

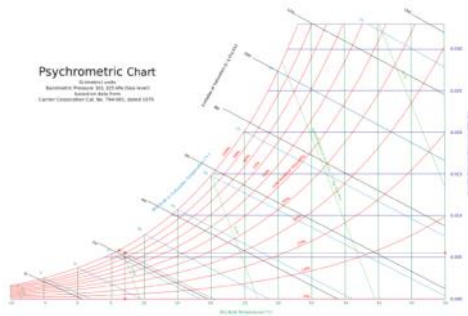
Task 1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

[Weather Forecast Website example](#)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.

Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019							
	13:00	14:00	16:00	18:00	20:00	21:00	22:00
Temperatura effettiva	10°C	10°C	9°C	6°C	7°C	7°C	8°C
Temperatura percepita	10°C	10°C	8°C	5°C	7°C	6°C	7°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	79 %	77 %	89 %	90 %	90 %	92 %	91 %
Pressione atmosferica	1016 hPa	1018 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa	1020 hPa

The time now is 8 pm from the data given in the website :
relative humidity is 90%
Total air pressure = 101.9 kPa
Temperature in kelvin scale T = 230 K



absolute humidity $w = 0.0055$

wet bulb temperature $T_{wb} = 6^\circ\text{C}$

$$w = \frac{0.622 P_v}{P_a} = \frac{0.622 P_v}{P - P_v} = 0.0055$$

introduce $P = 101.9 \text{ kPa}$

$$P_v \approx 0.893 \text{ kPa}$$

$$\phi = \frac{P_v}{P} = 90\%$$

for any ideal gas \Rightarrow water vapour, $R_{sp} = 0.4615$

$$P_v = 0.893 \text{ kPa}$$

$$m_v = \frac{0.893 \text{ V}}{0.4615 \times 230} \approx 8.41 \times 10^{-3} \text{ V}$$

$$m_{wg} = \frac{m_v}{90\%} \approx 9.34 \times 10^{-3} \text{ V}$$

Task 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 SeaP: 101.2 Time Zone: 1.00 (EUT) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Heating DB		Humidification (SP/AC/DB and HR)					Cooling (WB/AC/DB)					MICROSP/DB		
DB	WB	DB	WB	HR	DB	WB	DB	WB	HR	DB	WB	DB	WB	HR
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	19.2	12.4	10.6	3.4	250

Annual Cooling Dehumidification and Entropy Design Conditions

Cooling DB/AC/DB		Dehumidification (SP/AC/DB and HR)					Evaporation (DB/AC/DB)					MICROSP/DB		
DB	WB	DB	WB	HR	DB	WB	DB	WB	HR	DB	WB	DB	WB	HR
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2

Extreme Annual Design Conditions

Extreme Annual WB		Extreme Annual DB					n-Year Return Period Values of Extreme DB					Hours		
1%	2.5%	5%	Max	Min	Max	Min	1%	2.5%	5%	10%	20%	30%	40%	50%
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)
11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2

internal air load

Extreme Annual WTD			Max		Mean		Standard deviation		Cool years		m10 years		m20 years		m50 years	
1%	5%	25%	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)	(°C)
(a)	11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

internal gains:

calculate the sensible cooling load from internal gains:

$$Q_{igs} = 136 + 2.2 A_{cf} + 22 N_{bc} = 136 + 2.2 \times 22 + 22 \times 2 = 620 \text{ W}$$

calculate cooling of int gains,

$$Q_{igL} = 20 + 0.22 A_{cf} + 12 N_{bc} = 20 + 0.22 \times 2200 + 12 \times 2 = 88 \text{ W}$$

infiltration:

$$A_{ul} = 14 \text{ cm}^2_{me}$$

$$A_{es} = A_{wall} + A_{roof} = 200 + 144 = 344 \text{ m}^2$$

$$\text{thus, } A_L = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$T_{cooling} = 24^\circ\text{C} \quad T_{heating} = 20^\circ\text{C}$$

$$\Delta T_{cooling} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$\Delta T_{heating} = 20^\circ\text{C} - (-4.1^\circ\text{C}) = 24.1^\circ\text{C} = 24.1 \text{ K}$$

$$DR = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$IDF_{heating} = 0.1073 \frac{\text{L}}{\text{S} \times \text{cm}^2}$$

$$IDF_{cooling} = 0.033 \frac{\text{L}}{\text{S} \times \text{cm}^2}$$

air flow rate:

$$Q_{i,heating} = A_L + IDF_{heating} = 481.6 \times 0.1073 \approx 35.157 \frac{\text{L}}{\text{S}}$$

$$Q_{i,cooling} = A_L \times IDF_{cooling} = 481.6 \times 0.033 \approx 15.893 \frac{\text{L}}{\text{S}}$$

min whole building ventilation:

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 \times 200 + 3.5 \times (1+1) = 17 \frac{\text{L}}{\text{S}}$$

$$Q_{i-v,heating} = Q_{i,heating} + Q_v \approx 35.157 + 17 = 52.157 \frac{\text{L}}{\text{S}}$$

$$Q_{i-v,cooling} = Q_{i,cooling} + Q_v \approx 15.893 + 17 = 32.893 \frac{\text{L}}{\text{S}}$$

Given that $C_{sensible} = 1.23$, $C_{latent} = 3010$, $\Delta W_{cooling} = 0.0039$

$$Q_{inf-v,es} = C_s Q_{i,v} \Delta T_c \approx 1.23 \times 32.893 \times 7.1 = 287.25 \text{ W}$$

$$Q_{inf-v,cf} = C_l Q_{i,v} \Delta W_c \approx 3010 \times 32.893 \times 0.0039 = 386.13 \text{ W}$$

$$q_{inh-v_{ci}} = C_t Q_{i-vc} \Delta W_c \approx 300 \times 32,893 \times 0,0039 = 386,13 \text{ W}$$

$$q_{inh-v_{hs}} = C_s Q_{i-vh} \Delta T_{heating} = 1,23 \times 52,157 \times 24,1 = 1546,09 \text{ W}$$