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Green etherification of bioglycerol with 1-phenyl ethanol over supported heteropolyacid

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Received: 6 March 2011/Accepted: 25 April 2011 © Springer-Verlag 2011

Abstract Escalating demand for biodiesel production has generated surplus glycerol. Therefore, the consumption of glycerol for valuable conversions has become a global challenge. In an effort to convert glycerol, we have etherified it to make a biologically active component, 3-(1phenylethoxy) propane-1,2-diol. Etherification of glycerol with 1-phenyl ethanol was carried out by using heterogeneous acid catalysts. The process is green and clean. Different types of heteropolyacids (HPAs) supported on hexagonal mesoporous silica (HMS) and K-10 clay were prepared by incipient-wetness technique and screened to get high selectivity towards monoether of glycerol. 20% w/w dodeca-tungstophosphoric acid (DTP)/HMS was found to be the best. The effects of various reaction parameters such as speed of agitation, catalyst loading, mole ratio of reactants and temperature were evaluated systematically to prove that the reaction obeys Langmuir-Hinshelwood-Hougen-Watson (LHHW) type of mechanism. It was also observed that the reaction was free from any external mass transfer as well as intra-particle diffusion limitations and was intrinsically kinetically controlled. An overall second order kinetic equation was used to fit the experimental data, under the assumption that all the species are weakly adsorbed on the catalytic sites. Apparent activation energy was estimated as 27.0 kcal/mol. Solvent-free condition for this reaction has also added the green chemistry perception to the reaction.

Keywords Heteropolyacid · Hexagonal mesoporous silica · Bioglycerol · 1-Phenyl ethanol · Etherification · Solvent-free condition · Green chemistry

Abbreviations

$a_{\rm p}$	Solid-liquid interfacial area (cm ² /cm ³ of
	liquid phase)
A	Reactant species A—1-phenyl ethanol
AS	Chemisorbed A
В	Reactant species B—Glycerol
BS	Chemisorbed B
P	Monoether of glyceryl ether (product)
PS	Chemisorbed Product
W	Water
$C_{\rm A},C_{\rm B}$	Concentration of A and B (mol/cm ³)
$C_{\mathrm{A0}},C_{\mathrm{B0}}$	Initial concentration of A and B (mol/cm ³)
$C_{\mathrm{AS}},C_{\mathrm{BS}}$	Concentration of A and B at solid (catalyst)
	surface (mol/g cat)
$C_{\mathrm{PS}},C_{\mathrm{WS}}$	Concentration of P and W at solid (catalyst)
	surface (mol/g cat)
C_{S}	Concentration of vacant sites (mol/g cat)
C_{t}	Total concentration of the sites (mol/g cat)
C_{WP}	Weisz–Prater constant
$D_{ m P}$	Diameter of catalyst particle (m)
$D_{ m AB}$	Diffusion coefficient of A in B (m ² /s)
$D_{ m BA}$	Diffusion coefficient of B in A (m ² /s)
D_{e}	Effective diffusivity (cm ² /s)
<i>R</i> p	Radius of catalyst particle (m)
$-r_{\rm A}$	Rate of disappearance of A (cm ³ /gmol s)
$k_{\rm SLA}, k_{\rm SLB}$	Solid-liquid mass transfer coefficients (m/s)
K_{A}	Equilibrium constant for adsorption of A on
	catalyst surface (l mol ⁻¹ min ⁻¹)
$K_{ m B}$	Equilibrium constant for adsorption of B on
	catalyst surface (l mol ⁻¹ min ⁻¹)

Published online: 11 May 2011



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 k_{SR} Surface reaction rate constant for forward reaction (1 mol⁻¹ min⁻¹)

Surface reaction rate constant for reverse

reaction (1 mol⁻¹ min⁻¹)

 $K_{\rm P}$ Equilibrium constant for adsorption of P on

catalyst surface (min⁻¹)

 $K_{\rm W}$ Equilibrium constant for adsorption of W on

catalyst surface (min⁻¹)

 $r_{\rm obs}$ Observed rate of reaction (mol/g cat/s)

S Vacant site
Sh Sherwood number
t Time (min)

w Catalyst loading (g/cm³ of liquid phase)

 $X_{\rm A}$ Fractional conversion of A

Greek letters

 $k_{SR'}$

ε Porosity

 $\rho_{\rm p}$ Density of catalyst particle (g/cm³)

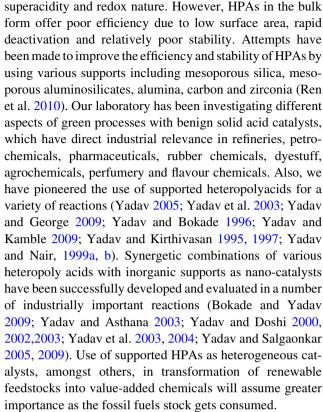
 τ Tortuosity (-)

 μ Viscosity of reaction mixture (kg/m.s)

Introduction

Heterogeneous catalysis by heteropoly acids has recently emerged as an innovative method for green chemistry practices. Heteropoly acids (HPAs), their salts and polyoxometalates (POMs) are attractive since they are low in toxicity, highly stable towards humidity, recyclable and air stable. Heteropoly acids are more active catalysts than conventional inorganic and organic acids for various reactions in solutions (Kozhevnikov 2002; Nakato et al. 1997, Yaday 2005). The use of HPAs in non-polar solvents improves product selectivity and also provides their easy separation from the reaction mixture. Today, catalysis by heteropoly acids (HPAs) is a potential area due to its economic and green benefits (Yadav and Kirthivasan 1995, 1997; Yadav and Bokade 1996; Kozhevnikov 2007). A variety of organic reactions that are catalysed by Bronsted acids such as H₂SO₄, HCl and other protonic acids or Lewis acids such as AlCl₃, FeCl₃, etc. proceed in the presence of heteropoly acids or polyoxometalates, more efficiently, under milder conditions, with greater selectivity, better yields and shorter reaction time. Supported heteropolyacid catalysts have been employed for both alkylation and acylation (Mizuno and Misono 1998; Miyaji et al. 2003; Kamiya et al. 2007; Kamiya et al. 2008). It has been demonstrated that the acidic cesium salts of HPAs are highly water-tolerant catalysts for hydration of olefins (Kimura et al. 1997) and hydrolysis of esters (Nakato et al.

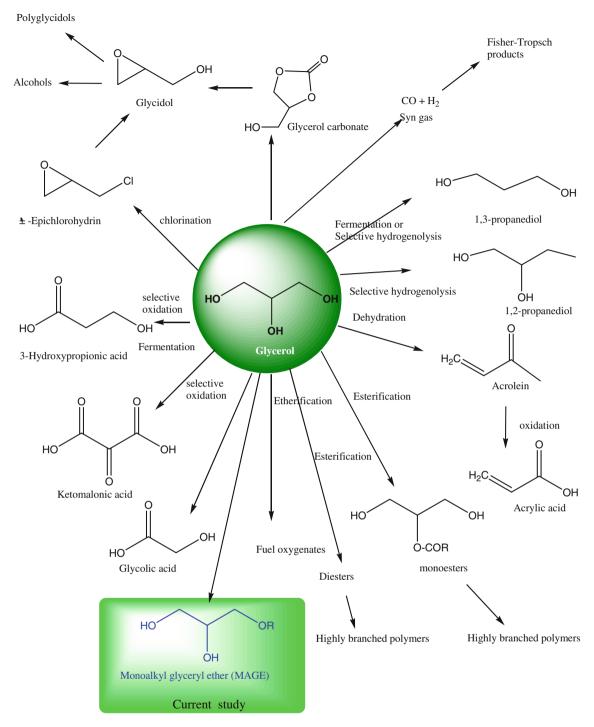
Amongst many other solid acid systems, HPAs having Keggin anion structures are most active due to their



Biodiesel processes via transesterification produce 10% w/w of glycerol as the co-product. The production of glycerol in 2009 was 1.72 MMTA worldwide and the production of biodiesel will be economically viable if the co-product glycerol is converted into several value-added products. Glycerol finds applications in a plethora of areas from personal care to technical applications (Aresta et al. 2005; Zhou et al. 2008; Behr et al. 2008; Pagliaro et al. 2007; Jerome et al. 2008). There is a significant market for polymers, ethers and other compounds. Glycerol can be converted into variety of valuable products by reactions such as hydrogenolysis, dehydration, esterification, etherification, oxidation, etc. (Scheme 1). The volume of products such as epichlorohydrin, propanediols, acrolein/acrylic acid and Fisher-Tropsch products, which are currently produced by petrochemical routes is huge and glycerol as a renewable source will be very attractive in coming years. Taken together, all these chemicals have huge demand and since the source is renewable, these catalytic processes will be very attractive commercially.

Etherification of glycerol with alkanols is commercially attractive to provide value-added monoalkyl glyceryl ether (MAGE). Since glycerol has three hydroxyl groups with similar pKa values, the control of the regioselectivity is the main key of the process to minimise waste and by-products production. MAGEs resulting from these transformations are highly valuable chemicals since they exhibit a wide spectrum of biological activities such as anti-inflammatory





Scheme 1 Value-added chemicals which could be derived from bioglycerol using different catalytic processes

(Chalmers et al. 1996), antibacterial, antifungal (Haynes et al. 1994; Boeryd et al. 1971), immunological stimulation (Brohult et al. 1986) and anti-tumour properties (Mori and Kabata 1998; Weber 1988). They are also important precursors for the preparation of 1,3-dioxolan-2-ones (Horibe et al. 2000; Okutsu and Kitsuki 2004) and bis(sodium

sulphonate ester) type cleavable surfactants (Ono et al. 1998). Glycerol ethers also have many potential uses, such as fuel additives, solvents (Queste et al. 2006) and cryogenics (Koshchii 2002). There is a dearth of literature on the etherification of glycerol to value-added MAGEs. The production of MAGEs from glycerol was investigated



using alkyl chlorides (Wessendorf 1995). Gu et al. (2008) have reported etherification reactions between benzyl, propargyl and allyl alcohols, olefins and dibenzyl ethers with glycerol to give the corresponding MAGEs in moderate to excellent yields. Reactions of glycerol with isobutene (Klepacova et al. 2005) or *tert*-butanol with acid catalysts afford *tert*-butyl-glycerol ethers, which have potential for blending with diesel (Wessendorf 1995). Recently, catalytic reductive alkylation for the synthesis of linear 1-*O*-alkyl mono-and di-glycerol ethers in one step has also been reported (Shi et al. 2009). A range of transformations of glycerol under microwave conditions using Starbon-derived materials is also known (Luque et al. 2008).

Most of the available literature for the conversion of glycerol to glycerol ethers is limited to synthesis of alkyl ethers (e.g. *t*-butyl ether of glycerol). A few of the described processes use sulphuric acid, phosphoric acid or *p*-toluene sulphonic acid as a catalyst which are homogeneous. The reaction mass is neutralised at the end of the reaction leading to effluent containing dissolved salts. The acids are corrosive and need special material of construction and not viable to use on industrial scale.

There is no report on the synthesis of 3-(1-phenylethoxy) propane-1,2-diol from glycerol and 1-phenylethanol using heterogeneous catalysis. This is a biologically active compound with uses as anti-inflammatory, antibacterial, antifungal, immunological stimulation and anti-tumor properties. The selectivity of this reaction towards monoetherification of the terminal –OH group in glycerol is challenging. A reasonable estimate of demand for such a valuable chemical could be about 500 TPA and as its properties get evaluated and its availability on a commercial scale increases, its market share will also increase substantially.

The combination of all the processes will result in the utilisation of massive volume of waste glycerol generated in bio-diesel process. Eventually, this product adds to the family of glycerol platform. Some of these products could be manufactured using the same battery of reactors and separators in a multi-product industry.

We have developed a green and clean process embracing solvent less, single step and easy approach using a heterogeneous catalyst within shorter reaction times. Since supported heteropolyacids have been extensively studied in our laboratory as nano-catalysts, it was thought worthwhile to employ them in the current work and study the kinetics also (Scheme 2). There is no report on modelling and kinetics.

The main reaction is the mono etherification of glycerol at primary OH group. This product on further addition of 1-phenyl ethanol generates di-ether which is a minor reaction. Etherification at secondary OH group is also a

minor side reaction. The current work gives high selectivity towards monoether product in short reaction duration.

Experimental

Chemicals

The following chemicals were procured from firms of repute and used without further purification: 1-phenyl ethanol (Merck, Germany), glycerol (Merck, Germany), *N*-methyl pyrollidone (S.D. Fine chem. Ltd., Mumbai), dodecatungstophosphoric acid (Sisco research labs, Mumbai), tetraethylorthosilicate (Merck, Germany), hexadecylamine (Spectrochem Ltd., Mumbai, India), ethanol (S.D. Fine chem. Ltd., Mumbai) and methanol (S.D. Fine chem. Ltd., Mumbai).

Screening of various catalysts

Various heteropoly solid acid catalysts like *dodeca*-tung-stophosphoric acid supported on hexagonal mesoporous silica (DTP/HMS), *dodeca*-tungstophosphoric acid supported on montmorrilonite clay (DTP/K-10), *dodeca*-molybdophosphoric acid supported on hexagonal mesoporous silica (DMP/HMS), *dodeca*-molybdophosphoric acid supported on montmorrilonite clay (DMP/K-10), caesium-incorporated *dodeca*-tungstophosphoric acid (Cs-DTP/k-10) and caesium-incorporated *dodeca*-molybdophosphoric acid (Cs-DMP/K-10) were prepared by incipient-wetness technique and screened for the reaction of glycerol with 1-phenyl ethanol. 20% w/w DTP/HMS gave the highest conversion of about 94% in 2 h with selectivity of 75% to the desired mono ether product (Fig. 1).

Catalyst synthesis

HMS was synthesised by the following method: 5 g hexadecyl amine was dissolved in 41.8 g of ethanol and 29.6 g of distilled water. To this, 20.8 g of tetraethyl orthosilicate was added under vigorous stirring. The addition of ethanol improved the solubility of the template. The mixture was aged for 18 h at 30°C. The clear liquid above the white coloured precipitate was decanted and the precipitate HMS was dried on a glass plate. The template was removed by calcining the resulting material at 550°C in air for 3 h. 20% w/w DTP-HMS was freshly synthesised by the wet impregnation technique by dissolving 2 g of dodeca-tungstophosphoric acid in 20 cm³ methanol. The solution was added slowly drop wise to 8 g of hexagonal mesoporous silica under constant stirring till a thick paste was formed. This thick paste was kneaded until fine powder was obtained. The mixture was further dried in oven at



Scheme 2 Etherification of glycerol with 1-phenyl ethanol over solid acid catalyst

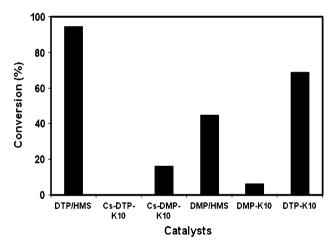


Fig. 1 Catalysts screening for etherification of glycerol with 1-phenyl ethanol. Reaction conditions: 1-phenyl ethanol 0.05 mol, glycerol 0.2 mol, 0.024 gm/cm³ catalyst, 25 cm³ total reaction volume, 1.0 cm³ *N*-methyl pyrrolidone as internal standard, speed of agitation 1,000 rpm, temperature 120°C

 $120^{\circ}\mathrm{C}$ and calcined at 285°C for 4 h to get the active solid acid catalyst.

Catalyst characterisation

20% w/w DTP-HMS catalyst was characterised by various techniques reported by our group earlier (Yadav and

George 2009; Yadav and Manyar 2003). The salient features of the characteristic results are mentioned here. In FT-IR, the broad band stretching from 1000 to 1200 cm⁻¹ was due to Si-O stretching vibration of HMS. The peak around 1626 cm⁻¹ indicated presence of bronsted acidic sites, 895 and 812 cm⁻¹ showed W-O-W asymmetric vibrations associated with Keggin ion. A smoother surface layer was clearly seen from the SEM micrographs with particle size in the range of 4-8 µm. The acidity of the catalyst was determined by ammonia TPD. A broad peak with a maximum between 100 and 140°C corresponding to desorption of weakly held physisorbed ammonia showed the presence of acidic sites in the catalyst. The adsorption desorption isotherms for the catalyst showed type IV isotherm with the hysteresis loop of type H₃, which is a characteristic of mesoporous solids. Characteristic nitrogen BET surface area obtained was very high around 600 m²/g and pore size was in the mesoporous region.

Reaction procedure

The reactions were carried out in a 50 cm³ capacity glass reactor of 4.8 cm i.d equipped with four equally spaced baffles and six bladed turbine impeller. The reaction temperature was maintained by means of a thermostatic oil bath, which was maintained at a desired temperature with an accuracy of $\pm 1^{\circ}$ C, in which the reaction assembly was



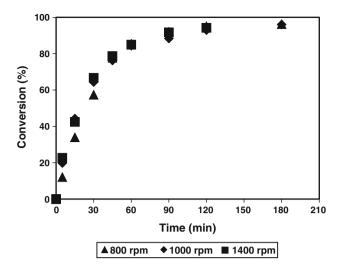


Fig. 2 Effect of speed of agitation on conversion of 1-phenyl ethanol. Reaction conditions: 1-phenyl ethanol 0.05 mol, glycerol 0.2 mol, 0.024 gm/cm³ DTP-HMS catalyst, 1.0 cm³ *N*-methyl pyrrolidone as internal standard, 25 cm³ total reaction volume, temperature 120°C

immersed. Standard experiments were carried out by taking 1-phenyl ethanol 0.05 mol, glycerol 0.2 mol, N-methyl pyrrolidone 0.5 cm³ as an internal standard which makes the total volume of the reaction mixture as 25 cm³. 0.024 g/cm³ 20% w/w DTP-HMS catalyst was added at 120°C. The reaction mixture was allowed to reach the desired temperature and the initial sample was collected. Agitation was then commenced at a known speed.

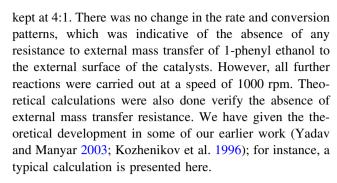
Method of analysis

Clear liquid samples were withdrawn at regular time intervals by reducing the speed of agitation momentarily to zero and allowing the catalyst to settle at the bottom of the reactor. Typically, glycerol was taken excess in the reaction solution and the conversions were based on the limiting reactant, 1-phenyl ethanol. Analysis of the reaction mixture was performed on GC (Chemito, model 1000) by using FID and a capillary wax column BP-20 (0.25 mm diameter and 30 m length). The product was confirmed by GC–MS (Perkin Elmer instrument, Clarus 500) with BP-1 capillary column (0.25 mm i.d., 30 m length) and EI mode of MS.

Results and discussions

Effect of speed of agitation

The effect of speed of agitation was studied in the range of 800–1400 rpm with 0.024 g/cm³ catalyst loading at 120°C (Fig. 2). The mole ratio of glycerol to 1-phenyl ethanol was



External mass transfer resistance

The rate of mass transfer could be calculated from the knowledge of mass transfer coefficients for both the reactants, which were obtained from their bulk liquid phase diffusivities. The inter-particle mass transfer resistance was calculated using the Wilke-Chang equation and Sherwood number. The diffusivity D_{AB} and D_{BA} was calculated from Wilke-Chang equation given by $D_{\rm AB}=117.3\times 10^{-18}\times (\psi\cdot M_{\rm B})^{0.5}{\rm T}/(\mu\times {\rm Va}^{-0.6})$ where $\psi=1$ (the association factor for glycerol), $M_{\rm B}$ molecular weight of glycerol, T reaction temperature, μ viscosity of reaction mixture, V_a molar volume of 1-phenyl ethanol. The value of D_{AB} was found to be 5.96 \times 10⁻¹⁰ m²/s. Similarly the value of $D_{\rm BA}$ was found to be 9.28×10^{-10} m²/s. The value of solid to liquid phase mass tranfer co-efficients $k_{\rm SLA}$ and $k_{\rm SLB}$ was calculated from Sherwood number $Sh = k_{\rm SL} \times D_{\rm p}/D_{\rm AB}$ and the values were found to be 0.58 and 0.89, respectively. To be on the safer side, the limiting value of the Sherwood number was taken as 2. The actual value is so far greater than 2 due to intense agitation (Yadav and Manyar 2003; Kozhenikov et al. 1996). The effect of mass transfer resistance due to A and B is given by $1/(k_{\rm SLA} \times a_{\rm p})$ and $1/(k_{\rm SLB} \times a_{\rm p})$ where $a_{\rm p}$ represents the solid-liquid interfacial area and the values obtained are 2.87×10^{-3} and 1.85×10^{-3} m³/kg, respectively. The initial rate (r_{Ai}) was calculated from standard reaction and was found to be 0.17 from which $1/r_{Ai}$ was calculated to 5.8 and it was very much greater than by $1/(k_{\rm SLA} \times a_{\rm p})$ and $1/(k_{\rm SLB} \times a_{\rm p})$. It confirms that the mass transfer rates were much higher than rates of reaction and hence speed of agitation had no influence on reaction rate.

Effect of catalyst loading

The effect of catalyst loading was studied over the range of 0.01–0.032 g/cm³ (Fig. 3). In the absence of external mass transfer resistance, the rate of reaction was directly proportional to the catalyst loading based on the entire liquid phase volume, which is due to the proportional increase in the number of active sites. Further reactions were carried out with 0.024 g/cm³ catalyst loading.



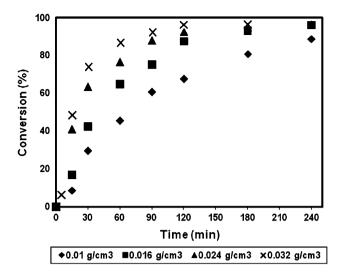


Fig. 3 Effect of catalyst loading on conversion of 1-phenyl ethanol. Reaction conditions: 1-phenyl ethanol 0.05 mol, glycerol 0.2 mol, 1.0 cm³ *N*-methyl pyrrolidone as internal standard, 25 cm³ total reaction volume, speed of agitation 1000 rpm, temperature 120°C

This catalyst is robust as has been proved in our earlier work (Yadav and Manyar 2003). The catalyst could be recovered and reused several times. It was recovered by filtration of the reaction mixture. The filtered catalyst was washed with methanol, dried in the oven at 120°C for 10 h and reused.

Effect of intra-particle diffusion resistance

The Weisz-Prater criterion was employed to assess the influence of intra-particle diffusion resistance. According to Weisz-Prater criterion, the dimensionless parameter $\{C_{\rm WP} = r_{\rm obs} Rp^2/D_{\rm e} [C_{\rm AS}]\}$ which represents the ratio of the intrinsic reaction rate to the intra-particle diffusion rate, can be evaluated from the observed rate of reaction, the particle radius (R_p) , effective diffusivity of the limiting reactant (D_e) and [C_{AS}] concentration of the reactant at the external surface of the particle. The effective diffusivity of 1-phenyl ethanol $(D_e - A)$ inside the pores of the catalyst was obtained from the bulk diffusivity (D_{AB}) , porosity (ε) and tortuosity (τ) as 7.95 \times 10⁻⁹ m²/s where $D_{\rm e} - {\rm B} = D_{\rm AB} \cdot \varepsilon/\tau$. The average values of porosity and tortuosity were taken as 0.4 and 3, respectively, as a conservative estimate. In the present case, the value of $C_{\rm WP}$ was calculated as 4.23×10^{-6} , which is less than 1. Hence, there was no intra-particle diffusion resistance.

Effect of mole ratio

Under solvent-less conditions, with excess of glycerol, the reaction mixture becomes highly viscous. The effect of

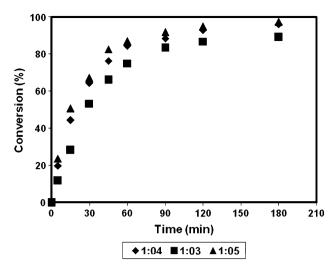


Fig. 4 Effect of mole ratio of 1-phenylethanol: glycerol on conversion of 1-phenyl ethanol. Reaction conditions: 1.0 cm³ *N*-methyl pyrrolidone as internal standard, Speed of agitation 1000 rpm, 25 cm³ total reaction volume, catalyst loading 0.024 gm/cm³, temperature 120°C

1-phenyl ethanol to glycerol ratio was studied at 1:3, 1:4 and 1:5 under otherwise similar conditions (Fig. 4). The rate of conversion of 1-phenyl ethanol was found to increase with the increase in the amount of glycerol. Below 1:3 ratio, glycerol and 1-phenyl ethanol becomes immiscible with each other and above 1:5 ratio the reaction mixture becomes highly viscous. Therefore, further reactions were carried out with 1:4 mol ratio.

Effect of temperature

The effect of temperature on conversion was studied between 100 and 140°C. It was observed that the rate of reaction increases with increase in temperature (Fig. 5). This would suggest a kinetically controlled mechanism. Above 120°C, the reaction occurs very fast and the kinetics would be difficult to predict. Therefore, 120°C was taken as optimum for the reaction.

Development of kinetic model

The above results were used to build a kinetic model. From the calculated values of mass transfer rates of A and B and the initial rate it was evident that the reaction was devoid of inter and intra-particle diffusion resistances. The reaction involves two reactants namely 1-phenyl ethanol (A) and glycerol (B) to give the desired product monoether of glyceryl ether (P) and water (W). A dual site reaction mechanism was proposed for this reaction. Thus, the reaction may be controlled by any of these 3 steps namely (1) adsorption, (2) surface reaction (3) desorption. It was



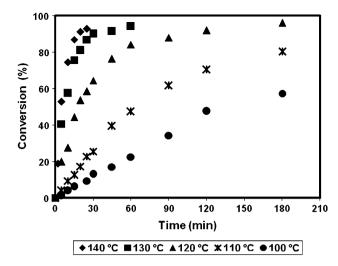


Fig. 5 Effect of temperature on conversion of 1-phenyl ethanol. Reaction conditions: 1-phenyl ethanol 0.05 mol, glycerol 0.2 mol, 1.0 cm^3 *N*-methyl pyrrolidone as internal standard, 25 cm^3 total reaction volume, speed of agitation 1000 rpm, catalyst loading 0.024 gm/cm^3

assumed that, reactants 1-phenyl ethanol and glycerol were weekly adsorbed on the catalyst.

Adsorption of 1-phenyl ethanol (A) on vacant site was given by

$$A + S \stackrel{K_A}{\leftrightarrow} AS \tag{1}$$

Adsorption of glycerol (B) on vacant site was given by

$$B + S \stackrel{K_B}{\longleftrightarrow} BS \tag{2}$$

Surface reaction of AS and BS leading to the formation of monoalkyl glyceryl ether (PS) on the site

$$AS + BS \stackrel{K_{SR}}{\leftrightarrow} PS + WS \tag{3}$$

Desorption of monoalklyl glyceryl ether (PS) and water (WS) is given by

$$PS \stackrel{1/K_P}{\leftrightarrow} P + S \tag{4}$$

$$WS \stackrel{1/K_W}{\leftrightarrow} W + S \tag{5}$$

The total concentration of the sites, C_t expressed as

$$C_{t} = C_{S} + C_{AS} + C_{BS} + C_{PS} + C_{WS}$$
 (6)

Or

$$C_{t} = C_{S} + K_{A}C_{A}C_{S} + K_{B}C_{B}C_{S} + K_{P}C_{P}C_{S} + K_{W}C_{W}C_{S}$$
(7)

The concentration of vacant sites,

$$C_{\rm S} = \frac{C_{\rm t}}{1 + K_{\rm A}C_{\rm A} + K_{\rm B}C_{\rm B} + K_{\rm P}C_{\rm P} + K_{\rm W}C_{\rm W}}$$
(8)

If the surface reaction (C) controls the rate of reaction, then the rate of reaction of A is given by

$$-r_{A} = -\frac{dC_{A}}{dt} = k_{SR}C_{AS}C_{BS} - k'_{SR}C_{PS}C_{WS}$$
 (9)

$$-\frac{dC_{A}}{dt} = \frac{k_{SR}\{K_{A}K_{B}C_{A}C_{B} - (K_{P}K_{W}C_{P}C_{W}/k_{SR})\}C_{t}^{2}}{(1 + K_{A}C_{A} + K_{B}C_{B} + K_{P}C_{P} + K_{W}C_{W})^{2}}$$
(10)

When the reaction is far away from equilibrium,

$$-\frac{dC_{A}}{dt} = \frac{k_{SR}K_{A}K_{B}C_{A}C_{B}C_{t}^{2}}{(1+\sum K_{i}C_{i})^{2}}$$
(11)

$$=\frac{k_{\rm r}wC_{\rm A}C_{\rm B}}{\left(1+\sum K_{\rm i}C_{\rm i}\right)^2}\tag{12}$$

where $k_{\rm r}w = k_{\rm SR}K_{\rm A}K_{\rm B}Ct^2$; w is catalyst loading. If the adsorption constants are very small, then the above equation reduces to

$$-\frac{\mathrm{d}C_{\mathrm{A}}}{\mathrm{d}t} = k_{\mathrm{r}}C_{\mathrm{A}}C_{\mathrm{B}}w\tag{13}$$

Let $C_{\rm B0}/C_{\rm A0}=M$, the molar ratio of 1-phenyl ethanol to glycerol at time t=0. Then, Eq. 13 can be written in terms of fractional conversion as

$$\frac{dX_{A}}{dt} = k_{\rm r} C_{A0} w (1 - X_{\rm A}) (M - X_{\rm A}) \tag{14}$$

This upon integration leads to:

$$\ln\left\{\frac{M - X_{A}}{M(1 - X_{A})}\right\} = k_{1}C_{A0}(M - 1)t \tag{15}$$

where

$$k_1 = k_r w \tag{16}$$

Thus a plot of $\ln (M - X_A)/M(1 - X_A)$ against time at different temperatures gave an excellent fit, thereby validating the model (Fig. 6) indicating that the reaction is an overall second order. The values of the rate constants

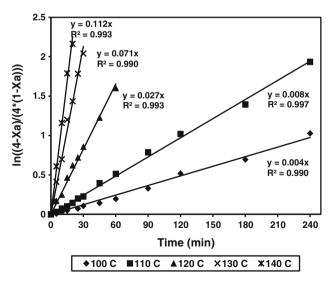


Fig. 6 Plot of $\ln (M - X_A)/M(1 - X_A)$ against time



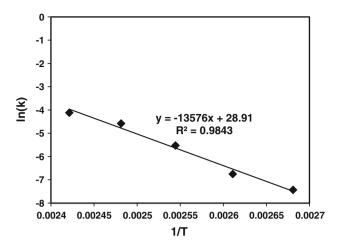


Fig. 7 Arrhenius plot

at different temperatures were calculated and an Arrhenius plot was used to estimate the apparent activation energy of the reaction (Fig. 7). The apparent activation energy was found to be 27 kcal/mol, which indicates intrinsic kinetically controlled reaction.

Economics of the process

In the usual homogeneously catalysed *trans*-esterification of bio-oils, it also contains variable amounts of excess alcohol, water, NaOH, and a mixture of soaps, unreacted fats and oils. The glycerol phase which is heavier than aqueous phase, settles at the bottom. It is subjected to neutralisation with acid, foam breaking and distillation. This impure glycerol is subjected to vacuum distillation. However, with reference to green chemistry, heterogeneous catalysis would be most advantages and we have shown independently how solid acids can give excellent yield of biodiesel and glycerol which do not produce soaps and other impurities (for instance, supported heteropolyacids; Bokade and Yadav 2009). Therefore, such good quality glycerol will be further used for 3-(1-phenylethoxyl) propane-1,2-diol.

Since it is a heterogeneous catalysed reaction, the quality of the product is superior with absence of any inorganic contaminants. The process gives 98% conversion with 75% selectivity to the mono O-alkyl product. The product can be separated easily.

Since the prices of glycerol are fluctuating, a rudimentary cost of production with recycles of methanol and unreacted starting materials can be arrived at. By taking the cost as: glycerol US \$ 0.80/kg, 1-phenylethanol \$ 4.50/kg, catalyst \$ 0.10/kg and processing cost of 30% of the raw materials, with recycle of unreacted reagents, the approximate cost of production 3-(1-phenylethoxy) propane-1,2-diol is \$6.22/kg.

Since this is a fine chemical, the cost of this product in the market is approximately \$ 8–10/kg, depending on volume. Therefore, the process will be green, clean and economical.

Conclusion

Heterogeneous acid catalysis by supported heteropoly acids offers substantial economic and environmental benefits. The etherification of glycerol with 1-phenyl ethanol was studied using a variety of catalysts amongst which 20% w/w DTP-HMS as the catalyst. This catalyst was found to be highly active and selective giving 75% selectivity towards mono ether product. The effects of various parameters on the rates of the reactions were discussed. A second order rate equation for the reaction mechanism was successfully developed and validated. The apparent activation energy 27.0 kcal/mol was estimated. This method has contributed substantially to the conversion of glycerol to more value-added chemicals.

Acknowledgments G. D. Yadav received support for personal chairs from Darbari Seth and R. T. Mody Distinguished Professor endowments and J.C. Bose National Fellowship from Department of Science and Technology, Govt. of India. Financial support from the CSIR-NMITLI is gratefully acknowledged. Payal Chandan received SRF from this grant. Nirupama Gopalaswami received a summer fellowship for undergraduate students from the National Academies.

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