

# High-gain twin-beam generation in waveguides: from Maxwell's equations to efficient simulation

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**Abstract:** We provide an efficient method for the calculation of the quantum state describing high-gain, twin-beam generation in waveguides that is derived from a canonical treatment of Maxwell's equations and accommodates self- and cross-phase modulation.

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## 1. Introduction

The generation of twin beams is an important technique for the production of nonclassical light. In early experiments, the twin beams were generated with low intensities over a manifold of modes. Recent developments in photonics have allowed for the tight confinement of the travelling waves participating in the three- or four-wave mixing process necessary for the generation of twin beams [1]. These developments have moved the focus of theoretical descriptions of twin beam generation from the perturbative regime to the nonperturbative regime. In this work, we construct a theory for the description of high-gain squeezing satisfying the following criteria:

- The theory is directly based on a canonical Hamiltonian formulation of the nonlinear macroscopic Maxwell equations.
- The creation and annihilation operators describe photons in the modes of integrated optical structures, and their evolution fully respects the effects of self- and cross-phase modulation as well as twin beam generation beyond the perturbative regime..
- The theory can be used to calculate the full quantum state  $|\Psi\rangle$  characterizing the twin beams.
- The equations of motion that result can be solved numerically with unprecedented ease.

Using these results we investigate and benchmark the simulation of the simplest waveguide SPDC geometry: a nonlinear region that is uniform over a finite region of 1-D space.

## 2. Deriving canonical equations of motion and solving them

We take  $\mathbf{B}$  and  $\mathbf{D}$  as the fundamental fields, which allows for a correct canonical quantization of the electromagnetic field in a nonlinear material [2]. The linear Hamiltonian of the field is  $H_L = \int d\mathbf{r} \left( \frac{\mathbf{B}^2}{2\mu_0} + \frac{(1+\chi^{(1)})^{-1}}{2\epsilon_0} \mathbf{D}^2 \right) = \int dk \sum_{\mu} \hbar \omega_{\mu}(k) b_{\mu k}^{\dagger} b_{\mu k}$ , and we write the displacement field as  $\mathbf{D}(\mathbf{r}) = \sum_{\mu} \int dk \sqrt{\frac{\hbar \omega_{\mu k}}{4\pi}} b_{\mu k} \mathbf{d}_{\mu k}(x, y) e^{ikz} + \text{H.c.}$ , where  $\mathbf{d}_{\mu k}(x, y)$  is the (properly normalized [2]) transverse profile of the field,  $\mu$  is a waveguide mode index, and  $\omega_{\mu k}$  is the frequency associated with wavevector  $k$  in mode  $\mu$ ; a similar decomposition holds for  $\mathbf{B}$ . The boson operators  $b_{\mu, k}$  satisfy the *equal-time* commutation relations  $[b_{\mu k}(t), b_{\mu' k'}(t)] = 0$  and  $[b_{\mu k}(t), b_{\mu' k'}^{\dagger}(t)] = \delta_{\mu, \mu'} \delta(k - k')$ .

In what follows we assume that the signal ( $\mu = s$ ) and idler ( $\mu = i$ ) beams generated in the nonlinear region are narrow enough in frequency that for each field we can approximate locally the dispersion relation as linear,  $k - \bar{k}_{\mu} \approx (\omega - \bar{\omega}_{\mu})/v_{\mu}$  where  $v_{\mu}$  is the group velocity of mode  $\mu$  and  $\bar{k}_{\mu}$  and  $\bar{\omega}_{\mu}$  are suitably defined central wavevectors and frequencies for each mode. We make the same assumption for the pump field  $\mu = p$  sent into the nonlinear region. We now consider the nonlinear part of the Hamiltonian,  $H_{NL} = \int d\mathbf{r} \left( -\frac{\chi^{(2)} \mathbf{D}^3}{3\epsilon_0^2 n_0^6} - \frac{\chi^{(3)} \mathbf{D}^4}{4\epsilon_0^2 n_0^8} \right)$  ( $n_0$  is a typical refractive index and  $\chi^{(i)}$  are the standard nonlinear susceptibilities) in which we use our expansion for the  $\mathbf{D}$  field and only keep energy-

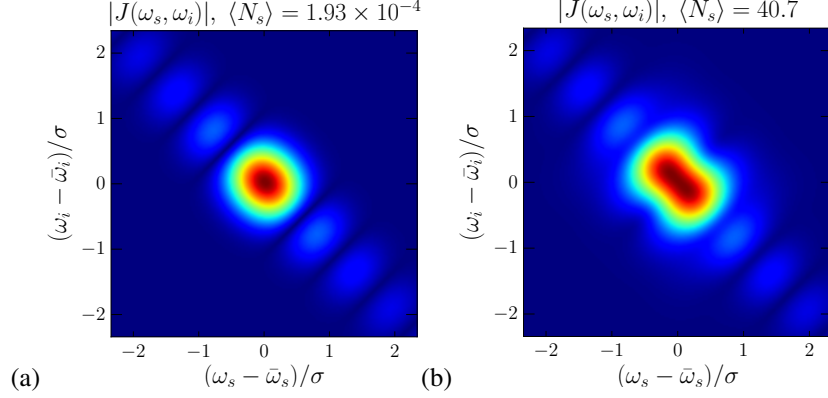


Fig. 1. Absolute value of the (a) low- and (b) high-gain joint spectral amplitude for a top-hat nonlinearity profile.

and phase-matched terms. Thus for the three-wave mixing terms we only keep terms of the form  $b_{pk}b_{sk'}^\dagger b_{ik''}^\dagger + \text{H.c.}$  giving rise to spontaneous parametric down-conversion, whereas for the four-wave wave mixing we keep only terms of the form  $b_{pk}^\dagger b_{pk'} b_{pk''}^\dagger b_{pk'''}^\dagger$  and  $b_{pk}^\dagger b_{pk'} b_{xk''}^\dagger b_{xk'''}^\dagger$  ( $x \in \{s, i\}$ ) giving rise to self-phase modulation of the pump and cross-phase modulation of the pump on the signal and idler. With the Hamiltonian in hand we can now calculate the equations of motion for the operators  $b_{\mu k}$  by simply taking  $\frac{\partial}{\partial t} b_{\mu k}(t) = \frac{i}{\hbar} [H_L + H_{NL}, b_{\mu k}(t)]$ . In the classical-undepleted pump limit one can introduce suitably defined Fourier transformed operators  $a_x(z, \omega)$ , with equations [3]

$$\frac{\partial}{\partial z} a_s(z, \omega) = i\Delta k_s(\omega) a_s(z, \omega) + i \frac{\gamma_{\text{XPM},s} h_s(z)}{2\pi} \int d\omega' \mathcal{E}_p(\omega - \omega') a_s(z, \omega') + i \frac{\gamma_{\text{PDC}} g(z)}{\sqrt{2\pi}} \int d\omega' \beta_p(z, \omega + \omega') a_i^\dagger(z, \omega'),$$

and likewise for the idler by switching  $s \leftrightarrow i$ . In the last equation  $\Delta k_x = \left(\frac{1}{v_x} - \frac{1}{v_p}\right)(\omega - \bar{\omega}_x)$ ,  $\gamma_{\text{PDC}} \propto \chi^{(2)}$  and  $\gamma_{\text{XPM}} \propto \chi^{(3)}$  characterize the strength of the three- and four-wave mixing interactions and  $h_x(z)$  and  $g(z)$  their spatial extent. Finally,  $\beta_p(z, \omega)$  is the classical spectral distribution of the pump, which evolves due to SPM according to  $\partial_z \beta_p(z, \omega) = i\gamma_{\text{SPM}} \int d\omega' \mathcal{E}_p(\omega - \omega') \beta_p(z, \omega')$  where  $\mathcal{E}_p(\omega) = \int d\omega' \beta_p^*(z_0, \omega' - \omega) \beta_p(z_0, \omega')$ . These equations can be solved numerically using matrix exponentiation, and lead to the following linear Bogoliubov transformation

$$a_s^{(\text{out})}(\omega) = \int d\omega' U^{s,s}(\omega, \omega') a_s^{(\text{in})}(\omega') + \int d\omega' U^{s,i}(\omega, \omega') a_i^{(\text{in})}(\omega'), \quad (1)$$

The input/output  $a_x^{\text{in/out}}(\omega)$  operators are related to the proper-evolving-in-time Heisenberg operators via

$$b_{xk}^{\text{in/out}} \equiv b_{xk}(t_{0/1}) e^{i\omega(k)t_{0/1}} = \sqrt{v_x} e^{-\Delta k_x z_{0/1}} a(z_{0/1}, \omega(k)) = \sqrt{v_x} a^{\text{in/out}}(\omega(k)), \quad (2)$$

where recall  $x \in \{s, i\}$ , we assumed a linear dispersion relation, and  $z_{0/1}$  and  $t_{0/1}$  are positions and times long before/after the pump as entered the nonlinear region. Due to the  $SU(1, 1)$  symmetry of the equations of motion one can show that the transfer functions  $U^{x,x'}(\omega, \omega')$  can be jointly decomposed

$$U^{s,i}(\omega, \omega') = \sum_l \sinh(r_l) [\rho_s^{(l)}(\omega)] [\tau_i^{(l)}(\omega')], \quad (U^{i,i}(\omega, \omega'))^* = \sum_l \cosh(r_l) [\rho_i^{(l)}(\omega)]^* [\tau_i^{(l)}(\omega')], \quad (3)$$

and a similar equation for the signal by letting  $s \leftrightarrow i$ . Based on this decomposition, and noting that the initial state in the signal and idler beams is vacuum, we can finally write the output state  $|\Psi\rangle = \exp\left(\int d\omega d\omega' J(\omega, \omega') a_s^{(\text{in})\dagger}(\omega) a_i^{(\text{in})\dagger}(\omega') - \text{H.c.}\right) |\text{vac}\rangle$  where the joint spectral amplitude (JSA) is given by  $J(\omega, \omega') = \sum_l r_l \rho_s^{(l)}(\omega) \rho_i^{(l)}(\omega')$ . This completes the program sketched in the Introduction. In Fig. 1 we use the method just described to obtain the low- and high- gain regimes for a waveguide with a top-hat nonlinearity profile. In the low gain regime where the mean photon number in the signal or idler modes is  $\langle N_s \rangle = \langle N_i \rangle \sim 2 \times 10^{-4} \ll 1$  the JSA is simply the product of the pump function (which we assumed Gaussian) and the Fourier transform of the nonlinearity

profile, which for a top-hat functions results in a sinc function. This can be contrasted with the high -gain regime  $\langle N_s \rangle = \langle N_i \rangle \sim 41$  where due to time-ordering effects the JSA has a much more complicated frequency dependence that can be understood as interference between many different Magnus-expansion terms [4]. Note that for a grid size of  $600 \times 600$  points the JSAs presented in the figure require just a few seconds to be generated in a desktop computer, which should be compared with the hours it takes using other methods [5].

The theory we have developed has also been used to explain a recent high-gain experiment [6] where the JSA is not only modified by the effects of time-ordering but also by self- and cross-phase modulation.

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