

# WEEK 8

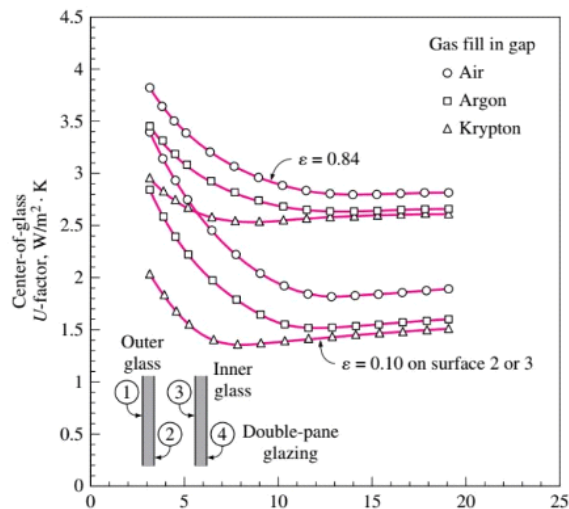
Tuesday, November 26, 2019 9:50 PM

Politecnico di Milano

MSc. Sustainable Architecture and Landscape Design

Fabiola Anahí Mogrovejo León

**Task 1** Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating ? ( keep the gap thickness to be 13 mm)



Changing the air to argon and krypton in a double-pane glazing without coating:

**U\_factor\_withair= 2.8 W/m<sup>2</sup> \* K**

U\_factor\_withArgon= 2.65 W/m<sup>2</sup> \* K, which is 5.35% less of Heat transfer.

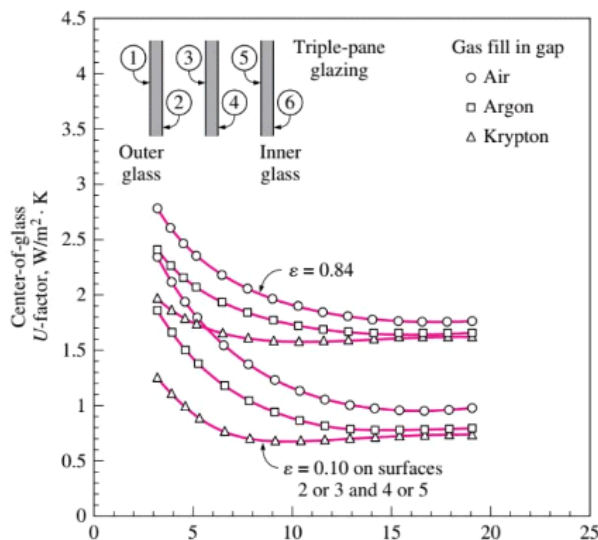
U\_factor\_withKrypton= 2.55 W/m<sup>2</sup> \* K, which is 8.93% less of Heat transfer.

Changing the air to argon and krypton in a double-pane glazing with coating:

**U\_factor\_withair= 1.8 W/m<sup>2</sup> \* K**

U\_factor\_withArgon= 1.52 W/m<sup>2</sup> \* K, which is 15.55% less of Heat transfer.

U\_factor\_withKrypton= 1.4 W/m<sup>2</sup> \* K, which is 22.22% less of Heat transfer.



Changing the air to argon and krypton in a triple-pane glazing without coating:

**U\_factor\_withair= 1.53 W/m<sup>2</sup> \* K**

U\_factor\_withArgon= 1.515 W/m<sup>2</sup> \* K, which is 0.98% less of Heat transfer.

U\_factor\_withKrypton= 1.505 W/m<sup>2</sup> \* K, which is 1.63% less of Heat transfer.

Changing the air to argon and krypton in a triple-pane glazing with coating:

**U\_factor\_withair= 1 W/m<sup>2</sup> \* K**

U\_factor\_withArgon= 0.75 W/m<sup>2</sup> \* K, which is 25% less of Heat transfer.

U\_factor\_withKrypton= 0.6 W/m<sup>2</sup> \* K, which is 40% less of Heat transfer.

**Task 2** Consider the house that we analyzed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m<sup>2</sup> on the west fixed 3.6 m<sup>2</sup> on the south and an operable 3.6 m<sup>2</sup> on

the other windows which are fixed 14.4 m<sup>2</sup> on the west, fixed 3.6 m<sup>2</sup> on the south and an operable 3.6 m<sup>2</sup> on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminum?

$$\Delta T_{cooling} = 31.9 - 24 = 7.9 \text{ }^{\circ}\text{C}$$

$$\Delta T_{heating} = 20 - (-4.8) = 24.8 \text{ }^{\circ}\text{C}$$

$$DR = 11.9 \text{ }^{\circ}\text{C}$$

From the table:

$$U = 2.84$$

$$SHGC = 0.54$$

- **Fixed on the west 14.4 m<sup>2</sup>**

$$U_{window_{west}} = 2.84 \frac{W}{m^2 K}$$

**Heating factor:**

$$HF_{window_{west}} = U_{window_{west}} (\Delta T_{heating}) = 2.84 (24.8) = 70.432 \frac{W}{m^2}$$

$$Q_{\square window_{west}} = HF_{window_{west}} \times A_{window_{west}} = 70.432 * 14.4 = \mathbf{1014.2 \text{ W}}$$

**Cooling factor:**

$$CF_{window_{west\_heatTrasnferPart}} = U_{window_{west}} (\Delta T_{cooling} - 0.46 DR) = 2.84 (7.9 - 0.46 * 11.9) = 6.9 \frac{W}{m^2}$$

$$PXI_{window_{west}} = E_D + E_d = 559 + 188 = 747$$

$$SHGC = 0.54$$

NO internal shading so IAC = 1

From the table for western window of a detached house FFs = 0.56

$$CF_{window_{west\_IrradiationPart}} = PXI \times SHGC \times IAC \times FF_s = 747 * 0.54 * 1 * 0.56 = 225.9 \text{ W/m}^2$$

$$CF_{window_{west}} = CF_{window_{west\_heatTrasnferPart}} + CF_{window_{west\_IrradiationPart}} = 6.9 + 225.9 = 232.8 \frac{W}{m^2}$$

$$Q_{\square window_{west}} = CF_{window_{west}} \times A_{window_{west}} = 232.8 * 14.4 = \mathbf{3373.12 \text{ W}}$$

**If the frame is aluminium:**

$$U_{window_{west}} = 3.61 \frac{W}{m^2 K}$$

$$SHGC = 0.56$$

**Heating factor:**

$$HF_{window_{west}} = U_{window_{west}} (\Delta T_{heating}) = 3.61 (24.8) = 89.53 \frac{W}{m^2}$$

$$Q_{\square window_{west}} = HF_{window_{west}} \times A_{window_{west}} = 89.53 * 14.4 = \mathbf{1289.23 W}$$

**Cooling factor:**

$$CF_{window_{west\_heatTrasnferPart}} = U_{window_{west}} (\Delta T_{cooling} - 0.46 DR) = 3.61 (7.9 - 0.46 * 11.9) = 8.76 \frac{W}{m^2}$$

$$PXI_{window_{west}} = E_D + E_d = 559 + 188 = 747$$

$$SHGC = 0.56$$

NO internal shading so IAC = 1

From the table for western window of a detached house FFs = 0.56

$$CF_{window_{west\_IrradiationPart}} = PXI \times SHGC \times IAC \times FF_s = 747 * 0.56 * 1 * 0.56 = 234.26 W/m^2$$

$$CF_{window_{west}} = CF_{window_{west\_heatTrasnferPart}} + CF_{window_{west\_IrradiationPart}} = 8.76 + 234.26 = 243.02 \frac{W}{m^2}$$

$$Q_{\square window_{west}} = CF_{window_{west}} \times A_{window_{west}} = 243.02 * 14.4 = \mathbf{3499.49 W}$$

- Fixed on the south 3.6 m2

$$U_{window_{south}} = 2.84 \frac{W}{m^2K}$$

**Heating factor:**

$$HF_{window_{south}} = U_{window_{south}} (\Delta T_{heating}) = 2.84 (24.8) = 70.432 \frac{W}{m^2}$$

$$Q_{\square window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 70.432 * 3.6 = \mathbf{253.56 W}$$

**Cooling factor:**

$$CF_{window_{south\_heatTrasnferPart}} = U_{window_{south}} (\Delta T_{cooling} - 0.46 DR) = 2.84 (7.9 - 0.46 * 11.9) = 6.9 \frac{W}{m^2}$$

$$PXI_{window_{south}} = E_D + E_d = 348 + 209 = 557$$

$$SHGC = 0.54$$

NO internal shading so IAC = 1

From the table for southern window of a detached house FFs = 0.47

$$CF_{\text{window}_{\text{south\_IrradiationPart}}} = PXI \times SHGC \times IAC \times FF_S = 557 * 0.54 * 1 * 0.47 = 141.36 \text{ W/m}^2$$

$$CF_{\text{window}_{\text{south}}} = CF_{\text{window}_{\text{south\_heatTrasnferPart}}} + CF_{\text{window}_{\text{south\_IrradiationPart}}} = 6.9 + 141.36 \\ = 148.26 \frac{\text{W}}{\text{m}^2}$$

$$Q_{\text{window}_{\text{south}}} = CF_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}} = 148.26 * 3.6 = \mathbf{533.74 \text{ W}}$$

**If the frame is aluminium:**

$$U_{\text{window}_{\text{south}}} = 3.61 \frac{\text{W}}{\text{m}^2\text{K}}$$

SHGC= 0.56

**Heating factor:**

$$HF_{\text{window}_{\text{south}}} = U_{\text{window}_{\text{south}}} (\Delta T_{\text{heating}}) = 3.61 (24.8) = 89.53 \frac{\text{W}}{\text{m}^2}$$

$$Q_{\text{window}_{\text{south}}} = HF_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}} = 89.53 * 3.6 = \mathbf{322.3 \text{ W}}$$

**Cooling factor:**

$$CF_{\text{window}_{\text{south\_heatTrasnferPart}}} = U_{\text{window}_{\text{south}}} (\Delta T_{\text{cooling}} - 0.46 DR) = 3.61 (7.9 - 0.46 * 11.9) \\ = 8.76 \frac{\text{W}}{\text{m}^2}$$

$$PXI_{\text{window}_{\text{south}}} = E_D + E_d = 348 + 209 = 557$$

$$SHGC = 0.56$$

NO internal shading so IAC = 1

From the table for southern window of a detached house FFs = 0.47

$$CF_{\text{window}_{\text{south\_IrradiationPart}}} = PXI \times SHGC \times IAC \times FF_S = 557 * 0.56 * 1 * 0.47 = 146.6 \text{ W/m}^2$$

$$CF_{\text{window}_{\text{south}}} = CF_{\text{window}_{\text{south\_heatTrasnferPart}}} + CF_{\text{window}_{\text{south\_IrradiationPart}}} = 8.76 + 146.6 \\ = 155.36 \frac{\text{W}}{\text{m}^2}$$

$$Q_{\text{window}_{\text{south}}} = CF_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}} = 155.36 * 3.6 = \mathbf{559.3 \text{ W}}$$

**- Operable window on the south 3.6 m2**

$$U_{\text{window}_{\text{south}}} = 2.84 \frac{\text{W}}{\text{m}^2\text{K}}$$

**Heating factor:**

$$HF_{\text{window}_{\text{south}}} = U_{\text{window}_{\text{south}}} (\Delta T_{\text{heating}}) = 2.84 (24.8) = 70.432 \frac{\text{W}}{\text{m}^2}$$

$$Q_{\square window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 70.432 * 3.6 = \mathbf{253.56 \text{ W}}$$

**Cooling factor:**

$$CF_{window_{south\_heatTrasnferPart}} = U_{window_{south}} (\Delta T_{cooling} - 0.46 DR) = 2.84 (7.9 - 0.46 * 11.9) \\ = 6.9 \frac{W}{m^2}$$

$$PXI_{window_{south}} = E_D + E_d = 348 + 209 = 557$$

$$SHGC = 0.46$$

*NO internal shading so IAC = 1*

*From the table for southern window of a detached house FFs = 0.47*

$$CF_{window_{south\_IrradiationPart}} = PXI \times SHGC \times IAC \times FF_S = 557 * 0.46 * 1 * 0.47 = 120.42 \text{ W/m}^2$$

$$CF_{window_{south}} = CF_{window_{south\_heatTrasnferPart}} + CF_{window_{south\_IrradiationPart}} = 6.9 + 120.42 \\ = 127.32 \frac{W}{m^2}$$

$$Q_{\square window_{south}} = CF_{window_{south}} \times A_{window_{south}} = 127.32 * 3.6 = \mathbf{458.35 \text{ W}}$$

**If the frame is aluminium:**

$$U_{window_{south}} = 4.62 \frac{W}{m^2K}$$

$$SHGC = 0.55$$

**Heating factor:**

$$HF_{window_{south}} = U_{window_{south}} (\Delta T_{heating}) = 4.62 (24.8) = 114.57 \frac{W}{m^2}$$

$$Q_{\square window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 114.57 * 3.6 = \mathbf{412.45 \text{ W}}$$

**Cooling factor:**

$$CF_{window_{south\_heatTrasnferPart}} = U_{window_{south}} (\Delta T_{cooling} - 0.46 DR) = 4.62 (7.9 - 0.46 * 11.9) \\ = 11.21 \frac{W}{m^2}$$

$$PXI_{window_{south}} = E_D + E_d = 348 + 209 = 557$$

$$SHGC = 0.55$$

*NO internal shading so IAC = 1*

*From the table for southern window of a detached house FFs = 0.47*

$$CF_{window_{south\_IrradiationPart}} = PXI \times SHGC \times IAC \times FF_S = 557 * 0.55 * 1 * 0.47 = 143.98 \text{ W/m}^2$$

$$CF_{window_{south}} = CF_{window_{south\_heatTrasnferPart}} + CF_{window_{south\_IrradiationPart}} = 11.21 + 143.98 \\ = 155.19 \frac{W}{m^2}$$

$$Q_{\square window_{south}} = CF_{window_{south}} \times A_{window_{south}} = 155.19 * 3.6 = \mathbf{558.68 \text{ W}}$$