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## SECTION 1

### BEAM MODULATION

#### 1.1 Introduction

The e+p scattering rate largely depends on the five beam parameters: horizontal position ( $X$ ), horizontal angle ( $X'$ ), vertical position ( $Y$ ), vertical angle ( $Y'$ ), and energy ( $E$ ). Changes in these beam parameters when the beam polarization is reversed create false asymmetries. Although attempt has been made to keep changes in beam parameters during reversal as small as possible, also need to correct for such false asymmetries. A challenge for the Q-weak experiment was to keep these helicity-correlated parameter differences as small as possible and measure the detector sensitivities. The goal of the beam modulation system is to occasionally induce controlled beam parameter changes  $\Delta T_i$ , measure the resulting detector false asymmetry  $A_{\text{false}}$ , and determine the detector sensitivities  $\frac{\partial A}{\partial T_i}$ . This technique will allow to correct for the beam false asymmetries as shown in Equation 1.1.1. Even if these corrections were small under ideal running conditions, the modulation system described in this chapter will allow to quickly determine if undesirable changes have occurred.

it has been attempted

it is necessary to

$$A_{\text{false}} = \sum_{i=1}^5 \left( \frac{\partial A}{\partial T_i} \right) \Delta T_i \quad (1.1.1)$$

#### 1.2 Measurement Time vs Modulation Asymmetry

 Starting with the assumption that it would be helpful to measure the whole-detector sensitivities to 10% accuracy every few days (provided it can be done using only a small fraction of the beam time and without beam strikes or halo scraping) [1]. Stable sensitivities would yield few percent uncertainties by the end of the experiment which is much better than one would need to regress out the helicity-correlated differences seen in the previous parity violating experiment HAPPEX [2]. However, frequent whole-detector sensitivity measurements might reveal important changes in the beam or the target cell position, the presence of an unmeasured beam parameter, or even a broken glue joint in the main detector. Furthermore, accurate single octant sensitivities (which would be

uncertainties  
of a few  
percent

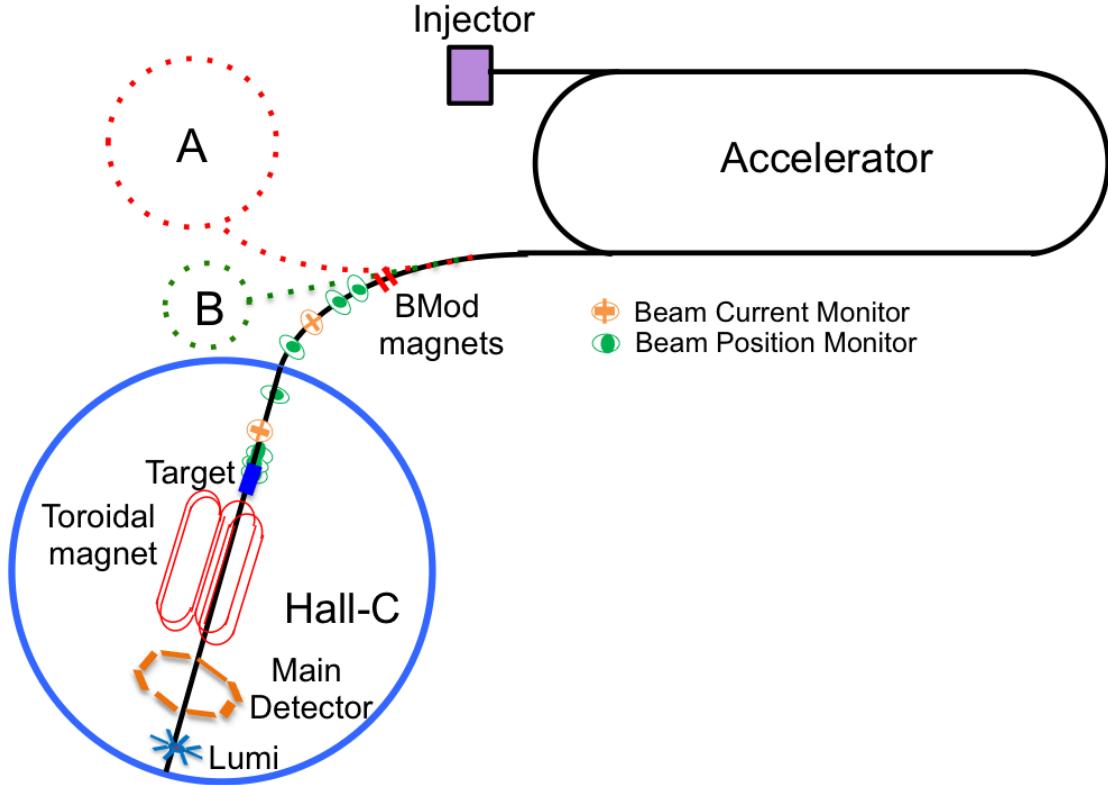


Figure 1.1 Simple schematic cartoon of the accelerator. The beam modulation magnets are shown in Hall-C beamline. The BPMs, BCMs, and other key components of the experiment are shown in the Hall-C beamline.

obtained as a by-product) are an essential prerequisite to extract the  $\sin \phi$  and  $\cos \phi$  dependence which are characteristic of residual transverse beam polarization.

For the size and duration of the modulations discussed here, the natural beam jitter and the SEE BPM (section ??) electronic noise of roughly  $5 \mu\text{m}/\sqrt{\text{Hz}}$  will be negligible. If this was not the case, measurement times would become much longer. This means the uncertainty on the detector sensitivities is dominated by the statistical uncertainty on the detector false asymmetry. At nominal luminosity, the Q-weak experiment has a rate of 800 MHz/octant, hence the whole-detector statistical sensitivity  $dA = 12.5 \text{ ppm}/\sqrt{t}(\text{sec})$ , or 1 ppm in 156.25 seconds. The clock times needed to measure a single beam sensitivity to 10% are therefore given by

$$t(s) = \frac{1}{\text{DF}} \frac{\left( \frac{12.5 \text{ ppm}}{A(\text{ppm})} \right)^2}{\left( \frac{dA}{A} \right)^2} = \frac{1}{\text{DF}} \left( \frac{12.5 \text{ ppm}}{A(\text{ppm})} \right)^2 (10)^2 \quad (1.2.1)$$

Table 1.1 Dead time calculation for beam modulation. The clock time needed to measure detector sensitivity for a single parameter and how it varies with asymmetries are shown here.

Modulation asymmetry [ppm]	Clock time required		
	10% DF [Hours]	1% DF [Hours]	0.1% DF [Hours]
1	43	430	4300
10	0.43	4.3	43

Table 1.1 estimates required clock time for a 10% measurement of a single beam sensitivity with different assumptions about the modulation asymmetry and the modulation duty factor. A modulation of 10 ppm would permit a measurement of all 5 sensitivities to 10%, require about 1-10 calendar days, and have minimal negative impact on production duty cycle. For fixed uncertainty, smaller amplitudes would require at least quadratic increases in measurement time or duty factor (DF). For fixed measurement time and duty factor, smaller amplitudes would cause at least linear increases in the uncertainties.

### 1.3 Modulation Amplitude

amplitudes?

The next important step was to estimate the modulation amplitude for beam position and angle necessary to achieve  $A_{\text{false}} = 10 \text{ ppm}$ . Detailed simulations on sensitivities have been performed using Geant-3 and is discussed in [3]. The simulated single octant detector sensitivities are dominated by the interaction of e+p elastic scattering with the defining collimator and are shown in the second column of Table 1.2. Except for energy, the whole detector sensitivities were much smaller. They were much more complicated since they were determined by imperfect cancellation of the linear sensitivities due to broken symmetries (coil misalignment, radiator radial positions), plus quadratic sensitivities which depend on beam offsets. It is not unreasonable to disagree as to what expected suppression factor to be used in going from single octant sensitivities to whole detector sensitivities. Therefore the relatively conservative cancellation factor was assumed to be 50 which leads to the modulation amplitude for position, angle, and energy to generate 10 ppm whole detector asymmetry and are shown in Table 1.2.

The estimated whole detector sensitivities were small. Compared to the Q-weak statistical uncertainty of  $\sim 5 \text{ ppb}$ , the beam parameter corrections resulting from the helicity-correlated differences seen in the previous parity violating experiments [2]  $\mathcal{O}(1 \text{ nm}, 0.1 \text{ nrad}, 0.1 \text{ ppm in energy})$  were negligible. Alternatively, this means the allowable uncertainty in determining the beam sensitivity is

Table 1.2 A crude estimate of the modulation amplitudes to generate 10 ppm whole detector asymmetries.

Beam Parameter	Single Octant Sensitivity	Assumed Cancellation	Whole Detector Sensitivity	Modulation Amplitude for 10 ppm
Position	10 ppb/nm	50	0.2 ppb/nm	50 $\mu\text{m}$
Angle	30 ppb/nrad	50	0.6 ppb/nrad	20 $\mu\text{rad}$
Energy	1 ppb/ppb	1	1 ppb/ppb	10 ppm ( $\sim 10 \text{ keV}$ )

100%, so a system capable of making a 10% measurement on all 5 beam sensitivities every 1-10 days is apparently overkill. The real value of such a beam modulation system may be to detect undesired changes in the experiment, or as insurance in case the e+p sensitivities prove to be much larger than anticipated, or for those cases where the sensitivities are known to be much larger e.g., for elastic scattering on  $^9\text{Be}$  or  $^{27}\text{Al}$  window-like targets, inelastic scattering on  $\text{LH}_2$  or  $^{27}\text{Al}$ , or the small angle scattering into the luminosity monitors.

was?

## 1.4 Optics Calculation

A software written by Valery Lebedev for linear and non-linear optics calculations, OptiM [4], and an input deck prepared by Jay Benesch [5] (JLab) were used to simulate the Hall-C beamline (3C).

The 3C beamline substantially modified before Q-weak to accommodate the Compton polarimeter.

A schematic view of the Hall-C beamline (songsheet<sup>1</sup>) along with the other halls are shown in Figure 1.2. The goal for the beam modulation system was to achieve robust modulation in  $X$ ,  $X'$ ,  $Y$ ,  $Y'$ , and  $E$  at the target. These modulations do not have to be strictly pure, but they have to be linearly independent so that have solutions for the individual sensitivities. The asymmetries from position modulations were an order of magnitude larger than the corresponding asymmetries from angle modulations for similar sized magnet kicks in the Q-weak and will be discussed in later section of this chapter. This fact, plus the relatively large statistical noise in the detector asymmetries, plus the certainty of small drifts in the optics, suggested that mixed mode modulation is unlikely to be robust. Running times and uncertainties were also quite difficult to estimate for the mixed mode modulation. Therefore, relatively pure modulations in which ~90% of the asymmetry arises from the variable of interest was attempted to produce.

it was attempted to produce

<sup>1</sup>The CAD drawings informally referred as songsheets at Jefferson Lab. The CAD annotation is static. Only element names are shown in the drawings.

were

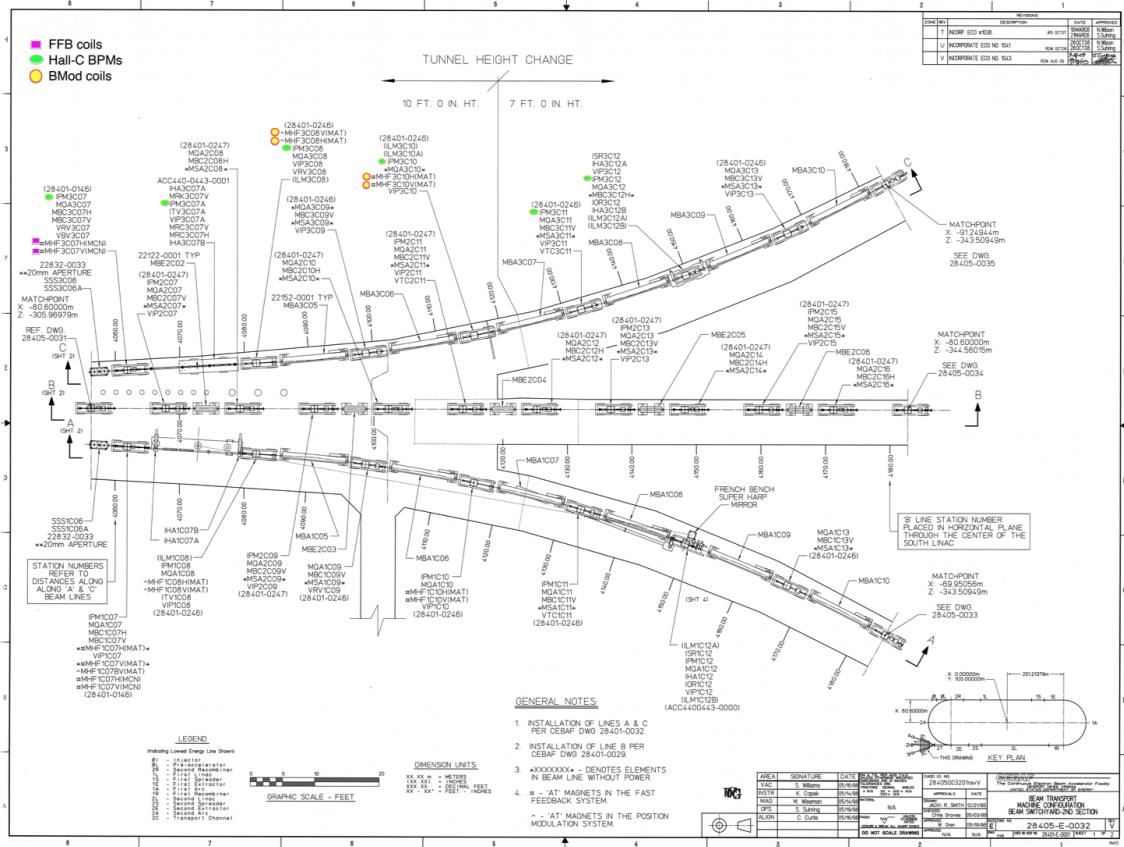


Figure 1.2 Jefferson Lab and its beamline schematic for all three experimental halls using Computer Aided Design (CAD) drawings (informally referred as songsheets at Jefferson Lab) are shown. Beam modulation magnets, fast feed back coils, and BPMs in the Hall-C beamline are labeled separately.

### 1.4.1 Simulation using OptiM

The main OptiM deck [6] contain the information about the location, field strength, size, orientation etc. for each component of the Hall-C beamline. The OptiM deck was used to obtain transfer matrices, obit excursion, beta functions, and simulated trajectories between any two beamline elements in forward or inverse direction.

### 1.4.2 Inverse Beamline

An insightful starting exercise was to start with a pure position or angle deviation at the target and use OptiM to send tracks in the upstream direction which was named as inverse beamline or orbit. Figure 1.3 shows the orbit from the target to the Lambertson (beginning of the 3C

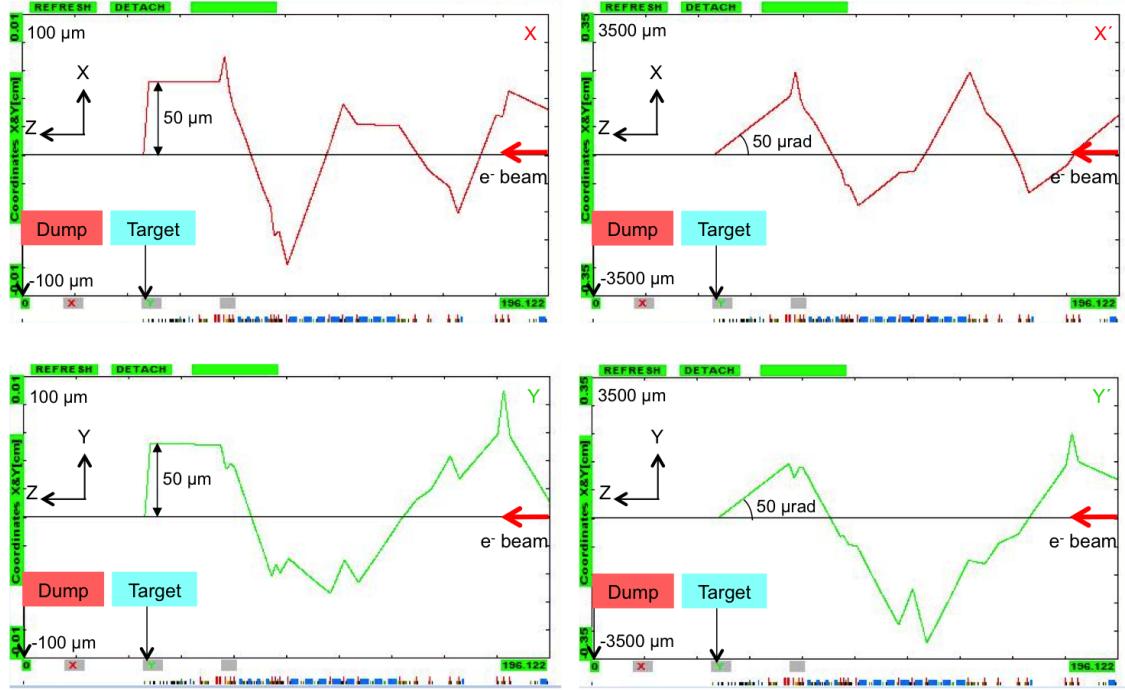


Figure 1.3 Inverse orbit excursions simulation from OptiM. The direction of the beam is from right to left. The tiny blue and red boxes on the horizontal axis at the bottom of the figures are dipoles and quadrupoles, respectively. The location of the target and beam dump are also marked. The orbit excursion for the relatively pure  $X$ ,  $X'$ ,  $Y'$  and  $Y$  motion at the target are shown in the four panels (from top left in clockwise direction).

line). All 4 panels have the same qualitative features: the beam moves to the right with piece-wise continuous motion, there is a discontinuity at each quadrupole location, and there is at least one zero crossing. The reason this inverse trajectory is so interesting is that, due to time-reversal invariance of electromagnetic interactions, it provides the information how to perturb a forward beam to obtain a pure position or angle change at the target. As long as the inverse orbit stays inside the beampipe, such a figure is an **existence proof** that pure modulation at the target is possible with a forward beam.

**about**

#### 1.4.3 Forward Beamline with Position or Angle Kicks

The simplest way to perturb an arbitrary forward beam onto the magic trajectory obtained using inverse beamline is to kick the beam with a single small dipole at one of the zero crossings. However, if driving coils were restricted to the first half of the 3C arc, this strategy was not feasible because there was only one zero crossing in that region (corresponding to pure  $X'$  modulation), with no

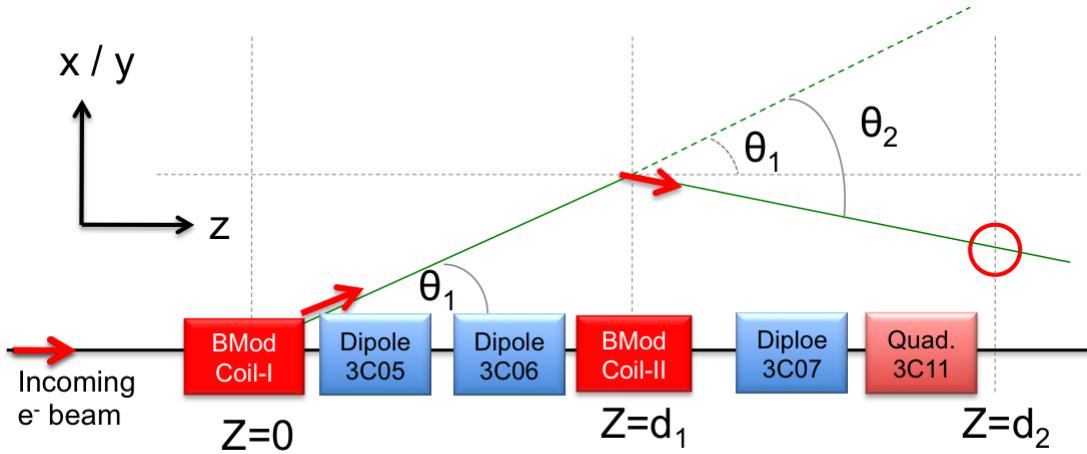


Figure 1.4 A sketch of beam modulation concept. A pair of magnets ( $Z=0$  and  $Z=d_1$ ) with opposite kick were used to match a trajectory at any arbitrary point ( $Z=d_2$ ) in the beamline. There were two big dipoles between the modulation magnets. Using simple algebra  $\theta_1$  and  $\theta_2$  can be expressed in terms of position and angle at the match point. Hence required field integral in the beam modulation magnets can be calculated to generate a particular trajectory (details calculation in APPENDIX ??).

of the

zeros corresponding to  $X$ ,  $Y$ , or  $Y'$  modulation. A better approach was then suggested by Mike Tiefenback [7], similar to that used in the JLab Fast Feedback System (FFB) [8,9]. As schematically shown in Figure 1.4, pairs of separated coils could be used to take an arbitrary forward ray, offset its position and angle, and re-inject it along the appropriate trajectory to produce a pure position or angle change at the target. Detailed OptiM solutions for forward rays are shown in Figure 1.5 for a pair of coils separated by 9.5 m. Note that position modulation of  $\pm 250 \mu\text{m}$  at the target yields orbit deviations of similar magnitude in the beamline, while angle modulation of  $\pm 50 \mu\text{rad}$  at the target yields orbit deviations of up to 3 mm. The size of the latter orbit deviations is large enough to cause some concern about scraping of the beam or halo. (The impact on the Compton polarimeter laser  $X$  electron beam lock has not been examined.) Hence the angle kick was reduced by an order of magnitude smaller to match the size of the orbit deviations. This might be a better match to size of natural beam jitter, but the time required in Table 1.2 for a single 10% measurement would increase by at least a factor of 100. The field integrals for that yielded pure modulations at the Q-weak target something wrong with this sentence using most updated available OptiM deck [6] were calculated and are shown in Table 1.3. These field integrals were converted to currents using the measured MAT coil field constant of 330 G-cm/A. This two-coil scheme was very convenient, as any changes in the 3C line was easily simulated for the modulation system by re-tuning the ratio of coil currents without having to move coils.

the

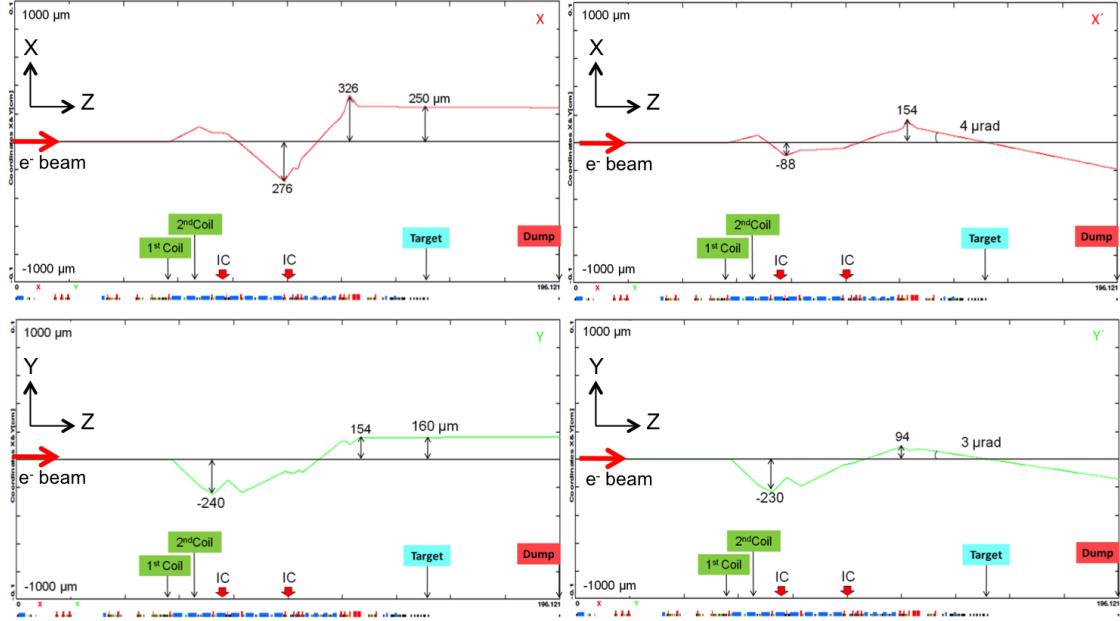


Figure 1.5 Forward orbit excursions simulation from OptiM. Beam moves from left to right. The ting blue and red boxes on the horizontal axis at the bottom of the figures are dipoles and quadrupoles, respectively. Simulated location of the modulation magnets and recommended location for ion chambers are shown in the figures. The forward orbit excursion for the relatively pure  $X$ ,  $X'$ ,  $Y'$  and  $Y$  motion at the target are shown in the four panels (from top left in clock wise direction).

Table 1.3 Required filed integrals for the modulation dipole pair to generate relatively pure position and angle at the target from OptiM are shown here. Coil currents to produce such filed integrals are calculated. The ratio between coil current in 2nd and 1st coil is defined as tune parameters. The negative tune parameters signifies the out of phase current in the two coils.

Beam Parameter	Amplitude for 10 ppm	$I_1$ [A]	$\int \vec{B} \bullet d\vec{l}_1$ [G-cm]	$I_2$ [A]	$\int \vec{B} \bullet d\vec{l}_2$ [G-cm]	Tune
$X$	250 $\mu\text{m}$	0.159	52.4	-0.372	-122.9	-1.875
$X'$	4 $\mu\text{rad}$	0.554	183.0	-1.872	-618.0	-3.864
$Y$	160 $\mu\text{m}$	-0.242	-80.0	0.060	20.0	-0.367
$Y'$	3 $\mu\text{rad}$	-1.606	-530.0	0.771	254.0	-0.489

#### 1.4.4 Forward Rays with Energy Kick

The beam energy was modulated using a superconducting RF cavity in the South Linac of the accelerator. The effect of a simulated 10 ppm energy kick from OptiM is shown in Figure 1.6. At 3C12, the point of highest dispersion (the middle of the 3C arc), the induced motion is shown by a 41  $\mu\text{m}$  red spike. From a comparison of Figures 1.5 and 1.6, it is pretty clear that energy

changes could not possibly be confused with position or angle changes. Further downstream in the beamline, the small green bump represents the dispersion inside the vertically bending Compton chicane. Because of the lower dispersion, the induced motion in the Compton was only about  $5 \mu\text{m}$ , much smaller than the nominal JLab electron beam rms width. The energy change at the target was identified in terms of change in beam position at 3C12 and at any arbitrary location. A pair of BPMs at the beginning or the end of the 3C arc would seem most natural choice for energy change measurement. Any two  $X$  BPMs on the beamline could be used as long as the magnifications were favorable. But there were advantages to work in terms of target position ( $X_T$ ) and angle ( $X'_T$ )  because 1) these were the coordinates that were used in the simulations to estimate the beam sensitivities, and 2) there were seven BPMs in the drift region upstream of the target provided flexibility to determine  $X_T$  and  $X'_T$  with relatively high accuracy [10]. Previous experiments typically used two BPMs in front of the target, which lacks the above two advantages. The position or angle at 3C12 in terms of target parameters can be expressed as

$$\overleftrightarrow{X}_{3\text{C}12} = M \overleftrightarrow{X}_T \quad (1.4.1)$$

Expanding the Eq. 1.4.1, we get

$$\begin{bmatrix} X \\ X' \\ Y \\ Y' \\ \frac{dE}{E} \end{bmatrix}_{3\text{C}12} = \begin{bmatrix} M_{11} & M_{12} & M_{13} & M_{14} & M_{15} \\ M_{21} & M_{22} & M_{23} & M_{24} & M_{25} \\ M_{31} & M_{32} & M_{33} & M_{34} & M_{35} \\ M_{41} & M_{42} & M_{43} & M_{44} & M_{45} \\ M_{51} & M_{52} & M_{53} & M_{54} & M_{55} \end{bmatrix} \begin{bmatrix} X \\ X' \\ Y \\ Y' \\ \frac{dE}{E} \end{bmatrix}_T \quad (1.4.2)$$

where the matrix elements were obtained from [6] and can be written as

$$M = \begin{bmatrix} 0.69 & -928 & 0 & 0 & 411 \\ -5 \times 10^{-4} & 2.1 & 0 & 0 & -0.5 \\ 0 & 0 & -0.60 & -3.5 \times 10^4 & -1 \\ 0 & 0 & -6 \times 10^{-4} & -5 & -1 \times 10^{-3} \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix} \quad (1.4.3)$$

Using Eq. 1.4.2 and 1.4.3 the energy change at the target can be written in terms of horizontal position change at 3C12, and horizontal position and angle changes at the target as

$$\Delta \left( \frac{dE}{E} \right)_T = \frac{1}{M_{15}} \Delta X_{3C12} - \frac{M_{11}}{M_{15}} \Delta X_T - \frac{M_{12}}{M_{15}} \Delta X'_T \quad (1.4.4)$$

More ~~detailed~~ calculation about the energy modulation can be found in [11].

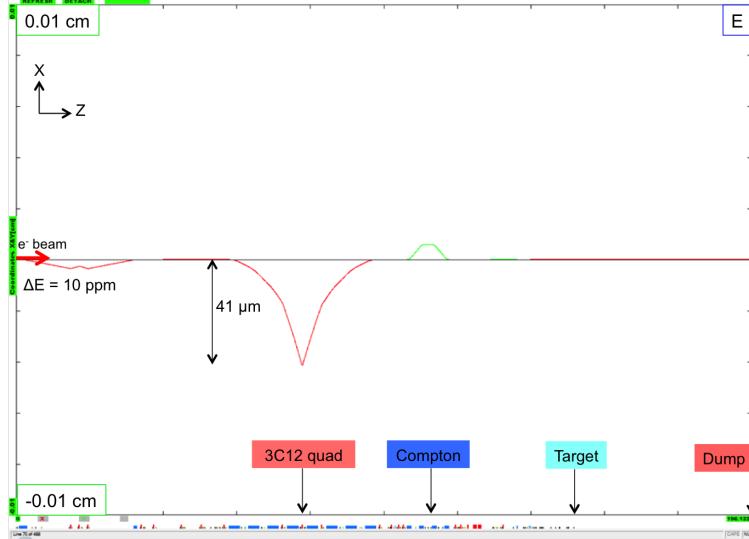


Figure 1.6 Forward orbit excursions simulation for energy modulation from OptiM. Beam moves from left to right. The energy was changed by 10 ppm using a horizontal corrector in the simulation. The pronounced horizontal position (red) change of 41  $\mu\text{m}$  at the middle of the arc is due to the energy change of 10 ppm. A small vertical position (green) bump can be identified at the Compton region.

## 1.5 Beam Modulation Hardware

The hardware of the beam modulation system spans ~~in~~ three different regions: BSY service building, accelerator beamline, and ~~in~~ Hall-C. In the BSY service building ~~there were two signal generators controlled by an IOC. The sinusoidal signals from signal generator were sent to power amplifier and the amplified signals were sent to two pairs of air core coils, and one SRF cavity in the beamline. The read-backs from signal generators, power amplifiers, current transducers to measure the coil current, and BPM responses were sent to two sets of ADCs at the Q-weak cage at Hall-C counting house and at BSY service building to monitor the system and to perform further analysis. A trigger from parity violating DAQ in the Hall-C counting house was sent to the IOC at BSY service building to start the process. The schematic diagram of the beam modulation hardware is shown in Figure 1.7.~~

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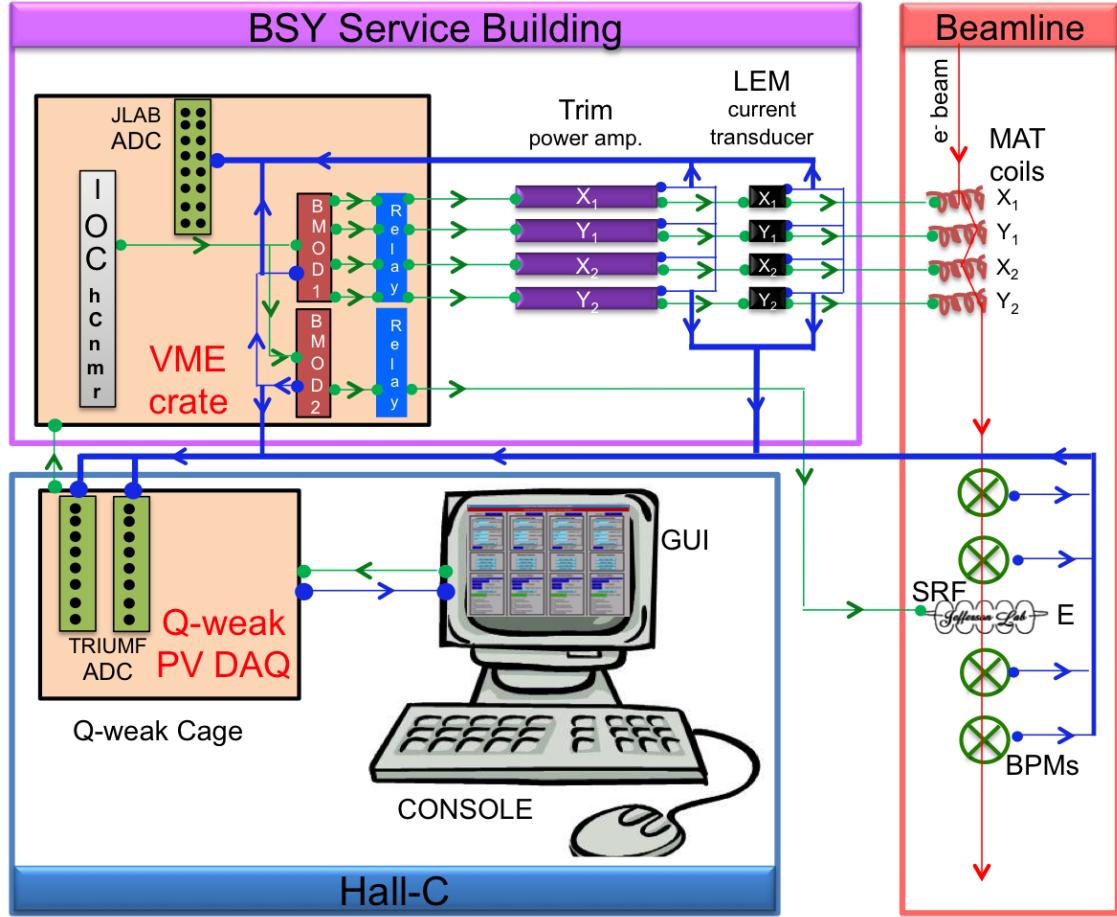


Figure 1.7 Beam modulation hardware sketch. BMod hardware spans in three different regions: BSY service building, accelerator beamline, and in Hall-C. In BSY service building there were two VME-4145 signal generators controlled by an IOC (iochcmr). The sinusoidal signals from signal generator were sent to Trim-I power amplifier and amplified signals were sent to two pair of MAT coils, and one SRF cavity (SL20 vernier) in the beamline. The read-backs from signal generators, power amplifiers, current transducers, BPMs, and cavity were sent to two TRIUMF-made ADCs at Q-weak cage and one JLab-made ADC at BSY service building. The drive or input signals are shown by green and red read-backs by blue lines respectively. In order to trigger the process, a signal from parity violating DAQ in the Hall-C counting house were sent to the IOC.

### 1.5.1 Air-Core Coils

Two pair of JLab MAT(HF) air-core coils were used to perturb the electron beam for the modulation system as they produced sufficient field integral, were readily available, and were compact enough (10 cm) to be inserted easily in almost anywhere in the beamline. Their properties have been measured and summarized by Sarin Philips in [12]. The MAT coils were calibrated in bench test and the most critical parameters are summarized in Table 1.4. The total impedance of the coil was related

the to frequency ( $f$ ) as  $X_{\text{total}} = 1.6 \Omega + 2\pi f(0.0038 \text{ H})$ . The reduction in field due to the skin effect in a standard stainless steel beampipe was determined to be roughly 10% at 1 KHz, and less than a few percent at nominal frequency of 125 Hz. The skin effect was ignored as the used frequency of the sinusoidal modulation was 125 Hz, which was constrained by the power amplifier (see section 1.5.5).

Table 1.4 Basic properties of the air core MAT coils used for the beam modulation system.

Magnet Parameter	Value
Magnet Constant ( $B/I$ )	33 G/A
$\int \vec{B} \bullet d\vec{l} = (B/I) \times \text{Length}$	(330 G-cm/A) × I
Length	10 cm
Inductance	3.8 mH
Resistance	1.6 Ω

### 1.5.2 IOC

A VME based Input Output Controller (IOC) *hcnmr* at BSY service building was used to operate the beam modulation system. IOC was a chassis containing a processor, various input/output (I/O) modules, and VME modules that provide access to other I/O buses [13]. The IOC used to establish communication with two VME 4145 Signal Generator ~~board~~ boards through two patch panels and controlled the drive signal of VME 4145 board via a database access library that works on Unix, vxWorks<sup>2</sup>, and EPICS databases.

### 1.5.3 VME 4145 Signal Generator

Two GE Fanuc Intelligent Platforms' VME-4145 programmable function generator boards [14] were used to drive two ~~pair~~<sup>pairs</sup> of MAT coils (shown in Figure 1.7). The VME-4145 has an analog output board that provides four high-quality analog output channels with 16-bit resolution. Each output has a dedicated Digital-to-Analog Converter (DAC), and can source or sink  $10 \text{ mA} \pm 10 \text{ V}$ . Each channel has a dedicated 64 Kword<sup>3</sup> waveform buffer. Each buffer may be segmented to provide independent subwaveforms. The unit was capable ~~to download~~<sup>of downloading</sup> an arbitrary bipolar waveform and then replay it. Any arbitrary waveform like square, sine, triangle, and sawtooth may be programmed. Two ~~pair~~<sup>pairs</sup> of MAT coils were driven using sine waveform from the four channels of the first VME-4145 board. Only two channels of the second board were used. One channel was used ~~to drive~~<sup>the</sup> superconducting RF cavity for energy modulation with a sine waveform and ~~other~~<sup>the</sup> channel was used

<sup>2</sup>VxWorks is a real-time operating system developed as proprietary software by Wind River Systems of Alameda, California, USA. First released in 1987, VxWorks is designed for use in embedded systems.

<sup>3</sup>KWord is a deprecated word processor and a desktop publishing application, part of the KOffice suite [15].

to produce a ramp (sawtooth) wave to monitor the phase of the all five drive signals. Each waveform was generated start to finish and then the next was seamlessly started. All of the waveforms were preloaded before waveform generation begins. An external trigger input from Q-weak main DAQ was used to start playback of the waveform. **This feature allowed to trigger the drive signal and ramp wave channels to synchronize in phase.** The boards were programmed to run in the continuous mode (Type II) which **scan** the waveform table **and** ran for 510 cycles and then halted. The next cycle started again when the boards were triggered from the Q-weak DAQ.

#### 1.5.4 Relay Board

**scans? scanned?**

Two sets of JLab-made 16-channel relay output register modules [16] were used to make it easy to keep everything safe and tidy for the modulation system. The board consists of four 16-bit registers used to control 16 relays and read-back status information. The front panel contains indicator LED's for power, heartbeat and relay on/off status. Relay contacts are brought out on a 50-pin D connector. A DC shift of  $\sim 0.015$  V was observed in the sinusoidal drive signal due to the relay boards which seem to have no effect on the driven coils (more details in [17]).

#### 1.5.5 Trim Power Amplifier

Four 1 to 12 A series pass regulator power supplies, known as Trim Card I, were used as power amplifier~~s~~ to control two ~~pair~~ pairs of the MAT dipoles for the beam modulation system. The Trim-I was programmable, 200 W, bipolar, power supply and was realized as a single plugin circuit board, approximately with dimension  $9'' \times 20''$ . A new generation plug-compatible supply Trim-II was being developed to replace the Trim-I by JLab accelerator group [18]. Thirty two Trim cards were housed in card-cages within a single rack (BS04B14) at BSY service building. But only four of those cards

the were used for modulation system and rest were used to power other components in the beamline.

The Trim cards consisted a Motherboard which helped to interconnect with cards, distribute power, and house the power amplifier section (shown in Figure 1.10). A 48-pin connector, mounted on the rear apron, used to engage a mating connector in the card cage where  $\pm 27$  V bulk power, 5 V power, and RS-485 communication were derived. External programming commands and data read-backs were exchanged with the EPICS via a RS-485 data link. The cards had display module in the front connected to digital temperature sensor which was used to set warning flags or shutdown the trim card in case of overheating. The Trim cards setup suffers from a discontinuity when conduction changes from the positive to negative pass bank transistor arm as the output passes though the zero

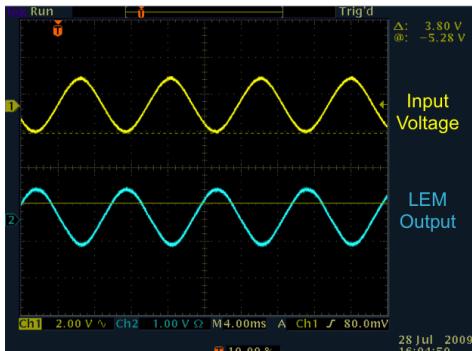
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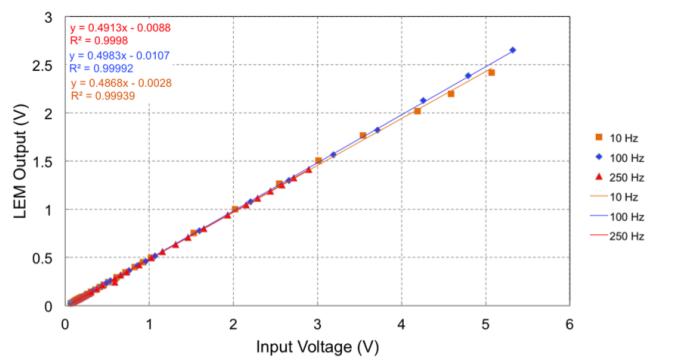
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point. This effect was suppressed by the feedback loops, and was problematic for fast ramps or step changes. The drive signal for the modulation was constrained by this phenomena, and instead of square or triangular waves, a sinusoidal wave was chosen. Originally, the Trim cards were designed to operate in the DC regime, but managed to amplify up to 250 Hz smooth sine wave linearly. Near the higher frequency and saturation current, the Trim cards locked itself to prevent any potential damage.



(a) Drive signal and LEM output from oscilloscope



(b) LEM output vs drive signal for different frequencies

Figure 1.8 LEM current transducer output response (blue) to input sine drive signal (yellow) seen by oscilloscope (left). The output from the LEM was out of phase with input signal. The figure on the right shows LEM calibration up to 5 V of input signal. The frequency dependence of the input signals were studied up to 250 Hz. The gain of the LEMs were  $\sim 0.5$ .

### 1.5.6 LEM Current Transducer

Four LEM CT-10T [19] were used to monitor the current through the two pair of the MAT dipoles. The LEM has two pins for the input current in one side and two power supply pins ( $\pm 15$  V) on the other side along with two pins for output voltages. The LEMs were calibrated up to 5.5 V of input voltage, where as nominal input operating voltage during the experiment was  $\sim 1$  V. The calibration was performed using a bench top and VME-4145 signal generators. A typical drive signal and its readback signal by a LEM are shown in Figure 1.8 (a) and the variation of LEM output with input drive voltage has been shown in Figure 1.8 (b). There was a  $180^\circ$  phase shift between the input (or Trim) signal and the LEM output signal. The measured gain was  $\sim 0.5$  for all the LEMs. There was no frequency dependence of the gain for the LEMs in the voltage domain 0 - 5 V as shown in Figure 1.8 (b). The LEMs were assembled in an insulated box and installed in the Hall-C patch panel VME crate in the BSY service building [20] and were connected in series with the

MAT dipoles. During the experiment, there was -75 mV, 240 Hz square wave noise injection in the beamline due to the cable connection fault in the LEM chassis. So, LEMs were disconnected during most of the production data taking. They were only turned on for tests and calibration during the commissioning period of the experiment. During preliminary bench test, LEM LA 50-P current transducer [21] was used to monitor the current. LEM LA 50-P used the induction method to measure the current; hence there was no series connection with the coils for the measurements. Use of the induction current transducer has a lesser chance to inject noise in the system. For future work, one might consider LEM LA 50-P or similar current transducer for precision parity measurements. The LEM current transducers have also helped to calibrate the strength of the magnets during the commissioning tests. More details about LEMs and its calibration are described in [22].

### 1.5.7 Energy Modulation Hardware

A 125 Hz sinusoidal signal was sent to an energy vernier SL-20 of a cryo-module in South linac of the accelerator to modulate the energy. One of the standard features of the accelerator is the use of Fast Feed Back (FFB) system (Section ??) to maintain a steady beam position. Unfortunately, the energy FFB system did a perfect job of countering the 125 Hz energy modulation signal. The energy monitor BPM 3C12X <sup>saw</sup> ~~see~~ no response in Figure 1.9 (bottom) for the energy modulation signal (top) when the FFB was on. So, the FFB system ~~had~~ been paused during the energy modulation to avoid any suppression from the FFB system.

### 1.5.8 ADCs

Two sets of TRIUMF built 18-bit analog to digital converters (ADCs) were used to study the readback signals from different components of the beam modulation system. Each module has eight ADC channels which were synchronized and triggered by the MPS signal sent by the helicity board. The ramp wave and 5 drive signals ( $X$ ,  $X'$ ,  $Y$ ,  $Y'$ ,  $E$ ) from VME function generator, 4 readback signals from LEM current transducer, 4 readback signals from Trim-II power amplifiers were read by the TRIUMF ADCs (more details in section ?? and [24, 25]).

All the readback channels (above mentioned 14 channels and a readback from SL-20 vernier for energy modulation) were also sent to a 32-channel JLab made ADC module [26] which was used to monitor the peaks of the signals. The ADC has 16-bit resolution and supports up to a 100 kHz sample rate. The ADC was configured by 36 16-bit registers and read the analog input data. The data format can be configured depending on the selected bipolar or unipolar input range. The analog

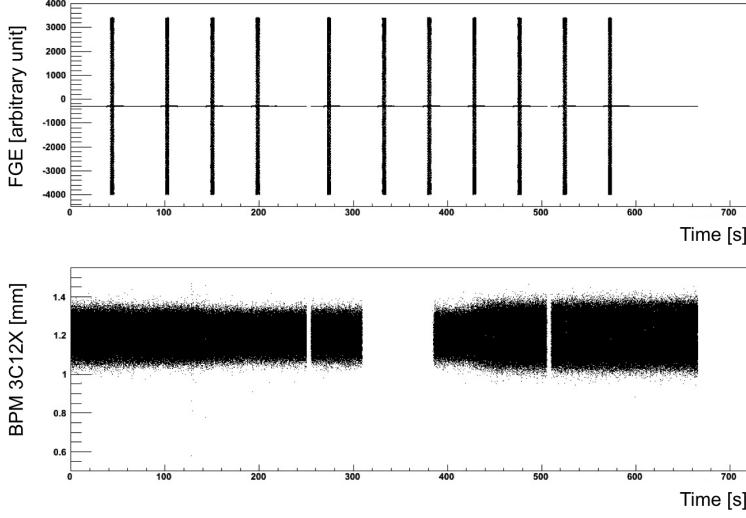


Figure 1.9 The effect of Fast Feed Back (FFB) system on energy modulation [23]. Top panel shows function generator drive signal vs time. Bottom panel shows the response of the BPM 3C12X (which is located in the middle of the arc and supposed to see maximum response for energy modulation) for the same drive signals. No response was observed in the BPM when FFB was on. The missing portions of the BPM response ~~was~~ were removed by the software stability cut in order to avoid beam trips.

inputs were fully differential and ~~was~~ configured to detect the peak of the input signals. The input connectors for the analog inputs are 50-pin D style connectors. The front panel contains indicator LED's for power and heartbeat. The JLab made peak detection ADC was used as a standalone (independent of Q-weak parity violating data acquisition system) modulation readback system and was installed in the BSY service building.

## 1.6 Hardware Components Calibration and Important Constraints

Extensive bench tests were performed with the beam modulation system so that (except for the absence of long drive cables) it would be possible to predict how the installed system would work. The Trim amplifier was controlled via an analog input from a simple bench-top function generator at the beginning and latter with VME 4145 board. The signal generator produces ~~sine wave~~ <sup>sine waves</sup> ~~amplitude and frequency~~ as the input voltage to the Trim-II power amplifier. The amplified signal goes to  $\sim 10$  cm long MAT coil through a single LEM current transducer either in phase or out of phase from two coils. The currents through the coils were measured by ammeter. The magnetic fields of the coils were measured by the Tesla meter. All the individual components were tested and calibrated in the bench test. The bench test setup is shown in Figure 1.10.

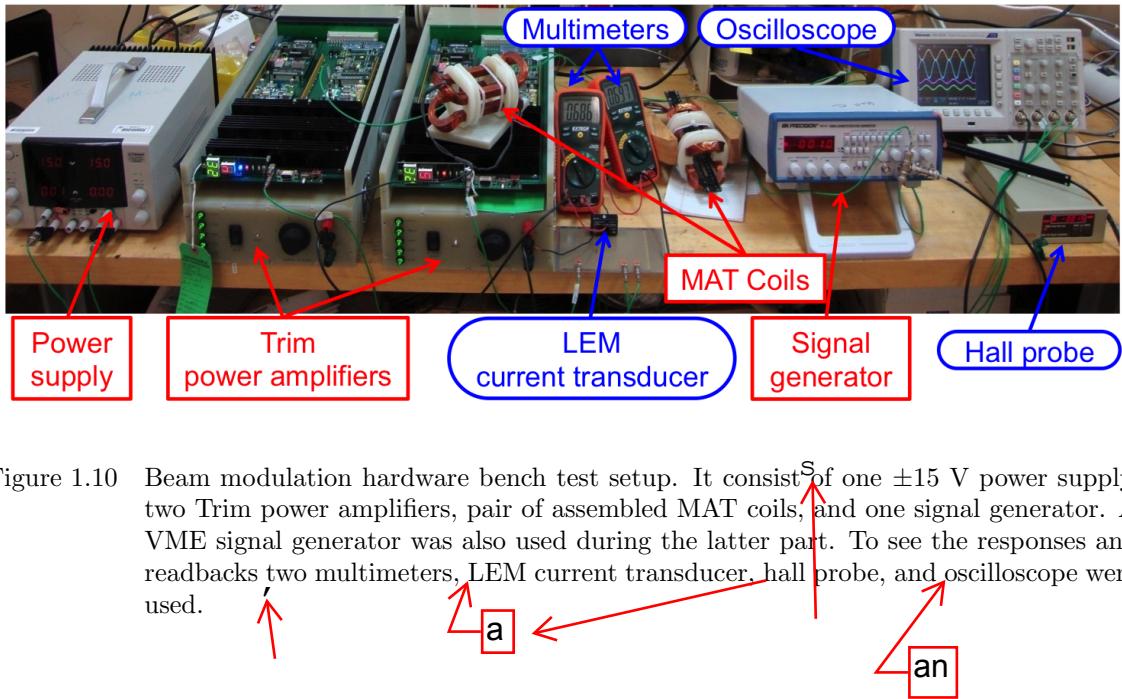


Figure 1.10 Beam modulation hardware bench test setup. It consists of one  $\pm 15$  V power supply, two Trim power amplifiers, pair of assembled MAT coils, and one signal generator. A VME signal generator was also used during the latter part. To see the responses and readbacks two multimeters, LEM current transducer, hall probe, and oscilloscope were used.

### 1.6.1 Coil Positioning

There were significant constraints on where perturbing coils could be located. One absolute requirement was that coils be located upstream of the high dispersion point at 3C12 (the center of the 3C arc) so that modulations in  $X$ ,  $X'$ , and  $E$  could be disentangled. Another highly desirable constraint was that the coils be located downstream of any expected deviations from design optics. Accelerator operations agreed to complete matching in 3C beamline by quadrupole MQA3C08, the beginning of the 3C arc dipole string. Considerations of robustness and purity therefore excluded regions upstream of this point, leaving only the first half of the 3C arc as a potential site for coils.

This coil positioning and orbit excursions were simulated using OptiM. Initially, it was attempted to insert both coils into a single  $\sim 1$  m drift, but the angle kicks of interest required excessively high field integrals and the approach did not work. Separating the coils by more than 1 meter required straddling other beamline elements. The coils were mounted between two dipoles (since the orbit inside a dipole is plotted effectively like a drift) with no intervening quadrupoles or active elements between them. The 1st pair of MAT coils, MHF3C08H ( $X_1$ ) and MHF3C08V ( $Y_1$ ), were installed in the drift 0D7028, which was located just after quadrupole 3C08 and before the dipole 3C05. The 2nd pair of MAT coils, MHF3C10H ( $X_2$ ) and MHF3C10V ( $Y_2$ ), were installed in the drift 0D7034, which was located between dipoles 3C06 and 3C07. The separation between these two pairs of coils was about  $\sim 9.5$  m. The first coil  $X_1$  was located  $\sim 92.7$  m upstream of the Q-weak target. The  $X_1$  and

$X_2$  coils were pulsed at a time and in opposite phase to produce relatively pure horizontal position or angle changes at the target, for virtually any tune of the beamline as shown in Figure 1.4.

### 1.6.2 Waveform

The Trim power amplifier was unable to drive square or even triangular waveforms in the frequency range of interest. Satisfactory results were obtained only with sinusoidal waveform, hence was used to drive the magnets. The preferred waveform was to generate at least square-ish modulation (similar to the square helicity reversal) and needed different power amplifier. Due to budget and schedule pressure existing Trim amplifiers were used.



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### 1.6.3 Waveform Phase

A 1 V of sawtooth wave with the same frequency of 125 Hz as sinusoidal drive signal from VME 4145 was used to monitor the phase of the drive signals. The sawtooth ramp wave goes to 0 to 1 V as the phase of the sinusoidal drive signal goes from 0 to  $360^\circ$  (Figure 1.11). The drive signal and ramp wave were triggered together to match and lock the phase. The edges of the ramp wave were not very sharp hence were removed during the analysis to avoid any edge effect. The edges were recreated using a ramp fill method in the software as described in [27].

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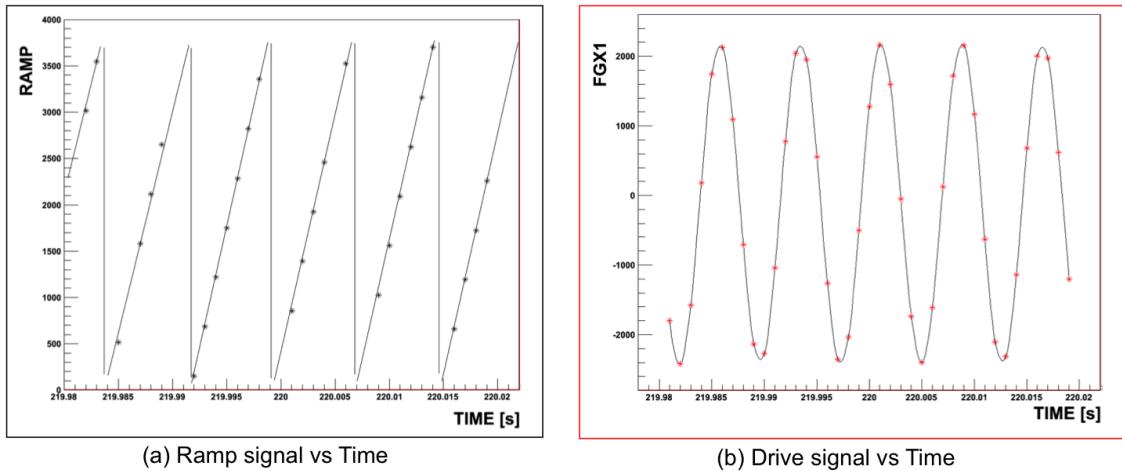


Figure 1.11 Zoomed ramp and drive signal from a beam modulation cycle during a typical production run. (a) Ramp signal vs time. The ramp signal is a sawtooth wave used to track the phase of the other sinusoidal drive signals. (b) Drive signal vs time. The drive signal is a sinusoidal wave with fixed phase.

#### 1.6.4 Frequency Range

The frequency of the waveform was tested for the range of 10-500 Hz and nominal 3 A (peak) output. The Trim cards ~~were~~ reliably drove sinusoidal waveforms up to 250 Hz. At that frequency, the coil impedance becomes approximately  $X_{\text{total}} = 1.6 \Omega + 2\pi f (0.0038 \text{ H}) = 7.6 \Omega$ , so the amplifier has to provide 22.8 V (peak). The maximum output voltage of the Trim-II amplifier appeared to be approximately  $\pm 27 \text{ V}$ , but it was not strictly bipolar due to the use of NPN diodes for one polarity and PNP diodes for the other. So while one could go a bit higher in frequency than 250 Hz, there would be a rapidly increasing risk of generating asymmetrical sine-like waves (and hence a small DC beam position offset). During production data collection, the nominal drive signal frequency was 125 Hz to stay inside the linear region of the Trim operation. Another criteria for choosing the frequency was to avoid the power line frequencies (60, 120, 180, etc. Hz) suppressed by FFB system.

#### 1.6.5 Maximum Current

With sustained operation, the coils became quite hot to the touch at  $I_{\text{peak}} = 7.07 \text{ A}$  ( $I_{\text{rms}} = 5 \text{ A}$ ). This was significantly above Q-weak's nominal maximum current  $I_{\text{peak}} = 3 \text{ A}$ , but it is worth discussing since future experiments at higher beam energy might try to push the envelope. Although measurements at 1% duty factor would take only 36 seconds per hour, one must assume that a parity violation experiment will eventually take long, dedicated beam modulation runs. Unless cooling fans ~~were~~ installed, damage to the enamel-insulated wires or any plastic components could result if  $I_{\text{peak}} = 7.07 \text{ A}$  is significantly exceeded. The "smoke point" of the magnets ~~were~~ was not determined, but bear in mind that  $P = I^2 R$ , so the temperature would increase rapidly with current above  $I_{\text{peak}} = 7.07 \text{ A}$ . It is hopefully understood that  $I_{\text{peak}} = 7.07 \text{ A}$  refers to the peak current of a sinusoidal waveform, and not to a maximum DC current which would have ~~a factor of 2 greater~~ twice the power dissipation. Constraint on maximum current based on machine protection simulation is discussed in the Section 1.9.

#### 1.6.6 Magnetic Field Calibration of the MAT Coils

The MAT coils were calibrated using ~~a~~ bench test setup, as shown in Figure 1.10. The magnetic field was measured using a GMW Hall Probe. The measured field integral for 10 cm MAT coil was  $\sim 330 \text{ G-cm/A}$ . The field was reasonably stable for the span of the coil (Figure 1.12 (a)). There was no current dependence of the field, as shown in Figure 1.12 (b). The magnetic field for the MAT coils falls quite sharply with distance beyond the coil span reduces the possibility of interaction with other active elements in the beamline. ???

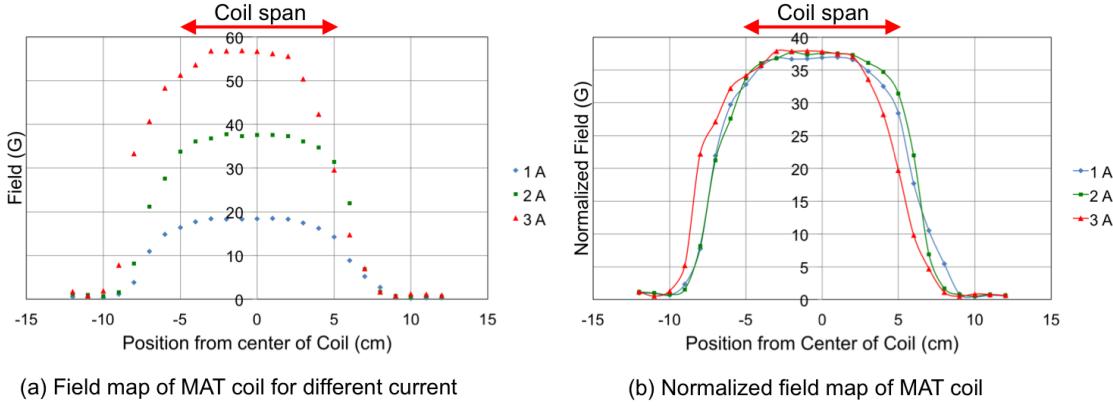


Figure 1.12 Field map of MAT coil for different input coil currents (left). The field was linear in the region of the coil span of 10 cm. The field profile did not change with coil current upto 3 A. The field was normalized with respect to 1 A (right).

## 1.7 Controls and Software Sketch

A standalone control system for the beam modulation system was designed by Scott Higgins [28–30]. The drive signals of two VME-4145 signal generator boards controlled via an EPICS database access library that works on Unix and vxWorks. In the control system the first VME-4145 card was referred as BMOD1 and the second card as BMOD2. Each function generator card has 4 channels and they are named as CHAN0, CHAN1, CHAN2, and CHAN3. All four channels of BMOD1 and CHAN0 and CHAN3 of BMOD2 were used for the modulation system. The EPICS variable for the master switch was BEAMMODSWITCH. A value for BEAMMODSWITCH of 0 was considered as OFF and 1 was ON. This switch allowed operations to control whether or not to allow any beam modulation requests. The off state was entered when the master switch was set to OFF. In the OFF state the Relays to the Trim cards were set to ground. The OFF state was the default state for the system after an IOC reboot. The CONFIG state was entered when the operations toggles the master switch from OFF to ON. Once the board was in the CONFIG state all the channels in BMOD1 and one channel BMOD2 were allowed to load a sine wave, whereas CHAN0 of BMOD2 was allowed to load ramp wave. The inputs controlling the sine wave were frequency and amplitude. The allowed frequency range was set to be 10–250 Hz, and amplitude was limited to  $\pm 0.3$  A as discussed in previous sections. A negative amplitude would shift the phase of the sine wave by  $180^\circ/\pi$ . The amplitude output for ramp wave was between 0 and 1 V. The ramp wave period started at 0 volt and then slope linearly increased to the amplitude entered. Then the ramp wave was loaded the same way as other drive signals. Before the transitions to the trigger state one must need to enter the number of periods for the sinewave or rampwave to

the

run the system. This setting ~~ranged~~ from 1 to 511. A value of 511 would cause the hardware to run the sinewave or rampwave continuously which was a feature of the hardware. Nominal cycle for the system was set to 510. The trigger state was entered by writing a value of 1 to the EPICS variable TRIGGER state.

The sine waves could be initiated by both a hardware and software trigger. The software trigger was a button that is activated by writing a value of “1” to the EPICS variable. This feature was primarily used in testing the system. The hardware trigger was initiated from the Hall-C parity violating DAQ. All of the 8 channels shared the same hardware trigger so any of the channels that were in the TRIGGER state would initiate sine wave outputs. It should be noted that if another trigger comes in while the VME-4145 is outputting a sine wave, the output will be interrupted and the card will start the sine wave from the beginning. There were 2 things that could cause a channel to leave the trigger state. ~~If~~ operations selects Beam Modulation Off with the master switch or the user selects to leave the trigger state. The EPICS variables to leave the trigger state is activated by writing a value of “1”.

run

If the user entered the trigger state after having previously ~~ran~~ a sinewave, the last loaded sine wave would be executed. There was no need to reload the sine wave in the CONFIG state if amplitude and frequency were to stay the same. If however, the user desired to change either the frequency or amplitude, a new sinewave must be loaded. There was a time delay in the reporting of the running of a sinewave from the VME-4145. A sine wave could be triggered and finished before the card reported that it was actively running a sinewave. Therefore there was no deterministic way to see the status of the card generating a wave for a particular channel in real time, at least not by monitoring the VME-4145. An external method was needed. A JLab made ADC was used to monitor ~~the~~ those channels in real time. There was a signal that went back to the hall which showed the output of the VME-4145 function generator. The goal of this signal was to show real time values written to the trim card. In order for the output of the function generator to reach the trim card, a relay ~~must~~ be set. The signal going back to the Hall-C of the function generator was between the relay board and the trim card. There were 2 RELAYS for each VME-4145 function generator channel. Both ~~was~~ were set for the channel to be connected the trim card. A value of “1” meant the relay was enabled and the function generator was connected to the trim card. A value of “0” meant the relay was off and the trim card was tied to ground. More details about the modulation control system can be found in technical documents [28, 30].

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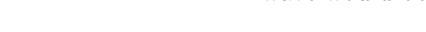














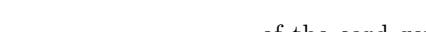










































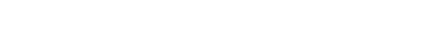














































































































































































































## 1.8 Modulation Modes

Two possible modulation modes were exercised during the experiment. One with single coil modulation, where all four coils  $X_1$ ,  $X_2$ ,  $Y_1$ , and  $Y_2$  were pulsed individually and was mainly used to calibrate and test the system during commissioning period. The other mode was one pair of coils pulsed together to achieve relatively pure position and angle at the target, and was used as nominal mode for the modulation operation. A pulse with combination of  $X_1$ , and  $X_2$  was used for horizontal position and angle, and combination of  $Y_1$ , and  $Y_2$  was used for vertical position and angle motion. The energy modulation was the same for both the modes. The motivations for using a pair over a single dipole were greater flexibility in coil positioning, coil positions being independent of beamline optics, and a compact configuration. The nominal current through the MAT dipole for the pair mode is shown in Table 1.3. A unique pattern number was assigned in the software to identify the different modulation mode, and parameter as listed in Table 1.5.

Table 1.5 Different beam modulation modes and related pattern numbers. In single coil mode, just one coil pulsed and the response is a linear combination of position and angle. In pair of coils, two coils were pulsed at a time to produce relatively pure position or angle.

Mode	Parameter	Coils Pulsed	Pattern Number
Single coil	$X$ and $X'$	$X_1$	1
	$X$ and $X'$	$X_2$	2
	$Y$ and $Y'$	$Y_1$	3
	$Y$ and $Y'$	$Y_2$	4
	$E$	$E$	5
Pair of coils	$X$	$X_1$ and $X_2$	11
	$Y$	$Y_1$ and $Y_2$	12
	$E$	$E$	13
	$X'$	$X_1$ and $X_2$	14
	$Y'$	$Y_1$ and $Y_2$	15

## 1.9 Machine Protection Analysis

A simulation was performed to check the maximum possible excursion in the beamline due to beam modulation magnet kicks. The nominal field integrals for the modulation MAT coils are given in Table 1.3 and the corresponding excursions are shown in Figure 1.5. For this simulation, the modulation kicks were increased by increasing the nominal field by 5 times to enhance the effect (these excursions are linearly scaled). The beam excursions with this conditions were 1.3 mm at the upstream of the target and 1.0 mm at the beam dump. The tune parameters in Table 1.3 were

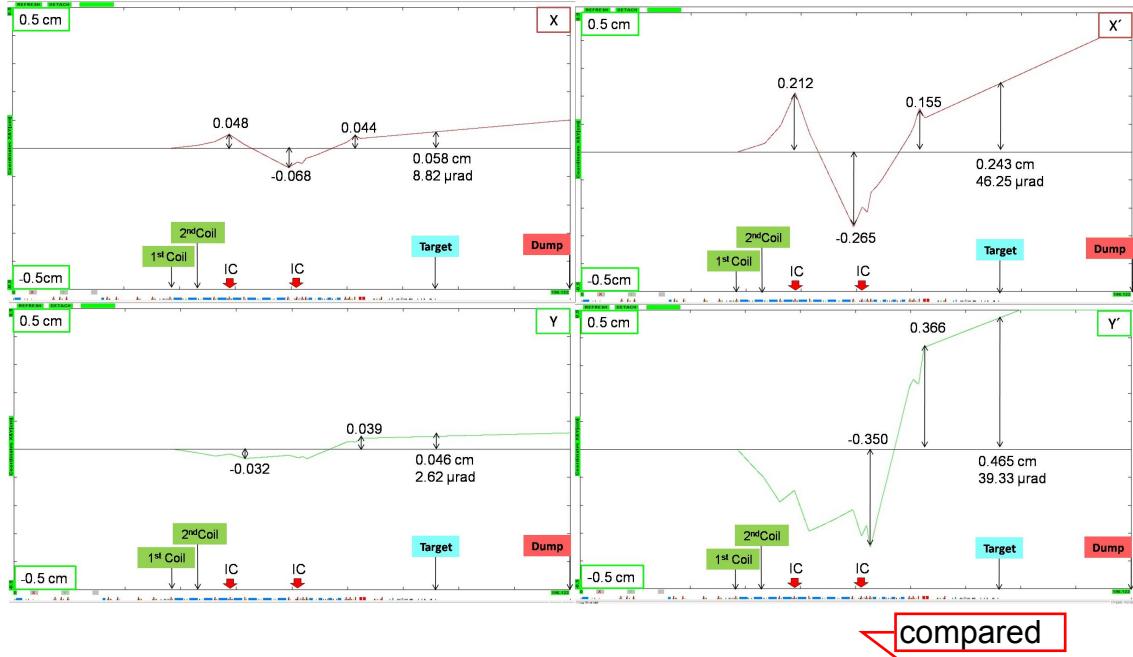


Figure 1.13 Orbit excursions using a pair of coils with incorrect polarity on one of the coil. Beam moves from left to right. Large excursions were observed for angle ~~compare~~ to position. The used field strength to pulse the coils for this simulation ~~were~~ 5 times higher than that ~~was~~ used as nominal field strength during the experiment. The location for ion chambers (IC) ~~were~~ recommended based on this study and is shown by the thick arrows at the bottom of the figure.

negative, which implies the opposite polarity of the magnets. To check the worst possible scenario, ~~was~~ the polarity of the magnets ~~were~~ reversed (using the same 5 times of nominal field) ~~and~~, the simulated ~~shown~~ orbits are ~~sown~~ in Figure 1.13. The reversed polarity deviations upstream of the target ~~was~~ was 3.6 mm and 6.6 mm at the beam dump. The same simulation with only one coil energized deviations was 2.4 mm upstream of the target and 3.8 mm at the beam dump for  $I_{max} = 0.6$  A. Considering all of ~~these~~ ~~the~~ cases, the maximum obtained excursion was about 4.6 mm at the target for ~~a~~ maximum current of 0.6 A. For angles ~~the~~ the excursions were much larger than position excursion ~~and~~ mainly in the regions middle of the arc (around quadrupole 3C12) and end of the arc (around quadrupole 3C17). The deviation at the beam dump was 6.6 mm for  $I_{max} = 0.6$  A. For protection of the machine, considering ~~was~~ all the above cases, the recommended place to install ion chambers (IC) ~~were~~ at the highest beam excursion region of the beamline around 3C12 and 3C17 (as shown in Figure 1.13). The worst case scenario found to be the case of incorrect polarity. In order to avoid any mishap, when system ~~was~~ commissioned, a hard coded software limit of  $I_{max} = 0.3$  A was implemented for the safety of the accelerator. More details about the machine protection analysis can be found in Q-weak internal technical document [31].

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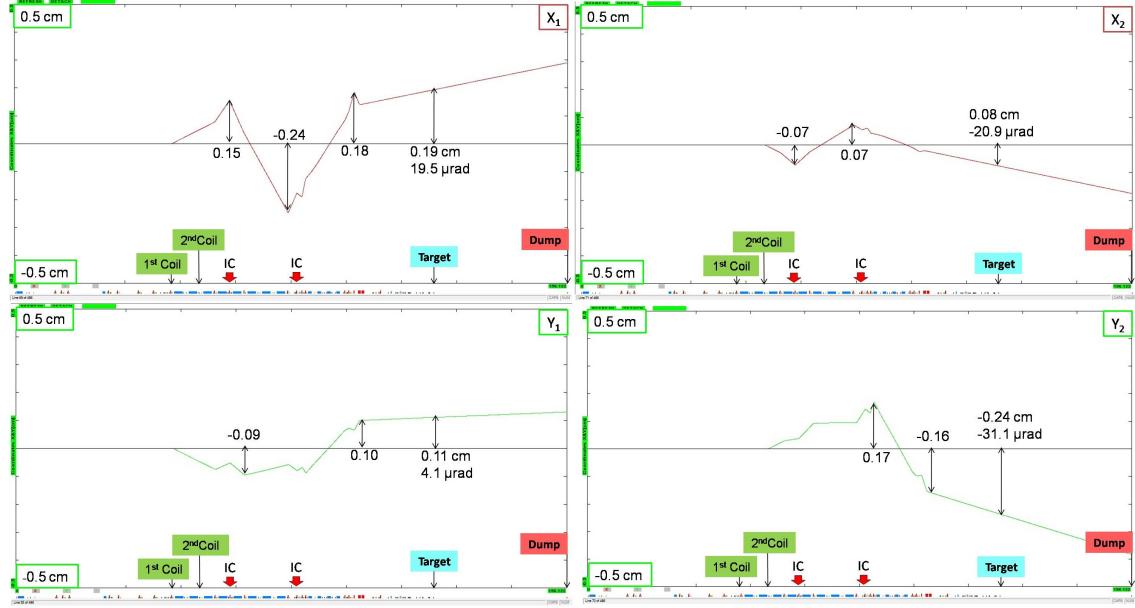


Figure 1.14 Orbit excursions with only one coil energized. Beam moves from left to right. Large excursions were observed for  $X_1$  and  $Y_2$  coils. The maximum current used for all the coils was  $I_{\max} = 0.6$  A. A hard coded restriction of  $I_{\max} = 0.3$  A in the software was set for the safety of the accelerator based on this analysis.

## 1.10 Beam Modulation Cycle

A typical beam modulation cycle vs time during production run is shown in Figure 1.15. A micro cycle ran for 510 cycles with a nominal frequency of 125 Hz for each beam parameter. So the consisted cycle for each parameter was  $\sim 4$  s. One macro cycle consists of the  $X$ ,  $X'$ ,  $E$ ,  $Y$ ,  $Y'$  cycles and ran for 320 s. Each macro cycle was then continuously repeated. The configuration time between each micro cycle was  $\sim 75$  s. Modulation ran with a duty factor of  $\sim 6\%$ . A zoomed version of the ramp and sinusoidal drive signal from the Figure 1.15 is shown in Figure 1.11.

## 1.11 Response to Modulation Signal and Applications

Main detector response to horizontal position ( $X$ ) modulation is shown in Figure 1.16. The Detectors 1 and 5 show detector coordinate is shown in the center of the figure. Detector 1 and 5 shows the maximum response for the  $X$  modulation and are anti correlated to each other. Negligible response has been seen in octants 3 and 7. Detector responses correlated with modulation were used to extract sensitivities for the main detector and is discussed in the next chapter.

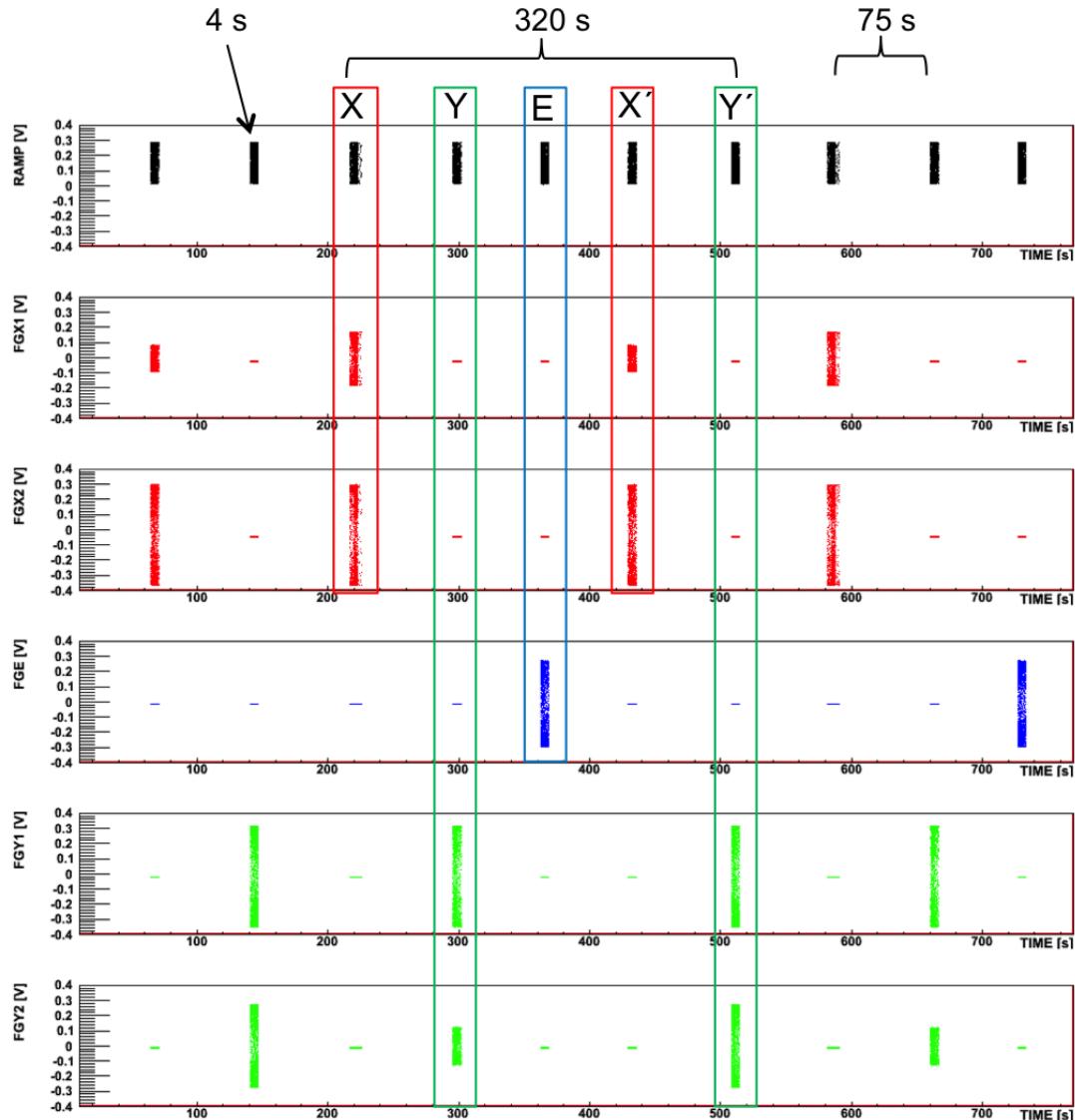


Figure 1.15 Beam modulation cycle during a typical production run. 1st panel shows ramp wave to calibrate sinusoidal signals vs time. 2nd and 3rd panels show sinusoidal drive signals for horizontal position ( $X$ ) and angle ( $X'$ ) modulation vs time. 4th panel shows sinusoidal drive signals for energy ( $E$ ) modulation vs time. 5th and 6th panels show sinusoidal drive signal for vertical position ( $Y$ ) and angle ( $Y'$ ) modulation vs time. The cycle for each parameter is  $\sim 4$  s. One macro cycle consists of the  $X$ ,  $X'$ ,  $E$ ,  $Y$ ,  $Y'$  cycles and ran for 320 s.

A typical BPM response to nominal modulation drive signal is a sinusoidal of amplitude  $\sim 200 \mu\text{m}$ , as shown in Figure 1.17. Compared with natural beam jitter, this is an order of magnitude larger and has fewer correlations among the parameters, providing an independent way of measuring sensitivities. Figure 1.17 shows a pair of drive signals for  $X$  modulation in top two panels, where as

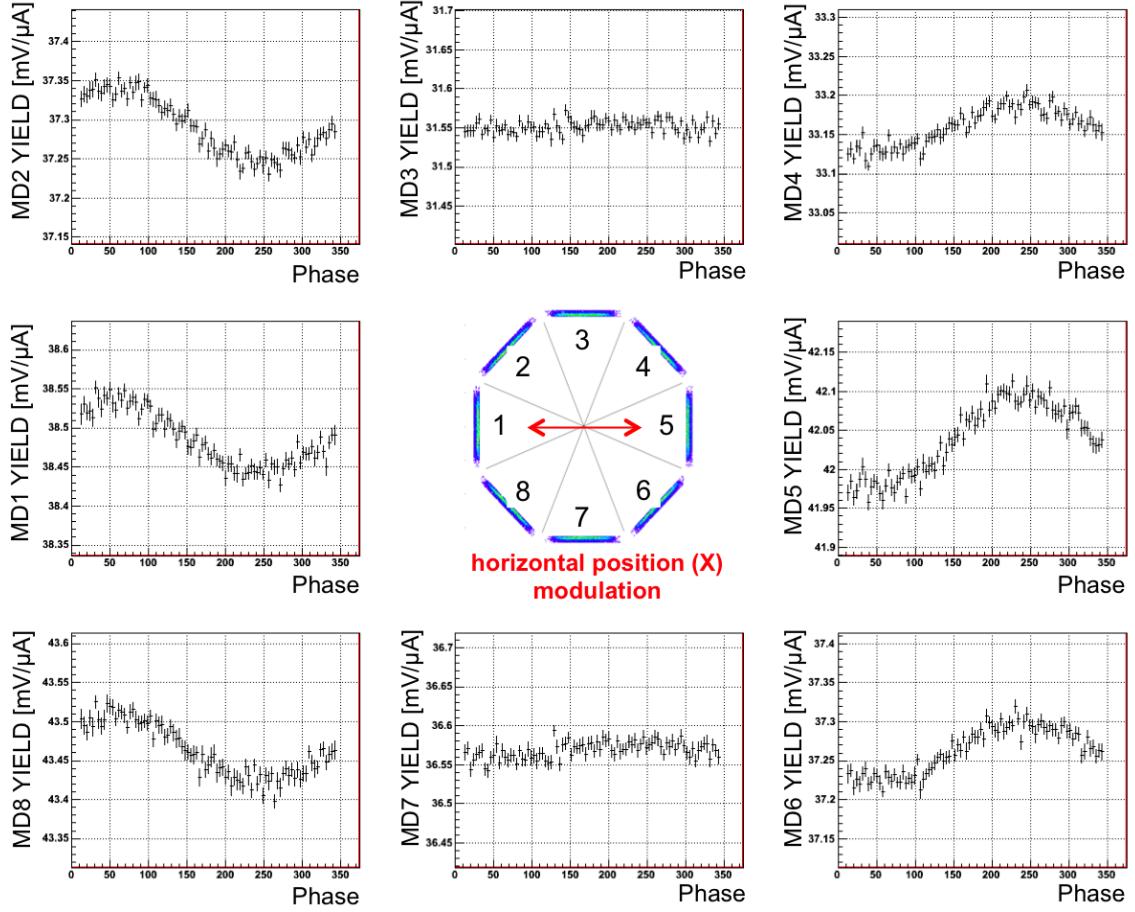


Figure 1.16 Main detector response to  $X$  position modulation. Main detector yields vs modulation phase (ramp wave) plotted for each detector.

the target BPM  $X$  and  $Y$  responses are shown in the bottom two panels. As expected, the the BPM  $X$  shows a significant sinusoidal response to the horizontal drive signal but no response in Besides  $Y$ . Beside measuring sensitivities, the BPM response to the modulation signal helped to track any optics change in the Hall-C beamline. The Following chapter will discuss the application and products of beam modulation system.

the

## 1.12 Extension to Other JLab Parity Violation Experiments

The beam modulation system described in this chapter should be useful for other parity violation experiments such as the Moeller experiment at 11 GeV in Hall-A, JLab [32]. Some basic limitations should be kept in mind. First of all, the modulation amplitude of the system described here will scale like  $E_{\text{beam}}$  (GeV)/1.165, hence the amplitudes at 11 GeV will be smaller by an order of magnitude.

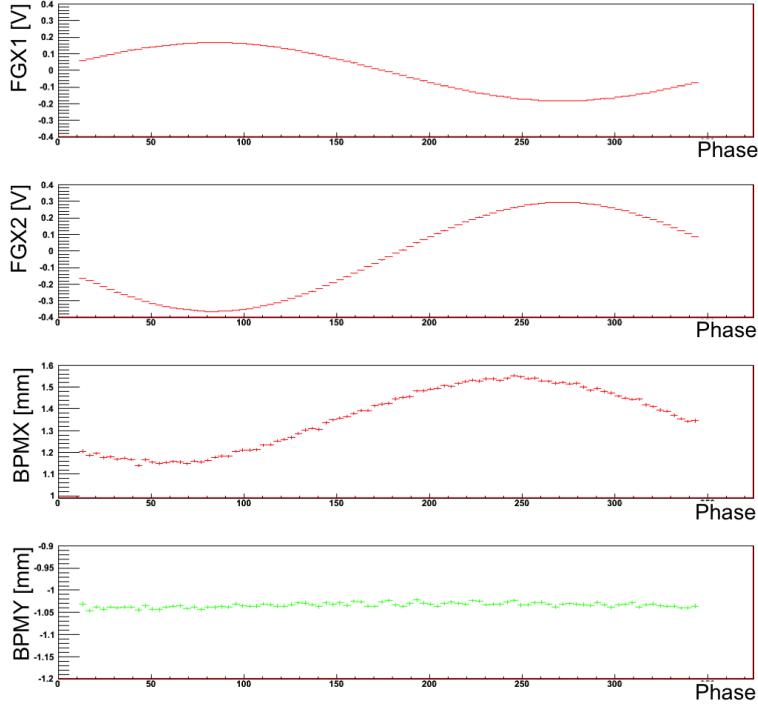


Figure 1.17 Target BPM response to  $X$  position modulation. The signals were plotted vs modulation phase. The drive ~~signals~~ in coils  $X_1$ , and  $X_2$  are shown in top two panels and the corresponding BPM response in  $X$ , and  $Y$  are shown in bottom two panels.

If the amplitude becomes smaller than the random beam jitter, convergence will be greatly slowed. The air-core coils can be driven harder if the duty factor is limited or fans are used to cool the coils, but at about 5 A (rms) they become hot enough to risk damaging the enamel coatings on the wires under continuous duty. Secondly, at the frequencies of interest, the coil is an almost purely inductive load, so the voltage needed to drive a given current is nearly proportional to frequency. If ~~wishes~~ one ~~wish~~ to modulate the beam faster than the 250 Hz system described here, faster, higher voltage power amplifiers than the Trim-II would be needed. Alternatively, larger field integrals could be obtained for a given current by replacing air-core coils with ferrite magnets. Finally, because the final quadrupole is closer to the target in the Hall-A beamline (1C) line [33], it should be somewhat easier to generate a given angle kick at a given beam energy as compared to the 3C line.

### 1.13 Summary

The beam modulation system presented here was designed for sinusoidal modulation up to 250 Hz which was robust and well-suited for experiments measuring small parity violating asymmetries like

the Q-weak experiment. At the cost of 1% of beam time for one parameter, the system was able to measure all sensitivities to 10% accuracy each day. The pairs of coils were tuned to deliver relatively positions pure position or angle modulations, making it much less likely that one when encounter singular are encountered matrices when solving for the sensitivities. The system was independent of the design optics as changing the the ratio of coil currents to incorporate any optics change in the beamline compare the drives the signal. to move the coils physically. For 1.165 GeV electron beam using 125 Hz sinusoidal drive signal the Trim power amplifier was able to provide the desired beam modulation amplitudes with existing air-core HF (MAT) coils. The modulation system worked quite well for the span of two years during the Q-weak experiment and collected data noninvasively with production running. However, providing similar amplitudes for the Moller PV experiment at 12 GeV in Hall-A may require an upgrade of the amplifier or magnets.

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