









Week9 Zhou Yuhan

2019年12月5日 21:46

Task1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

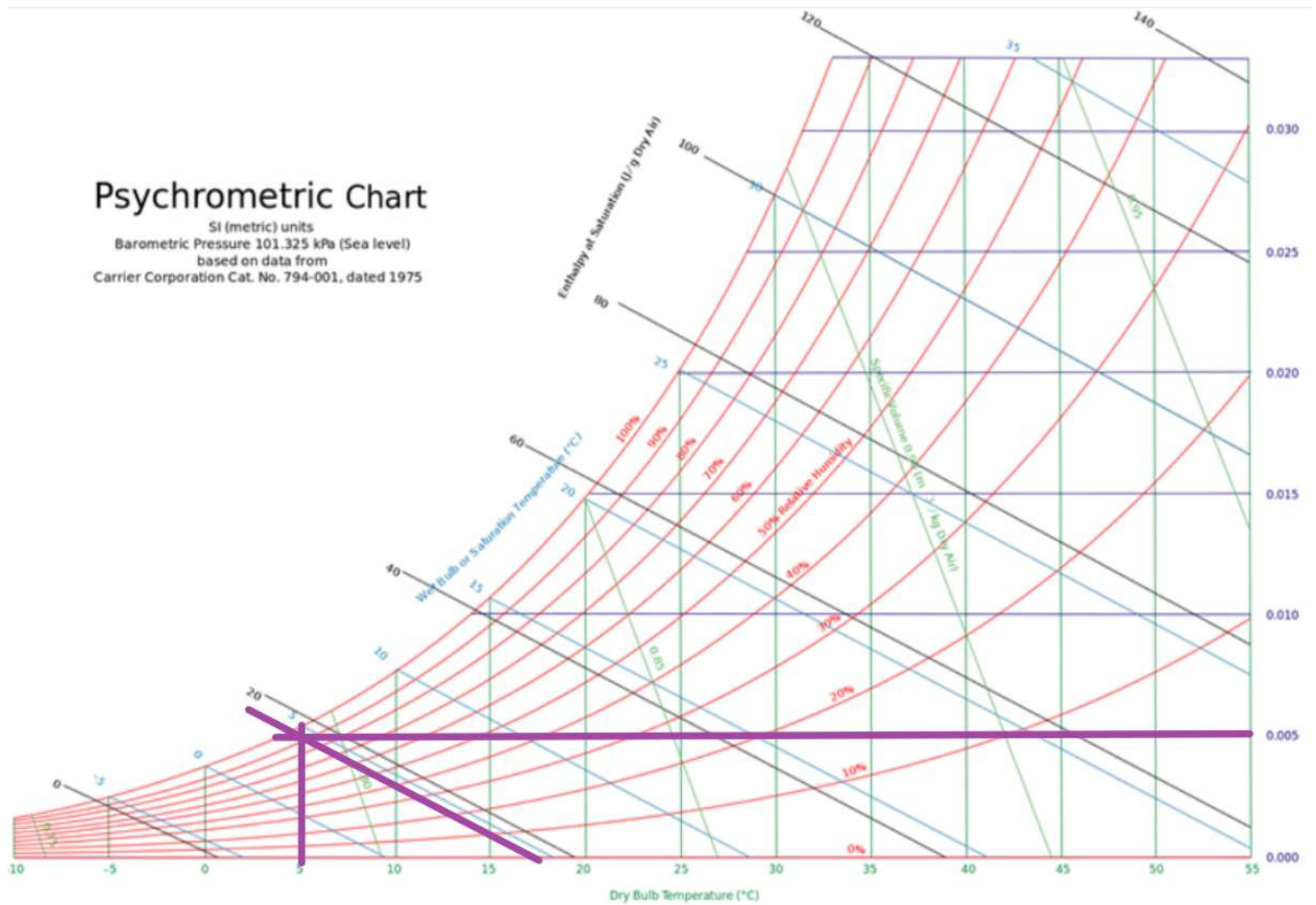
Tempo domani a Piacenza Venerdì, 06 Dicembre 2019							
	05:00	07:00	10:00	14:00	18:00	19:00	21:00
	 PartlyCloud	 PartlyCloud	 LightCloud	 PartlyCloud	 LightCloud	 PartlyCloud	 PartlyCloud
Temperatura effettiva	2°C	2°C	5°C	8°C	5°C	5°C	5°C
Temperatura percepita	2°C	0°C	5°C	8°C	5°C	5°C	4°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	95 %	98 %	89 %	77 %	91 %	92 %	95 %
Pressione atmosferica	1025 hPa	1025 hPa	1025 hPa	1023 hPa	1021 hPa	1022 hPa	1021 hPa
Intensità del vento	3 km/h	6 km/h	4 km/h	3 km/h	4 km/h	4 km/h	5 km/h
Direzione del vento	 O	 NO	 O	 NO	 SW	 SW	 SW
Probabilità di nebbia	1 %	8 %	0 %	0 %	0 %	0 %	0 %
Punto di rugiada	2°C	2°C	3°C	4°C	3°C	3°C	4°C
Nuvole	44 %	46 %	27 %	74 %	35 %	49 %	43 %
Nuvole basse	20 %	44 %	23 %	72 %	34 %	48 %	42 %
Nuvole medie	11 %	1 %	20 %	51 %	13 %	13 %	1 %
Nuvole alte	27 %	4 %	0 %	1 %	0 %	0 %	1 %

Chosen time:10:00

Temperature $T=5^{\circ}\text{C}$

Relative humidity $\phi=89\%$

Total air pressure $P=1025\text{hPa}=102.5\text{kPa}$



Absolute Humidity=0.005

Wet bulb temperature= 5 °C

The mass of water vapour (M_v)

$$P_v = \frac{p\omega}{0.622 + \omega} = 0.84 \text{ kg}$$

$$V_{\text{roomA}} = 20 \times 6 \times 6 = 720 \text{ m}^3$$

$$M_v = \frac{P_v V_{\text{roomA}}}{R_v T} = 4.7 \text{ kg}$$

Task 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy.

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N

Long: 17.95E

Elev: 10

StdP: 101.2

Time Zone: 1.00 (EUW)

Period: 86-10

WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
(1) 2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

(2)	Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
			0.4%		1%		2%		0.4%		1%		2%			
			DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180

(3)	Dehumidification DP/MCDB and HR									Enthalpy/MCDB					Hours 8 to 4 & 12.8/20.6	
	0.4%			1%			2%			0.4%		1%		2%		
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236

Extreme Annual Design Conditions

Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB							
				Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years	
1%	2.5%	5%		Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
(4) 11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

Internal Gains:

$$Q_{\text{insensible}} = 136 + 2.2A_{\text{fc}} + 22N_{\text{oc}} = 136 + 2.2 \times 200 + 22 \times 2 = 620\text{W}$$

$$Q_{\text{iglatent}} = 20 + 0.22A_{\text{fc}} + 12N_{\text{oc}} = 20 + 0.22 \times 200 + 12 \times 2 = 88\text{W}$$

The Infiltration:

$$A_{\text{es}} = A_{\text{wall}} + A_{\text{roof}} = 200 + 144 = 344 \text{ m}^2$$

$$A_{\text{L}} = A_{\text{es}} \times A_{\text{ul}} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$T_{\text{cooling}} = 24^\circ\text{C}$$

$$T_{\text{heating}} = 20^\circ\text{C}$$

$$\Delta T_{\text{cooling}} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C}$$

$$\Delta T_{\text{heating}} = 20^\circ\text{C} - (-4.1)^\circ\text{C} = 24.1^\circ\text{C}$$

$$DR = 7.1^\circ\text{C} = 7.1\text{K}$$

$$IDF_{\text{heating}} = 0.073 \frac{L}{S \cdot \text{cm}^2}$$

$$IDF_{\text{cooling}} = 0.033 \frac{L}{S \cdot \text{cm}^2}$$

Infiltration airflow rate:

$$Q_{\text{i.heating}} = A_{\text{L}} \times IDF_{\text{heating}} = 481.6 \times 0.073 = 35.15 \frac{L}{s}$$

$$Q_{\text{i.cooling}} = A_{\text{L}} \times IDF_{\text{cooling}} = 481.6 \times 0.033 = 15.89 \frac{L}{s}$$

Ventilation:

$$Q_v = 0.05A_{\text{fc}} + 3.5(N_{\text{br}} + 1) = 0.05 \times 200 + 3.5(1 + 1) = 17 \frac{L}{s}$$

$$Q_{\text{i-v.heating}} = Q_{\text{i.heating}} + Q_v = 35.15 + 17 = 52.15 \frac{L}{s}$$

$$Q_{\text{i-v.cooling}} = Q_{\text{i.cooling}} + Q_v = 15.89 + 17 = 32.89 \frac{L}{s}$$

$$C_{\text{sensible}} = 1.23$$

$$C_{\text{latent}} = 3010$$

$$\Delta\omega_{\text{cooling}} = 0.0039$$

$q_{\text{inf-ventilation cooling sensible}} = C_{\text{sensible}} Q_{\text{i-u. cooling}} \Delta T_{\text{cooling}} = 1.23 \times 32.89$
 $\times 7.1 = 287.25 \text{ W}$
 $q_{\text{inf-ventilation cooling latent}} = C_{\text{latent}} Q_{\text{i-u cooling}} \Delta \omega_{\text{cooling}} =$
 $3010 \times 32.89 \times 0.0039 = 386.13 \text{ W}$
 $q_{\text{inf-ventilation heating latent}} = C_{\text{sensible}} Q_{\text{i-wheating}} \Delta T_{\text{Theating}} = 1.23 \times 52.15 \times$
 $24.1 = 1546 \text{ W}$