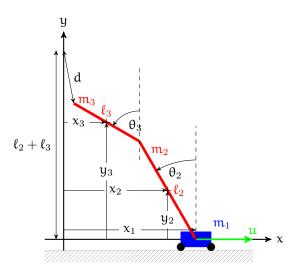
Cart and Double Pendulum Dynamics

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July 1st 2014

The cart and double pendulum dynamical system consists of a cart with mass \mathfrak{m}_1 and an attached double pendulum. The double pendulum consists of two pieces, the first of mass \mathfrak{m}_2 and length ℓ_2 and the second has mass \mathfrak{m}_3 and length ℓ_3 . Both joints are frictionless and unactuated, the double pendulum can move freely in the vertical plane. The goal position is balancing the double pendulum vertically above $\mathfrak{x}=0$, and the discrepancy is the distance \mathfrak{d} . The system is actuated by applying a force \mathfrak{u} horizontally to the cart. The state of the system is given by the horizontal position of the cart \mathfrak{x}_1 , the two angles \mathfrak{d}_2 and \mathfrak{d}_3 . (both measured anti-clockwise from vertically up) and the time derivatives of these three variables, $\dot{\mathfrak{x}}_1$, $\dot{\mathfrak{d}}_2$ and $\dot{\mathfrak{d}}_3$.



The cart can move horizontally, with an applied external force $-20N \leqslant u \leqslant 20N$, and coefficient of friction b = 0.1 Ns/m. The other physical values are $m_1 = m_2 = m_3 = 0.5 kg$ and $\ell_2 = \ell_3 = 0.6 m$ (doesn't correspond to figure). Thus, the moment of inertia around the midpoint of each part of the pendulum is $I_2 = I_3 = 0.015 kg \, m^2$.

Equations of Motion

The geometric relationships gives the following conditions for the coordinates of the midpoint of the two penduli:

$$x_2 = x_1 - \frac{1}{2}\ell_2 \sin \theta_2,$$
 $y_2 = \frac{1}{2}\ell_2 \cos \theta_2,$ (1)

$$x_3 = x_1 - \ell_2 \sin \theta_2 - \frac{1}{2} \ell_3 \sin \theta_3, \quad y_3 = \ell_2 \cos \theta_2 + \frac{1}{2} \ell_3 \cos \theta_3.$$
 (2)

The squared velocities of the centres of gravity are

$$v_1^2 = \dot{x}_1^2, \qquad v_2^2 = \dot{x}_1^2 - \ell_2 \dot{x}_1 \dot{\theta}_2 \cos \theta_2 + \frac{1}{4} \ell_2^2 \dot{\theta}_2^2,$$
 (3)

$$\nu_3^2 = \dot{x}_1^2 - 2\ell_2 \dot{x}_1 \dot{\theta}_2 \cos \theta_2 - \ell_3 \dot{x}_1 \dot{\theta}_3 \cos \theta_3 + \ell_2^2 \dot{\theta}_2^2 + \frac{1}{4} \ell_3^2 \dot{\theta}_3^2 + \ell_2 \ell_3 \dot{\theta}_2 \dot{\theta}_3 \cos \theta_2 \cos \theta_3. \tag{4}$$

The system Lagrangian is

$$\begin{split} \mathsf{L} &= \mathsf{T} - \mathsf{V} \, = \, \tfrac{1}{2} \mathsf{m}_1 \mathsf{v}_1^2 + \tfrac{1}{2} \mathsf{m}_2 \mathsf{v}_2^2 + \tfrac{1}{2} \mathsf{m}_3 \mathsf{v}_3^2 + \tfrac{1}{2} \mathsf{I}_2 \dot{\theta}_2^2 + \tfrac{1}{2} \mathsf{I}_3 \dot{\theta}_3^2 - \mathsf{m}_2 \mathsf{g} \mathsf{y}_2 - \mathsf{m}_3 \mathsf{g} \mathsf{y}_3 \, \Rightarrow \\ \mathsf{L} &= \tfrac{1}{2} (\mathsf{m}_1 + \mathsf{m}_2 + \mathsf{m}_3) \dot{x}_1^2 - (\tfrac{1}{2} \mathsf{m}_2 + \mathsf{m}_3) \ell_2 \dot{x}_1 \dot{\theta}_2 \cos \theta_2 + (\tfrac{1}{6} \mathsf{m}_2 + \tfrac{1}{2} \mathsf{m}_3) \ell_2^2 \dot{\theta}_2^2 - \tfrac{1}{2} \mathsf{m}_3 \ell_3 \dot{x}_1 \dot{\theta}_3 \cos \theta_3 + \\ & \tfrac{1}{6} \mathsf{m}_3 \ell_2^2 \dot{\theta}_2^2 + \tfrac{1}{3} \mathsf{m}_3 \ell_2 \ell_3 \dot{\theta}_2 \dot{\theta}_3 \cos(\theta_2 - \theta_3) - (\tfrac{1}{2} \mathsf{m}_2 + \mathsf{m}_3) \mathsf{q} \ell_2 \cos \theta_2 - \tfrac{1}{3} \mathsf{m}_3 \mathsf{q} \ell_3 \cos \theta_3, \end{split}$$

where $g = 9.82 \text{m/s}^2$ is the acceleration of gravity.

The equations of motion are

$$\frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i} - \frac{\partial L}{\partial q_i} \; = \; Q_i, \label{eq:Qi}$$

where $Q_{\mathfrak{i}}$ are the non-conservative forces. In our case

$$\frac{\partial L}{\partial \dot{x}_1} = (m_1 + m_2 + m_3)\dot{x}_1 - (\frac{1}{2}m_2 + m_3)\ell_2\dot{\theta}_2\cos\theta_2 - \frac{1}{2}m_3\ell_3\dot{\theta}_3\cos\theta_3, \tag{5}$$

$$\frac{\partial L}{\partial x} = 0, \tag{6}$$

$$\frac{\partial L}{\partial \dot{\theta}_2} = (\frac{1}{3}m_2 + m_3)\ell_2^2 \dot{\theta}_2 - (\frac{1}{2}m_2 + m_3)\ell_2 \dot{x}_1 \cos \theta_2 + \frac{1}{2}m_3\ell_2\ell_3 \dot{\theta}_3 \cos(\theta_2 - \theta_3), \tag{7}$$

$$\frac{\partial \hat{L}}{\partial \theta_2} = (\frac{1}{2}m_2 + m_3)\ell_2(g + \dot{x}_1\dot{\theta}_2)\sin\theta_2 - \frac{1}{2}m_3\ell_2\ell_3\dot{\theta}_2\dot{\theta}_3\sin(\theta_2 - \theta_3), \tag{8}$$

$$\frac{\partial L}{\partial \dot{\theta}_{3}} = \frac{1}{3} m_{3} \ell_{3}^{2} \dot{\theta}_{3} - \frac{1}{2} m_{3} \ell_{3} \dot{x}_{1} \cos \theta_{3} + \frac{1}{2} m_{3} \ell_{2} \ell_{3} \dot{\theta}_{2} \cos(\theta_{2} - \theta_{3}), \tag{9}$$

$$\frac{\partial L}{\partial \theta_3} \ = \ \tfrac{1}{2} m_3 \ell_3 (g + \dot{x}_1 \dot{\theta}_3) \sin \theta_3 + \tfrac{1}{2} m_3 \ell_2 \ell_3 \dot{\theta}_2 \dot{\theta}_3 \sin(\theta_2 - \theta_3), \tag{10}$$

leading to the equations of motion

$$\begin{split} (\mathfrak{m}_1 + \mathfrak{m}_2 + \mathfrak{m}_3) \ddot{x}_1 - (\tfrac{1}{2} \mathfrak{m}_2 + \mathfrak{m}_3) \ell_2 (\ddot{\theta}_2 \cos \theta_2 - \dot{\theta}_2^2 \sin \theta_2) - \tfrac{1}{2} \mathfrak{m}_3 \ell_3 (\ddot{\theta}_3 \cos \theta_3 - \dot{\theta}_3^2 \sin \theta_3) \ = \ \mathfrak{u} - b \dot{x}_1, \\ (\tfrac{1}{3} \mathfrak{m}_2 + \mathfrak{m}_3) \ell_2 \ddot{\theta}_2 - (\tfrac{1}{2} \mathfrak{m}_2 + \mathfrak{m}_3) (\ddot{x}_1 \cos \theta_2 + g \sin \theta_2) + \tfrac{1}{2} \mathfrak{m}_3 \ell_3 [\ddot{\theta}_3 \cos (\theta_2 - \theta_3) + \dot{\theta}_3^2 \sin (\theta_2 - \theta_3)] \ = \ 0, \\ \tfrac{1}{3} \ell_3 \ddot{\theta}_3 - \tfrac{1}{2} (\ddot{x}_1 \cos \theta_3 + g \sin \theta_3) + \tfrac{1}{2} \ell_2 [\ddot{\theta}_2 \cos (\theta_2 - \theta_3) - \dot{\theta}_2^2 \sin (\theta_2 - \theta_3)] \ = \ 0. \end{split}$$

Collecting the six state variables $z = (\dot{x}_1, \dot{\theta}_2, \dot{\theta}_3, x_1, \theta_2, \theta_3)$ the equations of motion can be conveniently expressed as six coupled differential equations

$$\frac{dz}{dt} = \begin{array}{cc} A^{-1} & B \\ I & 0 \end{array}$$

Linearized Dynamics

Linearizing the dynamics aroud the goal state, we can write the following approximation

$$\frac{dz}{dt} \simeq q^{-1}(Az + bu), \qquad q = 2\ell_2\ell_3(m_1(4m_2 + 3m_3) + m_2(m_2 + m_3)), \qquad b = \begin{bmatrix} 2\ell_2\ell_3(4m_2 + 3m_3) \\ 6\ell_3(2m_2 + m_3) \\ -6\ell_2m_2 \\ 0 \\ 0 \end{bmatrix},$$

and

$$A \, = \, \begin{bmatrix} -2\ell_2\ell_3(4m_2+3m_3)b & 0 & 0 & 0 & 3\ell_2\ell_3(m_2+2m_3)(2m_2+m_3)g & -3\ell_2\ell_3m_2m_3g \\ -6\ell_3(2m_2+m_3)b & 0 & 0 & 0 & 3\ell_3(m_2+2m_3)(4m_1+4m_2+m_3)g & -9\ell_3m_3(2m_1+m_2)g \\ 6\ell_2m_2b & 0 & 0 & 0 & -9\ell_2(m_2+2m_3)(2m_1+m_2)g & 3\ell_2(4m_1(m_2+3m_3)+m_2(m_2+4m_3))g \\ q & 0 & 0 & 0 & 0 & 0 \\ 0 & q & 0 & 0 & 0 & 0 \\ 0 & 0 & q & 0 & 0 & 0 & 0 \end{bmatrix}.$$

Loss Function

The instantaneous loss is given by

$$F = 1 - \exp(-\frac{d^2}{2a^2}),$$

were d^2 is the squared distance between the tip of the pendulum and the point at distance $\ell_2 + \ell_3$ above the origin, and a is the width parameter. Note that the instantaneous loss does not depend on the speed variables, \dot{x}_1 , $\dot{\theta}_2$ and $\dot{\theta}_3$. The squared distance is

$$d^2 = (x_1 - \ell_2 \sin \theta_2 - \ell_3 \sin \theta_3)^2 + (\ell - \ell_2 \cos \theta_2 + \ell_3 \cos \theta_3)^2 = (\tilde{z} - \mu)^\top Q(\tilde{z} - \mu),$$

where \tilde{z} is z augmented by four coordinates $\sin \theta_2, \sin \theta_3$ and $\cos \theta_2, \cos \theta_3$ and

$$Q \ = \ C^{\top}C, \quad C \ = \ \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 & -\ell_1 & 0 & -\ell_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \ell_1 & 0 & \ell_2 \end{bmatrix}, \quad \mu \ = \ \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 \end{bmatrix}^{\top}.$$

The expected loss, averaging over the possibly uncertain states is therefore

$$\mathbb{E}[\mathsf{F}(\tilde{z})] \; = \; 1 - \int \mathsf{F}(\tilde{z}) \mathsf{p}(\tilde{z}) d\tilde{z},$$

which can be evaluated in closed form for Gaussian $p(\tilde{z})$, see reward.pdf. Since the augmented state \tilde{z} will not generally be Gaussian even if z is Gaussian, we project on to the closest Gaussian by matching first and second moments.