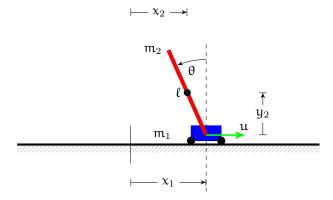
## The Cart and Pole Task

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The cart and pole dynamical system consists of a cart (mass  $m_1$ ) and an attached pedulum (mass  $m_2$ , length  $\ell$ ) which swings freely in the plane. The pendulum angle,  $\theta$ , is measured anti-clockwise from hanging down (diagram would be useful). The cart can move horizontally, with an applied external force u, and coefficient of friction r. Typical values are:  $m_1 = 0.5 \text{kg}$ ,  $m_2 = 0.5 \text{kg}$ ,  $\ell = 0.6 \text{m}$  and r = 0.1 N/m/s. The coordinates  $\kappa_2$  and  $\kappa_2$  of the midpoint of the pendulum are

$$x_2 = x_1 - \frac{1}{2}\ell\sin\theta, \qquad y_2 = \frac{1}{2}\ell\cos\theta,$$

and the squared velocity of the cart and the midpoint of the pendulum are

$$\nu_1^2 \; = \; \dot{x}_1^2, \qquad \nu_2^2 \; = \; \dot{x}_2^2 + \dot{y}_2^2 \; = \; \dot{x}_1^2 + \tfrac{1}{4} \ell^2 \dot{\theta}^2 - \ell \dot{x}_1 \dot{\theta} \cos \theta.$$

The system Lagrangian is

$$\begin{array}{ccc} L \ = \ T - V \ = \ \frac{1}{2} m_1 \nu_1^2 + \frac{1}{2} m_2 \nu_2^2 + \frac{1}{2} I \dot{\theta}^2 - m_2 g y_2 \ \Rightarrow \\ \\ L \ = \ \frac{1}{2} (m_1 + m_2) \dot{x}_1^2 + \frac{1}{6} m_2 \ell^2 \dot{\theta}^2 - \frac{1}{2} m_2 \ell (\dot{x}_1 \dot{\theta} + g) \cos \theta \end{array}$$

where we have used the angular moment of inertia around the pendulum midpoint is  $I = \frac{1}{12}m\ell^2$ , and  $g = 9.82m/s^2$  is the accelleration of gravity.

The equations of motion are

$$\frac{d}{dt}\frac{\partial L}{\partial \dot{q}_i} - \frac{\partial L}{\partial q_i} \; = \; Q_i, \label{eq:Qi}$$

where  $Q_i$  are the non-conservative forces. In our case

$$\begin{split} \frac{\partial L}{\partial \dot{x}_1} &= (m_1 + m_2) \dot{x}_1 - \frac{1}{2} m_2 \ell \dot{\theta} \cos \theta, \qquad \frac{\partial L}{\partial x_1} &= 0, \\ \frac{\partial L}{\partial \dot{\theta}} &= \frac{1}{3} m_2 \ell^2 \dot{\theta} - \frac{1}{2} m_2 \ell \dot{x}_1 \cos \theta, \qquad \qquad \frac{\partial L}{\partial \theta} &= \frac{1}{2} m_2 \ell (\dot{x}_1 \dot{\theta} + g) \sin \theta, \end{split} \tag{1}$$

$$\frac{\partial L}{\partial \dot{\theta}} \; = \; \tfrac{1}{3} m_2 \ell^2 \dot{\theta} - \tfrac{1}{2} m_2 \ell \dot{x}_1 \cos \theta, \qquad \qquad \frac{\partial L}{\partial \theta} \; = \; \tfrac{1}{2} m_2 \ell (\dot{x}_1 \dot{\theta} + g) \sin \theta, \qquad \qquad (2)$$

leading to the equations of motion

$$\boxed{(\mathfrak{m}_1+\mathfrak{m}_2)\ddot{\mathsf{x}}_1-\frac{1}{2}\mathfrak{m}_2\ell\ddot{\theta}\cos\theta+\frac{1}{2}\mathfrak{m}_2\ell\dot{\theta}^2\sin\theta\ =\ \mathfrak{u}-r\dot{\mathsf{x}}_1,\qquad 2\ell\ddot{\theta}-3\ddot{\mathsf{x}}_1\cos\theta-3g\sin\theta\ =\ 0.}$$

Collecting the four variables  $z = (x_1, \theta, \dot{x}_1, \dot{\theta})$  the equations of motion can be conveniently expressed as four coupled differential equations

$$\frac{\mathrm{dz}}{\mathrm{dt}} = \begin{cases} z_3 \\ z_4 \end{cases}$$

$$\frac{-2m_2\ell z_4^2 \sin z_2 + 3m_2g \sin z_2 \cos z_2 + 4u - 4rz_3}{4(m_1 + m_2) - 3m_2 \cos^2 z_2}$$

$$\frac{-3m_2\ell z_4^2 \sin z_2 \cos z_2 + 6(m_1 + m_2)g \sin z_2 + 6(u - rz_3) \cos z_2}{4\ell(m_1 + m_2) - 3m_2\ell \cos^2 z_2},$$

which can be simulated numerically.

## Linearized Dynamics

Linearizing the dynamics around the goal state, we can write the following approximation

$$\frac{\mathrm{d}z}{\mathrm{d}t} \; \simeq \; \mathsf{q}^{-1}(\mathsf{A}z + \mathsf{B}\mathfrak{u}), \qquad \mathsf{A} \; = \; \begin{bmatrix} 0 & 0 & \mathsf{q} & 0 \\ 0 & 0 & 0 & \mathsf{q} \\ 0 & 3\ell \mathsf{m}_2 \mathsf{g} & -4\ell \mathsf{r} & 0 \\ 0 & 6(\mathsf{m}_1 + \mathsf{m}_2)\mathsf{g} & -6\mathsf{r} & 0 \end{bmatrix}, \qquad \mathsf{B} \; = \; \begin{bmatrix} 0 \\ 0 \\ 4\ell \\ 6 \end{bmatrix}$$

where  $q = \ell(4m_1 + m_2)$ .

## Loss Function

The instantaneous loss is given by

$$\mathsf{F} \ = \ 1 - \exp(-\frac{\mathsf{d}^2}{2\mathfrak{a}^2}),$$

were  $d^2$  is the squared distance between the tip of the pendulum and the point at distance  $\ell$  above the origin, and a is the width parameter. Note that the instantaneous loss does not depend on the speed variables,  $\dot{x}_1$  and  $\theta$ . The squared distance is

$$d^{2} = x^{2} + (\ell - y)^{2} = (x_{1} - \ell \sin \theta)^{2} + (\ell - \ell \cos \theta)^{2} = (\tilde{z} - \mu)^{\top} O(\tilde{z} - \mu),$$

where  $\tilde{z}$  is z augmented by two coordinates  $\sin\theta$  and  $\cos\theta$  and

$$Q \; = \; C^{\top}C, \qquad C \; = \; \begin{bmatrix} 1 & 0 & 0 & 0 & -\ell & 0 \\ 0 & 0 & 0 & 0 & \ell \end{bmatrix}, \qquad \mu \; = \; \begin{bmatrix} 0 & 0 & 0 & 0 & 1 \end{bmatrix}^{\top}.$$

The expected loss, averaging over the possibly uncertain states is therefore

$$\mathbb{E}[\mathsf{F}(\tilde{\mathbf{z}})] \; = \; 1 - \int \mathsf{F}(\tilde{\mathbf{z}}) \mathsf{p}(\tilde{\mathbf{z}}) d\tilde{\mathbf{z}},$$

which can be evaluated in closed form for Gaussian  $p(\tilde{z})$ , see reward.pdf. Since the augmented state  $\tilde{z}$  will not generally be Gaussian even if z is Gaussian, we project on to the closest Gaussian by matching first and second moments.