

Week 9

Monday, December 2, 2019 1:14 AM

Week # 9 Assignment

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Date: 04/12/2019

Task 1:

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine:

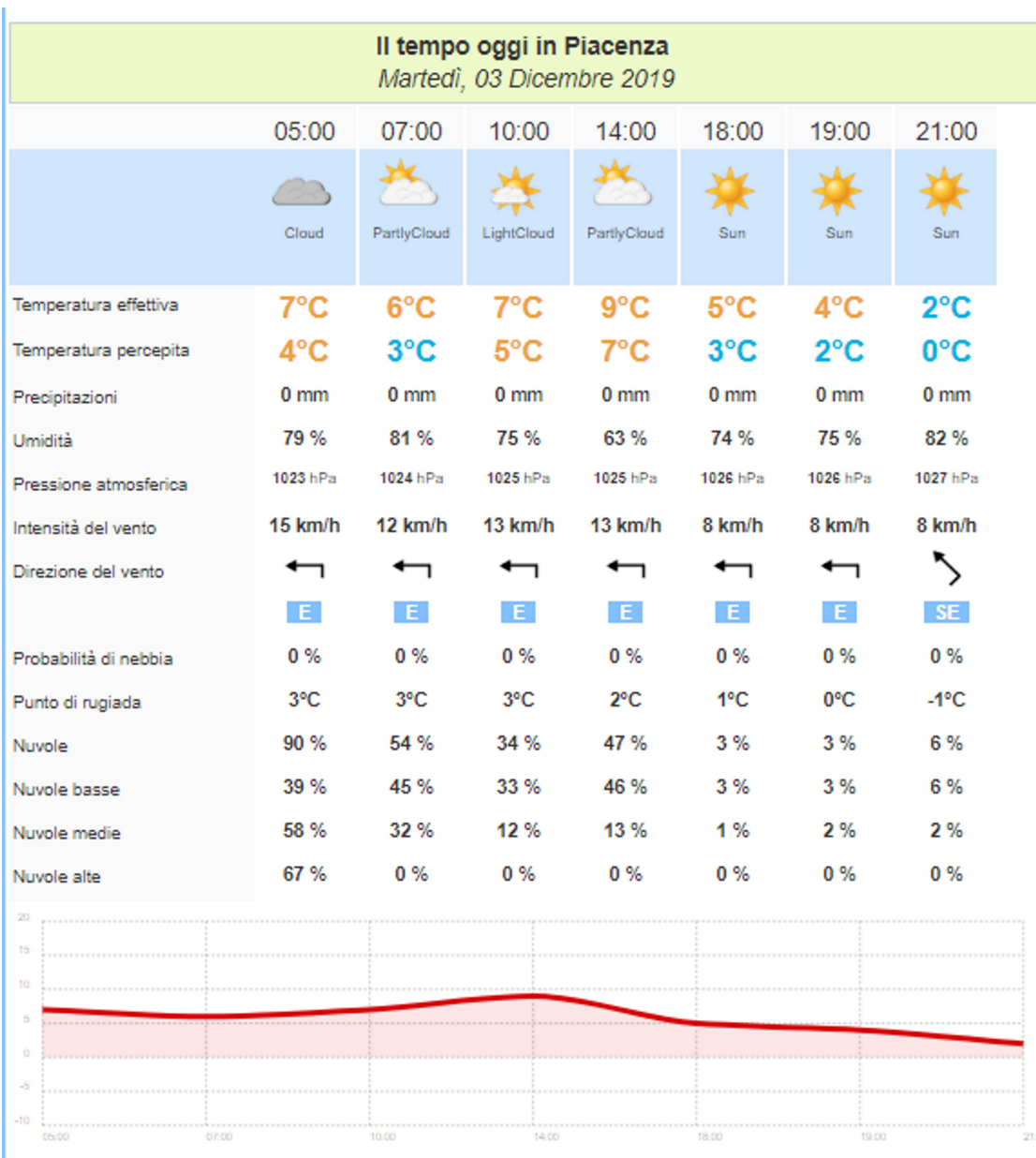
1- the absolute humidity

2- the wet-bulb temperature

3- the mass of water vapor in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

[Weather Forecast Website example](#)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.



Solving the exercise at 05:00 AM on Tuesday 03/12/2019

- The relative humidity: 79%
- Air total Pressure: 1023 hPa (102.3 Kpa)
- Temperature to be utilized: 7 C

Estimating Aula A approx. dimensions:

- Length: 20 m
- Width: 8 m
- Height: 5 m

First, let's try to calculate the relative pressure:

$$\phi = \frac{m_v}{m_g} \rightarrow m_g \text{ the mass of water at sat condition}$$

From Steam tables I can find the saturation pressure of water @ 7 °C = 1.001 kPa

Reference website: https://www.engineeringtoolbox.com/water-vapor-saturation-pressure-d_599.html?vA=7&units=C#

$$\phi = \frac{P_v}{P_g} = \frac{P_v}{P_g} \rightarrow P_g = P_{sat} 7^\circ\text{C} = 1.001 \text{ kPa}$$

$$\phi = \frac{P_v}{P_g} \rightarrow P_v = \phi \times P_g = 0.79 \times 1.001 = 0.79079 \text{ kPa}$$

$$\text{partial pressure of dry air: } P_a = P - P_v = 102.3 \text{ kPa} - 0.79079 \text{ kPa} = 101.51 \text{ kPa}$$

Second, let's try to calculate the absolute humidity:

$$\omega = 0.622 \frac{P_v}{P_a} = 0.622 \frac{0.79079}{101.51} = 0.00779 \frac{\text{kg}_{\text{vapour}}}{\text{kg}_{\text{dryAir}}}$$

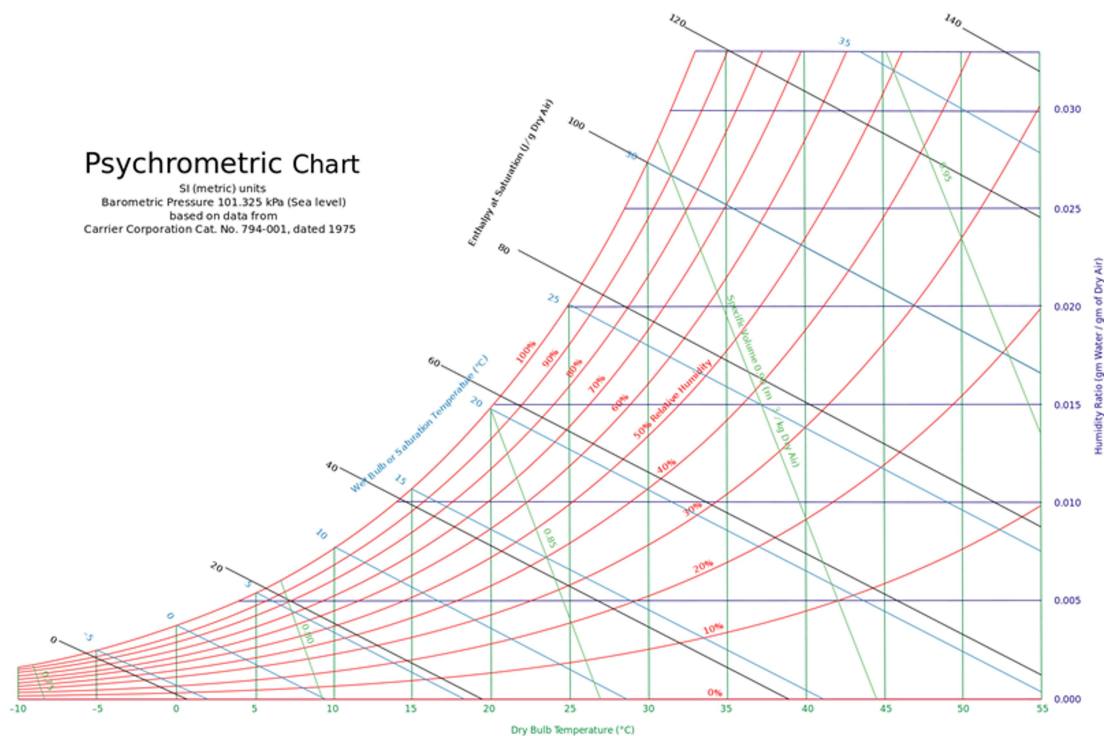
$$\text{For ideal gases : } m = \frac{PV}{R_{sp}T}$$

$$\text{So for air : } m_a = \frac{P_a V_a}{R_a T} \quad R_{sp.} = \frac{R_{global}}{M_{gas}} \rightarrow \text{You can also find them in Tables } R_a = 0.287, R_v = 0.4615$$

$$m_a = \frac{101.51 \times (20 \times 8 \times 5)}{0.287 \times (273 + 7)} = 1010.55 \text{ kg of dry air}$$

$$m_v = \frac{0.79079 \times (20 \times 8 \times 5)}{0.4615 \times (273 + 7)} = 4.895 \text{ kg}$$

The mass of water vapor in the air in Classroom A is 4.895 Kg.



From the psychrometric chart above, we find that the wet bulb temperature is around 5.7 C

Task 2:

Utilize the same methodology we went through in the class:

Determine

- The sensible and latent load corresponding to internal gains
- The infiltration in a house
- The ventilation loads

With a

- good construction quality
- same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
		0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180

	Dehumidification DP/MCDB and HR						Enthalpy/MCDB						Hours 8 to 4 & 12.8/20.6			
	0.4%			1%			0.4%			1%				2%		
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth		MCDB	Enth	MCDB
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	

Extreme Annual Design Conditions

Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB							
				Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years	
1%	2.5%	5%		Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

Considering the same house as the one located in Piacenza:

- Building height 2.5 m
- average construction quality
- located in Brindisi
- two occupants
- one bed room
- conditioned floor area 200 m²
- wall area 144 m²

➤ Calculating Internal gains:

$$\dot{Q}_{ig_{sensible}} = 136 + 2.2 * A_{cf} + 22 N_{oc} = 136 + 2.2 * 200 + 22 * 2 = 136 + 440 + 44 = 620 \text{ W}$$

$$\dot{Q}_{ig_{latent}} = 20 + 0.22 * A_{cf} + 12 N_{oc} = 20 + 0.22 * 200 + 12 * 2 = 20 + 44 + 24 = 88 \text{ W}$$

➤ Infiltration

Calculating the maximum flow rate of air:

Table 3 Unit Leakage Areas

Construction	Description	A_{ul} , cm ² /m ²
Tight	Construction supervised by air-sealing specialist	0.7
Good	Carefully sealed construction by knowledgeable builder	1.4
Average	Typical current production housing	2.8
Leaky	Typical pre-1970 houses	5.6
Very leaky	Old houses in original condition	10.4

For an good construction quality, the average leakage area is 1.4 cm²/m²

$$A_L = A_{es} A_{ul}$$

where

A_{es} = building exposed surface area, m²

A_{ul} = unit leakage area, cm²/m² (from [Table 3](#))

Exposed surface = Wall area + roof area

$$A_{es} = 144 + 200 = 344 \text{ m}^2$$

$$A_L = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$Q_i = A_L \text{IDF}$$

where

A_L = building effective leakage area (including flue) at reference pressure difference = 4 Pa, assuming discharge coefficient

$C_D = 1$, cm²

IDF = infiltration driving force, L/(s·cm²)

Table 5 Typical IDF Values, L/(s·cm²)									
H, m	Heating Design Temperature, °C					Cooling Design Temperature, °C			
	-40	-30	-20	-10	0	10	30	35	40
2.5	0.10	0.095	0.086	0.077	0.069	0.060	0.031	0.035	0.040
3	0.11	0.10	0.093	0.083	0.072	0.061	0.032	0.038	0.043
4	0.14	0.12	0.11	0.093	0.079	0.065	0.034	0.042	0.049
5	0.16	0.14	0.12	0.10	0.086	0.069	0.036	0.046	0.055
6	0.18	0.16	0.14	0.11	0.093	0.072	0.039	0.050	0.061
7	0.20	0.17	0.15	0.12	0.10	0.075	0.041	0.051	0.068
8	0.22	0.19	0.16	0.14	0.11	0.079	0.043	0.058	0.074

On the 1st row of the above table, we have the H: 2.5m height.

From the weather data for the city of BRINDISI, we note that:

- Heating DB is 4.1
- Cooling DB is 31.1

$$IDF_{heating} = 0.066 \frac{L}{s \cdot cm^2}$$

$$IDF_{cooling} = 0.032 \frac{L}{s \cdot cm^2}$$

Calculate the volume:

$$\dot{V}_{infiltration_{heating}} = A_L \times IDF = 481.6 * 0.066 = 31.78 \frac{L}{s}$$

$$\dot{V}_{infiltration_{cooling}} = A_L \times IDF = 481.6 * 0.032 = 15.41 \frac{L}{s}$$

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1)$$

where

- Q_v = required ventilation flow rate, L/s
- A_{cf} = building conditioned floor area, m²
- N_{br} = number of bedrooms (not less than 1)

$$\dot{V}_{ventilation} = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05*200 + 3.5*2 = 10+7=17 \text{ L/S}$$

$$\dot{V}_{inf-ventilation_{heating}} = 31.78 + 17 = 48.78 \text{ L/s}$$

$$\dot{V}_{inf-ventilation_{cooling}} = 15.41 + 17 = 32.41 \text{ L/s}$$

➤ Ventilation Loads

From the past lessons:

- Cooling Temperature $T_{cooling} = 24\text{ }^{\circ}\text{C}$
- Heating Temperature $T_{heating} = 20\text{ }^{\circ}\text{C}$

For BRINDISI data weather tables:

$$\Delta T_{cooling} = 31.1\text{ }^{\circ}\text{C} - 24\text{ }^{\circ}\text{C} = 7.1\text{ }^{\circ}\text{C}$$

$$\Delta T_{heating} = 20\text{ }^{\circ}\text{C} - (-4.1)\text{ }^{\circ}\text{C} = 24.1\text{ }^{\circ}\text{C}$$

$$C_{sensible} = 1.23, C_{latent} = 3010$$

*(don't remember why we adopt these numbers or from where we got them
C sensible and C latent, in the exercise solved in class)*

$$\omega_{out} = 0.0132 \frac{kg_{water}}{kg_{dryAir}} \text{ (from cooling DB = } 31.1^{\circ}\text{C)}$$

$$\omega_{in} = 0.0093 \frac{kg_{water}}{kg_{dryAir}} \text{ (from cooling MCWB = } 24.3^{\circ}\text{C)}$$

$$\Delta\omega = 0.0132 - 0.0093 = 0.0039 \frac{kg_{water}}{kg_{DryAir}}$$

$$\dot{Q}_{inf-ventilation_{cooling_{sensible}}} = C_{sensible} \dot{V} \Delta T_{cooling} = 1.23 * 32.41 * 7.1 = 283.036\text{ W}$$

$$\dot{Q}_{inf-ventilation_{cooling_{latent}}} = C_{latent} \dot{V} \Delta\omega_{cooling} = 3010 * 32.41 * 0.0039 = 380.46\text{ W}$$

$$\dot{Q}_{inf-ventilation_{heating_{sensible}}} = C_{sensible} \dot{V} \Delta T_{heating} = 1.23 * 48.78 * 24.1 = 1445.98\text{ W}$$