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Heat transport and power balance analysis in AUG

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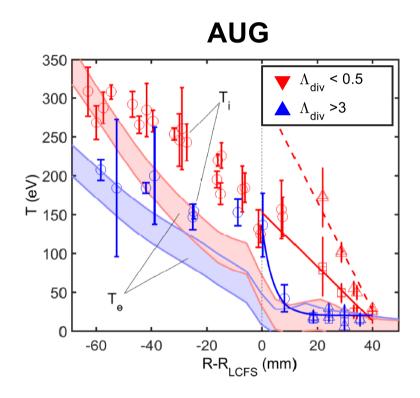
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In 2014-2016, around 30 L-mode discharges were carried out in AUG with equivalent configuration. Data base of filament properties, I_{sat} , T_{e} , T_{i} profiles, etc.

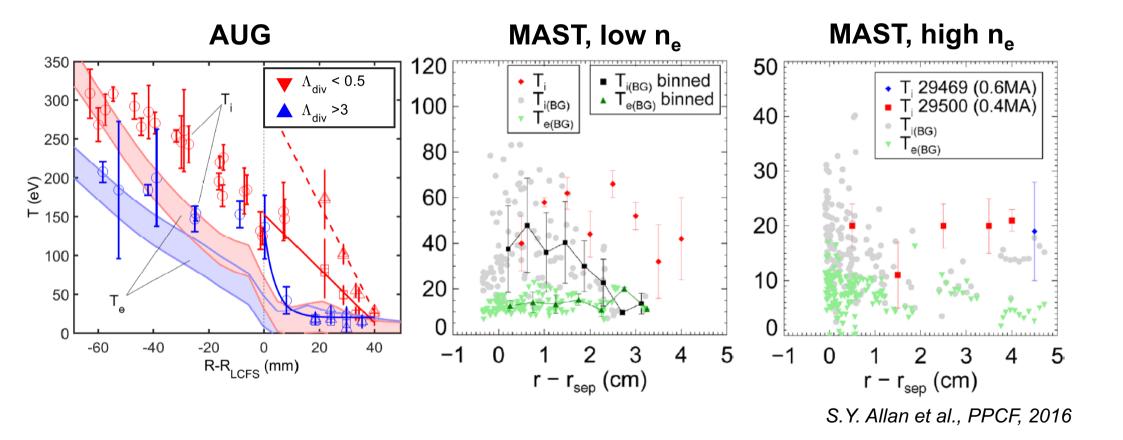
D. Carralero et al. NF, 2014; D. Carralero et al., PRL, 2015; D. Carralero et al., NF, 2017.





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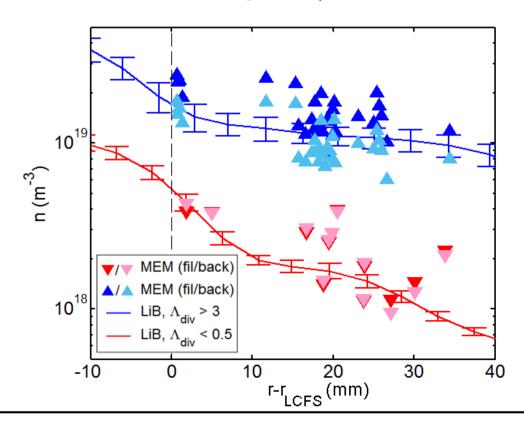




In 2014-2016, around 30 L-mode discharges were carried out in AUG with equivalent configuration. Data base of filament properties, I_{sat}, T_e, T_i profiles, etc.

Data is **consistent** with other diagnostics:

$$n_e = \frac{2I_{sat}}{A_{probe}Z} \sqrt{\frac{T_e + T_i}{m_D}}$$



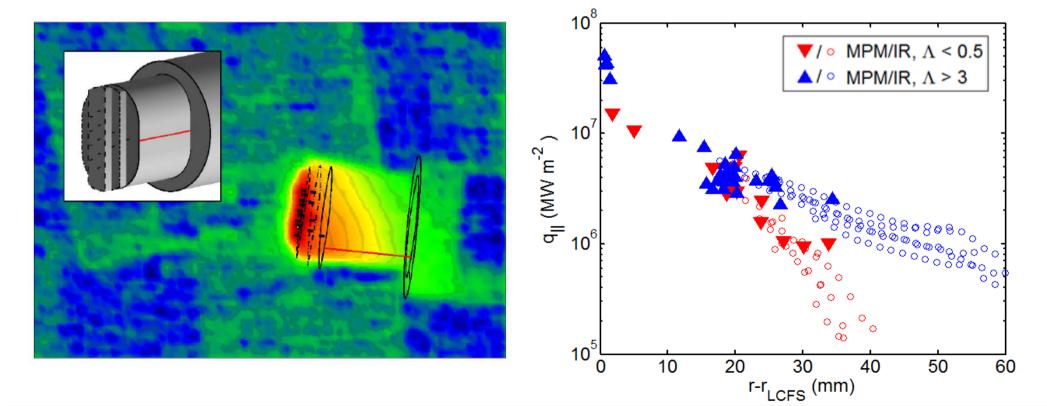
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In 2014-2016, around 30 L-mode discharges were carried out in AUG with equivalent configuration. Data base of filament properties, I_{sat} , T_{e} , T_{i} profiles, etc.

Data is **consistent** with other diagnostics:

$$q_W = \frac{I_{sat}}{A_{probe}Ze} (T_e[\gamma_i \tau_i (1 - R_E) + \gamma_e] + E_{rec})$$

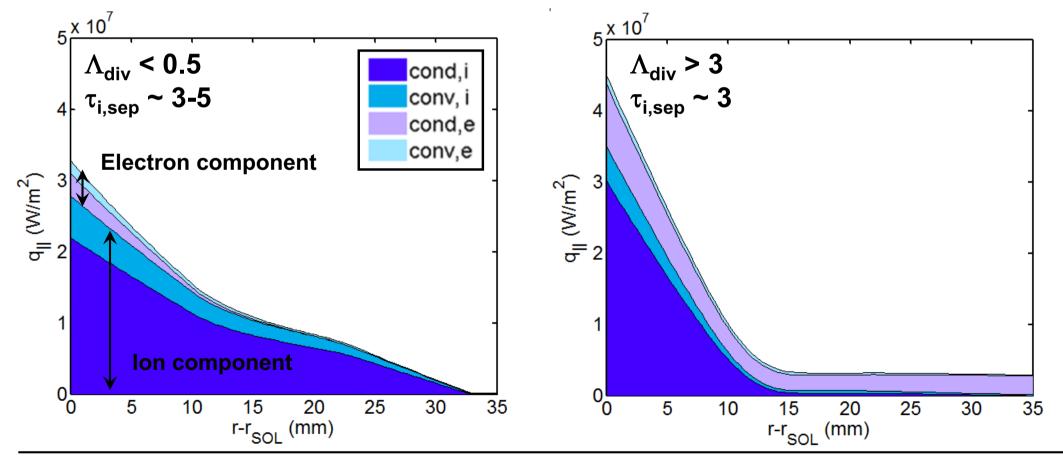


Parallel heat flux



Under these conditions, ion conduction dominates parallel transport.

$$q_{\parallel} = \frac{2}{7} \kappa_{0,i} \frac{T_i^{7/2} - T_{div}^{7/2}}{L_{\parallel}} + \frac{1}{2} n c_s M (5T_i + m_D(c_s M)^2) + \frac{2}{7} \kappa_{0,e} \frac{T_e^{7/2} - T_{div}^{7/2}}{L_{\parallel}} + \frac{5}{2} n c_s M T_e$$

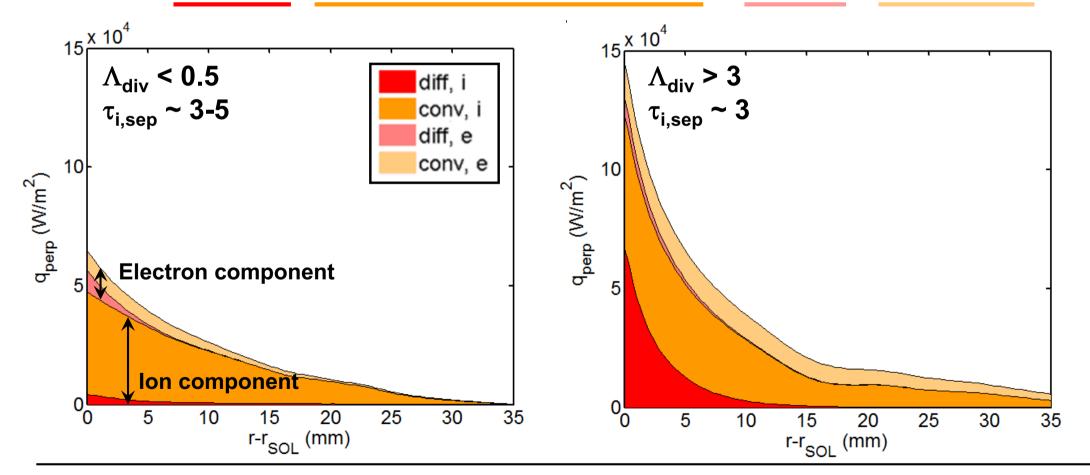


Perpendicular heat flux



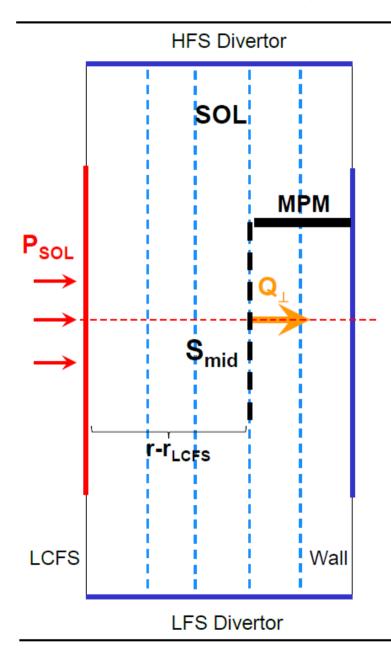
Similarly, ion convection dominates perpendicular transport

$$q_{\perp} = n\chi_i \nabla_{\perp} T_i + \frac{1}{2} \left(5\Gamma_{\perp,eff} T_{i,eff} + \Gamma_{\perp} m_D (c_s M)^2 \right) + n\chi_e \nabla_{\perp} T_e + \frac{5}{2} \Gamma_{\perp,eff} T_{e,eff}$$

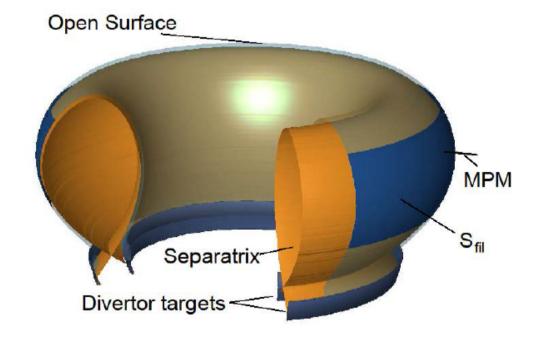


An estimation of global transport



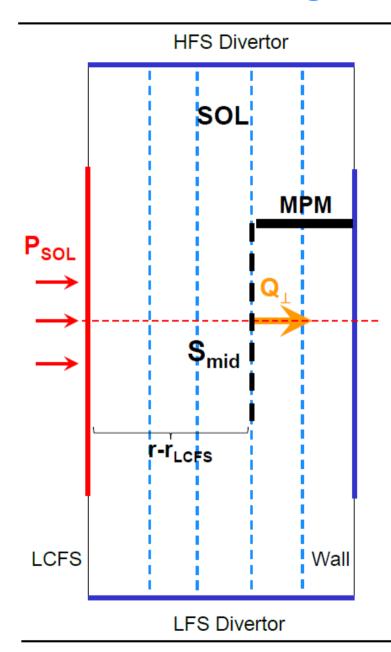


For a given r-r_{LCFS}, a relevant surface for total midplane perpendicular transport can be defined, $Q_{\perp} = q_{\perp} S_{mid}$.

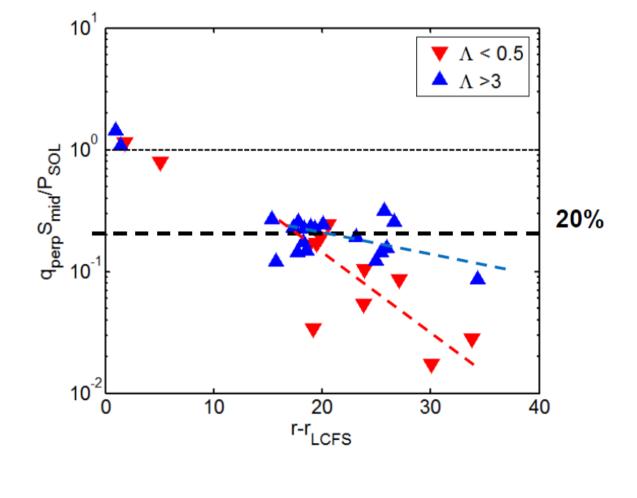


An estimation of global transport



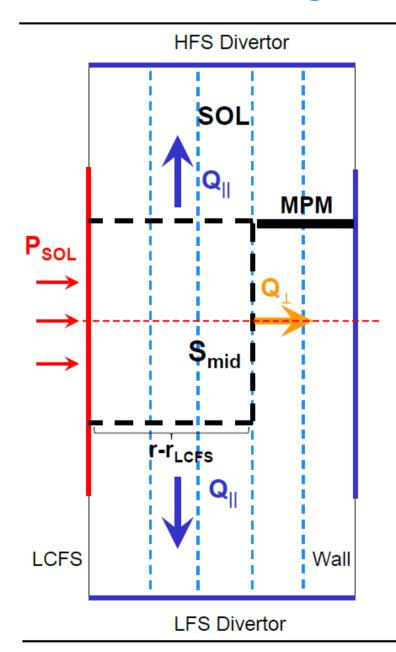


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An estimation of global transport





For a given r-r_{LCFS}, a relevant surface for total midplane perpendicular transport can be defined, $Q_{\perp} = q_{\perp} S_{mid}$.

Finally, the total parallel flux leaving the midplane before the r-r_{LCFS} flux surface:

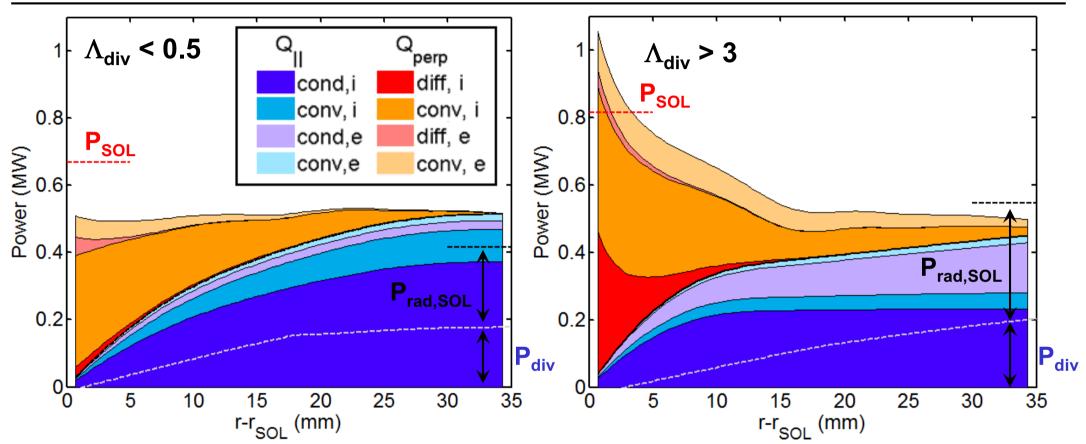
$$Q_{\parallel}(r) = 2\pi \int_{r_{LCFS}}^{r} q_{\parallel} \frac{B_z}{B} dr$$

Power balance can be done on the defined domain for each r-r_{LCFS}.

This is not the heat flux arriving onto the target!

Global transport: SOL power balance





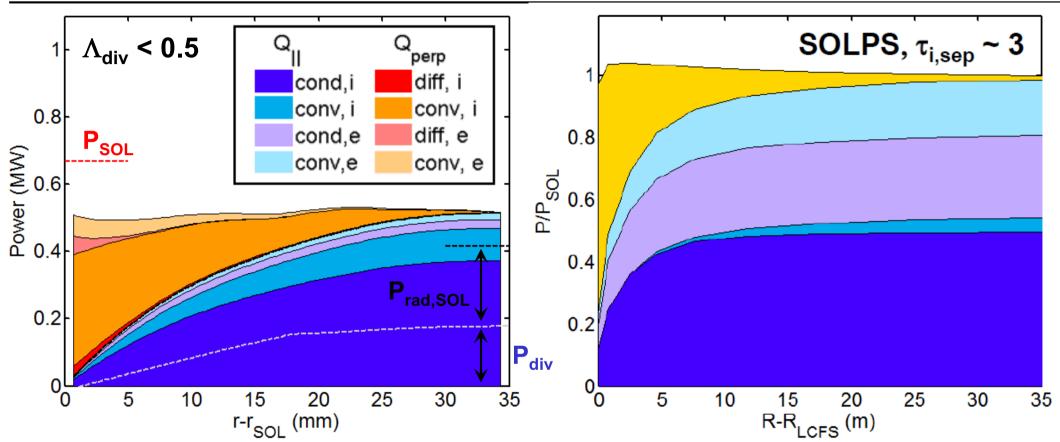
The quantitative analysis makes sense: total power input/output is matched within ~20%.

Main features are recovered:

- Electron transport is not dominant
- ► A substantial fraction of P_{SOL} still remains in Q_⊥ for r-r_{LCFS} ~ 20 mm

Global transport: Comparison to SOLPS





SOLPS simulations have been carried out to compare with the experimental power balance. No shoulder formation has been simulated yet, and only $\tau_i \sim 3$ was achieved.

- We can see a qualitative agreement with experimental results.
- ▶ Just with τ_i ~ 3, electron parallel transport is no longer dominant.

This is still work in progress!

Outlook



Further lines of work from these results:

Experiment

- Improvement of T_i and T_e database.
- Power balance analysis of H-mode shoulder formation.
- Comparison of parallel transport results with probe/IR divertor data.

Modelling

- Full development of equivalent SOLPS scenarios.
- Comparison of perpendicular transport to experimental values.
- Simulation of turbulent transport using HESEL/GEMR.
- Development of effective transport coefficient based on turbulence properties.
- EMC3-EIRENE simulation of neutral fluxes, incl. effect of ionization, CX, etc.

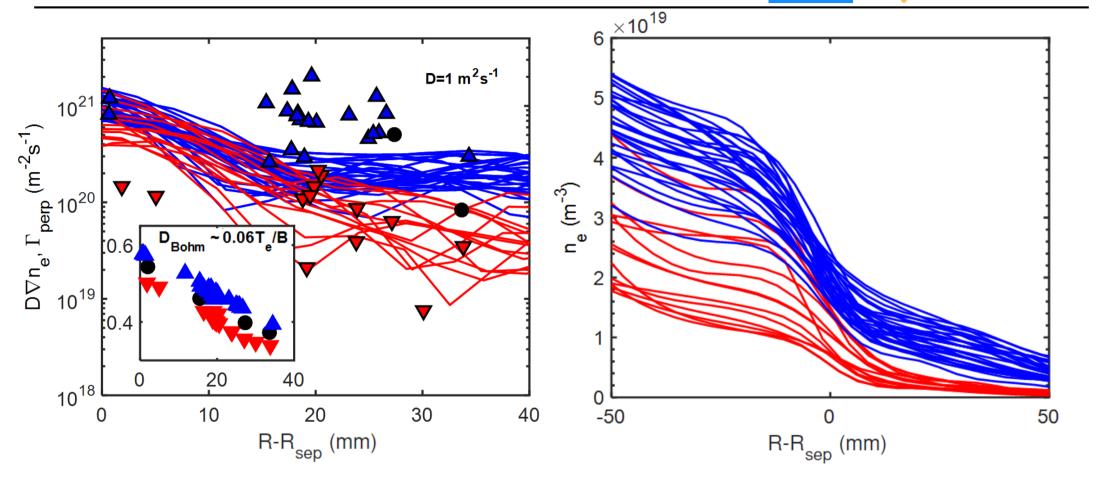
Finally, implications of these results for ITER/DEMO should be addressed.



Additional Slides

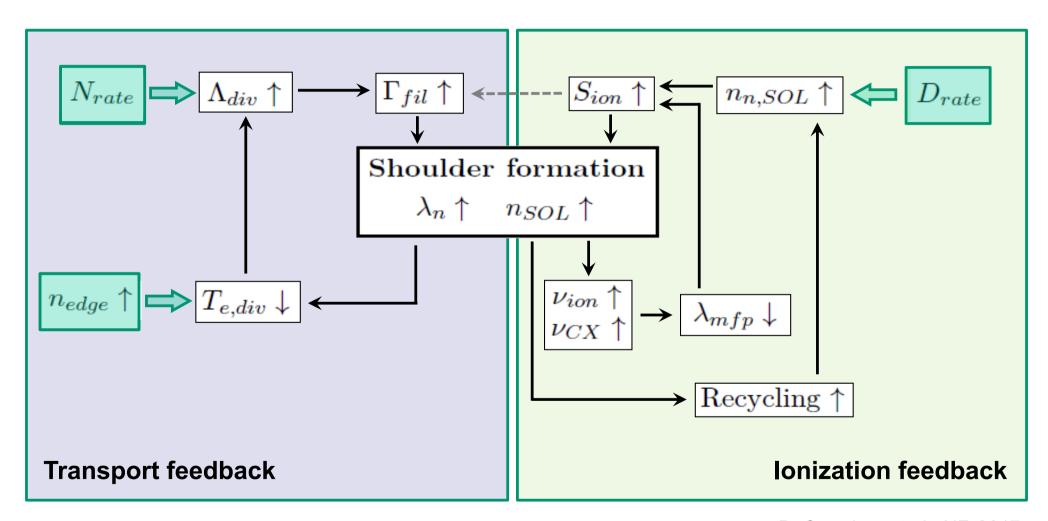
Filamentary transport





A general framework





D. Carralero et al., NF, 2017.