STABILIZATION OF ZIRCONIA WITH COMBINED ADDITIVES AND A STUDY OF THE SOLID SOLUTION STABILITY

A. B. Andreeva, É. K. Keler, and A. I. Leonov

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It is known that zirconium dioxide forms, with other refractory oxides of similar ionic radius, solid solutions that are stabilized in the cubic or tetragonal structure [1-6].

The commonest oxide-stabilizers are MgO and CaO, added in amounts of 10-15 mole %. However solid solutions on this basis are prone to decomposition upon the prolonged action of elevated (1000-1400°C) temperatures, and the zirconia is destabilized [5, 7-9].

In the search for more stable materials ZrO_2 has been stabilized with oxides of rare and rare-earth metals. Studies have shown that stable solid solutions are produced by yttrium oxide. However its wide industrial use has been limited because of its high cost and scarcity.

The present authors carried out a study to clarify the possibilities of obtaining more highly spalling resistant, cheaper, and more stable zirconia materials.

In the investigation a number of compositions were compiled based on zirconia, incorporating combined additives of two or more stabilizing oxides. The properties were studied in comparison with two-component solid solutions $\rm ZrO_2-MgO$, and $\rm ZrO_2-CaO$. All the oxides used in the compositions were chemically pure and had a grain size of less than $5~\mu$. The mixtures were carefully blended by the wet method in an agate mortar, dried, and pressed at 300 kg/cm² into specimens which were then fired in a periodic kiln heated with kerosene at $1550-1750^\circ$ with a 4 h soak. To determine the bending strength prisms were pressed measuring $30~\times~7~\times~2.5~\rm mm$, and for the dilatometric studies specimens measuring $65~\times~8~\times~8~\rm mm$. The phase composition of the fired specimens was determined by x-ray, dilatometric, and microscopic methods. The compositions of the specimens and their properties after firing at 1750° are given in Table 1.

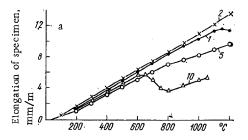
TABLE 1. Sintering and Properties of Specimens Fired at 1750° with a 4 h Soak

Specimen No.	Composition of specimen, mole %	Shrinkage, %	Water absorption, %	Apparent density, g/cm ³	Apparent porosity, %	Bending strength, kg/cm ²	Structure of Specimen*
1 2 3 4 5 6 7 8 9 10 11 12	$\begin{array}{c} 90 \% \ ZrO_2 + 10 \% \ MgO \\ 85 \% \ ZrO_2 + 15 \% \ MgO \\ 90 \% \ ZrO_2 + 6 \% \ MgO + 4 \% \ CaO \\ 90 \% \ ZrO_2 + 6 \% \ MgO + 5 \% \ CaO \\ 93 \% \ ZrO_2 + 5 \% \ MgO + 2 \% \ Y_2O_3 \\ 92 \% \ ZrO_2 + 5 \% \ MgO + 3 \% \ Y_2O_3 \\ 90 \% \ ZrO_2 + 5 \% \ MgO + 5 \% \ Y_2O_3 \\ 90 \% \ ZrO_2 + 5 \% \ MgO + 5 \% \ Nd_2O_3 \\ 90 \% \ ZrO_2 + 5 \% \ MgO + 5 \% \ La_2O_3 \\ 94 \% \ ZrO_2 + 5 \% \ MgO + 1 \% \ Nd_2O_3 \\ 90 \% \ ZrO_2 + 8 \% \ MgO + 2 \% \ Y_2O_3 \\ 90 \% \ ZrO_2 + 10 \% \ Y_2O_3 \\ \end{array}$	32,0 27,0 27,0 29,0 27,0 26,0 26,0 25,5 30,0 25,1 28,0 26,5	0,35 0,2 0,2 0,5 0,4 0,2 0,35 0,5 1,3 0,5	5,0 5,0 5,25 5,2 5,3 5,35 5,5 5,1 5,1 5,2 5,2	1,9 1,0 1,0 2,6 2,1 1,1 0,0 1,7 2,5 6,5 0 2,5	1580 1200 1000 1600 2000 1800 1400 1300 1100 2000	K+about 10 % M K K K K K+10 % M K K K K K+20 % M K+20 % M K

^{*} In this and subsequent tables K indicates cubic, and M indicates monolithic

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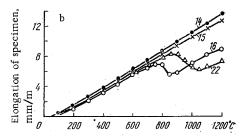


Fig. 1. Linear expansion of solid solutions of zirconia. Specimens fired at 1750°. Figures on the curves indicate specimen No. (see Tables 1 and 3).

TABLE 2. Comparison of Stability of Two- and Three-Component Solid Solutions Based on Zirconia*

No.	Original	Quantity of monoclinic phase, % after heating at 1200°C						
Specimen (see Tabl		150 h	300 h	400 h	500h			
1 2 3 4 5 6 7 8 9 11	K+about 10%M K K K K K+10%M K K	100 100 >60 >80 15 0	100 100 >70 >90 20 0 0 >70	 >85 25 15 0	 30 15 0			
9 11 12	K+20%M K K	>50 100 0 0	100 0 0	10 0	20 0			

^{*} Specimens synthesized at 1750° with a soak of 4 h, tested as powders ($<5 \mu$)

The comparable specimens were sintered almost identically: the water absorption was from 0 to 0.4%, and the apparent porosity from 0 to 2.5%. All the specimens had the cubic structure; complete stabilization of the zirconia was achieved except for compositions Nos. 1, 5, 9, and 10 which contain 10-20% monoclinic phase. A relatively high strength is possessed by specimens stabilized with combined magnesium - yttrium additives.

Dilatometric studies showed that in the specimen densely stabilized with magnesium oxide (Fig. 1a, curve 2) there are no polymorphic inversion effects, but the coefficient of thermal expansion is rather high $[(11.5-12.0)\cdot 10^{-6}\ deg^{-1}]$. Incomplete stabilization causes only residual development of polymorphism in the zirconia, but it is connected with low volume changes, and does not produce breakdown of the specimens (Fig. 1a). The thermal expansion coefficient of the compositions containing yttrium and neodymium is much less (about $8\cdot 10^{-6}\ deg^{-1}$).

Specimens were tested for stability during isothermal heating at 1200° and with a soaking time of from 100 to 500 h. In order to accelerate the decomposition of the solid solutions we tested them in the ground state (less than 5 μ). The test results are given in Table 2.

The maximum stability was shown by zirconium – yttrium and three-component solid solutions ($ZrO_2-MgO-Y_2O_3$), which after testing for 500 h preserved completely or almost completely their original cubic structure.

In the specimens of composition $\rm ZrO_2-MgO-CaO$ and $\rm ZrO_2-MgO-Nd_2O_3$, after 300 h testing more than 70% of the monoclinic phase was formed. The least resistance was shown by the solid solutions of the compositions $\rm ZrO_2-MgO$, and $\rm ZrO_2-MgO-La_2O_3$, which completely decomposed after 125 h testing.

We synthesized zirconia—CaO solid solutions with an addition of a second stabilizing oxide. The composition, sintering, and properties of the mixtures are given in Table 3.

The specimens of these compositions during firing to 1750° are sintered in the same way as zirconia—magnesia (see Table 1). In all compositions solid solutions are formed with the cubic structure; in some cases stabilization was incomplete (Nos. 13, 16, 19, and 22). The mechanical strength of the specimens critically depends on the additives and their quantities; the best facfors were obtained from compositions Nos. 14, 17, 18, 20, and 21.

The results for stability testing given in Table 4 show that the most stable are ternary solid solutions ($\rm ZrO_2-\rm CaO-\rm Y_2\rm O_3$). Other compositions proved to be much less stable. After 150 h testing they develop from 35 to 60% monoclinic phase; with further heating decomposition was continued.

The dilatometric investigation of zirconia-CaO solid solutions show that during firing up to 1500 and 1650° the specimens with the combined additive, being in total less than 10 mole %, are not completely stabilized (curves 16 and 22, Fig. 1b).

The curves exhibit bends that are due to the residual inversions of the monoclinic zirconia; however, these volume changes are comparatively small and occur more smoothly than in pure zirconia. The specimens did not crack.

TABLE 3. Sintering and Properties of Specimens Fired at 1750°

Specimen No.	Composition of specimen, mole %	Shrinkage, %	Water absorption, %	Apparent density, g /cm³	Apparent porosity, %	Bending strength, kg /cm²	Structure of speci- men
12 13 14 15 16 17 18 19 20 21 22	$\begin{array}{l} 90 \% \ ZrO_2 + 10 \% \ Y_2O_3 \\ 95 \% \ ZrO_2 + 5 \% \ CaO \\ 90 \% \ ZrO_2 + 10 \% \ CaO \\ 90 \% \ ZrO_2 + 6 \% \ CaO + 4 \% \ MgO \\ 93.5 \% \ ZrO_2 + 5 \% \ CaO + 1.5 \% \ Y_2O_3 \\ 93 \% \ ZrO_2 + 5 \% \ CaO + 2 \% \ Y_2O_3 \\ 92 \% \ ZrO_2 + 5 \% \ CaO + 3 \% \ Y_2O_3 \\ 90 \% \ ZrO_2 + 5 \% \ CaO + 5 \% \ La_2O_3 \\ 90 \% \ ZrO_2 + 8 \% \ CaO + 2 \% \ Y_2O_3 \\ 90 \% \ ZrO_2 + 5 \% \ CaO + 5 \% \ Nd_2O_3 \\ 88 \% \ ZrO_2 + 9 \% \ CaO + 3 \% \ Nb_2O_5 \end{array}$	28,0 24,5 26,5 26,0 26,8 27,6 28,0 29,0 27,0	0,6 5,0 0,1 0,2 0,3 0,2 0,4 0,5 0,1 0,2 3,0	5,3 4,30 5,35 5,25 5,2 5,2 5,2 5,2 5,2 5,3 4,4	3,0 21,5 0,5 1,0 1,6 1,0 2,1 2,5 0,5 2,0 13,2	1100 500 2000 1450 1800 2000 2300 1600 2250 2330 300	K 60% K + 40% M K K K + about 10% M K K + 20% M K K + 20% M

TABLE 4. Comparison of the Stability of Two- and Three-Component Solid Solutions Based on Zir-conia*

Specimen No.	Structure of original solid solu- tion	Quantity of monoclinic phase, % after heating at 1200°C						
		150 h	300 h	400h	500 h			
12 14 15 16 17 18 19 20 21 22	K K K K+10%M K K K+20%M K K+20%M	0 >30 60 15 0 60 60 60 240 45	0 60 85 20 10 10 80 0 >60 >70	0 >80 >90 30 15 10 >90 90 90	0 			

^{*} Specimens synthesized at 1750°C with a soak of 4 h.

The investigations showed that the solid solutions of zirconia with magnesia and CaO, containing additions of yttrium oxide, acquire an enhanced resistance against thermal decomposition. The most resistant proved to be ternary solid solutions of $\rm ZrO_2-MgO-Y_2O_3$, and $\rm ZrO_2-CaO-Y_2O_3$ with a content of 2-5% $\rm Y_2O_3$.

The results of the work formed the basis for further detailed investigation of the mechanism and kinetics of the formation of such solid solutions, and a study of their physicoengineering properties and their stability in the high temperature region (about 2000°C).

Considering the thermal-shock resistance and the high engineering properties of double zirconia-yttria solid solutions, replacement in them of a large part of the yttrium oxide by alkaline earth oxides can be considered as a measure for reducing the proportion of the expensive and scarce yttrium oxide in the composition of zirconia products of very high refractoriness.

CONCLUSIONS

The stability of solid solutions of ZrO_2 – MgO and ZrO_2 – CaO may be critically increased by incorporating small additions (1-2%)

of yttrium oxide. Complete discontinuation of the decomposition of these solid solutions occurs with an addition of $3\% \text{ Y}_2\text{O}_3$.

Stabilization of zirconium dioxide by combined additions is achieved with a lower concentration of oxide-stabilizers compared with the required concentration of each of them separately. This permits a substantial reduction in the expenditure on costly and scarce additives, for instance, oxides of rare-earth elements, and vttrium.

The synthesized ternary solid solutions possess valuable physicoengineering properties, such as high mechanical strength, and a lower average coefficient of thermal expansion than double solid solutions.

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