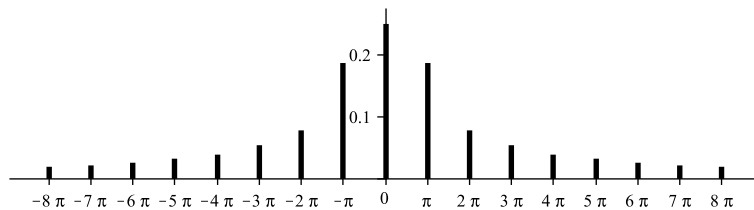
Therefore, the steady-state solution  $x_{ss}$  has the complex Fourier series

$$x_{ss}(t) = \frac{1/4}{k} + \sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} \frac{c_n}{k - mn^2\pi^2 + ibn\pi} e^{in\pi t}$$

where  $m = 1$ ,  $b = 0.1$ , and  $k = 24$ . That is,

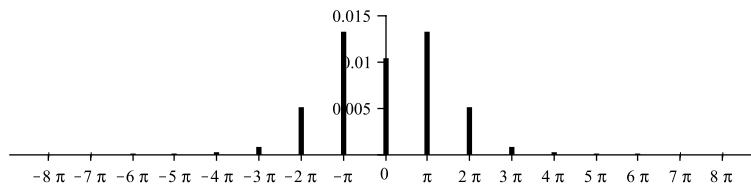
$$x_{ss}(t) = \frac{1}{96} + \sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} \frac{c_n}{24 - n^2\pi^2 + 0.1in\pi} e^{in\pi t}.$$

The following picture shows the amplitude spectrum of the driver.



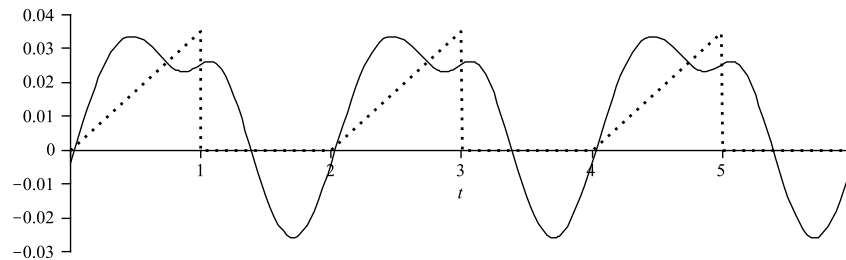
The driver's amplitude spectrum.

And here is the amplitude spectrum of the steady-state solution.



The amplitude spectrum of the steady-state solution.

The steady-state amplitude spectrum shows that the constant and the first three harmonics are enough to build an almost perfect picture of the steady-state motion. See the plot below, showing a scaled version of the driver and the steady-state approximation using 3 harmonics. The effects of the first two harmonics are especially evident. See Exercise 11 in Exercise Set 5.



The scaled driver (dotted) and the steady-state solution using the constant term and the first three harmonics.

Interesting Observation. Using the constant and the first three harmonics yields only a mediocre approximation of the driver. See the plot in Example 1 of the Part I handout. However, the driver's power spectrum on page 4 of Part I clearly shows that its first three harmonics in the driver carry almost all of its power.