Induced Water Condensation and Bridge Formation by Electric Fields in Atomic Force Microscopy

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We present an analytical model that explains how, in humid environments, the electric field near a sharp tip enhances the formation of water menisci and bridges between the tip and a sample. The predictions of the model are compared with experimental measurements of the critical distance where the field strength causes bridge formation.

Introduction

The formation of nanometer-sized water bridges between an atomic force microscope (AFM) tip and a sample is a phenomenon that has produced great interest in the last years. New applications in imaging and nanofabrication have driven efforts to understand nanometer-size capillarity. ¹⁻⁴ Capillary transport of molecules from the AFM tip to the solid substrate was used by Piner et al.⁵ to "write" patterns of molecules of submicrometer dimensions. ⁶ Water bridges also play an important role in contacts between objects, where they affect friction and energy dissipation. ⁷

Interest in this topic has sparked theoretical efforts to model different aspects of capillarity meniscus formation between a tip and a surface,⁸ structured pores,⁹ capillary forces between spherical particles and substrates¹⁰ and between surfaces,¹¹ and also the kinetics of capillary condensation.¹² Most models are based on macroscopic approximations,^{13,14} molecular-level grand canonical Monte Carlo simulations,¹⁵ and density functional theory,¹⁶ all of them involving substantial computational effort.

In this paper, we develop a simple analytical expression that can be used to determine in a quantitative way the presence and shape of the water film that forms between tip and sample in humid environments. This film grows under the influence of the electric field, forming a meniscus that becomes unstable when a critical field is reached, at which point it suddenly forms a bridge between tip and surface. In AFM, the capillary force bends the lever, which, for small spring constants, can bring the tip in contact with the surface. This is observed experimentally as a sudden jump-to-contact. Our approximation allows us to determine the distance and the voltage at which this capillary jump takes place. Apart from providing a simple way to calculate the critical field and distance, it improves our understanding of the mechanisms of water-induced jump-tocontact, which is important in noncontact AFM imaging in humid environments.¹⁷

After presenting the model, we will compare its predictions to experimental values of the jump-to-contact distances as a function of humidity and electric field.

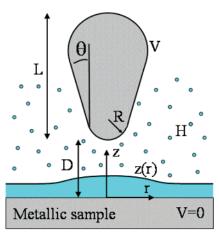


Figure 1. Tip—sample geometry with a water film (blue) used in the theoretical treatment. Humidity (H) induces water condensation on the substrate with a surface profile characterized by the function z(r).

Theoretical Model

In the model, the system is assumed to be an axially symmetric metallic tip in the shape of a truncated cone or pyramid of length L and semiangle θ , terminated with a spherical cap of radius R. Its axis is perpendicular to a flat metallic sample (Figure 1). The tip and sample surfaces are assumed to be covered with an initial water layer in equilibrium with the ambient humidity H. In the absence of electric fields, this film conforms to the surface geometry. The thickness of this initial layer is not important. The profile of this film on the sample surface is represented by the function z(r), where z is the distance to the metallic surface, and r is the lateral distance to the tip apex. Although a similar film can also exist on the tip, it will be neglected for simplicity. Under these conditions, the condensation energy U_c of the water film is given by

$$U_{c} = 2\pi K T \frac{\rho}{m} \ln(1/H) \int_{0}^{\infty} z(r) r dr$$
 (1)

where ρ and m are the molecular density and molecular mass of water, respectively. In the absence of electric field, z(r) should be a plane, but, under an applied potential, this simple geometry deforms into a different shape.

Because of its high dielectric constant and the possible presence of solvatable ions at the surface, the water film can

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be assumed to act as a conductor so that its potential is the same as that of the metallic sample. Although the mobility of ions is small compared with that of electrons, their effect can be appreciable on insulating surfaces exposed to humidity. 18 In the experiments described in this paper, these effects are not appreciable, and both electronic polarization and mobile ions can be considered contributions to the high value of the dielectric

In the presence of a field E, the electrostatic energy of the system U_e can be expressed as 19

$$U_{\rm e} = -\frac{\epsilon_0}{2} \int_V \frac{\epsilon - 1}{\epsilon} E_0^2 \mathrm{d}V \tag{2}$$

where V is the volume of condensed water, ϵ is the dielectric constant of the liquid, and E_0 is the electric field before water film condensation. It has been shown²⁰ that, for metallic samples, the electrostatic field can be approximated by that produced by a sphere of radius R at a voltage V, which is given by a set of point charges inside the tip:

$$E_0 = -2RV \sum_{i=1}^{\infty} \frac{\tilde{q}_i}{\tilde{r}_i^2} \tag{3}$$

with the values of q_i and r_i being given by the image charge series of a sphere in front of a plate.²¹ Combining these equations, we obtain the electrostatic energy for a generic function z(r):

$$U_{\rm e} = -4\pi\epsilon_0 R^2 V^2 \int_0^\infty \frac{\epsilon - 1}{\epsilon} z(r) r \left(\sum_{i=1}^\infty \frac{\tilde{q}_i}{\tilde{r}_i^2} \right)^2 dr \tag{4}$$

When water condenses to form a film, U_e decreases and U_c increases. The film profile is determined by minimization of the total energy, $U_{\text{tot}} = U_{\text{e}} + U_{\text{c}}$. Since, along the vertical axis through the tip, the field E is minimum at the liquid surface, the electrostatic energy should decrease when the film thickness h increases. Since this field is also a maximum relative to the rest of the surface, water will start condensing at this location. When the electric field reaches a threshold value at a voltage V_{th} , condensation will accelerate because E increases when h increases, until the liquid surface contacts the tip. In this simple approximation, the field $E_0 = E(z = 0, r = 0)$ is the key parameter to obtain V_{th} . Assuming that E_0 is constant over the whole liquid volume, the electrostatic energy is

$$U_{\rm e} = -4\pi\epsilon_0 R^2 V^2 \frac{\epsilon - 1}{\epsilon} \left(\sum_{i=1}^{\infty} \frac{\tilde{q}_i}{\tilde{z}_i^2} \right)^2 \int_0^{\infty} z(r) r \mathrm{d}r$$
 (5)

The total energy $U_{\rm tot} = U_{\rm e} + U_{\rm c}$ must be negative to induce the formation of a liquid bridge, that is, the electrostatic energy gain must be larger than the condensation energy. V_{th} can then be obtained from $U_{\text{tot}} = 0$:

$$V_{\text{th}}^2 = \frac{KT\rho}{2R^2m} \frac{\epsilon}{\epsilon - 1} \left(\sum_{i=1}^{\infty} \frac{\tilde{q}_i}{\tilde{z}_i^2} \right)^{-2} \ln(1/H)$$
 (6)

From V_{th} , the threshold electric field to induce the formation of liquid bridges can be calculated:

$$E_{\rm th} = \sqrt{\frac{2KT\rho\epsilon \ln(1/H)}{m\epsilon_0(\epsilon - 1)}}$$
 (7)

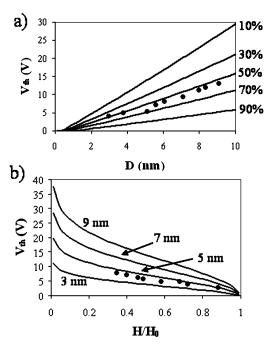


Figure 2. Threshold voltage for the formation of a water bridge as a function of tip-sample distance (a), and as a function of RH (b). Dots are experimental results from ref 22.

For large tip radii, $E_{th} = V_{th}/D_b$, where D_b is the distance at which the water bridge forms, causing a jump-to-contact event. For small radii, the threshold voltage and bridge distance do not scale linearly, and eq 6 should be used.

For water $(m/\rho = 2.7 \times 10^{-28} \text{ m}^3 \text{ and } KT = 0.026 \text{ eV}),^{24}$ this equation takes the form $E_{\text{th}} = 3.5 (\ln(1/H))^{1/2} \text{ V/nm}$. Threshold voltages for the formation of water necks calculated using eq 6 are shown in Figure 2 as a function of tip-sample separation (a) and humidity (b), and compared with published data from Garcia et al.²² As can be seen, the agreement with the experimental data is very good. 14 Although the assumption of a flat film is sufficient to predict a reasonable value for V_{th} , it cannot explain the effects that result from the real shape of the water meniscus before the bridge is formed. The fact that $U_{\rm e}$ and $U_{\rm c}$ have the same dependence on z(r) (both are proportional to the volume) implies that the water surface profile cannot be obtained from the above formula alone. To obtain z(r), two additional contributions to the energy need to be included. 14 One is the van der Waals energy $U_{\rm VdW}$, and the other is the surface tension of water, U_s . Since the van der Waals force is short-range, its contribution will be important only when the distance between the water film and the metallic sample is a few angstroms. Assuming that the two surfaces are almost planar, U_{VdW} can be written as

$$U_{\text{VdW}} = \int_0^\infty \frac{|A|r}{6\pi (r)^2} dr \tag{8}$$

where A is the Hamaker constant. The capillarity term U_s appears due to the increase of the water surface area when the initially flat layer produces a bulging meniscus under the tip. The surface tension contribution is

$$U_{\rm s} = \int_0^\infty 2\pi \alpha r \sqrt{1 + z^2} \mathrm{d}r \tag{9}$$

where $\alpha = 73$ mN/m is the surface tension of water, and z' is the slope of z(r). Although the surface tension of water can change as a function of voltage,²³ the change is too small to

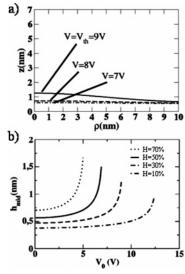


Figure 3. (a) Water meniscus profile calculated for different voltages by minimization of the energy. Tip radius R=50 nm; distance D=7 nm; humidity H=30%. The last stable solution is found at V=9V. An increment of the voltage over this value produces a water bridge. (b) Height of the meniscus under the tip apex ($\rho=0$ in Figure 4a) for different values of the RH. $R_{\rm tip}=50$ nm, d=7 nm.

influence the results. The surface tension and the van der Waals energy are included in the simulation only to stabilize the mathematical solution when $r \to \infty$. The main contributions to the total energy, however, are the condensation and electrostatic energies, as we have shown in the analytical model. Using these contributions together with the electrostatic energy U_e , the profile z(r) is obtained by minimization of the total energy:

$$\frac{\partial U_{\text{tot}}}{\partial z(r)} - \frac{d}{dr} \frac{\partial U_{\text{tot}}}{\partial z'(r)} = 0$$
 (10)

where $U_{\text{tot}} = U_{\text{e}} + U_{\text{VdW}} + U_{\text{c}} + U_{\text{s}}$.

The functional dependence of the electrostatic field is not easy to calculate because it depends on the entire function z(r). For that reason, we use the radial field approximation (RFA), which assumes that the electric field is the same as that inside a spherical capacitor, with the spherical tip being the central electrode. ¹⁴

In Figure 3a, we show water profiles obtained using the RFA. The profile barely changes until the voltage is close to $V_{\rm th}$. In the case shown in the figure, it changes appreciably only when the voltage is larger than 7 V, which produces a bulge of a few angstroms, that is, one or two water layers. As the voltage gets closer to the threshold, any small perturbation can precipitate the formation of a bridge. Figure 3b shows the height of the film under the tip as a function of voltage for different relative humidities. The height diverges when $V = V_{\rm th}$. The initial water thickness was obtained in this case from the balance between van der Waals and condensation energies.²⁴

Experimental Section

In AFM experiments, the threshold distance for bridge formation can be determined from the jump-to-contact as the tip approaches the surface with different applied voltages. This jump, however, must be distinguished from that due to the pure mechanical instability of the cantilever spring. This occurs at the point where the slope of the force—distance curve is equal to the cantilever spring constant K. Assuming that the electrostatic force follows a 1/D dependence, as shown in reference 25, the mechanical instability jump-to-contact distance $D_{\rm mech}$

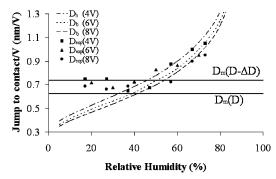


Figure 4. Jump-to-contact distance normalized to the bias voltage for a TiN tip approaching a gold surface at different voltages as a function of RH. Lines are drawn for the theoretically predicted bridge threshold formation values $D_{\rm b}$ (dashed lines) and for the mechanical instability $D_{\rm m}$ (solid horizontal lines). The two horizontal lines correspond to the average distance D and the distance of closest approach due to the noise $(D-\Delta D)$. Tip R=126 nm.

can be easily calculated. The expression in nanometer units is

$$D_{\rm m}({\rm nm}) = 0.1667 \sqrt{\frac{R({\rm nm})}{K({\rm N/m})}} V({\rm V})$$
 (11)

Depending on the tip radius, spring constant, applied voltage, and relative humidity (RH), bridge formation or mechanical instability will be responsible for the jump-to-contact. Since this quantity is readily accessible in AFM studies, we used it to test the above theories.

The experiments were carried out at room temperature (22 \pm 2 °C) with a home-built AFM²⁶ controlled by RHK electronics. The microscope was enclosed in a glovebox where humidity control was achieved by circulating dry N₂ to decrease the humidity (H) or by bubbling the N₂ through deionized water to increase the humidity. Humidity and temperature were measured using a thermohygrometer from RadioShack. Values from 10 to 80% could be maintained with a variation of \pm 1% per hour. The absolute values of H have an uncertainly of \pm 5%. Tips from Ultrasharp Mikromash coated with conductive TiN were used with cantilever spring constants of 9 N/m, as determined using Sader's method.²⁷

Figure 4 shows the measured jump-to-contact distances (normalized to the bias voltage) over a gold surface and their dependence on humidity for various applied voltages. We also show the calculated curves of $D_{\rm b}$ (due to water bridge formation) and $D_{\rm m}$ (due to mechanical instability). As mention above, the threshold voltage and the distance $D_{\rm b}$ of bridge formation do not scale proportionally, so that the calculated curves (dashed lines) do not coincide exactly. At 6 V, the two lines cross at around 40% RH. Below that value, $D_{\rm m}$ is smaller than $D_{\rm b}$, indicating that the humidity is too low to produce a water meniscus before the tip jumps to the surface due to the mechanical instability. Above 40% RH, meniscus and bridge formation occurs before the mechanical instability.

In Figure 5a, we show the measured force versus D curve for a low RH (20%), where the jump-to-contact is due to the mechanical instability, which occurs at 4.4 nm. The inset shows the force as a function of 1/D, which gives a straight line with a slope directly related to the tip radius.²⁵ In the present case, $R = 126 \pm 10$ nm.

In Figure 5b, we show another F versus D curve with the same tip but at higher humidity (67%). In this case, the tip jumps to the surface because of the formation of a water bridge, as shown by the value of F', which is smaller than the spring constant of the cantilever.

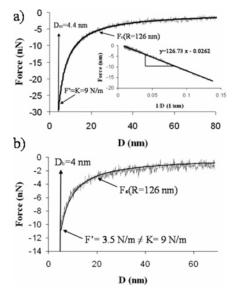


Figure 5. (a) Electrostatic force vs tip—sample distance for a RH of 20% and a bias voltage of 6 V. The inset shows the force vs 1/D, a straight line with a slope proportional to the tip radius, 126 nm in this case. The mechanical instability (jump-to-contact) occurs at 4.4 nm, where the slope is indeed very close to the cantilever spring constant. (b) Electrostatic force vs tip—sample distance for a RH of 67% and V = 4V. The jump-to-contact occurs at 4 nm. At this distance, the force derivative F' is smaller than the cantilever spring constant, indicating that the jump-to-contact is due to the formation of a water bridge

Conclusion

We have developed a simple analytical approximation that makes it possible to quantitatively analyze the effect of enhanced water condensation due to the electric field. The theory gives the threshold voltage for bridge formation with excellent accuracy.

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