

# One-dimensional MHD code tests

Xuyao Hu

Department of Physics, New York University

December 16, 2016

# Contents

- 1 Introduction – MHD system
- 2 Algorithm
- 3 Numerical results

# 1 Introduction – MHD system

## 2 Algorithm

## 3 Numerical results

# Introduction – MHD system

Magnetohydrodynamics (MHD) is extremely important in various fields such as Astrophysics, Geophysics and Plasma Physics.

An ideal MHD system is governed by hydrodynamics equations and Maxwell's equations, which can be written in a conservative form as

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0 , \quad (1)$$

$$\frac{\partial \rho \mathbf{v}}{\partial t} + \nabla \cdot (\rho \mathbf{v} \mathbf{v} - \mathbf{B} \mathbf{B} + \mathbf{P}_T) = 0 , \quad (2)$$

$$\frac{\partial E}{\partial t} + \nabla \cdot [(E + P_T) \mathbf{v} - \mathbf{B} (\mathbf{B} \cdot \mathbf{v})] = 0 , \quad (3)$$

$$\frac{\partial \mathbf{B}}{\partial t} - \nabla \times (\mathbf{v} \times \mathbf{B}) = 0 , \quad (4)$$

where  $P_T = P + \frac{1}{2} B^2$ .

# Introduction – 1D MHD problem

“One-dimensional”  $\implies$  All physical quantities depends only on **one** position variable (say,  $x$  in 3D Cartesian coordinates) and time  $t$ .

$$\frac{\partial \mathbf{U}}{\partial t} + \frac{\partial \mathbf{F}}{\partial x} = 0, \quad (5)$$

with

$$\mathbf{U} = \begin{pmatrix} \rho \\ \rho v_x \\ \rho v_y \\ \rho v_z \\ E \\ B_y \\ B_z \end{pmatrix}, \quad \mathbf{F} = \begin{pmatrix} \rho v_x \\ \rho v_x^2 + P_T - B_x^2 \\ \rho v_x v_y - B_x B_y \\ \rho v_x v_z - B_x B_z \\ (E + P_T)v_x - (\mathbf{B} \cdot \mathbf{v})B_x \\ B_y v_x - B_x v_y \\ B_z v_x - B_x v_z \end{pmatrix}, \quad (6)$$

and  $B_x = \text{constant}$ .

1 Introduction – MHD system

2 Algorithm

3 Numerical results

# Algorithm – Piecewise Linear Method (PLM)

Use PLM to reconstruct the “left” and “right” states at each cell interface

$$Q_{i+1/2}^L = Q_i + 0.5 \minmod(\theta(Q_i - Q_{i-1}), 0.5(Q_{i+1} - Q_{i-1}), \theta(Q_{i+1} - Q_i)) , \quad (7)$$

$$Q_{i+1/2}^R = Q_{i+1} - 0.5 \minmod(\theta(Q_{i+1} - Q_i), 0.5(Q_{i+2} - Q_i), \theta(Q_{i+2} - Q_{i+1})) , \quad (8)$$

where  $\theta = 1.1$ ,  $Q$  denotes  $\rho$ ,  $v_x$ ,  $v_y$ ,  $v_z$ ,  $P$ ,  $B_x$ ,  $B_y$ ,  $B_z$ .

# Algorithm – HLL vs. HLLD

- **HLL** – determine the flow through each interface using **one** intermediate state

$$\mathbf{F}_{\text{HLL}} = \begin{cases} \mathbf{F}_L & \text{if } S_L > 0 , \\ \mathbf{F}^* & \text{if } S_L \leq 0 \leq S_R , \\ \mathbf{F}_R & \text{if } S_R < 0 . \end{cases} \quad (9)$$

See Miyoshi & Kusano (2005) for more details.



# Algorithm – HLL vs. HLLD

- **HLL** – determine the flow through each interface using **one** intermediate state

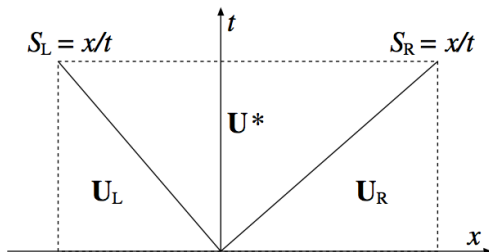


Fig. 1. Schematic structure of the Riemann fan with one intermediate state.

See Miyoshi & Kusano (2005) for more details.

# Algorithm – HLL vs. HLLD

- **HLLD** – determine the flow through each interface using **four** intermediate state

$$F_{\text{HLLD}} = \begin{cases} F_L & \text{if } S_L > 0 , \\ F_L^* & \text{if } S_L \leq 0 \leq S_L^* , \\ F_L^{**} & \text{if } S_L^* \leq 0 \leq S_M , \\ F_R^{**} & \text{if } S_M \leq 0 \leq S_R^* , \\ F_R^* & \text{if } S_R^* \leq 0 \leq S_R , \\ F_R & \text{if } S_R < 0 . \end{cases} \quad (9)$$

See Miyoshi & Kusano (2005) for more details.

# Algorithm – HLL vs. HLLD

- **HLLD** – determine the flow through each interface using **four** intermediate state

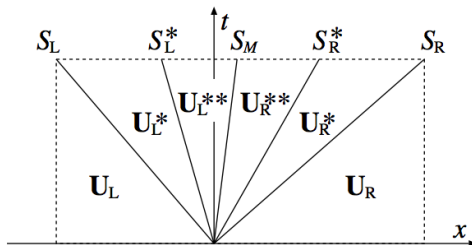


Fig. 3. Schematic structure of the Riemann fan with four intermediate states.

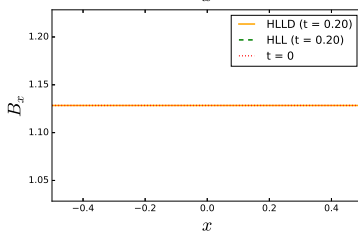
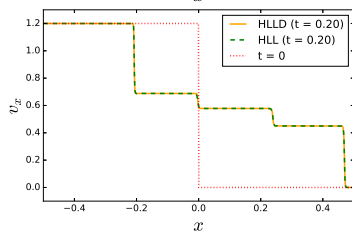
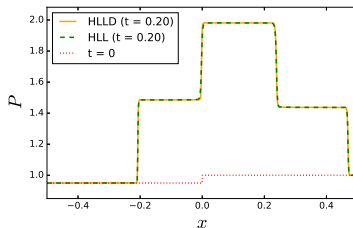
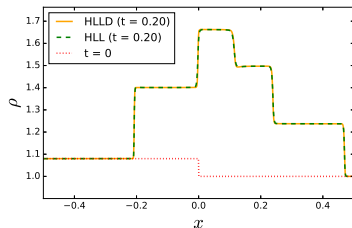
See Miyoshi & Kusano (2005) for more details.

1 Introduction – MHD system

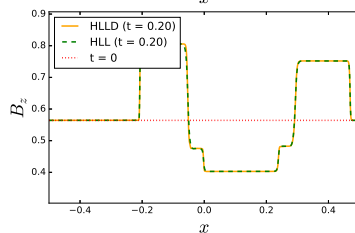
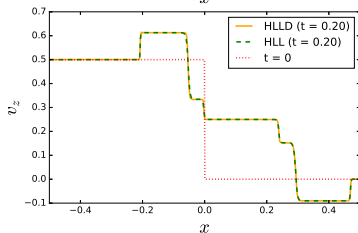
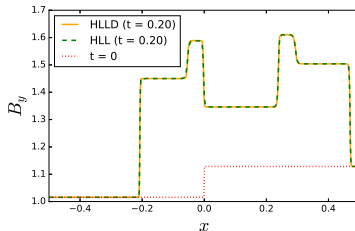
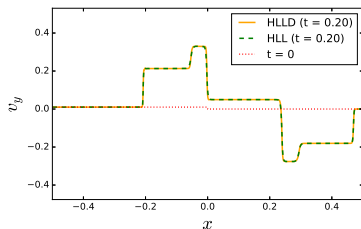
2 Algorithm

3 Numerical results

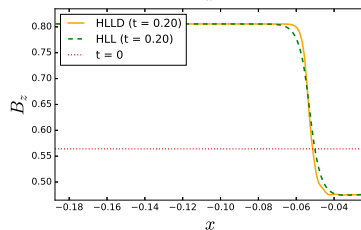
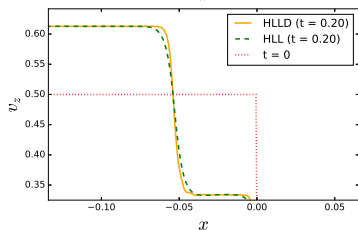
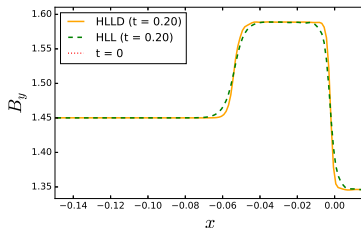
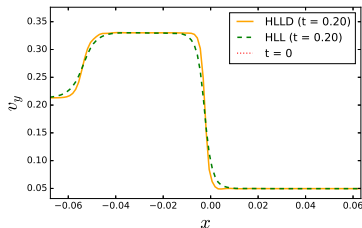
# Dai & Woodward shock tube



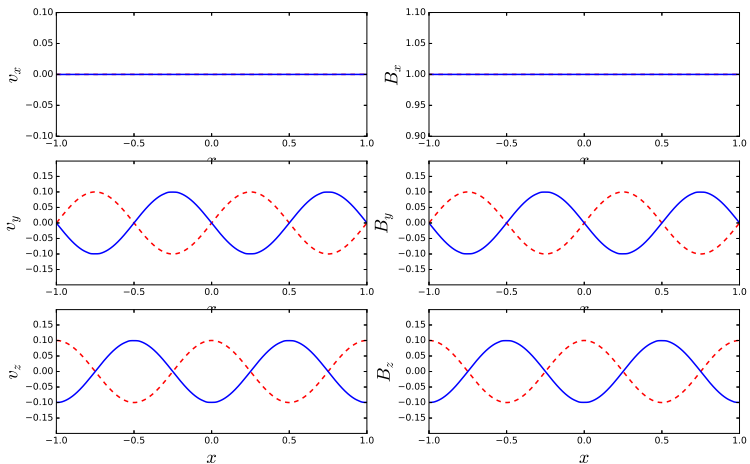
# Dai & Woodward shock tube



# Dai & Woodward shock tube



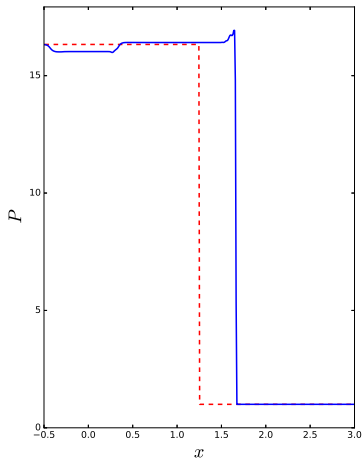
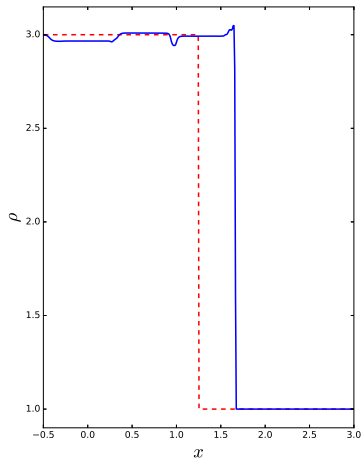
# Alfvén Wave



$t_{\text{final}} = 2.5$ . The density  $\rho$  and the pressure  $P$  basically remain constant.

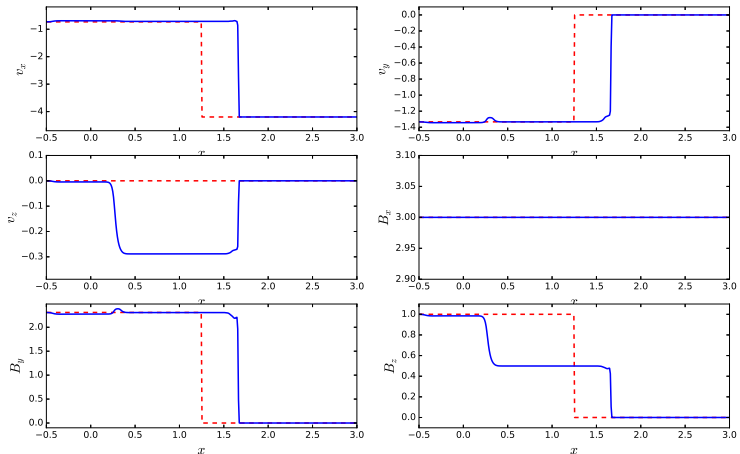


# Fast Switch-on (FS) shock test



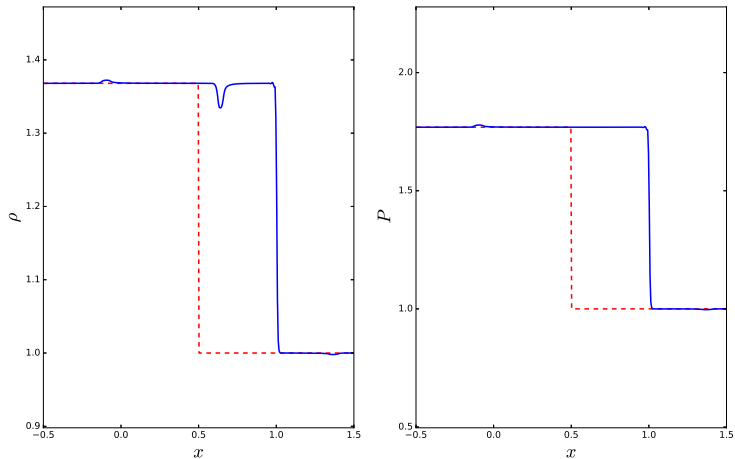
$t_{\text{final}} = 0.4$

# Fast Switch-on (FS) shock test



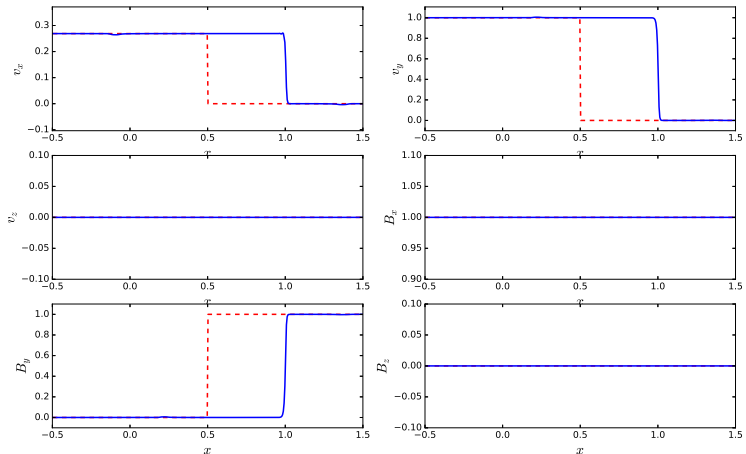
$t_{\text{final}} = 0.4$

# Slow Switch-on (SS) shock test



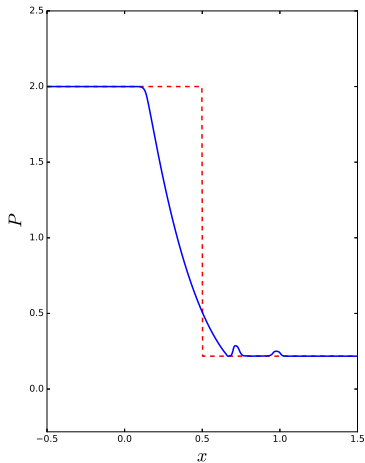
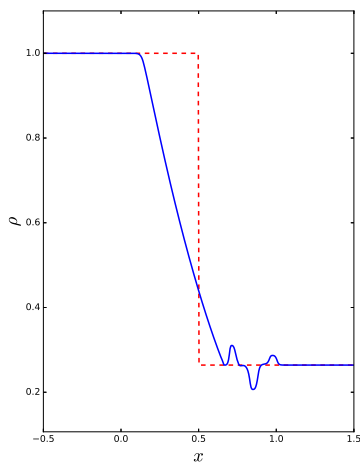
$t_{\text{final}} = 0.5$

# Slow Switch-on (SS) shock test



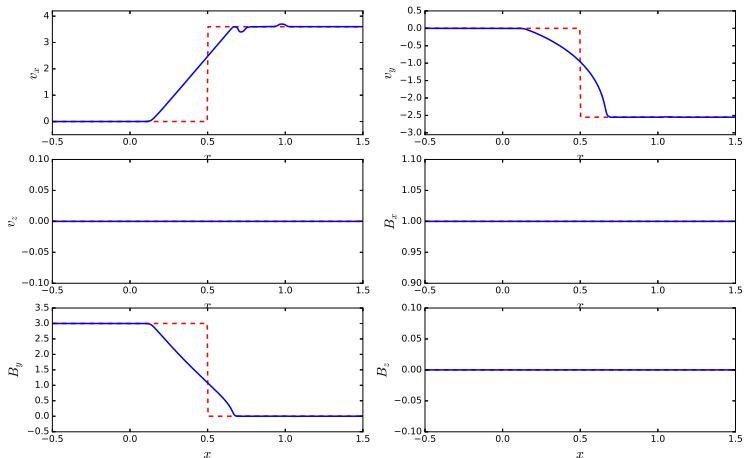
$t_{\text{final}} = 0.5$

# Fast Rarefaction (FR) waves test



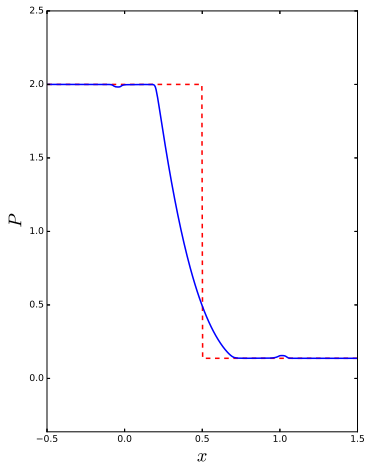
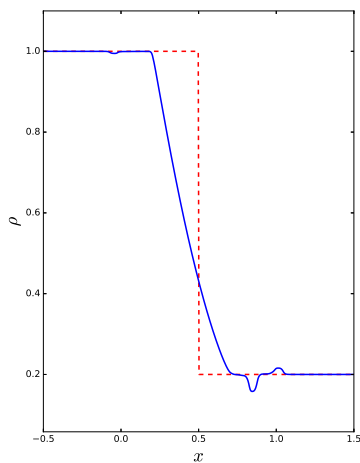
$t_{\text{final}} = 0.1$

# Fast Rarefaction (FR) waves test



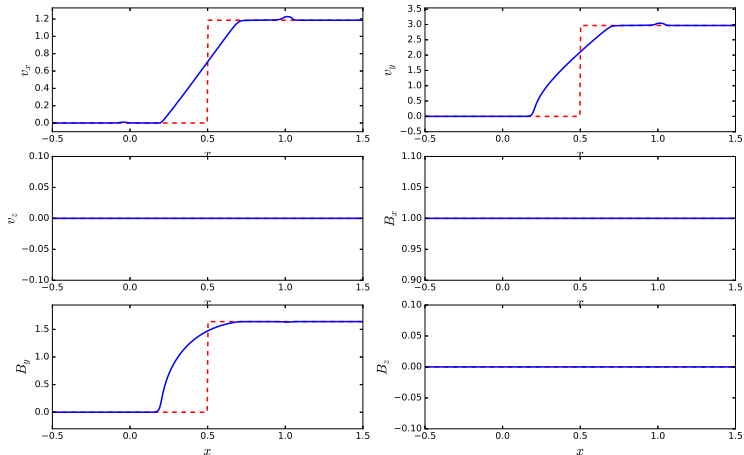
$t_{\text{final}} = 0.1$

# Slow Rarefaction (SR) waves test



$t_{\text{final}} = 0.3$

# Slow Rarefaction (SR) waves test



$t_{\text{final}} = 0.3$