

# A Stochastic Algorithm for the Isobaric–Isothermal Ensemble with Ewald Summations for All Long Range Forces

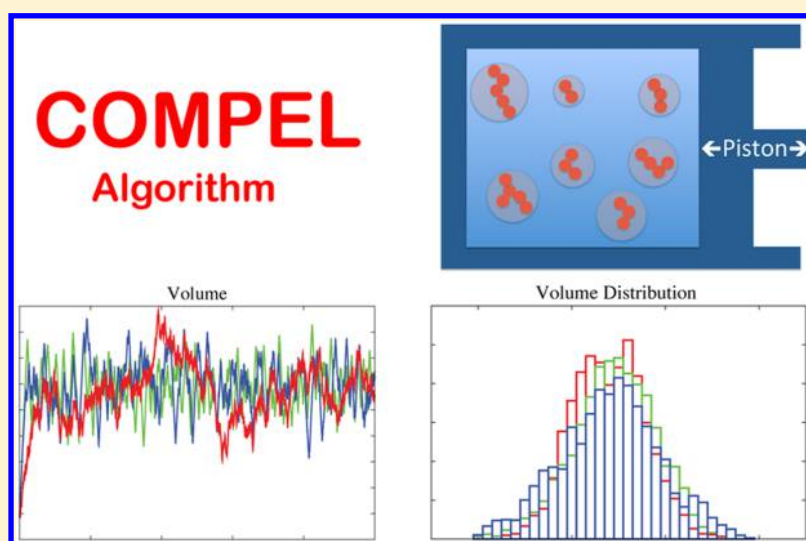
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**ABSTRACT:** We present an algorithm termed COMPEL (Constant Molecular Pressure with Ewald sum for Long range forces) to conduct simulations in the NPT ensemble. The algorithm combines novel features recently proposed in the literature to obtain a highly efficient and accurate numerical integrator. COMPEL exploits the concepts of molecular pressure, rapid stochastic relaxation to equilibrium, exact calculation of the contribution to the pressure of long-range nonbonded forces with Ewald summation, and the use of Trotter expansion to generate a robust, highly stable, symmetric, and accurate algorithm. Explicit implementation in the MOIL program and illustrative numerical examples are discussed.

## INTRODUCTION

Molecular dynamics (MD) is a powerful and flexible tool for the study of complex systems at the molecular and atomic level. The models and algorithms that we use today are the product of some 50 years of continuous development. A major direction of study throughout the years has been the design of algorithms that allow for the sampling of different statistical mechanical ensembles.

The macroscopic (thermodynamic) state of a statistical mechanical system can be characterized by the quantities that are fixed at defined values.<sup>1,2</sup> Experiments carried out in laboratory conditions are typically defined by constant pressure, temperature, and number of particles; these conditions correspond to the isobaric–isothermal ensemble, also known as the NPT ensemble. Although all ensembles are equivalent in the thermodynamic limit, switching between ensembles for

finite size systems can be challenging. For example, using the NVT ensemble to mimic NPT requires a specified choice of density. There is no simple way to estimate the density of nonhomogeneous systems such as solvated proteins, membranes, or micelles. Even in the case of liquid mixtures, only the densities of pure liquids are usually known. It is therefore essential to carry out equilibration simulations in which the volume can be adjusted such that the pressure matches a target value. Further complications arise when the system under study is subjected to driving forces that alter its thermodynamic state; in such a case, it is thus necessary to perform molecular dynamics simulations in which the volume is automatically adjusted so that the pressure remains constant.

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Many algorithms, including some quite recent proposals, have been suggested to sample from the NPT ensemble (e.g., see refs 3–6). In this paper, we present a stochastic algorithm for the isobaric–isothermal ensemble that combines the best features previously introduced in different contexts to obtain a comprehensive, accurate, and stable algorithm. Our approach exploits and combines state-of-the-art simulation techniques in two distinct areas: (i) algorithms for the integration of the equations of motion based on certain splittings of stochastic differential equations<sup>7–11</sup> and (ii) algorithms for the calculation of the forces based on Ewald summation.<sup>12–15</sup> We have implemented and evaluated our method in the molecular dynamics software package MOIL.<sup>16</sup>

In microcanonical molecular dynamics, Newton's equations of motion are solved to advance the system in time, thus generating a trajectory. One typically assumes ergodicity of the dynamics and hence that the trajectory samples all accessible configurations of the microcanonical ensemble (or NVE). For the isobaric–isothermal ensemble to be sampled, the simulation needs to incorporate additional mechanisms to control the temperature (thermostat) and pressure (barostat). The most common ways to impose a temperature control are velocity rescaling,<sup>17</sup> weak coupling method,<sup>18</sup> stochastic methods that mimic the behavior of a thermal bath, such as the Langevin equation,<sup>19</sup> and Nosé–Hoover dynamics.<sup>20</sup> Nosé introduced the idea that a thermal bath can be modeled using an additional degree of freedom over which one may integrate to provide the correct sampling of physical quantities. The approach has been referred to as a pseudomicrocanonical simulation, as the integration of the extended system is essentially conservative, while averages of quantities that are functions of position and momenta only correspond to the NVT ensemble. Nosé's seminal idea has led to a variety of different extended system methods.

All of the methods mentioned above are in principle able to reproduce correct thermodynamics, i.e., the correct microstate distribution of the corresponding ensemble. However, any thermostating algorithm alters the dynamics of the system with respect to Newton's equations of motion. These thermostat-dependent artifacts in the dynamics can hinder the quality of measurement of transport properties and kinetics. Of particular importance is the interplay between ergodic sampling of the thermodynamic ensemble and the need to capture dynamical approximation properties of the underlying Hamiltonian system. With respect to other methods, the Nosé–Hoover thermostat is thought to better preserve dynamical properties because the perturbation to the system is acting through a single auxiliary degree of freedom. Evans<sup>21</sup> pointed out that the perturbation of dynamics is  $O(1/\nu)$ , where  $\nu$  is the number of degrees of freedom. Recently, Basconi and Shirts,<sup>22</sup> in numerical experiments, have confirmed that the transport properties of several systems simulated using Nosé–Hoover are statistically indistinguishable from those of the same system simulated in the microcanonical ensemble. Leimkuhler and collaborators<sup>23</sup> have studied the transport properties of stochastic thermostat methods, observing that the combination of Nosé–Hoover with degenerate noise in the auxiliary thermostat variable only (Nosé–Hoover–Langevin dynamics<sup>24</sup>), for example, is capable of accurately representing dynamical properties.

For the control of pressure, most modern schemes build on the extended system approach of Andersen,<sup>25</sup> which maintains the pressure by allowing the volume of the simulation cell to

fluctuate under the control of an additional degree of freedom, sometimes referred to as a “piston”, which is usually implemented in combination with some sort of thermostat. A drawback of the Andersen barostat is that the mass of the piston determines the way in which the system approaches equilibrium. Although the average volume and magnitude of its fluctuations are correct, there is significant memory visible in the volume fluctuations. The volume as a function of time in fact contains regular oscillations (“ringing”) inversely proportional to the mass of the piston.<sup>26</sup> The ringing phenomenon leads to difficulties in the choice of parameters. A method for controlling the oscillations is the “Langevin piston” method due to Feller et al.,<sup>27</sup> which couples an underdamped Langevin dynamics process to the piston equation. We incorporate a similar technique here so that, in addition to producing reasonable dynamics and kinetics at the limit of a long time, we can also control the mixing time (the necessary waiting time during which the system relaxes to the appropriate equilibrium state) to be as short as possible.

Motions along bonds in molecular systems are typically the fastest degrees of freedom. These set an upper bound on the time step that can be used in integrating the equations of motion. For this reason, in MD, it is often beneficial to impose holonomic constraints to accelerate the simulation and to make it more stable by “freezing” the degrees of freedom with the fastest dynamics.<sup>28</sup> The use of NPT algorithms in the presence of constraints is not entirely straightforward; the problem was solved by Kneller and Mulders<sup>29</sup> and further investigated by Ciccotti et al.<sup>30</sup> Their approach is demanding and, fortunately, not necessary; the use of the alternate approach of molecular pressure is simpler and more efficient. In “molecular pressure”, the pressure is calculated using positions and momenta of molecules instead of atoms; the equivalence between the molecular and atomic formulations of the pressure was first proven by Ciccotti and Ryckaert.<sup>31,32</sup> This procedure avoids consideration of covalent bonding forces. The atomic and molecular pressure are a special case of a generalized scheme in which the pressure is expressed by using the positions and momenta of subsets of atoms within molecules.<sup>4</sup> The use of molecular pressure in MD recently gained new interest; see for example the recent implementation in the software Desmond of the Martyna–Tobias–Klein algorithm applied to molecular pressure.<sup>3</sup>

Through the use of molecular pressure, the NPT algorithm acts by rescaling molecular positions only, thus leaving bonds unaffected. Molecular pressure provides two advantages compared to pressure calculations based on atomic positions. First, to calculate the molecular pressure, we only need to calculate the virial of the intermolecular forces; i.e., only nonbonding interactions contribute to the pressure. Second, calculating the molecular virial greatly reduces fluctuations of pressure; once again, this is due to the fact that the virials of the rapidly changing forces due to the covalent potential are not included in the calculation.<sup>33</sup>

To build a time-stepping algorithm from a continuous equation of motion, a discretization scheme is required. In MD, it is common to use a symmetric Trotter expansion of the Liouville operator. This type of approach dates to the seminal paper of Ruth on symplectic integration,<sup>34</sup> and it has been used to build efficient integrators for a wide range of applications, such as multiple timestepping (e.g., RESPA).<sup>35</sup> In our case, we will use an underdamped Langevin equation for the motion of the piston. This equation can be decomposed into Hamiltonian

components and Ornstein–Uhlenbeck equations. The integrator for the Langevin equation can then be constructed by composing Hamiltonian flows with the exact distributional solution of the Ornstein–Uhlenbeck (linear stochastic) system. Although very natural, this type of method was introduced and studied relatively recently.<sup>7–11</sup>

The second key ingredient of molecular simulations is the model that we use to describe the system under consideration. The functional form of MD force fields has remained essentially the same for decades; however, the way interactions are calculated has evolved. The interacting potential between atoms consists of bonding and nonbonding terms. The bonding interactions are modeled by two-, three-, and four-body energy terms, whereas the nonbonded interactions consist of fixed-point charge electrostatic forces and a Lennard-Jones (LJ) potential that models hard-core and dispersive forces.

The calculation of nonbonding interaction is computationally expensive, and it tends to dominate the total runtime of MD simulations. In the early days, to save computer time, all of the interactions were set to zero at a given cutoff distance. Eventually, the analysis of artifacts due to truncation led to the use of Ewald summation for electrostatic interactions. Particle Mesh Ewald<sup>12</sup> is now a de facto standard in molecular simulations. Recently, the growing heterogeneity of simulated systems together with the availability of more computational power support applying a similar approach to Lennard-Jones (LJ) interactions.<sup>13</sup> LJ interactions decay with distance as  $r^{-6}$ , a decay rate that is much more rapid than electrostatic interactions ( $r^{-1}$ ), which explains the earlier focus on electrostatic terms. For example, Wennberg et al.<sup>36</sup> have shown that the use of a cutoff of 10 Å for LJ interactions introduces deviations up to 5% in the order parameters of lipid bilayers with respect to simulations with no cutoff, i.e., using Ewald summation.

Truncation of dispersive interactions is highly relevant in measuring pressure. The neglected interactions are all attractive and add up. This leads to errors in the estimation of the pressure that, at a typical cutoff of 10 Å, are on the order of hundreds of atm. Errors of this kind can be estimated in the case of isotropic, homogeneous liquids.<sup>37</sup> Lague et al.<sup>38</sup> calculated the long-range correction for anisotropic systems, such as membranes and proteins, by measuring the pressure with a very long distance cutoff once every few timesteps. The correction is then applied statically until a new long cutoff calculation is executed and a new estimate for the correction is available.

We propose an algorithm for constant molecular pressure in which all the long-range interactions are calculated using Ewald summation. The algorithm consists of a Nosé–Hoover thermostat coupled with a Langevin piston. The stochastic equations of motion are discretized using a reversible multiple time step Trotter expansion that takes advantage of the splitting method for the Langevin equation. We illustrate that the algorithm is highly accurate and stable and that it converges rapidly to the desired values. It is implemented in the simulation program MOIL.

This paper is organized as follows. The first section introduces the equations of motion. The second section is dedicated to the model and the representation of the potentials by Ewald summations. The third section is about molecular pressure and how it is measured. The fourth section outlines the discretization procedure and the explicit algorithm. The last section provides numerical examples.

## ■ EQUATIONS OF MOTION FOR THE ISOBARIC–ISOTHERMAL ENSEMBLE

The system consists of  $N$  molecules. A molecule is defined as a group of atoms that are covalently linked. The use of molecular pressure implies the study of gas and liquid phases. It does not make sense (for example) to investigate covalent solids, such as diamond, using molecular pressure. We will indicate the position vector of the center of mass of a molecule by  $\vec{R}_\mu$ , the momentum by  $\vec{P}_\mu$ , and the mass by  $M_\mu$ . The total number of atoms in the system is  $n$  with the number of atoms of molecule  $\mu$  being  $n_\mu$ . We indicate the coordinates of atom  $i$  in the coordinate system of molecule  $\mu$  by  $\vec{r}_{\mu i}$ , the momentum by  $\vec{p}_{\mu i}$ , and the mass by  $m_i$ . Thus, we have

$$\vec{R}_\mu = \frac{1}{M_\mu} \sum_{i=1}^{n_\mu} m_i \vec{r}_i, \quad M_\mu = \sum_{i=1}^{n_\mu} m_i \quad (1)$$

$$\vec{r}_i = \vec{R}_\mu + \vec{r}_{\mu i}, \quad i = 1, 2, \dots, n_\mu$$

We use the shorthand  $i \in \mu$  to indicate that atom  $i$  is in molecule  $\mu$ , thus the expression for the mass of molecule  $\mu$  could be written as  $M_\mu = \sum_{i \in \mu} m_i$

The atoms are subject to  $K$  holonomic constraints

$$\sigma_j(\vec{r}) = 0, \quad j = 1, 2, \dots, K \quad (2)$$

The number of degrees of freedom of the system is  $g = 3n - K$ . The force induced by the constraints on atom  $i$  that belongs to molecule  $\mu$  is  $\vec{G}_{\mu i}$ . The atoms interact through the potential  $U(\vec{r})$ , with  $\vec{F}_{\mu i}$  being the force acting on atom  $i$ , and  $\vec{F}_\mu$  representing the vector of all internal forces acting on molecule  $\mu$ .

The molecules are contained in a volume  $V$ , and the system is kept at equilibrium with a thermal bath at constant temperature  $T_{\text{ext}}$  and constant pressure  $\Pi_{\text{ext}}$ . The internal kinetic temperature of the system is the average of  $T^*$  given by

$$T^* = \frac{1}{gk_B} \left[ \sum_{i,\mu} \frac{\vec{p}_{\mu i}^2}{m_{\mu i}} + \sum_{\mu} \frac{\vec{P}_\mu^2}{M_\mu} \right] \quad (3)$$

and the internal molecular pressure is obtained by averaging<sup>32</sup>

$$\Pi^* = \frac{1}{3V} \sum_{\mu} M_\mu \dot{\vec{R}}_\mu^2 + \frac{1}{6V} \sum_{\mu} \sum_{\mu'} \sum_{i \in \mu} \sum_{j \in \mu'} (\vec{R}_\mu - \vec{R}_{\mu'}) \cdot (\vec{f}_{\mu i} - \vec{f}_{\mu' j}) - \frac{\partial U}{\partial V} \quad (4)$$

We explain how to calculate the molecular pressure for periodic boundary conditions in a dedicated section below.

To reproduce the sampling of the isobaric–isothermal ensemble, the equations of motion are not derived directly from a Hamiltonian but instead include additional degrees of freedom. In addition to the set of coordinates already defined, we introduce the variables  $V$ ,  $\eta$ , and  $\xi$  ( $\eta$  and  $\xi$  are dimensionless). The volume of the system,  $V$ , is viewed as a dynamical variable associated with the barostat with  $P_V$  representing the associated barostat “momentum” and  $M_V$  the “mass”. Note that the units of  $M_V$  are mass  $\times$  length<sup>−4</sup>.  $\eta$  is the coordinate associated with the thermostat, and  $P_\eta$  and  $M_\eta$  are the momentum and mass (units mass  $\times$  length<sup>2</sup>), respectively, associated with the coordinate  $\eta$ .  $\xi$  is associated with the coupling between the thermostat and the barostat and has momentum  $P_\xi$  and mass  $M_\xi$  (units mass  $\times$  length<sup>2</sup>).

Our formulation is based on the following equations of motion

$$\begin{aligned}
 \dot{\vec{r}}_{\mu i} &= \frac{\vec{p}_{\mu i}}{m_{\mu i}} \\
 \dot{\vec{p}}_{\mu i} &= \vec{F}_{\mu i} + \vec{G}_{\mu i} - \frac{m_{\mu i}}{M_{\mu}} \vec{F}_{\mu} - \vec{p}_{\mu i} \frac{P_{\eta}}{M_{\eta}} \\
 \dot{\vec{R}}_{\mu} &= \frac{\vec{P}_{\mu}}{M_{\mu}} + \vec{R}_{\mu} \frac{P_V}{3VM_V} \\
 \dot{\vec{P}}_{\mu} &= \vec{F}_{\mu} - \vec{P}_{\mu} \cdot \left[ \frac{P_{\eta}}{M_{\eta}} + \frac{P_V}{3VM_V} \right] \\
 \dot{V} &= \frac{P_V}{M_V} \\
 dP_V &= (\Pi^* - \Pi_{\text{ext}}) dt - P_V \left[ \frac{P_{\xi}}{M_{\xi}} + \gamma \right] dt + \sigma M_V^{1/2} dW \\
 \dot{\eta} &= \frac{P_{\eta}}{M_{\eta}} \\
 dP_{\eta} &= gk_B [T^* - T_{\text{ext}}] dt - \gamma_{\eta} P_{\eta} dt + \sigma_{\eta} M_{\eta}^{1/2} dW_{\eta} \\
 \dot{\xi} &= \frac{P_{\xi}}{M_{\xi}} \\
 \dot{P}_{\xi} &= \frac{P_V^2}{M_V} - k_B T_{\text{ext}}
 \end{aligned} \tag{5}$$

where  $W = W(t)$  is a one-dimensional Wiener process,  $\gamma$  is the friction constant for the volume control variable with units of reciprocal time, and  $\sigma = \sqrt{2\gamma k_B T_{\text{ext}}}$ ; likewise,  $\gamma_{\eta}$  and  $\sigma_{\eta}$  are the friction and stochastic amplitude for the stochastic process, respectively, attached to the thermostat variable.

The equations of motion above are similar to those of Marry and Ciccotti<sup>5</sup> (see also the earlier paper of Hunenberger<sup>4</sup>); the main difference to be found is in the equations for the momentum of the piston and thermostat, which are treated here using a stochastic approach. In experiments, we find that the use of stochastic perturbation in the barostat significantly reduced the problem of “ringing”, as observed by Feller et al.<sup>27</sup> in relation to the Andersen barostat.

In our simulations, the stochastic modification of the thermostat did not yield additional benefits as compared to the stochastic perturbation of the pressure variable alone, so we simply took  $\gamma_{\eta} = 0$  in the experiments presented here. However, the incorporation of this term is useful because it ensures ergodicity;<sup>39</sup> its inclusion may be valuable in simulations of certain types of systems with stiff harmonic internal coupling.

For  $\gamma = \gamma_{\eta} = 0$ , the equations of Marry and Ciccotti are recovered. In this case, the equations of motion above preserve the following quantity that we will refer to as the extended energy in the sequel

$$\begin{aligned}
 H' &= H(\vec{P}, \vec{R}, \vec{p}, \vec{r}) + gk_B T_{\text{ext}} \eta + k_B T_{\text{ext}} \xi + \Pi_{\text{ext}} V \\
 &+ \frac{P_V^2}{2M_V} + \frac{P_{\eta}^2}{2M_{\eta}} + \frac{P_{\xi}^2}{2M_{\xi}}
 \end{aligned} \tag{6}$$

where  $H(\vec{P}, \vec{R}, \vec{p}, \vec{r})$  is the sum of the kinetic and potential energies of the physical system expressed in molecular coordinates. The extended energy is not relevant in the stochastic setting; it is however particularly useful during the coding process to provide evidence for the correctness of the implementation.

## DERIVATION OF THE PARTITION FUNCTION

In this section, we illustrate that the equations of motion we discussed above reproduce the probability density distribution of the isobaric–isothermal ensemble, which before normalization is given by

$$\rho = \exp \left( \frac{H(\vec{P}, \vec{R}, \vec{p}, \vec{r}) + \Pi_{\text{ext}} V}{k_B T_{\text{ext}}} \right) \tag{7}$$

The complete derivation of the partition function for the case of zero friction and in the presence of constraints may be found in Kalibaeva et al.<sup>6</sup> The partition function for the deterministic equations of motions is found to be

$$\Omega = \int d\vec{\Gamma} \tilde{\rho}(\vec{\Gamma}) \tag{8}$$

where  $\vec{\Gamma}$  represents the collection of all physical and artificial variables

$$\vec{\Gamma} = (\vec{r}, \vec{p}, \vec{R}, \vec{P}, V, P_V, \eta, P_{\eta}, \xi, P_{\xi}) \tag{9}$$

$\int d\vec{\Gamma}$  represents the usual integral with respect to all variables, and

$$\begin{aligned}
 \tilde{\rho}(\vec{\Gamma}) &= \exp \left( -\frac{1}{k_B T_{\text{ext}}} [H(\vec{P}, \vec{R}, \vec{p}, \vec{r}) + \Pi_{\text{ext}} V + P_V^2/2M_V \right. \\
 &\quad \left. + P_{\eta}^2/2M_{\eta} + P_{\xi}^2/2M_{\xi}] \right)
 \end{aligned} \tag{10}$$

This is seen to easily correspond to the desired NPT distribution following integration over the auxiliary variables  $P_V, \eta, P_{\eta}, \xi$ , and  $P_{\xi}$ .

To demonstrate that  $\tilde{\rho}$  is preserved under the evolution of the deterministic equations, one may write out eqs 5 for  $\gamma = \gamma_{\eta} = 0$  in the compact form

$$\frac{d\vec{\Gamma}}{dt} = \vec{v}(\vec{\Gamma}) \tag{11}$$

The continuity equation corresponding to the evolution of the probability density of this system takes the form

$$\frac{\partial \rho}{\partial t} = \mathcal{L}_{\text{det}}^{\dagger} \rho \tag{12}$$

where

$$\mathcal{L}_{\text{det}}^{\dagger} \rho = -\nabla \cdot (\vec{v} \rho) \tag{13}$$

The dagger indicates that this is the adjoint of the Lie derivative associated with the system defined by eq 5, which acts on a function  $\phi$  of the phase variables as

$$(\mathcal{L}_{\text{det}} \phi)(\vec{\Gamma}) = \vec{v} \cdot \nabla \phi \tag{14}$$



Using the eqs 5 (with  $\gamma = \gamma_\eta = 0$ ) and the definition of  $\tilde{\rho}$  given above, it can be shown that

$$\mathcal{L}_{\text{det}}^\dagger \tilde{\rho} = 0 \quad (15)$$

meaning that  $\tilde{\rho}$  is a steady state of the equations.

For completeness, and for later discussion in the setting of discretization, we write out the operator  $\mathcal{L}$  below. This can be obtained directly by substitution of  $\tilde{v}$  (the vector field on the right-hand side of eq 5, taking  $\gamma = \gamma_\eta = 0$ ) into eq 14, we have

$$\begin{aligned} \mathcal{L}_{\text{det}} = & \frac{\tilde{p}_{\mu i}}{m_{\mu i}} \nabla_{\tilde{r}_{\mu i}} \\ & + \left[ \tilde{F}_{\mu i} + \tilde{G}_{\mu i} - \frac{m_{\mu i}}{M_{\mu}} \tilde{F}_{\mu} - \tilde{p}_{\mu i} \frac{P_{\eta}}{M_{\eta}} \right] \nabla_{\tilde{p}_{\mu i}} \\ & + \left[ \frac{\tilde{p}_{\mu}}{M_{\mu}} + \tilde{R}_{\mu} \frac{P_V}{3VM_V} \right] \nabla_{\tilde{R}_{\mu}} \\ & + \left[ \tilde{F}_{\mu} - \tilde{p}_{\mu} \cdot \left[ \frac{P_{\eta}}{M_{\eta}} + \frac{P_V}{3VM_V} \right] \right] \nabla_{\tilde{p}_{\mu}} \\ & + \frac{P_V}{M_V} \frac{\partial}{\partial V} \\ & + \left[ (\Pi^* - \Pi_{\text{ext}}) - P_V \left[ \frac{P_{\xi}}{M_{\xi}} \right] \right] \frac{\partial}{\partial P_V} \\ & + \frac{P_{\eta}}{M_{\eta}} \frac{\partial}{\partial \eta} \\ & + g k_B [T^* - T_{\text{ext}}] \frac{\partial}{\partial P_{\eta}} \\ & + \frac{P_{\xi}}{M_{\xi}} \frac{\partial}{\partial \xi} \\ & + \left[ \frac{P_V^2}{M_V} - k_B T_{\text{ext}} \right] \frac{\partial}{\partial P_{\xi}} \end{aligned} \quad (16)$$

The above discussion pertains to the deterministic case, where no stochastic perturbation is incorporated. Unfortunately, it is not possible to prove that the deterministic system is ergodic for the desired distribution. Following the usual approach taken in physics literature, one typically assumes that, given sufficient internal complexity of the dynamical system, the ergodic property will hold in some practical sense, meaning simply that sufficiently long averages taken along dynamic paths will correspond to equilibrium averages.

When  $\gamma \neq 0$  or  $\gamma_\eta \neq 0$ , the additional stochastic terms in eq 5 lead to a Fokker–Planck equation for the evolution of the probability density, which may be written as

$$\frac{\partial \rho}{\partial t} = (\mathcal{L}_{\text{det}}^\dagger + \delta \mathcal{L}^\dagger) \rho \quad (17)$$

where  $\mathcal{L}_{\text{det}}$  is as described above, and

$$\begin{aligned} \delta \mathcal{L}^\dagger \rho = & \gamma \frac{\partial}{\partial P_V} (P_V \rho) + \gamma k_B T_{\text{ext}} M_V \frac{\partial^2 \rho}{\partial P_V^2} \\ & + \gamma_\eta \frac{\partial}{\partial P_\eta} (P_\eta \rho) + \gamma_\eta k_B T_{\text{ext}} M_\eta \frac{\partial^2 \rho}{\partial P_\eta^2} \end{aligned} \quad (18)$$

where  $\tilde{\rho}$  is stationary with respect to the  $\delta \mathcal{L}^\dagger$  operator as well and thus with respect to the combined operator. Moreover, because the system is now subject to stochastic perturbations, it is possible to prove that the system is ergodic,<sup>39</sup> at least for the

case  $\gamma_\eta \neq 0$  and for a harmonic underlying system. The proposed equations of motion therefore reproduce the NPT ensemble.

## THE FORCE FIELD

The atoms in the system are subject to a force field that reflects the atom–atom interactions both within the simulation cell and between atoms of different cells. The potential energy may be written as

$$U = U_{\text{cb}} + U_{\text{nb}} \quad (19)$$

where  $U_{\text{cb}}$  represents terms involving covalently bound atoms and  $U_{\text{nb}}$  represents nonbonded interactions. The covalent terms comprise bonds, angles, dihedrals, and improper dihedral potentials

$$\begin{aligned} U_b = \sum_{i \in \text{bonds}} \frac{k_i}{2} (d_i - d_{i,0})^2 \quad U_\theta = \sum_{i \in \text{angles}} \frac{k_i}{2} (\theta_i - \theta_{i,0})^2 \\ U_\phi = \sum_{i \in \text{torsions}} \sum_{n=1}^3 a_{i,n} \cos(n\phi_i - \phi_{i,0})^2 \quad U_l = \sum_{i \in \text{improper torsions}} \frac{k_i}{2} (\phi_i - \phi_{i,0})^2 \end{aligned} \quad (20)$$

The covalent terms above and the constraint forces do not contribute to the molecular pressure; therefore, from now on, only noncovalent terms are taken into account.

We define the set  $\mathcal{M}$  as the set of atom pairs  $(ij)$  that are separated by less than three bonds. Nonbonding, nonimaged interactions for pairs of the  $\mathcal{M}$  set are either not calculated (separated by one or two bonds) or, if separated by three bonds (1–4 interactions), calculated using special terms.

For the nonbonding term, we need to take into account the fact that we will use periodic boundary conditions. If  $\vec{\delta}$  is the vector that shifts each periodic copy of the system, then the nonbonding terms are of the form

$$U_{\text{nb}} = U_C + U_6 + U_{12} \quad (21)$$

where

$$U_C = \frac{1}{2} \sum_{\vec{\delta}}^* \sum_{i,j=1}^n k_{cl} \frac{q_i q_j}{d_{ij}}, \quad d_{ij} = |\vec{r}_j - \vec{r}_i + \vec{\delta}| \quad (22)$$

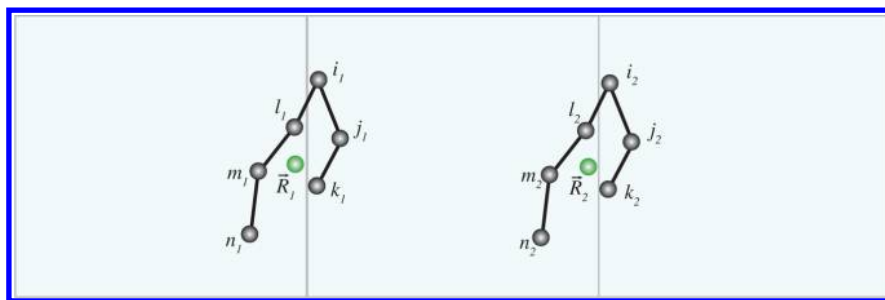
with  $q_i$  representing the charge on atom  $i$ , and the  $*$  appearing in the summation indicating that one should omit terms for which both  $\vec{\delta} = 0$  and  $(i, j) \in \mathcal{M}$ . Similarly

$$U_6 = -\frac{1}{2} \sum_{\vec{\delta}}^* \sum_{i,j=1}^n \frac{B_{ij}}{d_{ij}^6}, \quad U_{12} = \frac{1}{2} \sum_{\vec{\delta}}^* \sum_{i,j=1}^n \frac{A_{ij}}{d_{ij}^{12}} \quad (23)$$

These terms together describe the Lennard–Jones potential for modeling the van der Waals interaction.  $A_{ij}$  and  $B_{ij}$  are parameters associated with the repulsive and attractive interactions between atoms, respectively. We assume a product combination rule,  $A_{ij} = A_i A_j$ ,  $B_{ij} = B_i B_j$ , which is ideal for the implementation of Ewald summation. Other combination rules are possible, but in this case, the calculation of reciprocal summations are considerably more expensive.

In computing the fast decaying term  $U_{12}$ , we assume a distance-dependent cutoff, i.e., the interaction is taken to be zero for distances greater than some fixed value. Because of the rapid decay of this term, the error is negligible beyond say 10 Å.

The terms  $U_6$  and  $U_C$  are calculated without cutoff using the technique of Ewald summation, where we use the standard



**Figure 1.** When a molecule extends across the periodic boundary, atoms that belong to the same molecule interact through different periodic copies. When computing the molecular virial, atoms  $i_1, j_1, k_1$  are associated with the molecule centered in  $\vec{R}_1$ , whereas the atoms  $i_2, m_2, n_2$  are associated with a copy that is positioned at  $\vec{R}_2 = \vec{R}_1 + \vec{\delta}$ . Therefore, in implementing the molecular virial, it is necessary to allocate multiple molecular coordinates to a single molecule.

tin foil infinite boundary term. We define  $\vec{\eta}$  to be the reciprocal lattice vector; the structure factor is therefore

$$S(\vec{\eta}) = \sum_{j=1}^n q_j e^{i2\pi\vec{\eta} \cdot \vec{r}_j} \quad (24)$$

Up to an arbitrary constant  $\beta$ , the electrostatic potential may be written as the sum of four terms<sup>14</sup>

$$\begin{aligned} U_{C,\text{dir}} &= \frac{1}{2} \sum_{\vec{\delta}} \sum_{i,j=1}^n \frac{q_i q_j \operatorname{erfc}(\beta d_{ij})}{d_{ij}}, \quad d_{ij} = |\vec{r}_j - \vec{r}_i + \vec{\delta}| \\ U_{C,\text{rec}} &= \frac{1}{2\pi V} \sum_{\vec{\eta} \neq 0} \frac{\exp(-\pi^2 \eta^2 / \beta^2)}{\eta^2} S(\vec{\eta}) S(-\vec{\eta}) \\ U_{C,\text{corr}} &= -\frac{1}{2} \sum_{(i,j) \in \mathcal{M}} \frac{q_i q_j \operatorname{erf}(\beta |\vec{r}_j - \vec{r}_i|)}{|\vec{r}_j - \vec{r}_i|} \\ U_{C,\text{self}} &= -\frac{\beta}{\sqrt{\pi}} \sum_{i=1}^n q_i^2 \end{aligned} \quad (25)$$

In a similar way, the  $U_6$  potential may be decomposed as the sum of the following four terms<sup>15</sup>

$$\begin{aligned} U_{6,\text{dir}} &= \frac{1}{2} \sum_{\vec{\delta}} \sum_{i,j=1}^n B_i B_j \frac{1}{d_{ij}^6} \exp(-\beta^2 d_{ij}^2) \left( 1 + \beta^2 d_{ij}^2 + \frac{1}{2} \beta^4 d_{ij}^4 \right) \\ U_{6,\text{rec}} &= \frac{\pi^{9/2}}{3V} \sum_{\vec{\eta} \neq 0} |\vec{\eta}|^3 \left[ \frac{1}{2(\pi |\vec{\eta}| / \beta)^3} (1 - 2(\pi |\vec{\eta}| / \beta)^2) \right. \\ &\quad \times \exp(-(\pi |\vec{\eta}| / \beta)^2) + \sqrt{\pi} \operatorname{erfc}(\pi |\vec{\eta}| / \beta) \left. \right] \hat{S}(\vec{\eta}) \hat{S}(-\vec{\eta}) \\ U_{6,\text{corr}} &= -\frac{1}{2} \sum_{(i,j) \in \mathcal{M}} B_i B_j \frac{1}{|\vec{r}_j - \vec{r}_i|^6} \exp(-\beta^2 |\vec{r}_j - \vec{r}_i|^2) \\ &\quad \times \left( 1 + \beta^2 |\vec{r}_j - \vec{r}_i|^2 + \frac{1}{2} \beta^4 |\vec{r}_j - \vec{r}_i|^4 \right) \\ U_{6,\text{self}} &= -\frac{\beta^6}{12} \sum_{i=1}^n B_i^2 + \frac{\beta^3 \pi^{3/2}}{6V} \left( \sum_{i=1}^n B_i \right)^2 \end{aligned} \quad (26)$$

where the structure factor here is

$$\hat{S}(\vec{\eta}) = \sum_{j=1}^n B_j e^{i2\pi\vec{\eta} \cdot \vec{r}_j} \quad (27)$$

For the calculation of the reciprocal part of both  $U_6$  and  $U_C$ , the algorithm used is Particle Mesh Ewald (PME).<sup>12</sup>

## MOLECULAR PRESSURE

The atomic pressure is related to the trace of the internal stress tensor

$$P = \frac{1}{3} \operatorname{Tr}(\Pi) \quad (28)$$

where the stress tensor for a system of atoms in periodic boundary conditions is<sup>26,40,41</sup>

$$\Pi = \frac{1}{V} \left\langle \sum_i m_i \dot{\vec{r}}_i \otimes \dot{\vec{r}}_i \right\rangle + \frac{1}{2V} \left\langle \sum_{\vec{\delta}} \sum_i \sum_j \vec{f}_{ij}^{\vec{\delta}} \otimes (\vec{r}_i - \vec{r}_j + \vec{\delta}) \right\rangle \quad (29)$$

where  $\vec{f}_{ij}^{\vec{\delta}}$  indicates the force that copy  $\vec{\delta}$  of atom  $j$  exercises on atom  $i$ . The symbol  $\otimes$  indicates the tensor product. From this, we recover the well-known expression for the pressure

$$P = \frac{1}{3V} \left\langle \sum_i m_i |\dot{\vec{r}}_i|^2 \right\rangle + \frac{1}{3V} \left\langle \frac{1}{2} \sum_{\vec{\delta}} \sum_i \sum_j \vec{f}_{ij}^{\vec{\delta}} \cdot (\vec{r}_i - \vec{r}_j + \vec{\delta}) \right\rangle \quad (30)$$

The averaged quantity of the second term in the above expression is the atomic virial  $W_{\text{atm}}$ . In a similar way, the molecular pressure of a system with periodic boundary conditions can be written as<sup>5,26,32</sup>

$$\begin{aligned} P_{\text{mol}} &= \frac{1}{3V} \left\langle \sum_{\alpha} M_{\alpha} \dot{\vec{R}}_{\alpha}^2 \right\rangle \\ &\quad + \frac{1}{3V} \left\langle \frac{1}{2} \sum_{\alpha} \sum_{\beta} \sum_{\vec{\delta}} \sum_{i \in \alpha} \sum_{j \in \beta} \vec{f}_{ij}^{\vec{\delta}} \cdot (\vec{R}_{\alpha} - \vec{R}_{\beta} + \vec{\delta}) \right\rangle \end{aligned} \quad (31)$$

The averaged quantity in the second term of the above expression is the molecular virial  $W_{\text{mol}}$ . On average, the molecular pressure and the atomic pressure are equal as proven by Ciccotti and Ryckaert<sup>42</sup> for closed systems and by Akkermans and Ciccotti<sup>32</sup> for open systems with periodic boundary conditions.

The positions of atoms are identified by their molecular coordinates plus their relative coordinates; therefore, the molecular and atomic virials are related as follows

$$\begin{aligned}
W_{\text{mol}} &= \frac{1}{2} \sum_{\alpha} \sum_{\beta} \sum_{\vec{\delta}} \sum_{i \in \alpha} \sum_{j \in \beta} \vec{f}_{ij}^{\vec{\delta}} \cdot (\vec{R}_{\alpha} - \vec{R}_{\beta} + \vec{\delta}) \\
&= \frac{1}{2} \sum_{\alpha} \sum_{\beta} \sum_{\vec{\delta}} \sum_{i \in \alpha} \sum_{j \in \beta} \vec{f}_{ij}^{\vec{\delta}} \cdot (\vec{r}_i - \vec{r}_{ai} - \vec{r}_j + \vec{r}_{bj} + \vec{\delta}) \\
&= W_{\text{atm}} - \sum_{\alpha} \sum_{i \in \alpha} \vec{r}_{ai} \cdot \sum_{\beta} \sum_{\vec{\delta}} \sum_{j \in \beta} \vec{f}_{ij}^{\vec{\delta}} \\
&= W_{\text{atm}} - \sum_{\alpha} \sum_{i \in \alpha} \vec{r}_{ai} \cdot \vec{F}_i,
\end{aligned} \tag{32}$$

where we have used  $\vec{f}_{ij}^{\vec{\delta}} = -\vec{f}_{ji}^{\vec{\delta}}$ , and where  $\vec{F}_i$  is the total force applied to atom  $i$ . We will use this relation to calculate the molecular virial  $W_{\text{mol}}$  by computing the atomic virial and postprocessing it by subtracting the correction  $\sum_{\alpha} \sum_{i \in \alpha} \vec{r}_{ai} \cdot \vec{F}_i$  as shown above.

This approach results in a cleaner implementation. First, the molecular positions do not need to be communicated to the routines that perform the force calculation. Second, and more importantly, it solves a problem that arises when a molecule extends across the boundary of the simulation box (see Figure 1). In this case, atoms belonging to the same molecule actually interact through two different periodic copies, so in the implementation, we would have two different molecular coordinates associated with the same molecule. The implementation of the atomic virial does not have the same problem.

It is clear from the definition that the molecular virial of intramolecular forces is zero; therefore, from now on we will deal exclusively with the intermolecular potentials, i.e., we will not calculate the virial of bonds, angles, torsions, improper torsions, 1–3 or 1–4 interactions, or constraints. This is a major advantage of using the molecular pressure.

The expression we have derived so far for the atomic virial is not suitable to be utilized in conjunction with Ewald summation because the individual atomic forces are lost. Following previous work in the literature,<sup>14,26,40</sup> let us redefine the positions as

$$\vec{r}_i + \vec{\delta} = \mathbf{h}(\vec{s}_i + \vec{d}_i) \tag{33}$$

where  $\mathbf{h}$  is the  $3 \times 3$  matrix defined by

$$\mathbf{h} = [\vec{h}_1 | \vec{h}_2 | \vec{h}_3] \tag{34}$$

where the three vectors are the edges of the unit cell of the periodic box, the components of the vector  $\vec{s}$  lie in  $[0,1]$ , and the vector  $\vec{d}$  has integer components (representing the translation of the cell in each direction). If the simulation box is a cuboid, then  $\mathbf{h}$  is given by

$$\mathbf{h} = \begin{bmatrix} L_x & 0 & 0 \\ 0 & L_y & 0 \\ 0 & 0 & L_z \end{bmatrix} \tag{35}$$

We can now derive an alternative expression for the atomic virial in the case of a uniform deformation. In a uniform deformation, we keep  $\vec{s}$  constant and we change the size of the box by stretching or compressing the edges of the box  $L_{\gamma}$ . Thus

$$\begin{aligned}
\vec{r}_i - \vec{r}_j + \vec{\delta} &= (L_x(s_{i,x} - s_{j,x} + d_x), L_y(s_{i,y} - s_{j,y} + d_y), \\
&\quad L_z(s_{i,z} - s_{j,z} + d_z))
\end{aligned} \tag{36}$$

For a generic pair potential  $U = \frac{1}{2} \sum_{ij} U_{ij}$ , it is straightforward to show that the atomic virial can be expressed in terms of the deformation variables by<sup>40,41</sup>

$$\begin{aligned}
W_{\text{atm}} &= \left\langle \frac{1}{2} \sum_{\vec{\delta}} \sum_i \sum_j \vec{f}_{ij}^{\vec{\delta}} \cdot (\vec{r}_i - \vec{r}_j + \vec{\delta}) \right\rangle \\
&= - \left\langle \frac{1}{2} \sum_{\vec{\delta}} \sum_i \sum_j \nabla U_{ij}(\vec{r}_i - \vec{r}_j + \vec{\delta}) \cdot (\vec{r}_i - \vec{r}_j + \vec{\delta}) \right\rangle \\
&= - \left\langle \sum_{\sigma \in x,y,z} L_{\sigma} \frac{\partial U}{\partial L_{\sigma}} \right\rangle
\end{aligned} \tag{37}$$

Now, we can calculate the molecular pressure (in terms of the molecular forces) as

$$P_{\text{mol}} = \frac{1}{3V} \left[ \left\langle \sum_{\alpha} M_{\alpha} \vec{R}_{\alpha}^2 \right\rangle - \left\langle \sum_{\sigma \in x,y,z} L_{\sigma} \frac{\partial U_{\text{int}}}{\partial L_{\sigma}} \right\rangle - \left\langle \sum_{\alpha} \sum_{i \in \alpha} \vec{r}_{ai} \cdot \vec{F}_i^{\text{int}} \right\rangle \right] \tag{38}$$

We next give the corresponding terms of the virial in the context of Ewald summation. The atomic virial of the electrostatic potential is given in terms of the Ewald components (direct, reciprocal, and self) as<sup>14</sup>

$$W_{\text{C,atm}}^{\text{dir}} = \frac{1}{2} \sum_{\vec{\delta}}^* \sum_{i,j=1}^n q_i q_j \left[ \frac{\text{erfc}(\beta d_{ij})}{d_{ij}} + \frac{2\beta \exp(-\beta^2 d_{ij}^2)}{\sqrt{\pi}} \right] \tag{39}$$

$$W_{\text{C,atm}}^{\text{rec}} = \frac{1}{2\pi V} \sum_{\vec{\eta} \neq 0} \frac{\exp(-\pi^2 \eta^2 / \beta^2)}{\eta^2} \left[ 1 - \frac{2\pi^2 \eta^2}{\beta^2} \right] S(\vec{\eta}) S(-\vec{\eta}) \tag{40}$$

$$W_{\text{elec,atm}}^{\text{self}} = 0 \tag{41}$$

We omit the virial of the correction term because this potential does not contribute to the molecular pressure being intramolecular in nature.

With regard to the Lennard-Jones attractive component, the atomic virial has a similar decomposition

$$\begin{aligned}
W_{6,\text{atm}}^{\text{dir}} &= \frac{1}{2} \sum_{\vec{\delta}}^* \sum_{i,j=1}^n B_i B_j \frac{\exp(-\beta^2 d_{ij}^2)}{d^6} \left[ (6 + 2\beta^2 d_{ij}^2) \right. \\
&\quad \times \left( 1 + \beta^2 d_{ij}^2 + \frac{1}{2} \beta^4 d_{ij}^4 \right) - 2\beta^2 d_{ij}^2 (1 + \beta^2 d_{ij}^2) \left. \right]
\end{aligned} \tag{42}$$

$$\begin{aligned}
W_{6,\text{atm}}^{\text{rec}} &= \frac{\pi^{9/2}}{3V} \sum_{\vec{\eta} \neq 0} 4|\vec{\eta}|^3 \left[ \frac{\exp(-\pi^2 |\vec{\eta}|^2 / \beta^2)}{2(\pi |\vec{\eta}| / \beta)^3} \right. \\
&\quad \times (1 - 2(\pi |\vec{\eta}| / \beta)^2) + \sqrt{\pi} \text{erfc}(\pi |\vec{\eta}| / \beta) \left. \right] \hat{S}(\vec{\eta}) \hat{S}(-\vec{\eta}) \\
&\quad - \frac{\pi^{7/2}}{3V} \sum_{\vec{\eta} \neq 0} |\vec{\eta}|^4 \frac{3 \exp(-\pi^2 |\vec{\eta}|^2 / \beta^2)}{2(\pi |\vec{\eta}| / \beta)^4} \hat{S}(\vec{\eta}) \hat{S}(-\vec{\eta})
\end{aligned} \tag{43}$$

$$W_{6,\text{atm}}^{\text{self}} = \left( \sum_{i=1}^n B_i \right)^2 \frac{\beta^3 \pi^{3/2}}{6V} \tag{44}$$

As before, we do not calculate the virial of the correction term because, being an intramolecular term, it does not contribute to the molecular virial.

When LJ interactions are calculated using a distance cutoff, a truncation error is introduced; calculating the pressure by the use of the virial of the Ewald summation avoids any truncation error. Using a cutoff to truncate the LJ interaction is a common solution in MD; the error introduced in the evaluation of the forces is indeed negligible. Unfortunately, the bias introduced in the calculation of the pressure is significant; the neglected interactions are all attractive due to the long negative tail of the LJ potential. The resulting error in the value of the measured pressure is quite large at the typical cutoff distances of 10–12 Å. For a homogeneous isotropic liquid of density, it is possible to compute the pressure truncation error as

$$\Delta P_{\text{cut}} = -\frac{2\pi\rho^2}{3} \int_{r_{\text{cut}}}^{\infty} r^3 g(r) \frac{\partial U}{\partial r} dr \quad (45)$$

For example, for TIP3P water, the truncation error is ~200 atm at 10 Å and is still ~60 atm at 15 Å. The correction term is much more difficult to calculate for inhomogeneous and/or anisotropic liquids like mixtures of solvents or solutions, solvated proteins, and membranes. For addressing this issue, some heuristic methods have been proposed. Lague et al.<sup>38</sup> have proposed a method in which the truncation correction is calculated using a very long Lennard-Jones cutoff (every  $k$  steps); this approximation is valid under the assumption that the error is a quantity that varies adiabatically (i.e., slowly) in time.

## ■ DISCRETIZATION OF THE EQUATIONS OF MOTION

The phase space probability density  $\rho(t)$  evolves in a step of size  $\Delta t$  according to

$$\rho(\vec{\Gamma}, t + \Delta t) = e^{\Delta t \mathcal{L}} \rho(\vec{\Gamma}, t) \quad (46)$$

Functions  $\phi$  of the phase variables evolve under the adjoint of this operator, i.e., if  $\vec{\Gamma}(t + \Delta t; \vec{\Gamma}, t)$  represents the solution at time  $t + \Delta t$ , given that  $\vec{\Gamma}(t) = \vec{\Gamma}$ , then for any scalar valued function  $\phi$  of the phase variables, we have

$$\phi(\vec{\Gamma}(t + \Delta t; \vec{\Gamma}, t)) = (e^{\Delta t \mathcal{L}} \phi)(\vec{\Gamma}) \quad (47)$$

The operator  $e^{t\mathcal{L}}$  is referred to as the evolution operator.  $\mathcal{L}$  can be decomposed as

$$\mathcal{L}_{\text{det}} + \delta\mathcal{L} \quad (48)$$

where  $\mathcal{L}_{\text{det}}$  is the Lie-derivative of the deterministic part of the system, which is given in eq 16, and  $\delta\mathcal{L}$  is the Fokker–Planck operator corresponding to the linear stochastic differential equations (SDEs) combining dissipation and random forcing (see eq 18).

The natural method for integrating the equations, which is inspired by prior work in symplectic integrators for Hamiltonian systems, is to split the deterministic part into pieces that are directly and exactly integrable and to additionally treat the stochastic Ornstein–Uhlenbeck terms by exact distributional integration; the flows of each of the pieces are then composed to define the numerical method.<sup>7–11</sup>

A variety of splitting methods are possible. On the basis of previous experience, we employ a decomposition of  $\mathcal{L}$  into simple terms as

$$\mathcal{L} = \mathcal{L}_1 + \mathcal{L}_2 + \dots, \mathcal{L}_{14} + \delta\mathcal{L}_1 + \delta\mathcal{L}_2 \quad (49)$$

where the various components are as follows

$$\begin{aligned} \mathcal{L}_1 &= -\frac{P_V P_\xi}{M_\xi} \frac{\partial}{\partial P_V} & \mathcal{L}_2 &= (\Pi - \Pi_{\text{ext}}) \frac{\partial}{\partial P_V} \\ \mathcal{L}_3 &= \frac{P_V}{M_V} \frac{\partial}{\partial V} & \mathcal{L}_4 &= \frac{P_\eta}{M_\eta} \frac{\partial}{\partial \eta} \\ \mathcal{L}_5 &= \frac{P_\xi}{M_\xi} \frac{\partial}{\partial \xi} & \mathcal{L}_6 &= \left( \frac{P_V^2}{M_V} - k_B T_{\text{ext}} \right) \frac{\partial}{\partial P_\xi} \\ \mathcal{L}_7 &= -\frac{P_\eta}{M_\eta} p_{\mu i} \nabla_{p_{\mu i}} & \mathcal{L}_8 &= \left[ F_{\mu i} + G_{\mu i} - \frac{m_{\mu i}}{M_\mu} F_\mu \right] \nabla_{p_{\mu i}} \\ \mathcal{L}_9 &= -\left[ \frac{P_\eta}{M_\eta} + \frac{P_V}{3VM_V} \right] p_\mu \nabla_{p_\mu} & \mathcal{L}_{10} &= F_\mu \nabla_{p_\mu} \\ \mathcal{L}_{11} &= g k_B [T - T_{\text{ext}}] \frac{\partial}{\partial P_\eta} & \mathcal{L}_{12} &= \frac{P_V}{3VM_V} R_\mu \nabla_{R_\mu} \\ \mathcal{L}_{13} &= \frac{P_\mu}{M_\mu} \nabla_{R_\mu} & \mathcal{L}_{14} &= \frac{P_{\mu i}}{m_{\mu i}} \nabla_{p_{\mu i}} \\ \delta\mathcal{L}_1^\dagger &= \gamma \left( 1 + P_V \frac{\partial}{\partial P_V} + k_B T_{\text{ext}} M_V \frac{\partial^2}{\partial P_V^2} \right) \\ \delta\mathcal{L}_2^\dagger &= \gamma_\eta \left( 1 + P_\eta \frac{\partial}{\partial P_\eta} + k_B T_{\text{ext}} M_\eta \frac{\partial^2}{\partial P_\eta^2} \right) \end{aligned} \quad (50)$$

The operators  $\mathcal{L}_1, \dots, \mathcal{L}_6, \mathcal{L}_{11}$ , and  $\delta\mathcal{L}_1, \delta\mathcal{L}_2$  are responsible for updating the extended variables, whereas the remaining operators drive the evolution of atomic and molecular positions and momenta.

Operators  $\mathcal{L}_1, \mathcal{L}_7, \mathcal{L}_9$  and  $\mathcal{L}_{12}$  give rise to multiplication by an exponential factor

$$e^{C x \partial / \partial x} f(x) = f(e^C x) \quad (51)$$

whereas the other deterministic operators result in translations

$$e^{C \partial / \partial x} f(x) = f(x + C) \quad (52)$$

The stochastic terms are evolved using an exact weak (distributionally correct) solution of  $\exp(t\delta\mathcal{L})$ , which is easily written down. For example, for the SDE  $dX = -\gamma X dt + \sqrt{2k_B T \gamma} dW$ , an exact weak solution is

$$X(t) = e^{-\gamma t} X(0) + \sqrt{k_B T (1 - \exp(-2\gamma t))} R(t) \quad (53)$$

where  $R(t)$  is a standard Gaussian random variable with mean zero and unit variance.

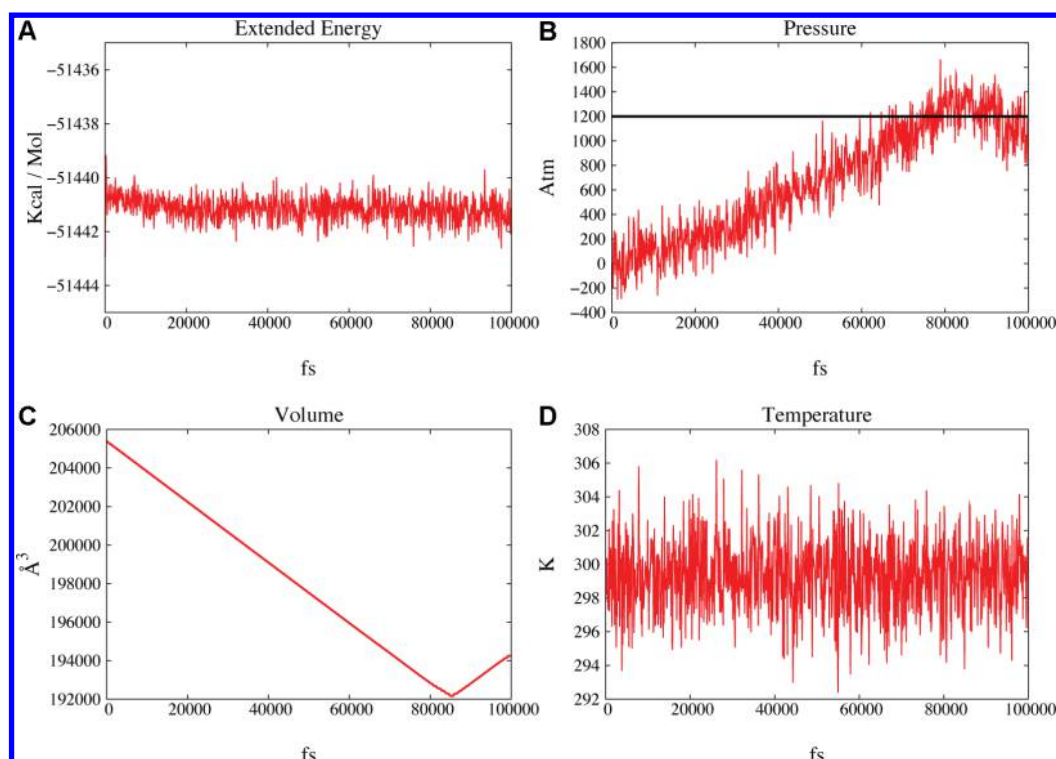
Rescaling the simulation box is an expensive task because the nonbonded interaction lists must be recomputed; thus, there is an advantage to delaying this task for several timesteps. This leads us to the use of a symmetric multiple timestepping procedure in which a longer time step is used between changes to the box size parameter  $V$  than is used for updating the other variables. Specifically, we employ a symmetric Trotter factorization based on performing  $\nu$  basic timesteps between changes of the box size of the following form

$$e^{\Delta t(\mathcal{A}+\mathcal{B})} \approx e^{\Delta t \mathcal{A}/2} (e^{\Delta t \mathcal{B}/\nu})^\nu e^{\Delta t \mathcal{A}/2} \quad (54)$$

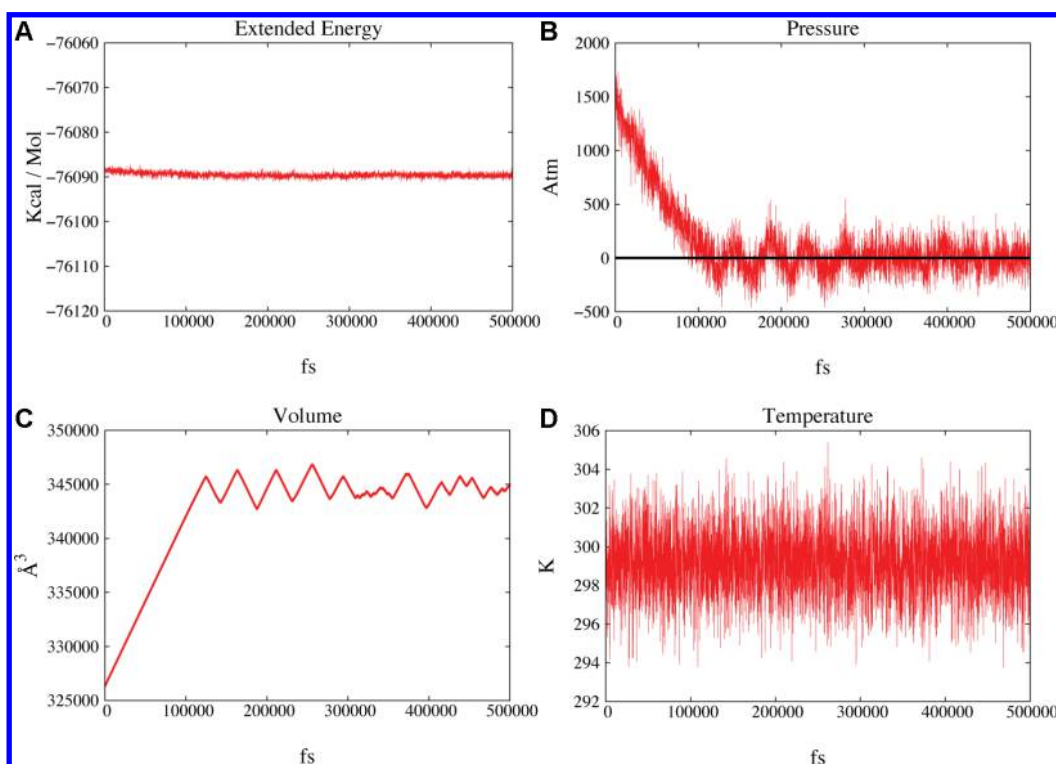
In our case

$$\mathcal{A} = \mathcal{L}_1 + \mathcal{L}_2 + \mathcal{L}_3 + \delta\mathcal{L}_1 + \delta\mathcal{L}_2, \quad \mathcal{B} = \mathcal{L} - \mathcal{A} \quad (55)$$





**Figure 2.** The peptide system is compressed to a target pressure of 1200 atm (see main text for details). In (A), the extended energy is shown as a function of time. In (B), the pressure is shown in red, and the black horizontal line marks the target pressure of 1200 atm. (C) and (D) show the volume and temperature as functions of time.



**Figure 3.** The membrane system is expanded to a target pressure of 1 atm (see main text for details). In (A), the extended energy is shown as a function of time. In (B), the pressure is shown in red, and the black horizontal line marks the target pressure. (C) and (D) show the volume and temperature as functions of time. After the initial expansion, periodic ringing is evident in both (B) and (C).

Each factor is approximated by a further decomposition into the enumerated components in such a way that the resulting discrete approximation is symmetric.

The constraint forces are treated using the SHAKE<sup>28</sup> and RATTLE<sup>44</sup> algorithms with the resulting explicit integrator reported in the [Appendix](#).

## NUMERICAL EXAMPLES

We use three systems to test the algorithm described above.

We first test the deterministic algorithm, i.e., we set  $\gamma = \gamma_\eta = 0$ , to verify the correctness of the implementation. We then compare the behavior of the stochastic algorithm for two different friction values with the behavior of the deterministic algorithm. In the simulation, the short time step was set to 1 fs, and the long time step (the one associated with the pressure control) was 8 fs.

The first system is the peptide LKKLGKKLLKKLLKKGL-KKL solvated in 6588 TIP3P<sup>45</sup> water molecules also containing 12 sodium ions and 22 chloride ions; the system has no net charge. The peptide was simulated with periodic boundary conditions in a cube with an edge of 59 Å. The Particle Mesh Ewald algorithm was used for both electrostatic and dispersive interactions. Short-range interactions were calculated to a distance of 9.8 Å; long-range interactions were calculated using a grid of  $64 \times 64 \times 64$  points.

We used the following coupling constants

$$M_V = 0.01 \frac{\text{g}\text{\AA}^{-4}}{\text{mol}}, \quad M_\eta = 500 \frac{\text{g}\text{\AA}^2}{\text{mol}}, \quad M_\epsilon = 10 \frac{\text{g}\text{\AA}^2}{\text{mol}}$$

The force field utilized for the peptide and the ions was OPLS<sup>46</sup> (all of the force field parameters utilized in this manuscript are available for download together with the molecular dynamics package MOIL at <http://clsb.ices.utexas.edu/web/moil.html>). The peptide was compressed from standard conditions to 1200 atm at a constant temperature of 300 K. The total simulation time was 100 ps. The system was compressed from a volume of  $\sim 206000 \text{ \AA}^3$  to a volume of  $\sim 192000 \text{ \AA}^3$ . The results of this test are shown in Figure 2. The compression phase lasted  $\sim 80$  ps. There is no significant drift of the conserved extended energy or the temperature; the fluctuations are  $\sim 1$  kcal/mol.

The second system used was a membrane composed of 128 DOPC molecules surrounded by 6097 TIP3P water molecules. The force field used for the DOPC molecules was the united-atom Berger force field<sup>47</sup> for the acyl chain atoms and OPLS<sup>46</sup> for the head groups; this setup was the same as that used in ref 48.

In this case, the size of the periodic box was initially set to  $66.026 \text{ \AA} \times 66.026 \text{ \AA} \times 74.854 \text{ \AA}$ . Ewald summation was used as before but with a grid of  $64 \times 64 \times 76$ . The membrane was expanded from  $\sim 1500$  atm to the standard conditions of 1 atm at constant temperature of 300 K. The total time of the simulation was 500 ps. The relaxation to standard conditions resulted in an expansion from a volume of  $\sim 323000 \text{ \AA}^3$  to a volume of  $\sim 345000 \text{ \AA}^3$ . The results of this test are shown in Figure 3.

The time trace of the extended energy (eq 6) shows an initial relaxation resulting in a decrease of a conserved quantity of  $\sim 1\text{--}2$  kcal/mol; after relaxation, there is no measurable energy drift. The temperature shows no drift. During the initial 120 ps, the system undergoes the main expansion; then, the membrane evolves at an approximately constant volume with fluctuations of  $\sim 1000 \text{ \AA}^3$ , i.e.,  $\sim 0.03\%$ . Typical oscillations of the volume are present with a period of  $\sim 30$  ps; this is the phenomenon of ringing.

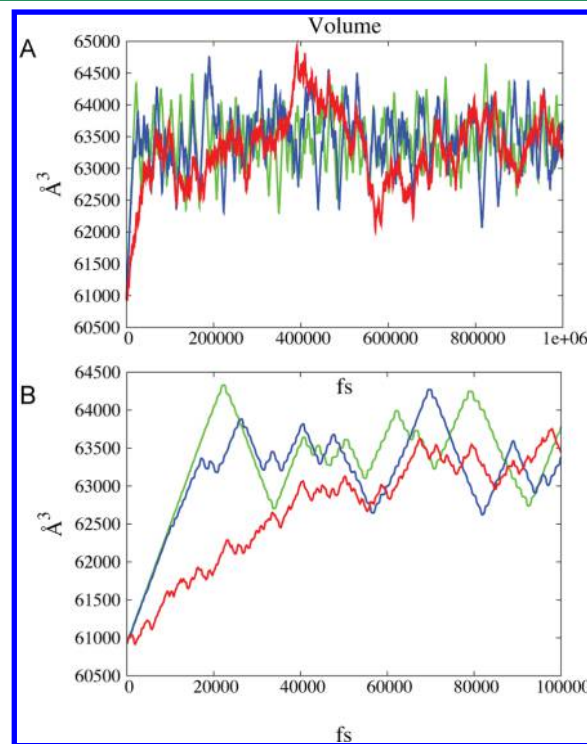
The last system we consider consists of 2033 TIP3P<sup>45</sup> water molecules. For this system, we analyze the behaviors of both the deterministic and the stochastic algorithms. The system was equilibrated to a target pressure of 1 atm from the initial condition of  $\sim 1000$  atm. The initial box size was set to  $39.35 \text{ \AA}$

$\times 39.35 \text{ \AA} \times 39.35 \text{ \AA}$ . Short-range electrostatic and dispersive interactions were calculated to a cutoff distance of 9.5 Å, whereas the remaining interactions were calculated in Fourier space using a grid of  $64 \times 64 \times 64$ . The following coupling constants were used

$$M_V = 1 \frac{\text{g}\text{\AA}^{-4}}{\text{mol}}, \quad M_\eta = 500 \frac{\text{g}\text{\AA}^2}{\text{mol}}, \quad M_\epsilon = 10 \frac{\text{g}\text{\AA}^2}{\text{mol}}$$

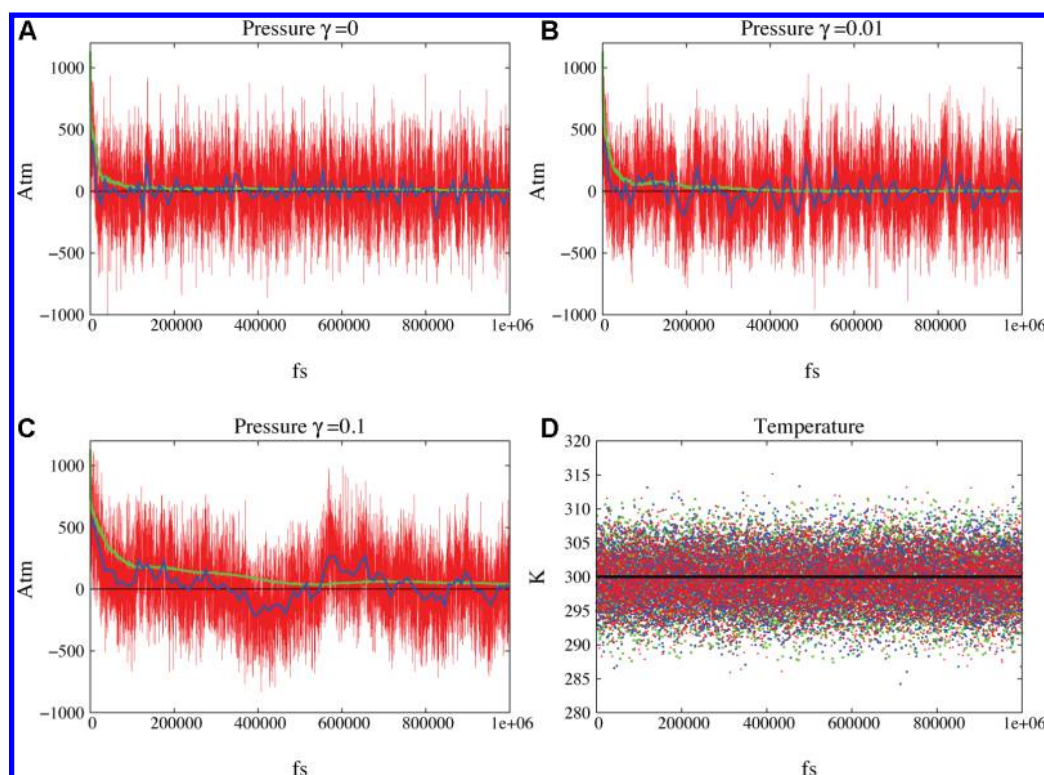
The system was simulated using three different values for the volume friction coefficient  $\gamma = 0/\text{ps}$ ,  $\gamma = 0.01/\text{ps}$ , and  $\gamma = 0.1/\text{ps}$ . The total simulation time was 1 ns for each setup.

The resulting evolution in time for the variable volume is shown in Figure 4. The expansion phase of the system lasts

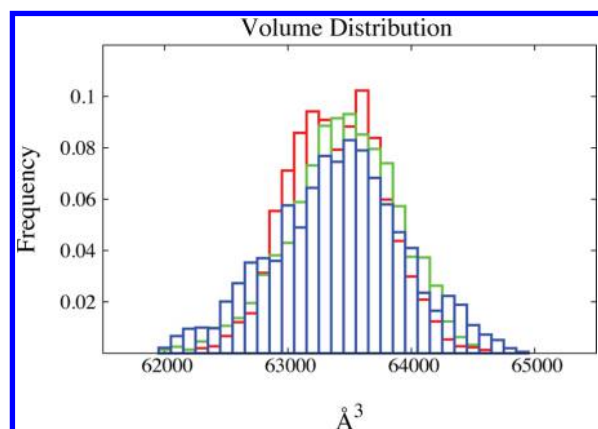


**Figure 4.** Volume as a function of time in constant pressure simulations. The results of the deterministic simulation are shown in green, and the simulations with friction  $\gamma$  equal to 0.01 and 0.1 are shown in blue and red, respectively. In (A), we plot a nanosecond simulation, and in (B), only the first 100 ps are shown. The ringing phenomenon is clearly present in the deterministic simulation and is reduced in the stochastic algorithm depending on the size of the friction coefficient. The relaxation time to the preset pressure also depends on the value of the friction coefficient.

20–70 ps depending on the value of the friction; the higher the friction, the slower the relaxation to equilibrium. Associated with higher friction, one also introduces a proportionately larger noise term; the effects of the noise are especially evident with the highest friction. After the initial expansion, we observe volume fluctuations near an average determined by the preset pressure. Periodic ringing is clearly present in the deterministic algorithm and is reduced with moderate friction and practically eliminated with the highest friction value. As shown in Figure 6, all of the runs exhibit the same probability distribution for the variable volume, as expected. The measured density of TIP3P water at the average volume is  $0.984 \text{ g/cm}^3$ . This value is consistent with what was previously found by Price et al.<sup>43</sup> when the TIP3P model is used in combination with PME. The



**Figure 5.** Simulation of a water box under constant pressure conditions. Pressure and temperature are shown for 3 values of the friction constant at 0, 0.01, and 0.1. (A), (B), and (C) show the instantaneous values of the pressure in red. The blue line indicates the value of the pressure averaged over 10 ps windows, and the green line indicates the running average. The black horizontal line is the target pressure. Convergence to the target pressure is evident in all of the runs. (D) shows the temperature as a function of time for the three simulations: green corresponding to friction coefficient  $\gamma$  equal to 0, and blue and red to 0.01 and 0.1, respectively. Once again, the horizontal black line indicates the target temperature.



**Figure 6.** Volume distribution for the water box (see text for details). Histograms are reported for the three different simulations: green bins are the results of the deterministic simulations, and blue and red are the results of simulations with friction coefficients of 0.01 and 0.1, respectively. The three simulations with different levels of stochasticity converge to the same average volume and share similar distributions for the volume variable.

time traces for pressure and temperature are reported in Figure 5.

## CONCLUSIONS

We developed a new algorithm that reproduces the isobaric–isothermal sampling. The algorithm integrates several previous ideas into a single, efficient, and accurate algorithm.

The inclusion of a stochastic forcing term avoids nonergodic behavior. By tuning the friction value, it is also possible to adjust the rate of decay to equilibrium, at least as measured by the decay of autocorrelation of the piston variable. Although we considered the use of stochastic noise in both thermostat and barostat variables, in our simulations, the ringing behavior was well-controlled by just the single stochastic process coupled to the piston. For this reason, and in light of works such as refs 22 and 23, it is reasonable to expect that our algorithm will inherit the good characteristics of the deterministic algorithms in reproducing kinetic and transport properties; even though we have not specifically investigated those properties here. Retaining the option for a deterministic algorithm (obtained by setting  $\gamma = 0$ ) provides a valuable tool for debugging in the form of the conserved effective energy.

As already observed by Feller et al.,<sup>27</sup> the inclusion of a stochastic term also eliminates the periodic oscillations in both pressure and volume. By using the molecular definition of pressure, we have reduced the number of operations necessary to calculate the pressure itself because intramolecular interactions can be neglected. In particular, no special treatment for holonomic constraints is required. We have also shown how the molecular pressure can be calculated by using the atomic virial of intermolecular interactions only. Finally, we calculated all of the long-range interactions and their stress tensors with Ewald sum. In this way, we have avoided any truncation error in calculating the pressure, and thus, we have also avoided the necessity to introduce any correction scheme. The resulting algorithm is implemented in the software package MOIL, and it has been tested on several complex systems.

## APPENDIX

In this section, we report the explicit algorithm as it is implemented in MOIL. For the definition of symbols, please

refer to the main text; we only remind that here  $\Delta t$  is the short time step and  $\nu$  is the ratio between long and short time steps. The implemented algorithm is

$$\begin{array}{ll}
 1 & e^{\mathcal{L}_1 \nu \Delta t / 2} \quad P_V \leftarrow P_V \exp\left(-\frac{P_\zeta \nu \Delta t}{M_\zeta 2}\right) \\
 2 & \Pi^* \leftarrow \frac{1}{3V} \sum_\mu M_\mu \dot{\vec{R}}_\mu^2 + \frac{1}{6V} \sum_\mu \sum_{\mu'} \sum_{i \in \mu} \sum_{j \in \mu'} (\vec{R}_\mu - \vec{R}_{\mu'}) \cdot (\vec{f}_{\mu i} - \vec{f}_{\mu' j}) \\
 3 & e^{\mathcal{L}_2 \nu \Delta t / 2} \quad P_V \leftarrow P_V + (\Pi^* - \Pi_{\text{ext}}) \frac{\nu \Delta t}{2} \\
 4 & e^{\delta \mathcal{L}_1 \nu \Delta t / 2} \quad P_V \leftarrow e^{-\gamma \nu \Delta t / 2} P_V + \frac{\sigma M_V^{1/2}}{\sqrt{2\gamma}} \sqrt{1 - e^{-\gamma \nu \Delta t}} R(t) \\
 5 & e^{\mathcal{L}_3 \nu \Delta t / 2} \quad V \leftarrow V + \frac{P_V \nu \Delta t}{M_V 2} \\
 \text{Repeat } \nu \text{ times steps 6 to 29} & \\
 6 & e^{\mathcal{L}_4 \Delta t / 2} \quad \eta \leftarrow \eta + \frac{P_\eta \Delta t}{M_\eta 2} \\
 7 & e^{\mathcal{L}_5 \Delta t / 2} \quad \xi \leftarrow \xi + \frac{P_\zeta \Delta t}{M_\zeta 2} \\
 8 & e^{\mathcal{L}_6 \Delta t / 2} \quad P_\zeta \leftarrow P_\zeta + \left(\frac{P_V^2}{M_V} - k_B T_{\text{ext}}\right) \frac{\Delta t}{2} \\
 9 & e^{\mathcal{L}_7 \Delta t / 2} \quad \vec{p}_{\mu i} \leftarrow \vec{p}_{\mu i} \exp\left(-\frac{P_\eta \Delta t}{M_\eta 2}\right) \\
 10 & e^{\mathcal{L}_8 \Delta t / 2} \quad \vec{p}_{\mu i} \leftarrow \vec{p}_{\mu i} + \left(\vec{F}_{\mu i} - \frac{m_{\mu i}}{M_\mu} \vec{F}_\mu\right) \frac{\Delta t}{2} \\
 11 & e^{\mathcal{L}_9 \Delta t / 2} \quad \vec{p}_\mu \leftarrow \vec{p}_\mu \exp\left[-\frac{\Delta t}{2} \left(\frac{P_\eta}{M_\eta} + \frac{P_V}{3VM_V}\right)\right] \\
 12 & e^{\mathcal{L}_{10} \Delta t / 2} \quad \vec{p}_\mu \leftarrow \vec{p}_\mu + \frac{\Delta t}{2} \vec{F}_\mu \\
 13 & \vec{p}_{\mu i} \leftarrow \text{SHAKE COORDINATES} \\
 14 & T^* \leftarrow \frac{1}{gk_B} \left[ \sum_{i, \mu} \frac{\vec{p}_{\mu i}^2}{m_{\mu i}} + \sum_\mu \frac{\vec{p}_\mu^2}{M_\mu} \right] \\
 15 & e^{\mathcal{L}_{11} \Delta t / 2} \quad P_\eta \leftarrow P_\eta + gk_B (T^* - T_{\text{ext}}) \frac{\Delta t}{2} \\
 16 & e^{\mathcal{L}_{12} \Delta t / 2} \quad \vec{R}_\mu \leftarrow \vec{R}_\mu \exp\left(\frac{\Delta t}{2} \frac{P_V}{3VM_V}\right) \\
 17 & e^{\mathcal{L}_{13} \Delta t} \quad \vec{R}_\mu \leftarrow \vec{R}_\mu + \Delta t \frac{\vec{p}_\mu}{M_\mu} \\
 18 & e^{\mathcal{L}_{14} \Delta t} \quad \vec{r}_{\mu i} \leftarrow \vec{r}_{\mu i} + \Delta t \frac{\vec{p}_{\mu i}}{m_{\mu i}} \\
 19 & \vec{F}_{\mu i}, \vec{F}_\mu \leftarrow \text{FORCES CALCULATION} \\
 20 & e^{\mathcal{L}_{12} \Delta t / 2} \quad \vec{R}_\mu \leftarrow \vec{R}_\mu \exp\left(\frac{\Delta t}{2} \frac{P_V}{3VM_V}\right) \\
 21 & e^{\mathcal{L}_{11} \Delta t / 2} \quad P_\eta \leftarrow P_\eta + gk_B (T^* - T_{\text{ext}}) \frac{\Delta t}{2} \\
 22 & e^{\mathcal{L}_{10} \Delta t / 2} \quad \vec{p}_\mu \leftarrow \vec{p}_\mu + \frac{\Delta t}{2} \vec{F}_\mu \\
 23 & e^{\mathcal{L}_9 \Delta t / 2} \quad \vec{p}_\mu \leftarrow \vec{p}_\mu \exp\left[-\frac{\Delta t}{2} \left(\frac{P_\eta}{M_\eta} + \frac{P_V}{3VM_V}\right)\right] \\
 24 & e^{\mathcal{L}_8 \Delta t / 2} \quad \vec{p}_{\mu i} \leftarrow \vec{p}_{\mu i} + \left(\vec{F}_{\mu i} - \frac{m_{\mu i}}{M_\mu} \vec{F}_\mu\right) \frac{\Delta t}{2} \\
 25 & e^{\mathcal{L}_7 \Delta t / 2} \quad \vec{p}_{\mu i} \leftarrow \vec{p}_{\mu i} \exp\left(-\frac{P_\eta \Delta t}{M_\eta 2}\right)
 \end{array}$$



$$\begin{aligned}
26 \quad & \vec{p}_{\mu i} \leftarrow \text{SHAKE MOMENTA} \\
27 \quad & e^{\mathcal{L}_6 \Delta t/2} P_{\xi} \leftarrow P_{\xi} + \left( \frac{P_V^2}{M_V} - k_B T_{\text{ext}} \right) \frac{\Delta t}{2} \\
28 \quad & e^{\mathcal{L}_5 \Delta t/2} \xi \leftarrow \xi + \frac{P_{\xi} \Delta t}{M_{\xi} 2} \\
29 \quad & e^{\mathcal{L}_4 \Delta t/2} \eta \leftarrow \eta + \frac{P_{\eta} \Delta t}{M_{\eta} 2} \\
30 \quad & e^{\mathcal{L}_3 \Delta t/2} V \leftarrow V + \frac{P_V \nu \Delta t}{M_V 2} \\
31 \quad & \Pi^* \leftarrow \frac{1}{3V} \sum_{\mu} M_{\mu} \dot{\vec{R}}_{\mu}^2 + \frac{1}{6V} \sum_{\mu} \sum_{\mu'} \sum_{i \in \mu} \sum_{j \in \mu'} (\vec{R}_{\mu} - \vec{R}_{\mu'}) \cdot (\vec{f}_{\mu i} - \vec{f}_{\mu' j}) \\
32 \quad & e^{\delta \mathcal{L}_1 \nu \Delta t/2} P_V \leftarrow e^{-\gamma \nu \Delta t/2} P_V + \frac{\sigma M_V^{1/2}}{\sqrt{2\gamma}} \sqrt{1 - e^{-\gamma \nu \Delta t}} R(t) \\
33 \quad & e^{\mathcal{L}_2 \nu \Delta t/2} P_V \leftarrow P_V + (\Pi^* - \Pi_{\text{ext}}) \frac{\nu \Delta t}{2} \\
34 \quad & e^{\mathcal{L}_1 \nu \Delta t/2} P_V \leftarrow P_V \exp \left( -\frac{P_{\xi} \nu \Delta t}{M_{\xi} 2} \right)
\end{aligned}$$

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### Notes

The authors declare no competing financial interest.

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