

# Probability Density Function for Adsorption Energies over Time on Heterogeneous Surfaces by Inverse Gas Chromatography

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The inverse gas chromatographic method of reversed-flow gas chromatography is extended to the measurement of the probability density function  $f(\epsilon)$  for the adsorption energies on heterogeneous surfaces, as a function of the experimental time. The values of  $f(\epsilon)$  are not found from the solution of an integral equation, but by their direct calculation from experimental data in a very simple way. The method is applied to the adsorption of  $(\text{CH}_3)_2\text{S}$  on  $\text{CaCO}_3$  and  $\text{CaCO}_3 + \text{C}$ , in the presence and in the absence of  $\text{NO}_2$ , at two temperatures around 303 and 323 K. The kinetic physicochemical parameters for the adsorption/desorption phenomena are also calculated for the above systems. The normalization of the  $f(\epsilon)$  found, with respect to time, is easily done.

## Introduction

The inverse gas chromatographic tool of reversed-flow gas chromatography (RF-GC) was recently applied<sup>1</sup> to measure the time distribution of adsorption energies,  $\epsilon$ , the local monolayer capacities,  $c_{\text{max}}^*$ , and the local isotherms,  $\theta_i(p, T, \epsilon)$  for some probe gases on heterogeneous solid surfaces in the presence of nitrogen as carrier gas. The method does not depend on analytical or numerical solutions of the classical integral equation

$$\Theta(p, T) = \int_0^\infty \theta_i(p, T, \epsilon) f(\epsilon) d\epsilon \quad (1)$$

where  $\Theta(p, T)$  is the overall experimental adsorption isotherm and  $f(\epsilon)$  is the probability density function for the adsorption energies, but on a time function of the chromatographic peaks obtained by short flow reversals of the carrier gas:

$$H^{1/M} = \sum_{i=1}^4 A_i \exp(B_i t) \quad (2)$$

where  $H$  is the peak height,  $M$  is the response factor of the detector,  $A_i$  is the preexponential factors, and  $B_i$  is the exponential coefficients of time  $t$ , when flow reversals were made. For convenience, Figure 1 of the previous publication<sup>1</sup> is repeated here. The calculation of  $B_i$  values from the experimental pairs  $H$ ,  $t$  and their physical content has been reported earlier.<sup>2,3</sup> The relevant mathematical model was based on two mass balances of the probe gaseous concentrations, the rate of change of the adsorbed concentration on the heterogeneous solid surface, and an isotherm for the local adsorbed equilibrium concentration on the solid. The term "local" means with respect to time, i.e., involving only a limited collection of adsorption sites active at time  $t$ .

The necessary relations for calculating from eq 2 the values of  $\epsilon$ ,  $c_{\text{max}}^*$  and  $\theta_i$  for the adsorption of gases on heterogeneous surfaces as a function of time have been derived<sup>1</sup> by combining eq 2 with the Jovanovic isotherm model:

$$\theta(p, T, \epsilon) = 1 - \exp(-Kp) \quad (3)$$

where

$$K = K^0(T) \exp(\epsilon/RT) \quad (4)$$

$R$  being the gas constant and  $K^0$  being given by eq 9 of ref 1.

Four auxiliary relations, involving  $A_i$ ,  $B_i$ , and  $t$  of eq 2, give as functions of them the gaseous concentration  $c_y$  (mol/cm<sup>3</sup>) of the adsorbate A (eq 4 of ref 1), its local adsorbed equilibrium concentration  $c_s^*$  (eq 5 of ref 1), and the two partial derivatives  $\partial c_s^*/\partial c_y$  and  $\partial^2 c_s^*/\partial c_y^2$  (eqs 6 and 14, respectively, of ref 1).

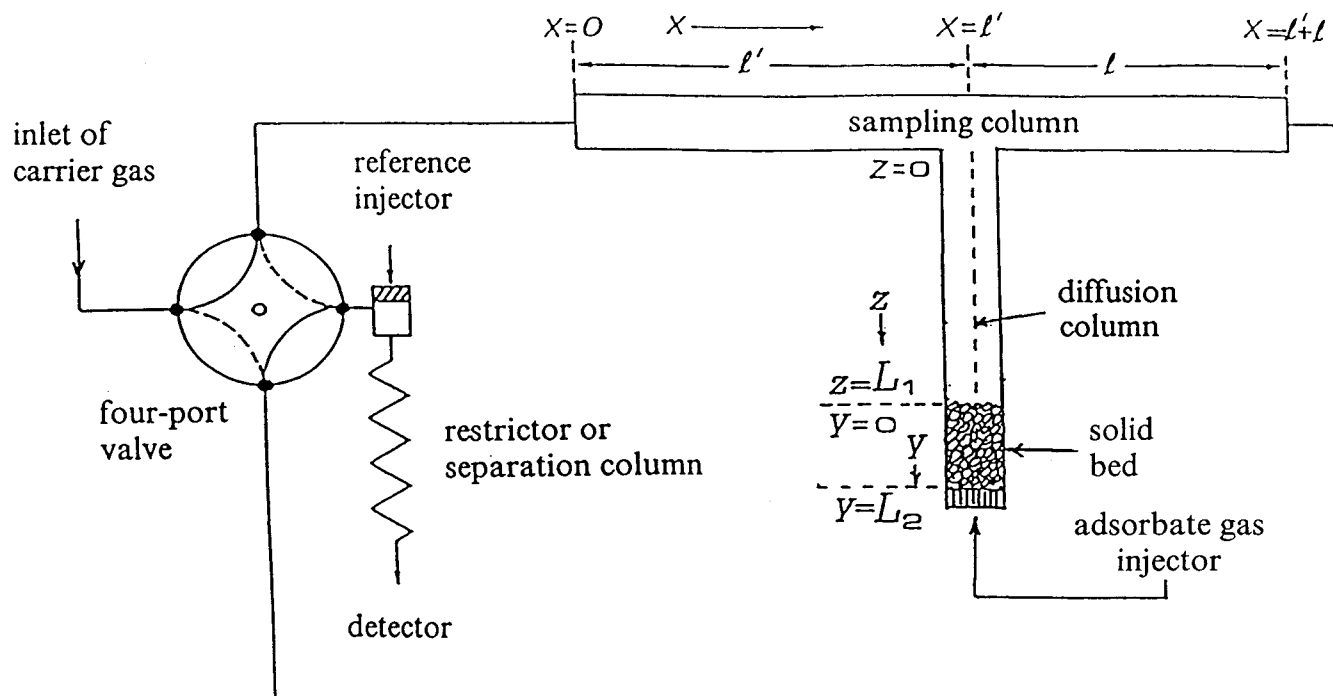
It has been shown before (eq 13 of ref 1) that the ratio of the last two partial derivatives, equals  $-KRT$ , where  $K$  is Langmuir's constant of eq 4.

Substituting in the above ratio of the two partial derivatives the right-hand sides of eqs 6 and 14 of ref 1, one finds, in view also of eq 4,

$$KRT = RTK^0 \exp(\epsilon/RT) = \frac{gD_1}{vL_1} \left\{ \frac{\sum_i A_i B_i^2 \exp(B_i t)}{[\sum_i A_i B_i \exp(B_i t)]^2} - \frac{1}{\sum_i A_i \exp(B_i t)} \right\} \quad (5)$$

where  $v$  (cm/s) is the corrected linear flow velocity of the carrier gas,  $L_1$  (cm) is the length of section  $z$  of the diffusion column (cf. Figure 1),  $g$  is the calibration factor of the chromatographic detector in cm (peak height)/mol cm<sup>-3</sup>, and  $D_1$  (cm<sup>2</sup>/s) is the diffusion coefficient of A in section  $z$  of the diffusion column.

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**Figure 1.** Schematic representation of the columns and gas connections showing the principle for using the reversed-flow technique as an inverse gas chromatographic tool.

The relation for calculating  $\epsilon$  (kJ/mol) from experimental data follows from the left part of eq 5, i.e.

$$\epsilon = RT [\ln(KRT) - \ln(RT) - \ln K^0] \quad (6)$$

whereas the relation for calculating  $c_{\max}^*$  (mol/g) and  $\theta_t$  are

$$c_{\max}^* = c_s^* + \frac{\partial c_s^* / \partial c_y}{KRT} \quad (7)$$

$$\theta_t = 1 - \frac{1}{c_{\max}^*} \frac{\partial c_s^* / \partial c_y}{KRT} \quad (8)$$

All above calculations are easily carried out by running the PC program in GW-BASIC available as Supporting Information of ref 1.

In the present work the probability density function with respect to the energy,  $f(\epsilon)$ , over time on a heterogeneous surface is approached, neither by seeking analytical solutions of the integral eq 1 nor by employing numerical solutions and estimation methods, as recently reviewed,<sup>2</sup> but by a direct calculation of  $f(\epsilon)$  from experimental data (eq 2) in a relatively simple way.

The new method for finding  $f(\epsilon)$  is exemplified by presenting results of dimethyl sulfide vapor adsorbed on pieces of Penteli marble (pure or covered with carbon black), in the absence and presence of gaseous nitrogen dioxide, in a pure nitrogen atmosphere.

## Theory

According to Jaroniec and Madey,<sup>4</sup> the probability function  $f(\epsilon)$  of eq 1, describing the adsorption energy distribution, is defined as "the derivative of the number of adsorption sites with respect to the adsorption energy". Since the number of adsorption sites is proportional to the local monolayer capacity  $c_{\max}^*$

of eq 7, one may define  $f(\epsilon)$  as

$$f(\epsilon) = \frac{\partial c_{\max}^*}{\partial \epsilon} = \frac{\partial c_s^*}{\partial \epsilon} + \frac{\partial^2 c_s^* / \partial c_y \partial \epsilon}{RTK^0 \exp(\epsilon/RT)} - \frac{\partial c_s^* / \partial c_y}{(RT)^2 K^0 \exp(\epsilon/RT)} \quad (9)$$

The far-right-hand side of the above equation was obtained from eq 7 by differentiation with respect to the energy  $\epsilon$ . It is obvious that  $f(\epsilon)$  is an explicit function of energy  $\epsilon$ ,  $f(\epsilon)d\epsilon$  giving the probability for adsorption energies in the interval between  $\epsilon$  and  $\epsilon + d\epsilon$ .

Since both  $c_{\max}^*$  and  $\epsilon$  change with the time of measurement,<sup>1</sup> the simplest way to calculate  $f(\epsilon)$  is through the relation

$$f(\epsilon; t) = \frac{\partial c_{\max}^*}{\partial \epsilon} = \frac{\partial c_{\max}^* / \partial t}{\partial \epsilon / \partial t} \quad (10)$$

In this equation  $t$  is a structural parameter and not a random variable. Thus,  $f(\epsilon)$  as defined by  $\partial c_{\max}^* / \partial \epsilon$  above is a function of two independent variables,  $\epsilon$  and  $t$ , but a probability density function of  $\epsilon$  only.

The numerator of the right-hand side of eq 10 above may be easily found from eq 7, and the denominator from eq 6, simply by differentiation with respect to  $t$ :

$$\frac{\partial c_{\max}^*}{\partial t} = \frac{\partial c_s^*}{\partial t} + \frac{1}{(KRT)^2} \left[ KRT \frac{\partial^2 c_s^*}{\partial c_y \partial t} - \frac{\partial c_s^*}{\partial c_y} \frac{\partial (KRT)}{\partial t} \right] \quad (11)$$

$$\frac{\partial \epsilon}{\partial t} = RT \frac{\partial \ln(KRT)}{\partial t} = \frac{1}{K} \frac{\partial (KRT)}{\partial t} \quad (12)$$

Dividing eq 11 by eq 12, according to eq 10, one obtains

$$f(\epsilon) = \frac{1}{RT} \left[ \frac{KRT(\partial c_s^* / \partial t) + \partial^2 c_s^* / \partial c_y \partial t}{\partial (KRT) / \partial t} - \frac{\partial c_s^* / \partial c_y}{KRT} \right] \quad (13)$$

All derivatives with respect to time in the above relation are

explicitly and analytically calculated from relations already given, namely,  $\partial c_s^*/\partial t$  from eq 5, of ref 1,  $\partial(KRT)/\partial t$  from eq 5, and  $\partial^2 c_s^*/\partial c_y \partial t$  from eq 6 of ref 1:

$$\frac{\partial c_s^*}{\partial t} = \frac{M_1}{M_2} \sum_i A_i \exp(B_i t) \quad (14)$$

$$\frac{\partial(KRT)}{\partial t} = M_2 \left\{ \frac{\sum_i A_i B_i^3 \exp(B_i t)}{[\sum_i A_i B_i \exp(B_i t)]^2} - \frac{2[\sum_i A_i B_i^2 \exp(B_i t)]^2}{[\sum_i A_i B_i \exp(B_i t)]^3} + \frac{\sum_i A_i B_i \exp(B_i t)}{[\sum_i A_i \exp(B_i t)]^2} \right\} \quad (15)$$

$$\frac{\partial^2 c_s^*}{\partial c_y \partial t} = M_1 \left\{ 1 - \frac{[\sum_i A_i \exp(B_i t)][\sum_i A_i B_i^2 \exp(B_i t)]}{[\sum_i A_i B_i \exp(B_i t)]^2} \right\} \quad (16)$$

where

$$M_1 = \frac{a_y k_1}{a_s} \quad \text{and} \quad M_2 = \frac{g D_1}{v L_1} \quad (17)$$

$a_y$  (cm<sup>2</sup>) is the cross sectional area of the void space in the solid bed,  $a_s$  (g/cm) is the amount of solid adsorbent per unit length of bed, and  $k_1$  (s<sup>-1</sup>) is the adsorption rate constant of A on the surface.

Finally, substitution of eqs 14–16 for the derivatives  $\partial c_s^*/\partial t$ ,  $\partial(KRT)/\partial t$  and  $\partial^2 c_s^*/\partial c_y \partial t$ , respectively, into eq 13, together with eq 5 for  $KRT$  and eq 6 of ref 1 for  $\partial c_s^*/\partial c_y$ , gives  $f(\epsilon)$  as an analytic function of the structural parameter  $t$ ,  $f(\epsilon; t)$ .

## Calculations

As before,<sup>1</sup> the calculations of the physicochemical quantities  $\epsilon$ ,  $c_y$ , and  $f(\epsilon)$  pertaining to heterogeneous surfaces start from the diffusion band of RF-GC experiments by recording the pairs  $H$ ,  $t$  and calculating the preexponential factors  $A_1$ ,  $A_2$ ,  $A_3$ , and  $A_4$  and the time coefficients  $B_1$ ,  $B_2$ ,  $B_3$ , and  $B_4$  of eq 2, together with the rate constant  $k_1$ , the calibration factor  $g$ , and the diffusion coefficient  $D_1$ , as previously reported.<sup>2</sup> The other quantities needed, i.e.,  $v$ ,  $a_y$ ,  $a_s$ ,  $L_1$ ,  $R$ ,  $k$ ,  $h$ ,  $T$ , and  $m$ , are known experimentally or they are physical constants from the literature.

Using all above quantities in eqs 9, 4, and 6 of ref 1 and eqs 5, 14, 15, and 16 here, one calculates  $K^0$ ,  $c_y$ ,  $\partial c_s^*/\partial c_y$ ,  $KRT$ ,  $\partial c_s^*/\partial t$ ,  $\partial(KRT)/\partial t$ , and  $\partial^2 c_s^*/\partial c_y \partial t$ , respectively. These are then used with eqs 6 and 13 to find the values of  $\epsilon$  and  $f(\epsilon)$ , respectively, for any chosen time  $t$ , measured from the introduction of the analyte gas A into the solid adsorbent bed.

Instead of the above procedure, one may use the PC program in GW-BASIC available as Supporting Information in the present work to conduct all above calculations and find directly from the experimental pairs  $H$ ,  $t$  the values of  $c_y$ ,  $\epsilon$ , and  $f(\epsilon)$ , together with the adsorption parameter  $k_1$ , the desorption rate constant  $k_{-1}$ , a possible first-order surface reaction rate constant  $k_2$ , the deposition velocity  $V_d$ , and the reaction probability  $\gamma$  of the probe gas A on the solid surface, the effective diffusion coefficient  $D_1$  of A into the carrier gas, and the detector calibration

**TABLE 1: Time Distribution of the Gaseous Concentration ( $c_y$ ), the Adsorption Energy ( $\epsilon$ ), and the Probability Density Function [ $f(\epsilon)$ ], for Penteli Marble (CaCO<sub>3</sub>, CaCO<sub>3</sub> + C), after Injecting 2  $\mu$ L of Liquid (CH<sub>3</sub>)<sub>2</sub>S, at 304.9 and 303.1 K**

time, min	CaCO <sub>3</sub> at 304.9 K			CaCO <sub>3</sub> + C at 303.1 K		
	10 <sup>6</sup> $c_y$ , mol/cm <sup>3</sup>	$\epsilon$ , kJ/mol	10 <sup>6</sup> $f(\epsilon)$ , mol <sup>2</sup> /(kJ g)	10 <sup>7</sup> $c_y$ , mol/cm <sup>3</sup>	$\epsilon$ , kJ/mol	10 <sup>7</sup> $f(\epsilon)$ , mol <sup>2</sup> /(kJ g)
14				0.382	94.3	0.0144
16				0.996	91.9	0.0843
18	0.129	92.2	0.00929	1.68	90.7	0.209
20	0.405	89.4	0.0906	2.40	90.1	0.375
22	0.677	88.2	0.245	3.13	89.7	0.570
24	0.940	87.6	0.453	3.83	89.5	0.781
26	1.19	87.3	0.694	4.50	89.5	0.996
28	1.42	87.1	0.948	5.13	89.5	1.20
30	1.64	87.1	1.20	5.71	89.6	1.40
32	1.84	87.2	1.43	6.24	89.8	1.57
34	2.02	87.3	1.63	6.71	90.0	1.72
36	2.18	87.6	1.79	7.14	90.3	1.84
38	2.33	87.9	1.91	7.51	90.7	1.93
40	2.45	88.3	1.98	7.84	91.0	1.99
42	2.56	88.8	2.00	8.12	91.5	2.01
44	2.66	89.3	1.96	8.36	92.0	2.00
46	2.73	90.0	1.87	8.57	92.5	1.95
48	2.80	90.8	1.73	8.74	93.2	1.87
50	2.85	91.8	1.53	8.88	93.9	1.75
52	2.89	93.1	1.27	8.99	94.8	1.59
54	2.91	94.8	0.967	9.07	95.8	1.39
56	2.93	97.5	0.608	9.14	97.2	1.15
58	2.94	103.4	0.198	9.18	99.0	0.865
60	2.94	102.3	0.263	9.21	101.8	0.533
62	2.93	97.1	0.774	9.22	108.5	0.150
64	2.92	94.6	1.33	9.22	105.5	0.290
68	2.87	91.7	2.60	9.18	98.4	1.36
72	2.81	89.8	4.07	9.11	95.5	2.74
76	2.73	88.5	5.74	9.01	93.6	4.50
80	2.64	87.5	7.63	8.89	92.2	6.77
84	2.55	86.6	9.76	8.76	91.1	9.69
88	2.45	85.9	12.2	8.62	90.1	13.5
92	2.35	85.2	14.8	8.47	89.1	18.4
96	2.25	84.6	17.8	8.31	88.3	24.8
100	2.15	84.1	21.2	8.16	87.5	33.3
110	1.90	82.9	31.7	7.77	85.5	69.4
120	1.68	81.9	46.1	7.39	83.6	149

factor  $g$ . The values  $M$  (of eq 2),  $a_y$ ,  $a_s$ ,  $v$ , and  $L_1$  needed in the calculations and some other known data are entered into the appropriate INPUT lines of the program, together with the ranges  $t_1$  and  $t_2$  in which  $c_y$ ,  $\epsilon$ , and  $f(\epsilon)$  are calculated and printed. Equations 9, 4, and 6 of ref 1 and eqs 5, 6, and 13–16 here may also be used with the PC program MATHEMATICA 3 to plot  $c_y$ ,  $\epsilon$ , and  $f(\epsilon)$  vs  $t$  between the two limits of the experimental time with a number of plot points of, e.g., 3000.

Since  $f(\epsilon; t)$  is an analytic function of the structural parameter  $t$ , it can be easily normalized to unity with respect to time

$$\int_{t_1}^{t_2} f(\epsilon; t) dt = 1 \quad (18)$$

by finding the value of the above integral between the two limits  $t_1$  and  $t_2$  of the experimental time and dividing  $f(\epsilon; t)$  by the result.

## Experimental Section

The apparatus and procedure were described elsewhere.<sup>3</sup> Section  $L_1$  (34.5–38.4 cm) was empty of any solid material, while  $L_2$  (8.6–6.8 cm) contained the solid bed. Both  $L_1$  and  $L_2$  were of Pyrex glass with an i.d. of 3.5 mm and heated to the same temperature. The sampling column  $l' + l$  (65 + 65 cm) was a stainless steel chromatographic tube of 4 mm i.d. No separation column, but only a restrictor, was used.

**TABLE 2: Time Distribution of the Gaseous Concentration ( $c_y$ ), the Adsorption Energy ( $\epsilon$ ), and the Probability Density Function [ $f(\epsilon)$ ], for Penteli Marble ( $\text{CaCO}_3$ ,  $\text{CaCO}_3 + \text{C}$ ), after Injecting 2  $\mu\text{L}$  of Liquid  $(\text{CH}_3)_2\text{S}$  and 2  $\mu\text{L}$  of Liquid  $\text{NO}_2$  at 303 and 301.7 K**

time, min	$\text{CaCO}_3$ at 303 K			$\text{CaCO}_3 + \text{C}$ at 301.7 K		
	$10^6 c_y$ , $\text{mol}/\text{cm}^3$	$\epsilon$ , $\text{kJ}/\text{mol}$	$10^7 f(\epsilon)$ , $\text{mol}^2/(\text{kJ g})$	$10^6 c_y$ , $\text{mol}/\text{cm}^3$	$\epsilon$ , $\text{kJ}/\text{mol}$	$10^7 f(\epsilon)$ , $\text{mol}^2/(\text{kJ g})$
10				0.451	88.4	0.0133
12				1.06	87.0	0.073
14				1.53	86.8	0.148
16	1.04	87.6	0.128	1.88	87.2	0.213
18	1.69	88.1	0.309	2.14	87.9	0.255
20	2.04	90.0	0.363	2.32	88.9	0.268
22	2.19	93.7	0.256	2.45	90.3	0.248
24	2.23	107.9	0.0218	2.52	92.4	0.195
26	2.20	92.8	0.686	2.56	96.1	0.107
28	2.15	83.1	26.0	2.57	106.7	0.0152
30	2.10	92.0	0.920	2.56	95.0	0.175
32	2.07	96.7	0.284	2.53	91.8	0.377
34	2.06	102.7	0.0815	2.49	89.8	0.629
36	2.08	94.2	0.439	2.43	88.4	0.947
38	2.13	91.0	0.901	2.38	87.2	1.35
40	2.21	88.8	1.61	2.32	86.2	1.89
42	2.31	86.9	2.88	2.25	85.2	2.64
44	2.44	84.9	5.60	2.19	84.2	3.76
46	2.58	82.4	14.4	2.12	83.1	5.62
48	2.73	74.4	349	2.06	81.8	9.36
50	2.90	81.7	19.7	2.00	79.8	20.7
52	3.07	83.0	12.1	1.94	69.8	1130
54	3.24	83.7	9.57	1.88	79.5	23.5
56	3.41	84.2	8.38	1.82	81.0	12.8
58	3.58	84.6	7.71	1.76	81.9	9.18
60	3.74	84.9	7.27	1.71	82.5	7.40
64	4.04	85.6	6.70	1.61	83.2	5.67
68	4.31	86.3	6.21	1.52	83.7	4.88
72	4.53	87.2	5.65	1.44	83.9	4.49
76	4.71	88.3	4.94	1.36	84.1	4.31
80	4.84	89.7	4.04	1.29	84.2	4.29
84	4.93	91.7	2.93	1.23	84.3	4.38
88	4.99	95.1	1.59	1.17	84.2	4.56
90	5.00	98.5	0.842	1.14	84.2	4.69
92	5.00	114.7	0.0351	1.11	84.1	4.84
96	4.99	95.3	1.75	1.06	84.0	5.22
100	4.95	91.8	3.75	1.02	83.8	5.70
110	4.75	87.7	9.72			
120	4.46	85.5	17.1			
130	4.13	84.1	25.9			
140	3.78	82.9	36.5			
150	3.43	82.0	49.1			

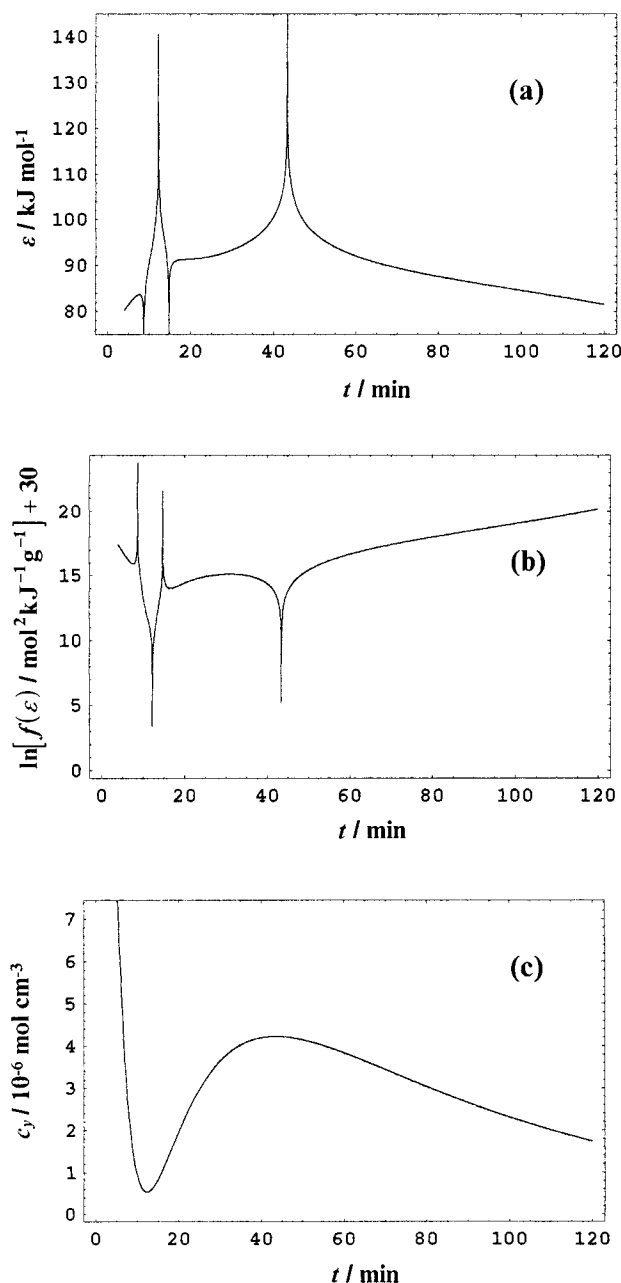
The  $\text{CaCO}_3$  was a Penteli marble (Greece), its analysis being given before.<sup>5</sup> It was ground to small pieces of 10–30 mesh, 0.6–1.25 g of which was placed in section  $L_2$  of the apparatus. The  $\text{CaCO}_3 + \text{C}$  material was prepared by shaking the above pieces of  $\text{CaCO}_3$  with 0.13 g of carbon black powder obtained from an automobile exhaust pipe. After sieving the resulted mixture, the 10–30 mesh fraction was retained and 1.26 g was used.

The  $(\text{CH}_3)_2\text{S}$ , being the main probe gas, was a product of Fluka (puriss), while  $\text{NO}_2$  was prepared in laboratory scale by heating  $\text{Pb}(\text{NO}_3)_2$  of analytical grade at atmospheric pressure and collected under cooling with liquid nitrogen, in the absence of moisture.

The carrier gas was nitrogen (99.99%) from Linde (Athens, Greece), dried by silica gel, with a flow rate of 22  $\text{cm}^3/\text{min}$ .

The probe gases were introduced through the injector of Figure 1 as liquids (2  $\mu\text{L}$ ). The second adsorbate ( $\text{NO}_2$ ) was injected 30 s after the first [ $(\text{CH}_3)_2\text{S}$ ].

Following the appearance of the continuously rising concentration–time curve in the flame ionization detector of a Shi-



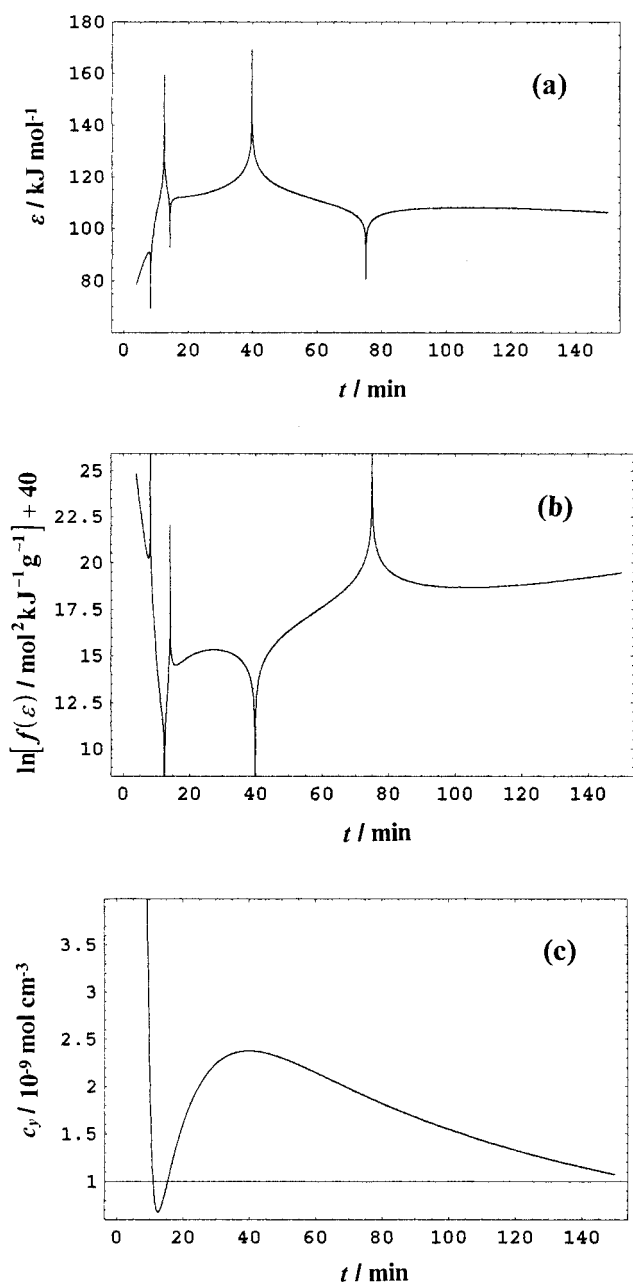
**Figure 2.** Plots of adsorption energy (a), probability density function (b), and gaseous concentration (c), as a function of experimental time, at 323 K, for the system  $(\text{CH}_3)_2\text{S}/\text{CaCO}_3$  in a nitrogen atmosphere.

madzu 14 chromatograph, the flow-reversing procedure of the carrier gas was started, lasting 10–20 s for each reversal, which is shorter than the gas hold-up time in both column sections  $I'$  and  $I$ . The narrow fairly symmetrical sample peaks created by the flow reversals were recorded, and their height  $H$  or the area under the curve was calculated and printed, together with the corresponding time  $t$ , by a C-R6A Shimadzu Chromatopac.

By entering the pair values of  $H$ ,  $t$  into the 3000–3040 DATA lines of the GW-BASIC program given in the Supporting Information here, together with the other unknown quantities in the INPUT lines 190–350, the physicochemical parameters and functions exposed and defined by eqs 6 and 13 of the previous sections and eq 4 of ref 1 are calculated and printed.

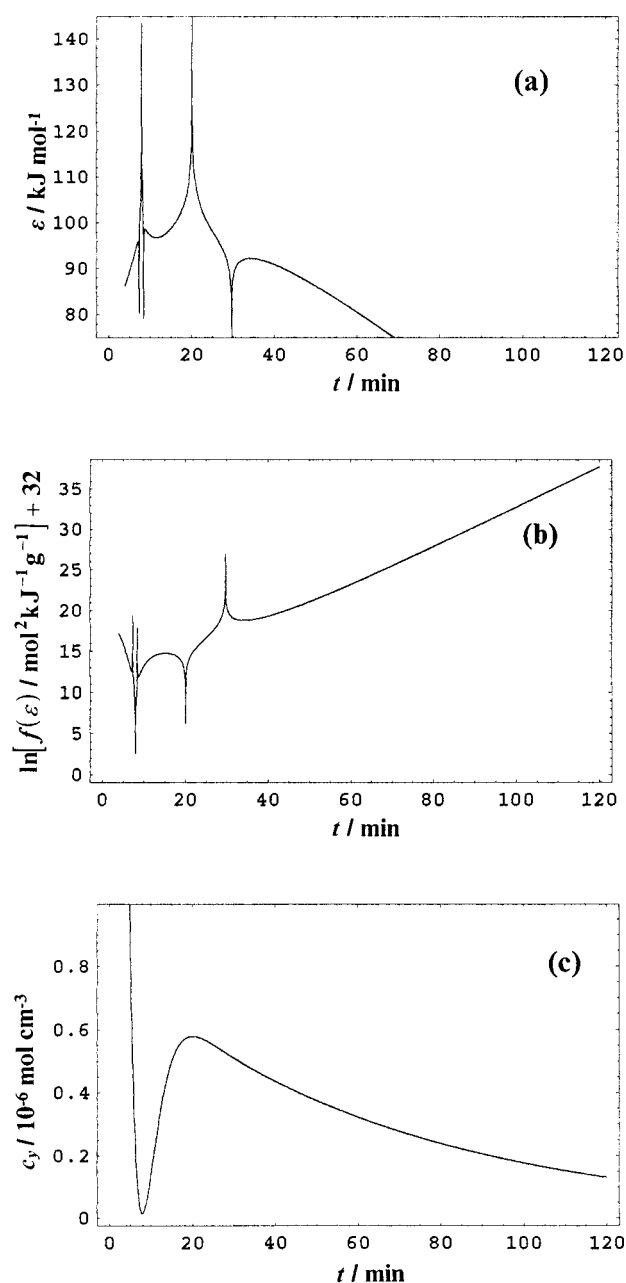
## Results and Discussion

The method described in the present work to measure directly from experimental data not only adsorption energies, local



**Figure 3.** Plots of adsorption energy (a), probability density function (b), and gaseous concentration (c), as a function of experimental time, at 323.2 K, for the system  $(\text{CH}_3)_2\text{S}/\text{CaCO}_3 + \text{C}$  in a nitrogen atmosphere.

monolayer capacities, and local adsorption isotherms, as previously described,<sup>1</sup> but also the probability density function for the adsorption energies as distributed over experimental time has been applied by using dimethyl sulfide and nitrogen dioxide as probe gases and Penteli marble as the solid adsorbent. The reason for choosing dimethyl sulfide as the main probe gas is that it is emitted by oceanic phytoplankton and constitutes the major natural source of sulfur in the troposphere. Nitrogen dioxide was chosen to see whether this well-known air pollutant in cities has any synergistic effect on the adsorption properties measured. As regards the solid, it is well-known that most Greek cultural heritage objects in the Acropolis of Athens and elsewhere have been constructed with Penteli marble, and adsorption properties such as those described here may throw some light on the mechanism of deterioration of art pieces by air pollutants. Needless to say that carbon black from the exhaust pipes of cars is one of the main kinds of airborne particles in



**Figure 4.** Plots of adsorption energy (a), probability density function (b), and gaseous concentration (c), as a function of experimental time, at 323 K, for the system  $(\text{CH}_3)_2\text{S} + \text{NO}_2/\text{CaCO}_3$  in a nitrogen atmosphere.

cities, being deposited onto clean solid surfaces, and therefore their effect on adsorption properties of marble is interesting.

Tables 1 and 2 list the values of the gaseous concentration  $c_y$  of  $(\text{CH}_3)_2\text{S}$ , its adsorption energy  $\epsilon$  on  $\text{CaCO}_3$  or  $\text{CaCO}_3 + \text{C}$ , and the corresponding probability density function  $f(\epsilon)$ , in the presence or absence of  $\text{NO}_2$ , at temperatures 301.7–304.9 K, as functions of various experimental times. The results with similar systems at a higher temperature (323 K) are presented as functions of time, using 3000 plot points. The same plots can be constructed with the systems of Tables 1 and 2.

The appearance of the function  $c_y = f(t)$  in Figures 2c–4 c is not typical for the so-called diffusion band of the RF-GC method, where it usually increases initially, passes through a maximum, and then declines with time. Here, this is preceded by a steep falling part related to a peak of high adsorption energy and a low value in the probability density function. These are



not observed at the lower temperatures of 301.7–304.9 K, as Tables 1 and 2 show.

The characteristics common to all regions of  $c_y$  are the minima in  $f(\epsilon)$  coinciding with the maxima in  $\epsilon$ . The presence of carbon particles on the surface of  $\text{CaCO}_3$  and of  $\text{NO}_2$  in the gas phase have noticeable effects on  $\epsilon$  and  $f(\epsilon)$ .

As pointed out in a previous publication,<sup>1</sup> the gas molecules at time  $t$  are not assumed to be exclusively adsorbed on sites  $i$  all of the same energy  $\epsilon_i$ , Figures 2a–4a showing the sweeping effect of the dynamic and changing with time procedure on collection of sites being active at time  $t$  and having a mean adsorption energy  $\epsilon$ . The maxima and minima in the function  $\epsilon = g(t)$  represent rather transition adsorption energies before their final leveling off with time.

The functions  $f(\epsilon)$  given in Tables 1 and 2 and Figures 2b–4b are unnormalized, but they can be normalized with respect to time, as mentioned in the Calculations, quite easily. For example, the integral of eq 18 for the system of Figure 3 was calculated with three choices of the time period and found to be

$$1.8294 \times 10^{-3} \quad \text{for} \quad t_1 = 0 \quad \text{and} \quad t_2 = 120 \text{ min}$$

$$1.8316 \times 10^{-3} \quad \text{for} \quad t_1 = 0 \quad \text{and} \quad t_2 = 150 \text{ min}$$

$$1.8326 \times 10^{-3} \quad \text{for} \quad t_1 = 0 \quad \text{and} \quad t_2 = 200 \text{ min}$$

Therefore, the normalizing factor in this case is 546.6, 546.0, and 545.7, respectively.

The kinetic physicochemical quantities for the adsorption phenomenon,  $k_1$ ,  $k_{-1}$ , and  $k_2$  have been calculated by the same

**TABLE 3: Adsorption Parameter ( $k_1$ ), Desorption Rate Constant ( $k_{-1}$ ), and Surface Reaction Rate Constant ( $k_2$ ) for  $(\text{CH}_3)_2\text{S}$  Adsorbed on  $\text{CaCO}_3$  and  $\text{CaCO}_3 + \text{C}$  in the Presence and in the Absence of  $\text{NO}_2$**

system	temp, K	$\text{NO}_2$	$10^3 k_1, \text{s}^{-1}$	$10^4 k_{-1}, \text{s}^{-1}$	$10^3 k_2, \text{s}^{-1}$
$\text{CaCO}_3$	304.9	no	7.23	1.00	2.48
$\text{CaCO}_3 + \text{C}$	303.1	no	3.01	1.77	0.187
$\text{CaCO}_3$	303	yes	0.772	12.4	1.25
$\text{CaCO}_3 + \text{C}$	301.7	yes	3.42	4.37	0.0279
$\text{CaCO}_3 + \text{C}$	323.2	no	1.87	177	-
$\text{CaCO}_3$	323	yes	2.55	92.3	1.81
$\text{CaCO}_3$	323	no	1.27	10.8	0.834

PC program given in the Supporting Information and are collected in Table 3.

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**Supporting Information Available:** The PC program in GW-BASIC, for calculating directly from the experimental pairs  $H$ ,  $t$  the various physicochemical quantities is available free of charge via the Internet at <http://pubs.acs.org>.

## References and Notes

- (1) Katsanos, N. A.; Arvanitopoulou, E.; Roubani-Kalantzopoulou, F.; Kalantzopoulos, A. *J. Phys. Chem. B* **1999**, *103*, 1152.
- (2) Katsanos, N. A.; Thede, R.; Roubani-Kalantzopoulou, F. *J. Chromatogr. A* **1998**, *795*, 133.
- (3) Abatzoglou, Ch.; Iliopoulou, E.; Katsanos, N. A.; Roubani-Kalantzopoulou, F.; Kalantzopoulos, A. *J. Chromatogr. A* **1997**, *775*, 211.
- (4) Jaroniec, M.; Madey, R. *Physical Adsorption on Heterogeneous Solids*; Elsevier: Amsterdam, 1988; p 13.
- (5) Katsanos, N. A.; Karaiskakis, G. *J. Chromatogr.* **1987**, *395*, 423.