# SOLID SOLUTIONS IN THE Cr<sub>2</sub>O<sub>3</sub>-α-Sb<sub>2</sub>O<sub>4</sub>-M<sub>0</sub>O<sub>3</sub> SYSTEM

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#### **Abstract**

DTA and XRD methods used to examine the  $Cr_2O_3$ – $\alpha$ - $Sb_2O_4$ – $MoO_3$  system have shown that a substitution solid solution of  $MoO_3$  in  $CrSbO_4$  is formed. A study of all the theoretically possible solid solution models has pointed to the fact that  $Mo^{6^+}$  ions are incorporated into the  $CrSbO_4$  crystal lattice, in the place of  $Sb^{5^+}$  ions and the compensation of redundant charges takes place through cation vacancies arising in an  $Sb^{5^+}$  sub-lattice. The solubility limit for  $MoO_3$  in  $CrSbO_4$  does not exceed 25.00 mol%.  $CrSbO_{4(s,s,)}$  is stable to  $\sim 1320^{\circ}C$ .

**Keywords:** Cr<sub>2</sub>O<sub>3</sub>–α-Sb<sub>2</sub>O<sub>4</sub>–MoO<sub>3</sub> system, DTA, solid solution models, XRD

### Introduction

The oxides  $MoO_3$ ,  $Sb_2O_4$  and  $Cr_2O_3$  and compounds formed in some systems built by the oxides find many applications, first of all, as catalysts [1–3]. Therefore, studies on reactions between oxides, leading to phases not known before, are of crucial importance.

It follows from our earlier works that components of the  $Cr_2O_3$ –MoO $_3$  system interact in the solid state to form one compound, that is,  $Cr_2(MoO_4)_3$  [4, 5]. The compound is stable in air to  $810^{\circ}C$  – an onset temperature of its breaking down to  $Cr_2O_3$ , accompanied by the sublimation of  $MoO_3$  [4]. On the other hand, the reaction in air between the oxides,  $\alpha$ -Sb $_2O_4$  and  $Cr_2O_3$ , brings about  $CrSbO_4$  [6, 7]. The compound decomposes at  $1380^{\circ}C$  upwards to yield  $Cr_2O_3$  and a gaseous product [6]. In contrast, the oxides,  $\alpha$ -Sb $_2O_4$  and  $MoO_3$ , fail to interact in the solid state. It is only known that the presence of  $MoO_3$  decreases the temperature of  $\alpha$ -Sb $_2O_4$   $\rightarrow \beta$ -Sb $_2O_4$  polymorphic conversion from 935 to  $850^{\circ}C$ ; with concurrent originating a low-concentrated solid solution of  $MoO_3$  in  $\beta$ -Sb $_2O_4$  [8].

Contrary to the oxide systems:  $MoO_3-Sb_2O_4$ ,  $Sb_2O_4-Cr_2O_3$  and  $Cr_2O_3-MoO_3$  that are known fairly well, the three-component  $Cr_2O_3-\alpha-Sb_2O_4-MoO_3$  system had not been an objective of research before ours [6, 9]. The results of our introductory investigation of  $Cr_2O_3$ ,  $\alpha-Sb_2O_4$  reactivity with  $MoO_3$  suggested that solid solutions of  $MoO_3$  in  $CrSbO_4$  were formed in the system under study [9].

The aim of this work was to verify the recent results achieved and to define the practical models of MoO<sub>3</sub> solid solutions in CrSbO<sub>4</sub>.

# **Experimental**

The following substances were used in the experiments:  $Sb_2O_3$  – pure (Merck, Germany),  $Cr_2O_3$  – pure (Aldrich, Germany),  $MoO_3$  – pure (POCh, Gliwice, Poland),  $\alpha$ - $Sb_2O_4$  (prepared by heating in air a commercial  $Sb_2O_3$ ),  $Cr_2(MoO_4)_3$  and  $CrSbO_4$  (prepared by methods described in works [4, 6]).

For the experiments 31 samples were prepared from the oxides,  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub>, MoO<sub>3</sub> and Cr<sub>2</sub>O<sub>3</sub> (Nos 1–5; 7; 8; 10; 11; 15; 16; 17–35) and 4 samples from the compounds Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, CrSbO<sub>4</sub> and suitable oxides (Nos 6; 9; 12; 14). The compositions of the samples have been tabulated in Tables 1 and 2.

**Table 1** Compositions of initial mixtures and X-ray phase analysis of samples representing the CrSbO<sub>4</sub>–MoO<sub>3</sub> system after the final heating cycle

<b>N</b> T -		Composition	- D1			
No.	MoO <sub>3</sub>	α-Sb <sub>2</sub> O <sub>4</sub>	Cr <sub>2</sub> O <sub>3</sub>	CrSbO <sub>4</sub>	$Cr_2(MoO_4)_3$	Phases found
1	2.50	48.75	48.75	_	_	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4$
2	5.00	47.50	47.50	_	_	$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
3	7.50	46.25	46.25	_	-	$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
4	10.00	45.00	45.00	_	-	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4$
5	15.00	42.50	42.50	_	_	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4$
6	20.00	_	_	80.00	_	$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
7	25.00	37.50	37.50	_	_	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4\!\!+\!\!MoO_3$
8	30.00	35.00	35.00	_	-	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4\!\!+\!\!MoO_3$
9	33.33	_	_	66.67	_	$CrSbO_{4(s.s.)}\!\!+\!\!MoO_3\!\!+\!\!\alpha\text{-}\!Sb_2O_4$
10	33.34	33.33	33.33	_	_	$CrSbO_{4(s.s.)}\!\!+\!\!MoO_3\!\!+\!\!\alpha\text{-}\!Sb_2O_4$
11	35.00	32.50	32.50	_	_	$CrSbO_{4(s.s.)}+MoO_3+\alpha$ - $Sb_2O_4^*$
12	50.00	-	-	50.00	_	$MoO_3+CrSbO_{4(s.s.)}+lpha-Sb_2O_4^{*}$
13	50.00	25.00	25.00	_	_	$MoO_3+CrSbO_{4(s.s.)}+lpha-Sb_2O_4^{*}$
14	-	50.00	-	_	50.00	$MoO_3 + CrSbO_{4(s.s.)} + \alpha - Sb_2O_4^{*}$
15	66.67	16.66	16.67	_	-	$MoO_3+CrSbO_{4(s.s.)}+lpha-Sb_2O_4^{*}$
_16	75.00	12.50	12.50		_	$MoO_3+CrSbO_{4(s.s.)}+\alpha-Sb_2O_4^*$

\*traces

The reagents were weighed in appropriate proportions, homogenised by milling, shaped into pellets and heated under conditions that would secure establishing equilibrium; i.e.:

400°C (1 h)→500°C (24 h)→550°C (48 h)→600°C (48 h) →650°C (48 h)→700°C (48 h)→750°C (48 h).

After each heating cycle the samples, still kept in the furnace, were slowly cooled down to ambient temperature, weighed in order to determine their mass change, milled and examined by DTA and XRD to establish their compositions.

Phases of the thermally treated samples were identified by XRD method (a diffractometer DRON-3,  $CoK_{\alpha}$  radiation, Fe filter) and with the help of PDF cards [10] and works [11].

DTA/TG measurements were made using an instrument of a SDT 2960 type (TA Instruments, USA). The measurements were made by DTA method in air, samples of  $\sim$ 7 mg each, the samples were placed in platinum crucibles, at a temperature range of  $20-1500^{\circ}$ C and heated at a rate of  $10 \text{ K min}^{-1}$ .

# Results and discussion

Table 1 shows the compositions of initial mixtures and X-ray phase analysis of samples representing the CrSbO<sub>4</sub>–MoO<sub>3</sub> system after the final heating cycle, that is, in a state of equilibrium.

After each cycle of heating the samples, the change in their mass was monitored. It was found that the sum of the mass losses recorded after consecutive heating cycles was fluctuating between 0.96 and 2.69% by mass. Hence it can be assumed that the mass losses follow from the presence of MoO<sub>3</sub> in the samples, the sublimation of the oxide starts to negligible extent at 550°C.

The mass re-counted from percentage by mass into percentage by mole of MoO<sub>3</sub> made up 1.5–3.7 mol%. Hence it can be acknowledged that the magnitude of the mass found in the samples is of inconsiderable importance to the results of our work.

XRD analysis showed that samples comprising up to 25.00 mol% of MoO<sub>3</sub> in their initial mixtures contained CrSbO<sub>4</sub> and  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> after the last heating cycle but they were lacking MoO<sub>3</sub>. X-ray diffraction patterns of the samples showed reflections, characteristic of CrSbO<sub>4</sub>, slightly shifted towards smaller angles (20), so they were corresponding to greater interplanar distances ( $d_{hkl}$ ).

Samples representing the other component concentration range of the  $CrSbO_4$ – $MoO_3$  system, say, over 25.00 mol% of  $MoO_3$ , comprised three phases:  $MoO_3$ ,  $CrSbO_4$  and  $\alpha$ - $Sb_2O_4$ .

These facts have led to the conclusion that MoO<sub>3</sub> forms a solid solution with CrSbO<sub>4</sub>, and Mo<sup>6+</sup> ions are built into the CrSbO<sub>4</sub> crystal lattice, in the place of Sb<sup>5+</sup> ions; the substitution could be evidenced by the presence of α-Sb<sub>2</sub>O<sub>4</sub>. The results of our previous works were somewhat different from the present ones and implied that it was the Cr<sup>3+</sup> ions that were substituted by Mo<sup>6+</sup> ions [9]. In face of the fact that Sb<sup>5+</sup> radius (61 pm) and that of Cr<sup>3+</sup> (60 pm) [12] are very similar, there is much probability of substituting either of them by Mo<sup>6+</sup> ions (59 pm) [12]. That possibility was taken into consideration in further studies depending on devising all theoretically acceptable models of the MoO<sub>3</sub> solid solutions in CrSbO<sub>4</sub>. As for the incorporation of

Mo<sup>6+</sup> ions into the CrSbO<sub>4</sub> lattice, in the place of Cr<sup>3+</sup>, the compensation of redundant positive charge is feasible by:

- originating cationic vacancies ( $\square$ ) in a  $Cr^{3+}$  sub-lattice bound with a concurrent removal of an equivalent number of Cr<sup>3+</sup> ions from the CrSbO<sub>4</sub> lattice. A solid solution corresponding to the model is described by a formula:  $Cr_{1-2x}\square_x Mo_x SbO_4$  (model I)
- originating cationic vacancies in the Sb<sup>5+</sup> sub-lattice the formula of the solid solution can be written as  $Cr_{1-5x}Mo_{5x}Sb_{1-3x}\square_{3x}O_4$  (model II) reduction of  $Cr^{3+}$  to  $Cr^{2+}$  ions:  $Cr^{3+}_{1-4x}Cr^{2+}_{3x}Mo_xSbO_4$  (model IIIA)
- reduction of Sb<sup>5+</sup> to Sb<sup>3+</sup> ions:  $Cr_{1-2x}^{-7x}Mo_{2x}Sb_{1-x}^{5+}Sb_x^{3+}O_4$  (model IIIB)

As for the models IIIA and IIIB, the contents of the initial mixture result from

the common expression:  $\text{Cr}_{1-x}\text{Mo}_x\text{SbO}_{4-3x}$ . With substitution by  $\text{Mo}^{6^+}$  of  $\text{Sb}^{5^+}$  ions in the  $\text{CrSbO}_4$  lattice, the compensation of redundant positive charges is feasible by:

- originating cationic redundancies in a  $Cr^{3+}$  sub-lattice:  $Cr_{1-x}\square_xSb_{1-3x}Mo_{3x}O_4$ (model IV)
- originating cationic redundancies in a Sb<sup>5+</sup> sub-lattice: CrSb<sub>1.6</sub>,  $\square_{x}$ Mo<sub>5</sub>, O<sub>4</sub> (model V)
- reduction of  $Sb^{5+}$  to  $Sb^{3+}$  ions:  $CrSb_{1-3x}^{5+}Sb_x^{3+}Mo_{2x}O_4$  (model VIA) reduction of  $Cr^{3+}$  to  $Cr^{2+}$  ions:  $Cr_{1-x}^{3+}Cr_x^{2+}Sb_{1-x}Mo_xO_4$  (model VIB)

Compositions of samples in terms of the oxides: MoO<sub>2</sub>, Cr<sub>2</sub>O<sub>3</sub>, α-Sb<sub>2</sub>O<sub>4</sub>, corresponding to models VIA and VIB are the same and result from the expression:  $CrSb_{1-x}Mo_{x}O_{4-x}$ .

Studies that aimed at finding which of the theoretical solid solution models is carried into effect consisted in synthesising samples possessing a composition matching each of the models presented. Table 2 shows contents of the oxide initial mixtures. Pellets made from the oxides were calcinated under conditions identical with those applied to the samples of the CrSbO<sub>4</sub>–MoO<sub>3</sub> system.

X-ray phase analysis of the samples after the final heating cycle (Table 2) have shown that their initial mixtures comprising up to 15 mol% of MoO<sub>3</sub>, with contents corresponding to models, I, II, III, IV and VI, contained, apart from a solid solution of MoO<sub>3</sub> in CrSbO<sub>4</sub>, α-Sb<sub>2</sub>O<sub>4</sub> whereas samples with the composition described by model V (samples 32 and 33) were mono-phases and contained the MoO<sub>3</sub> solid solution in CrSbO<sub>4</sub> only. The results indicate that the formation of the solid solution takes place following model V, that is, Mo<sup>6+</sup> ions are incorporated into the CrSbO<sub>4</sub> lattice, in the place of Sb<sup>5+</sup>, and the compensation of redundant positive charges is realised by formation of cationic vacancies in a Sb5+ sub-lattice. In order to verify the solubility limit for MoO3 in CrSbO4, a sample containing 25.00 mol\% of MoO<sub>3</sub> was prepared and its composition corresponding to model V. XRD analysis of the sample after the final heating cycle has proved it to be a three-phase and contain, beside CrSbO<sub>4(ss)</sub> and Cr<sub>2</sub>(MoO<sub>4</sub>)<sub>3</sub>, inconsiderable amounts of Cr<sub>2</sub>O<sub>3</sub>. This result provides a proof that the solubility limit for MoO<sub>3</sub> in the CrSbO<sub>4</sub> crystal lattice does not exceed 25 mol%; the proof can be tested through the phase composition of other samples obtained in this work.

**Table 2** Compositions of initial mixtures and X-ray phase analysis of samples representing theoretical models of the MoO<sub>3</sub> solid solutions in CrSbO<sub>4</sub> after the final heating cycle

No.	Composition of initial mixtures/mol%			Formula of the	Phases found
	MoO <sub>3</sub>	$\alpha$ -Sb <sub>2</sub> O <sub>4</sub>	Cr <sub>2</sub> O <sub>3</sub>	solid solutions	
17	2.50	50.00	47.50		$CrSbO_{4(s.s.)}+\alpha-Sb_2O_4$
18	5.00	50.00	45.00	$Cr_{1-2x}\square_x Mo_x SbO_4$ (model I)	$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
19	10.00	50.00	40.00		$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
20	15.00	50.00	35.00		$CrSbO_{4(s.s.)}\!\!+\!\alpha\!\!-\!Sb_2O_4$
21	20.00	50.00	30.00		$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4 + MoO_3$
22	25.00	50.00	25.00		$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4 + MoO_3$
23	35.00	50.00	15.00		$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4 + MoO_3$
24	45.00	50.00	5.00		$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4 + MoO_3$
25	10.00	46.00	44.00	$Cr_{1-5x}Mo_{5x}Sb_{1-3x}\square_{3x}O_4$	$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
26	15.00	44.00	41.00	(model II)	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4\!\!+\!\beta\text{-}Sb_2O_4$
27	10.00	47.50	42.50	$Cr_{l-4x}^{3+}Cr_{3x}^{2+}Mo_xSbO_4$ (model IIIA)	$CrSbO_{4(s.s.)}\!\!+\!\alpha\text{-}Sb_2O_4$
28	15.00	46.25	38.75	$Cr_{1-2x}Mo_{2x}Sb_{1-x}^{5+}Sb_{x}^{3+}O_{4}$ (model IIIB)	$CrSbO_{4(s.s.)}\!\!+\!\alpha\!\!-\!Sb_2O_4$
29	10.00	43.33	46.67		$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
30	15.00	40.00	45.00	$Cr_{1-x}\square_xSb_{1-3x}Mo_3O_4$ (model IV)	$CrSbO_{4(s.s.)} + \alpha - Sb_2O_4$
31	50.00	16.67	33.33	(model IV)	$CrSbO_{4(s.s.)}+Cr_2(MoO_4)_3+MoO_3$
32	10.00	42.00	48.00	$CrSb_{1-6x}\square_x Mo_{5x}O_4$	$CrSbO_{4(s.s.)}$
33	15.00	38.00	47.00	(model V)	$CrSbO_{4(s.s.)}$
34	10.00	42.50	47.50	${\operatorname{CrSb}_{l-3x}^{5}}^{+}{\operatorname{Sb}_{x}^{3+}}{\operatorname{Mo}_{2x}}{\operatorname{O}_{4}} \ (\operatorname{model VIA})$	$CrSbO_{4(s.s.)}\!\!+\!\alpha\!\!-\!Sb_2O_4$
35	15.00	38.75	46.25	$Cr_{l-x}^{3+}Cr_x^{2+}Sb_{1-x}Mo_xO_4$ (model VIB)	$CrSbO_{4(s.s.)}+\alpha$ - $Sb_2O_4$

DTA curves of samples with compositions presenting models I–IV and VI, viz. comprising the solid solutions of MoO<sub>3</sub> in CrSbO<sub>4</sub> and  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> after the final heating cycle, showed that the first endothermic effect started at ~1020°C, accompanied by the mass loss fluctuating between 15 and 25% by mass – recorded on TG curves. In accordance with the data published [13], at this temperature range starts decomposition of  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> to gaseous products, probably to Sb<sub>4</sub>O<sub>6</sub> (dimer) and O<sub>2</sub>. Loss in mass of the samples under study, starting at this temperature, corresponded to the contents of  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> in mixtures with the MoO<sub>3</sub> solution in CrSbO<sub>4</sub>. The fact justifies the reason that  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> remains in equilibrium with the MoO<sub>3</sub> solid solution in CrSbO<sub>4</sub> to ~960°C, say, to the temperature of the  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> decomposition.

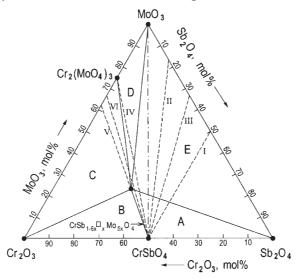
Another small endothermic effect recorded at ~1320°C on DTA curves of the samples was deemed to relate with mass of the samples, making up 47–53% by mass. The results of studying the after-DTA remains by XRD have shown that this effect

can pertain to the decomposition of the MoO<sub>3</sub> solid solution in CrSbO<sub>4</sub> to deposit Cr<sub>2</sub>O<sub>3</sub> and release gaseous products.

A small endothermic effect with an onset temperature fluctuating between 1320 and 1380°C was noticed on DTA curves comprising only the  $MoO_3$  solid solution in  $CrSbO_4$ . Mass decrement of ~60.00% by mass producing this effect is believed to be bound with decomposition of the  $MoO_3$  solid solution in  $CrSbO_4$ .

## **Conclusions**

- 1. Components of the  $Cr_2O_3-\alpha$ - $Sb_2O_4-MoO_3$  system interact to produce a substitution solid solution of  $MoO_3$  in  $CrSbO_4$  with a formula:  $CrSb_{1-6x}\square_x Mo_{5x}O_4$ .
- 2. Substitution of Sb<sup>5+</sup> by Mo<sup>6+</sup> in the CrSbO<sub>4</sub> crystal lattice gives rise to originating of redundant charges, the compensation of which is realised by arising vacancies in a Sb<sup>5+</sup> sub-lattice.
- 3. The solid product of the  $CrSb_{1-6x}\square_x Mo_{5x}O_4$  decomposition starting at ~1320°C is  $Cr_2O_3$ .
- 4. Solid solutions of  $MoO_3$  in  $CrSbO_4$  remain in equilibrium with  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub> up to ~1020°C, that is, at a temperature of thermal dissociation of  $\alpha$ -Sb<sub>2</sub>O<sub>4</sub>.
- 5. The results obtained have allowed to divide the  $Cr_2O_3$ – $\alpha$ - $Sb_2O_4$ – $MoO_3$  system into five subsidiary systems as it has been shown in Fig. 1.



 $\label{eq:Fig. 1} \begin{array}{l} \textbf{Fig. 1} \ \text{The component concentration triangle of the $Cr_2O_3$-$\alpha$-$Sb_2O_4$-$MoO_3$; ----- position of theoretical models of the $MoO_3$ solid solution in $CrSbO_4$; ----------- $CrSbO_4$-$MoO_3$ intersection; ---- division of the system studied into subsidiary system: $A - CrSbO_{4(s.s.)}$-$\alpha$-$Sb_2O_4$; $B - CrSbO_{4(s.s.)}$-$Cr_2O_3$; $C - CrSbO_{4(s.s.)}$-$Cr_2O_3$-$Cr_2(MoO_4)_3$; $D - CrSbO_{4(s.s.)}$-$Cr_2(MoO_4)_3$-$MoO_3$; $E - CrSbO_{4(s.s.)}$-$MoO_3$-$\alpha$-$Sb_2O_4$ } \end{array}$ 

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