















WEEK 9

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Task 1. Use a weather forecast website and utilize the psychrometric chart and the formula we went through in the class to determine the **absolute humidity**, **wet-bulb temperature**, and the **mass of water vapor in the air** in Aula A of Piacenza campus in the moment you are solving this exercise. Provide the input that you utilized.

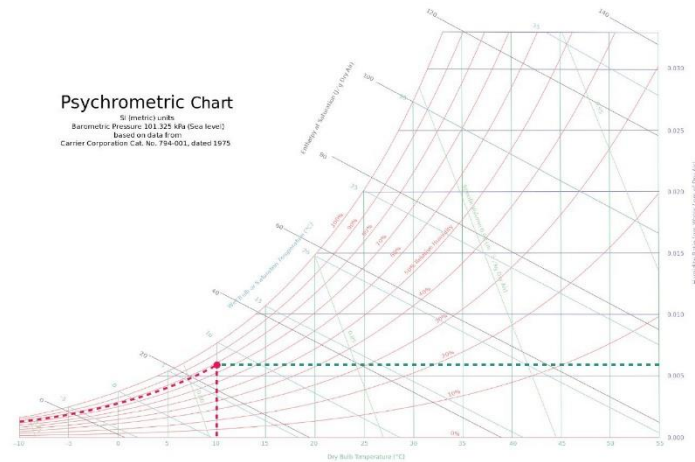
Data Used (December 2, 2019, 1pm)

Source	https://www.meteo-oggi.it/italia/regione-emilia-romagna/tempo-piacenza/
Relative Humidity	79%
Atmospheric Pressure	1016 hPa = 101.6 kPa
Effective Temperature	10°C
Aula A Dimensions	10 x 5 x 4m

	1:00 pm	14:00	4:00 pm	18:00	8:00 pm	21:00	22:00
	 PartlyCloud	 PartlyCloud	 LightCloud	 LightCloud	 PartlyCloud	 Cloud	 PartlyCloud
Effective temperature	10 ° C	10 ° C	9 ° C	6 ° C	7 ° C	7 ° C	8 ° C
Perceived temperature	10 ° C	10 ° C	8 ° C	5 ° C	7 ° C	6 ° C	7 ° C
Rainfall	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Humidity	79 %	77 %	89 %	90 %	90 %	92 %	91 %
Atmospheric pressure	1016 hPa	1015 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa	1020 hPa
Wind intensity	8 km / h	6 km / h	6 km / h	6 km / h	3 km / h	6 km / h	5 km / h
Wind direction	 NO	 OR	 NO	 OR	 S	 SELF	 IS
Probability of fog	0 %	0 %	0 %	0 %	0 %	0 %	0 %
Dew point	6 ° C	6 ° C	7 ° C	5 ° C	5 ° C	6 ° C	6 ° C
Clouds	65 %	55 %	16 %	24 %	86 %	100 %	76 %
Low clouds	4 %	0 %	15 %	7 %	38 %	100 %	49 %
Medium clouds	34 %	54 %	2 %	23 %	84 %	85 %	70 %
High clouds	55 %	7 %	0 %	0 %	0 %	0 %	0 %

Psychrometric Chart Method

Using the psychrometric chart and the weather data provided, the following values can be concluded:



Absolute Humidity	0.006
Wet-Bulb Temperature	8°C

Formula Method

Saturation Pressure of Water at 10°C = 1.227 kPa

www.engineeringtoolbox.com says

Water saturation pressure at 10 degree C:

1.227 kPa

0.0123 bar

0.0121 atm

0.178 psi

25.6 psf

$$\phi = \frac{m_v}{m_g} \text{ where } m_g = \text{the mass of water at sat condition}$$

$$\phi = \frac{m_v}{m_g} = \frac{P_v}{P_g} \text{ where } P_g = P_{sat} 10^\circ\text{C} = 1.227 \text{ kPa}$$

Partial Pressure of Water Vapor

$$\phi = \frac{P_v}{P_g} \rightarrow P_v = \phi \times P_g$$

$$P_v = \phi \times P_g$$

$$P_v = 0.79 \times 1.227 \text{ kPa} = 0.97 \text{ kPa}$$

Partial Pressure of Dry Air

$$P_a = P - P_v$$

$$P_a = 101.6 \text{ kPa} - 0.97 \text{ kPa} = 100.63 \text{ kPa}$$

Absolute Humidity

$$\omega = (0.622) \left(\frac{P_v}{P_a} \right)$$

$$\omega = (0.622) \left(\frac{0.97 \text{ kPa}}{100.63 \text{ kPa}} \right)$$

$$\omega = 0.0059 \frac{\text{kg}_{\text{vapor}}}{\text{kg}_{\text{DryAir}}}$$

Mass of Water Vapor in the Air

$$\text{For ideal gases: } m = \frac{PV}{R_{sp} T}$$

$$\text{For air: } m_a = \frac{P_a V_a}{R_a T}$$

$$m_v = \frac{P_v V_v}{R_v T} = \frac{(0.97 \text{ kPa})(10 \text{ m} + 5 \text{ m} + 4 \text{ m})}{(0.4615)(273 \text{ K} + 10)}$$

$$m_v = 1.48 \text{ kg}$$

Enthalpy

$$h = h_a + \omega h_v$$

$$\text{where } h_a = c_{pa} T = \left(1.005 \frac{\text{kJ}}{\text{kg}^\circ\text{C}} \right) (T \text{ in } ^\circ\text{C}) \text{ and } h_v = h_g(T) \approx 2501.3 + 1.82T$$

$$h = \left(1.005 \frac{\text{kJ}}{\text{kg}^\circ\text{C}} \right) (10^\circ\text{C}) + \left(0.0059 \frac{\text{kg}_{\text{vapor}}}{\text{kg}_{\text{DryAir}}} \right) \left[2501.3 + (1.82)(10^\circ\text{C}) \frac{\text{kJ}}{\text{kg}_{\text{vapor}}} \right]$$

$$h = 24.91505 = 24.92 \frac{\text{kJ}}{\text{kg}_{\text{DryAir}}}$$

Task 2. Utilize the same methodology we went through in the class and determine the **sensible and latent load** corresponding to **internal gains**, the **ventilation**, and the **infiltration** in a house with a **good construction quality** and with the **same geometry** as that of the example which is located in Brindisi, Italy.

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
		0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180

Given Information

Building Height	2.50m
Floor Area	200m ²
No. of Occupants	2
No. of Bedrooms	1
Wall Area	144m ²

Internal Gains

$$\begin{aligned}\dot{Q}_{ig_{sensible}} &= 136 + (2.2)(A_{cf}) + (22)(N_{oc}) \\ \dot{Q}_{ig_{sensible}} &= 136 + (2.2)(200m^2) + (22)(2) \\ \dot{Q}_{ig_{sensible}} &= 620 \text{ W} \\ \dot{Q}_{ig_{latent}} &= 20 + (0.22)(A_{cf}) + (12)(N_{oc}) \\ \dot{Q}_{ig_{latent}} &= 20 + (0.22)(200m^2) + (12)(2) \\ \dot{Q}_{ig_{latent}} &= 88 \text{ W}\end{aligned}$$

Infiltration

Find maximum flow of air. Find leakage area and use unit leakage area chart.

Unit Leakage for Good Construction

$$A_{ul} = 1.40 \text{ cm}^2/\text{m}^2$$

Leakage Area

$$\begin{aligned}A_l &= A_{ul}A_{ul} \\ A_l &= (200m^2 + 144m^2)(1.40 \text{ cm}^2/\text{m}^2) \\ A_l &= (344m^2)(1.40 \text{ cm}^2/\text{m}^2) \\ A_l &= 481.6 \text{ cm}^2\end{aligned}$$

Infiltration Rate

Table 5 Typical IDF Values, L/(s · cm ²)										
H, m	Heating Design Temperature, °C					Cooling Design Temperature, °C				
	-40	-30	-20	-10	0	10	30	35	40	
2.5	0.10	0.095	0.086	0.077	0.069	0.060	0.031	0.035	0.040	
3	0.11	0.10	0.093	0.083	0.072	0.061	0.032	0.038	0.043	
4	0.14	0.12	0.11	0.093	0.079	0.065	0.034	0.042	0.049	
5	0.16	0.14	0.12	0.10	0.086	0.069	0.036	0.046	0.055	
6	0.18	0.16	0.14	0.11	0.093	0.072	0.039	0.050	0.061	
7	0.20	0.17	0.15	0.12	0.10	0.075	0.041	0.051	0.068	
8	0.22	0.19	0.16	0.14	0.11	0.079	0.043	0.058	0.074	

$$Q_i = (A_l)(IDF)$$

$$IDF_{heating} = 0.065 \frac{L}{s \times \text{cm}^2}$$

$$IDF_{cooling} = 0.032 \frac{L}{s \times \text{cm}^2}$$

Infiltration Rate - Winter

$$\dot{V}_{\text{infiltration}} = (481.6 \text{ cm}^2) \left(0.065 \frac{\text{L}}{\text{s} \times \text{cm}^2} \right)$$
$$\dot{V}_{\text{infiltration}} = 31.30 \text{ L/s}$$

Infiltration Rate - Summer

$$\dot{V}_{\text{infiltration}} = (481.6 \text{ cm}^2) \left(0.032 \frac{\text{L}}{\text{s} \times \text{cm}^2} \right)$$
$$\dot{V}_{\text{infiltration}} = 15.41 \text{ L/s}$$

Ventilation

$$Q_v = 0.05 A_{cf} + 3.5(N_{BR} + 1)$$

where

Q_v = required ventilation flow rate [L/s]

A_{cf} = building conditioned floor area [m²]

N_{BR} = no. of bedrooms, not less than 1

$$\dot{V}_{\text{ventilation}} = (0.05)(200) + (3.5)(1 + 1) = 17.0 \text{ L/s}$$

$$\dot{V}_{\text{infiltration-ventilation heating}} = 31.30 \text{ L/s} + 17 \text{ L/s}$$

$$\dot{V}_{\text{infiltration-ventilation heating}} = 48.3 \text{ L/s}$$

$$\dot{V}_{\text{infiltration-ventilation cooling}} = 15.41 \text{ L/s} + 17 \text{ L/s}$$

$$\dot{V}_{\text{infiltration-ventilation cooling}} = 32.41 \text{ L/s}$$

Sensible and Latent Load

$$C_{\text{sensible}} = 1.23$$

$$C_{\text{latent}} = 3010$$

$$\Delta T_{\text{heating}} = 20^\circ\text{C} - 4.1^\circ\text{C} = 15.9^\circ\text{C}$$

$$\Delta T_{\text{cooling}} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C}$$

$$\dot{Q}_{\text{inf-vent heating sensible}} = C_{\text{sensible}} \dot{V} \Delta T_{\text{heating}}$$

$$\dot{Q}_{\text{inf-vent heating sensible}} = (1.23)(48.3 \text{ L/s})(15.9^\circ)$$

$$\dot{Q}_{\text{inf-vent heating sensible}} = 944.60 \text{ W}$$

$$\dot{Q}_{\text{inf-vent cooling sensible}} = C_{\text{sensible}} \dot{V} \Delta T_{\text{cooling}}$$

$$\dot{Q}_{\text{inf-vent cooling sensible}} = (1.23)(32.41 \text{ L/s})(7.1^\circ\text{C})$$

$$\dot{Q}_{\text{inf-vent cooling sensible}} = 283.04 \text{ W}$$

$$\dot{Q}_{\text{inf-vent cooling latent}} = C_{\text{latent}} \dot{V} \Delta \omega_{\text{cooling}}$$

$$\dot{Q}_{\text{inf-vent cooling latent}} = C_{\text{latent}} \dot{V} (\omega_{\text{out}} - \omega_{\text{in}})$$

$$\dot{Q}_{\text{inf-vent cooling latent}} = (3010)(32.41 \text{ L/s})(0.014 - 0.0095 \text{ kg vapor/kg dry air})$$

$$\dot{Q}_{\text{inf-vent cooling latent}} = 438.99 \text{ W}$$