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# Chromophore Relaxation in a Side-Chain Methacrylate Copolymer Functionalized with

4-[*N*-Ethyl-*N*-(2-hydroxyethyl)]amino-2'-chloro-4'-nitroazobenzene

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ABSTRACT: A side-chain methacrylate copolymer functionalized with the nonlinear optical chromophore 4-[N-ethyl-N-(2-hydroxyethyl)]amino-2'-chloro-4'-nitroazobenzene, disperse red-13, was prepared and characterized. The chromophore relaxation was investigated measuring the decay of the electrooptic coefficient  $r_{13}$  and the complex dielectric constant at different temperatures. Results obtained below and above  $T_g$  were analyzed using the Kohlrausch-Williams-Watts (KWW) equation, through the study of the temperature dependence of the KWW parameters. Above  $T_g$  the relaxation time experimental data were fitted to the Williams-Landel-Ferry (WLF) equation and its parameters determined. Chromophore relaxation leading to the decrease of electrooptic properties was found associated with a primary  $\alpha$  relaxation. The obtained WLF equation parameters were introduced into the Adam-Gibbs-Tool-Narayanaswamy-Moynihan equation, and the overall relaxation time temperature dependence was successfully obtained in terms of the fictive temperature, accounting for the sample thermal treatment and allowing optimized thermal treatment to be found. The copolymer KWW stretching parameter at the glass transition temperature lies close to the limit value for short-range interactions, i.e., 0.6, suggesting that the chromophore group is participating in primary  $\alpha$  relaxation.

## I. Introduction

The most common polymeric materials with nonlinear optical (NLO) properties are the side-chain polymers, which are synthesized by covalently linking organic NLO chromophore molecules to a given polymeric backbone. The azobenzene chromophore group confers to polymers their NLO features and also the reversible cis-trans photoisomerization, leading to optical switching, optical storage, and surface relief grating formation.<sup>2</sup> For second-order NLO optical processes, such as second-harmonic generation and the linear electrooptic effect (Pockel's effect), polymers must be submitted to the electric poling in order to generate polar orientation of the chromophore. Poling is usually performed either applying a bias voltage<sup>3</sup> to the sample or charging it in a corona triode.<sup>4,5</sup> The orientational order of chromophores that results is usually unstable, and a strong effort has been made to investigate relaxation processes of such NLO chromophores in order to obtain more stable polymeric materials. The electric polarization is a measure of such orientational order, and it is related to the linear electrooptic and second-harmonic generation effects.

Several relaxation models have been attempted for NLO polymers. In fact, the decay of the electrooptic coefficient can be fitted with different functions such as

biexponential,<sup>6</sup> Kohlrausch–Williams–Watts stretched exponential (KWW),<sup>7,8</sup> single-exponential plus KWW, van der Vorst,<sup>9</sup> and Dissado–Hill power laws.<sup>10,11</sup> The KWW decay function is given by:

$$\Phi(t) = \exp\left[-\left(\frac{t}{\tau}\right)^b\right] \tag{1}$$

Usually such an equation provides a good data fitting and meaningful parameters  $\tau$  and b,  $\tau$  representing a characteristic relaxation time and b the exponential stretching. The KWW equation was initially considered an empirical function, found to fit most of the experimental relaxation data, with no particular meaning for the b parameter. However, physical meaning can be achieved if one takes into account that the KWW equation is the solution for the Brownian motion of a particle interacting with randomly distributed traps or sinks. 12,13 Under this model a defined microscopic meaning for the *b* parameter can also be inferred. Thus, dependences of  $\tau$  and b on temperature are of great relevance to understand the microscopic behavior of polymers and also to predict the final NLO properties of the glassy state, obtained when cooling the material from the liquid state. Regarding phenomenological viscoelasticity, if b = 1, the relaxation process corresponds to a single relaxation time. For b < 1, the relaxation process is associated with a relaxation time distribution, that is, a relaxation spectrum centered at the characteristic relaxation time  $\tau$ . The lower the value of b is, the broader the relaxation spectrum will be. Tobolsky et al. have shown that an increase in molecular weight implies a decrease in b, <sup>14</sup> and Monteiro et al.

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**Figure 1.** Chemical structure of the random MMA-DR13 copolymer. X and Y values determine the percentage of each

associated the decrease in b with the increase in phase segregation in polyurethanes. 15 In other words, anything that makes the relaxation process more heterogeneous such as higher polydispersity or higher molecular weight implies in more possibilities of entanglements between the polymer chains and will contribute to a decrease of b and to the relaxation spectrum broadening.

In the present work, the preparation and characterization of the side-chain methyl methacrylate, MMA-DR13, an acrylic copolymer functionalized with different percentages of the chromophore disperse red-13, 4-[Nethyl-N-(2-hydroxyethyl) amino-2'-chloro-4-nitroazobenzene, DR13, are briefly described. A detailed study of the relaxation of chromophore orientation was performed by monitoring the electrooptic coefficient decay, in time domain, below the glass transition temperature,  $T_{\rm g}$ . Above  $T_{\rm g}$ , dielectric spectroscopy measurements were used, as the electrooptic decay was too fast to be measured. Electrooptic coefficient decay and dielectric spectroscopy results were analyzed using the KWW function, from which the dependences of  $\tau$  and b on temperature were determined. The temperature dependence of the relaxation time was calculated from dielectric data above  $T_g$ , and the obtained values were fitted to the Williams-Landel-Ferry (WLF) equation.  $^{16}$  The relaxation time values below  $T_{\rm g}$ , obtained from electrooptic measurements, were predicted by introducing WLF constants into the modified Adams-Gibbs (AG) equation, which accounts for the glass transition kinetics. 17

The article is organized as follows. Section II gives the experimental results of the copolymer preparation and its characterization, corona poling, and measurement techniques. Section III shows the results of the relaxation measurements, and section IV presents the discussion and conclusions.

#### **II. Experimental Section**

The random copolymer, MMA-DR13, shown in Figure 1, was prepared from solution copolymerization of methyl methacrylate (MMA, Aldrich) and 4-[N-ethyl-N-(2-methacryloxyethyl)]amino-2'-chloro-4'-nitroazobenzene (DR13MA). The DR13MA monomer was synthesized by the esterification of the commercial dye 4-[N-ethyl-N-(2-hydroxyethyl)]amino-2'-chloro-4'nitroazobenzene (DR13, Aldrich) with methacryloyl chloride. 18 The copolymerization of DR13MA and MMA monomers was performed using methyl ethyl ketone as solvent and 2,2'-

azobis(butyronitrile) (AIBN) as initiator, at reflux temperature for 9 h. The resultant copolymer was precipitated, exhaustively washed with methanol, and dried in a vacuum desiccator for about 72 h. Different ratios of DR13MA and methyl methacrylate monomers were used to prepare copolymers with chromophore weight ratios of 9 and 43 wt %, being designated as MMA-DR13(9 wt %) and MMA-DR13(43 wt %), respectively. Small quantities of MMA-DR13(4 wt %) were also prepared to be used as trial samples. Copolymers were characterized by UV-vis in DMF solution, using a Hitachi U2001 spectrophotometer, and by FTIR, samples in KBr pellets, using a BOMEM DA-8 spectrophotometer. Thermal behavior of the samples was characterized by differential scanning calorimetry (DSC), using a TA calorimeter model 2910 (ambient to 250  $^{\circ}\text{C},\,20\,^{\circ}\text{C/min}$  and under  $N_{2}),$  and thermogravimetry mass loss (TGA), using a Shymadzu Twi50 thermal analyzer (ambient to 700 °C, 10 °C/min and under  $N_2$ ).

Number-average  $(M_n)$  and by weight-average  $(M_w)$  molecular weights, as well the polydispersivity, were obtained by size exclusion chromatography (SEC) (THF as eluent and polystyrene standards). It was found that values of  $M_{\rm n}$  were ca. 23 000 and 18 000 g/mol for the MMA-DR13(9 wt %) and MMA-DR13-(43 wt %), respectively, while values of  $M_{\rm w}$  were 40 000 and 35 000. Thus, polydispersities are of the order of 1.7 and 1.9, respectively. Thin-layer chromatography (silica gel using dichloromethane/n-hexane 70/30) confirmed the absence of nonreacted monomers.

All copolymers in DMF solution showed a maximum optical absorption at 505 nm. Copolymer films showed a blue shift of 15 nm compared to the solution spectra, probably due to aggregation of the chromophores in the film, similarly to Langmuir-Blodgett films. 18 The main IR absorption bands of MMA were present: 2960, 2850 cm<sup>-1</sup> (C-H stretching), 1732 cm<sup>-1</sup> (C-O stretching of ester groups), 1242, 1252, and 1134 cm<sup>-1</sup> (asymmetric and symmetric C(=O)-O and O-C-C stretching vibrations of ester group). Regarding DR13MArelated absorptions, the following bands are present in the spectra of all copolymers: 1599 and 1500 cm<sup>-1</sup> (C=C stretching in benzene rings), 1518 cm<sup>-1</sup> (NO<sub>2</sub> asymmetric stretching), and  $1336~\text{cm}^{-1}$  (N $\ensuremath{\breve{O}}_2$  symmetric stretching).

Films with thickness of about 10  $\mu$ m were cast from chloroform copolymer solutions (0.5-2% w/w). All solutions were filtered with a syringe Millipore Durapore 0.45  $\mu$ m filter. Substrates such as optical crown type glass, glass covered with indium tin oxide (ITO), or aluminum plates were employed. Samples were dried for 30 min at room conditions and then submitted to a primary vacuum at 130 °C for 24 h for solvent removal.

To achieve the second-order NLO properties, i.e., to orient the side-chain chromophore dipolar groups, a corona triode setup was used.<sup>4,5</sup> Such a technique has been preferred to pole NLO polymers because it offers better radial uniformity polarization on sample4 and a good control of final surface potential, and the metallic grid gives protection against surface attack from corona species, which are known to deteriorate polymer surfaces. 4,19,20 The corona triode consisted of a sharp point, a stainless steel grid with a stainless steel mesh of wires of 0.1 mm diameter, and a metallic sample holder.<sup>4</sup> The corona triode was mounted inside an oven, allowing the temperature to be controlled. A voltage was applied to the grid, and a highvoltage supply (±20 kV, operating as a constant current source) was used to generate the corona discharge. A corona current of  $\pm 5~\mu A$  was used in the experiments. The electric contact between the sample holder and the conductive ITO layer was obtained using silver paint. Such a procedure avoids the interference of the glass slide on the poling conditions. The sample was heated to the temperature of 120 °C, a grid voltage ranging from  $400\ to\ 600\ V$  was applied, and the corona discharge turned on. Poling was performed for  $30\ min;$ subsequently, the sample was cooled to room temperature, with the corona discharge on, at a rate of about 10 °C/min. The poling process terminated at room temperature, and power supplies turned off. The above experimental conditions yielded maximum electrooptic activity in samples as reported elsewhere<sup>4</sup> in a detailed study.

**Figure 2.** Normalized heat capacity  $C_P^N$  curves obtained from differential scanning calorimetry thermograms for MMA–D13(9 wt %) and MMA–DR13(43 wt %) copolymers and PMMA.

A scanning Mach-Zhender interferometer was used to measure the electrooptic coefficient,  $r_{13}$ , of the poled MMA-DR13 copolymer. The experimental setup is similar to the one described by Singer et al.21 In these measurements, films deposited onto ITO glass substrates were used. The bare surface of the film was metallized with an  $\sim\!10$  nm aluminum layer by thermal evaporation in a vacuum, which is practically transparent to the 10 mW, He-Ne, 633 nm laser beam used in the electrooptic coefficient measurements. The light was linearly polarized, and the laser beam of diameter 2 mm impinged the sample at a right angle with respect to its surface. The electrooptic effect was produced in the samples by applying a modulation sinusoidal voltage to the aluminum electrode by means of a soft metallic spring to avoid mechanical stress. Interference fringes were scanned by applying a ramp voltage to a piezoelectric driven mirror. Measurement conditions were the following: modulation frequency of 2 kHz, frequency of fringe displacement within a range from 0.01 to  $0.05 \text{ s}^{-1}$ , and fringe visibility better than 60%.

The dielectric permittivity measurements were performed with a Solartron 1260 impedance analyzer in the frequency range from 1 Hz to 1 MHz, applying a 0.3 V sine voltage. For these measurements MMA-DR13 films were casted onto 1 mm aluminum circular plates, the upper electrode being a 200 nm aluminum layer deposited by vacuum thermal evaporation.

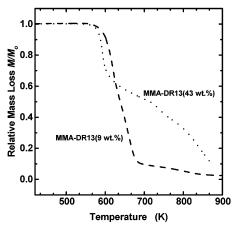
Note that temperature values are given in degrees Celsius, but in equations and in graphs their correspondig values on the Kelvin scale were used.

#### III. Results

**3.1. Copolymer Thermal Characterization.** DSC thermograms were obtained for some copolymers with different MMADR13 monomer contents (9 and 43 wt %), the normalized heat capacity,  $\mathcal{C}_P^N$ , being calculated using the following expression:<sup>22</sup>

$$C_P^{\rm N} = \frac{C_P(T) - C_{PL}(T)}{C_{PH}(T) - C_{PL}(T)}$$
 (2)

where  $C_P$  is the experimental value and  $C_{PH}$  and  $C_{PL}$  are the values of  $C_P$  obtained by extrapolation at highand low-temperature limits, i.e., far from  $T_g$ . Curves of Figure 2 show that  $T_g$  values, taken at  $C_P^{\rm N} \cong 0.5$ , are around 118 °C, decreasing slightly as chromophore content is increased. For comparison, it is also shown the corresponding curve of poly(methyl methacrylate), PMMA, sample ( $M_{\rm W}=350~000$ ). In the data analysis, to be shown in section IV, a  $T_g$  value of 118 °C was employed for all copolymers.



**Figure 3.** Thermogravimetric loss mass curves for MMA–DR13(9 wt %) and MMA–DR13(43 wt %) copolymers.

TGA loss mass measurements, shown in Figure 3, indicated that thermal degradation of the samples started around 327 °C, much higher than the temperatures used in this work. Thus, no degradation of the copolymer is expected to occur during measurements. In addition, the copolymer MMA–DR13(43 wt %) showed a decomposition curve with a different pattern, as compared to one of MMA–DR13(9 wt %). A possible explanation is that the highly conjugated chromophores could produce the cross-linking of the macromolecule chains with the action of temperature, resulting in systems that would be more difficult to decompose. As a consequence, the residual mass at the end of TGA curves are higher for higher chromophore contents.

**3.2. Isothermal Electrooptic Decay.** Under optimized corona poling conditions<sup>4</sup> the maximum values of  $r_{13}$  achieved, for MMA–DR13 samples with chromophore contents of 9 and 43 wt %, were 3 and 8 pm/V, respectively. For the sake of clearness, normalized values of  $r_{13}$  with respect to the initial ones will be shown.

Decay curves of normalized electrooptic coefficient,  $r_{13}$ , at different temperatures are shown in parts a and b of Figure 4 respectively for the MMA–DR13(9 wt %) and MMA–DR13(43 wt %) samples. These curves reveal that the decay increases with temperature and also that it is more accentuated for the MMA–DR13(43 wt %) sample.

The decay curves were best fitted to the KWW equation. Other decay functions such as the exponential, biexponential, biexponential plus KWW, or van der Vorst did not allow good fitting as obtained with the KWW function (results not shown here). As a consequence, the KWW function was used to analyze the relaxation data. This procedure is usually applied with success in the literature for NLO polymers. 4,23,24 The fitting curves are shown in Figure 4a,b by the full lines.

**3.3. Dielectric Relaxation.** It is worth mentioning that measurements of  $r_{13}$  could be performed only below  $T_{\rm g}$  because its decay at higher temperatures is too fast to be accurately measured using the Mach–Zender interferometer. An alternative procedure to probe the chromophore relaxation is from the dielectric response in the frequency domain. The complex dielectric permittivity  $\epsilon^* = \epsilon' + j\epsilon''$  is related to the KWW decay function  $\Phi(t)$ , eq 1, by the Laplace transform as:<sup>8</sup>

$$\frac{\epsilon^*(\omega) - \epsilon(\infty)}{\epsilon(0) - \epsilon(\infty)} = -\int_0^\infty \exp(-j\omega t) \left(\frac{\mathrm{d}\Phi(t)}{\mathrm{d}t}\right) \mathrm{d}t \qquad (3)$$

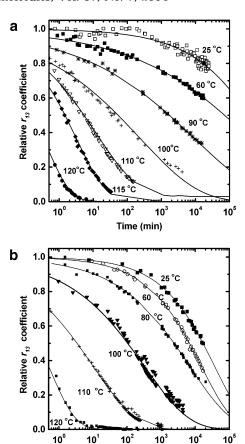
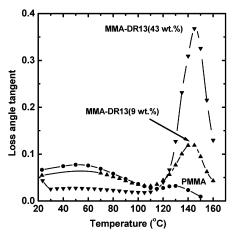


Figure 4. (a) Experimental results for electrooptic decay (points) and KWW fitting curves for MMA-DR13(9 wt %) sample. Temperatures of measurements are indicated in each curve. (b) Experimental results for electrooptic decay (points) and KWW fitting curves for MMA-DR13(43 wt %) sample. Temperatures of measurements are indicated in each curve.

Time (min)



**Figure 5.** Loss angle tangent data vs temperature taken at the frequency of 100 Hz, for MMA-DR13(9 wt %), MMA-DR13(43 wt %), and PMMA samples. The lines are guide lines.

where  $\epsilon(0)$  and  $\epsilon(\infty)$  are the real parts of low- and highfrequency limits of the dielectric permittivity, respectively. Determination of  $\tau$  and b KWW function parameters using eq 3 is not a straightforward process since the analytical evaluation of the integral of Laplace transform is not possible for all values of b. In this work, the approximations outlined by Weiss et al.<sup>25</sup> were used.

The tan  $\delta = \epsilon''/\epsilon'$  vs temperature curves, obtained at 100 Hz, are shown in Figure 5. Two relaxation peaks were observed; the lower one, around 60 °C, is associ-

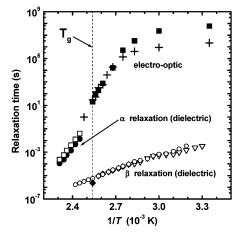


Figure 6. Relaxation times vs the inverse of the absolute temperature. Data represented by solid square and cross symbols were obtained from electrooptic coefficient measurements respectively for MMA-DR13(9%) and MMA-DR13-(43%) samples. Solid circle and open square symbols correspond to a relaxation data obtained from dielectric measurements respectively for MMA-DR13(9%) and MMA-DR13-(43%) samples. Finally, open circle, solid diamond, and open down triangle symbols correspond to  $\beta$  relaxation data obtained from dielectric measurements respectively for MMA-DR13(4%), MMA-DR13(9%), and MMA-DR13(43%) samples.

ated with a  $\beta$  relaxation and the higher one, around 140 °C, with an α relaxation. The curve of PMMA (Aldrich,  $M_{\rm w}=350~000$ ) is also included for comparison. (Only the  $\beta$  peak is observable at the frequency of 100 Hz in the temperature range displayed in the figure.) The  $\beta$ peak, corresponding to MMA-DR13 samples, should be attributed to the hindered rotation of the ester (-COOCH<sub>3</sub>) group of the MMA.<sup>26</sup> In the case of MMA-DR13(43 wt %) samples, it is believed that the  $\beta$  peak does not occur because of the higher volume that this bulky chromophore group occupies, making more hindered the chain rotation. The amplitude of the  $\alpha$  peak is highly dependent on the chromophore content. Thus, it seems that the chromophore side-group relaxation follows the  $\alpha$  relaxation. This behavior is somehow expected in side-chain NLO polymers rather than in guest-host since the chromophore molecules are bound to the copolymer backbone so that its orientational relaxation should be linked to the primary  $\alpha$  relaxation.

3.4. Temperature Dependence of Parameters. Figure 6 shows a plot of the KWW relaxation time,  $\tau$ , versus the reciprocal of temperature. The data were obtained from the fitting of the  $r_{13}$  decay curves and also from the tan  $\delta$  curves employing the Weiss procedure;<sup>25</sup>  $\tau$  values for both  $\alpha$  and  $\beta$  peaks were found. It is worth mentioning two points: first,  $\tau$  values corresponding to the  $\beta$  relaxation peaks are much smaller in comparison to the corresponding ones for the  $\alpha$  relaxation and also of those determined from the electrooptic decay; second,  $\tau$  values obtained from  $r_{13}$  decay, below  $T_{\rm g}$ , and from  $\alpha$ peaks, above  $T_g$ , seem to lie along the same curve. From this result one may conclude that the  $r_{13}$  decay and the tan  $\delta$  peak arises from the same relaxation processes; i.e., they are associated with the dipolar chromophore disordering, the  $\alpha$  relaxation process in the copolymer. Furthermore, the  $\tau(T)$  vs 1/T dependence for the  $\alpha$ relaxation (Figure 6) clearly shows a deviation from Arrhenius behavior at high temperatures, indicating the fragile character<sup>12,27</sup> of MMA-DR13 glass former.

Results for the dependence of KWW b parameter on temperature, not shown here, reveal small changes in the investigated temperature range. From nearly constant at low temperatures it presents a small increase near  $T_g$  and stabilizes at higher temperatures. Generally speaking, one can say that, for both compositions, 98% of the values fall into the interval 0.50  $\pm$  0.06, and the value of b at  $T_{\rm g}$  is in the interval 0.55  $\pm$  0.05. The meaning for these values will be discussed in the next section. It should be pointed out that the shape of the electrooptic decay curves of Figure 4 is dependent on the sample particular aging process. As a consequence, the  $\tau$  and b parameters obtained from the fit of these data to KWW equation will be also dependent on aging, in such a way that these parameters are seen to increase as one goes from fast cooling to slow cooling from  $T_{\rm g}$ . Typically, for a decay at 60 °C,  $\tau$  can increase up to 1 order of magnitude as one goes from cooling at a rate of about 20 °C/min to about 0.2 °C/min, while b increases up to 1.5 times in the same conditions. However, a general equation accounting for the  $\tau(T)$  dependence in terms of the aging process can be found from the dielectric relaxation data obtained above  $T_g$ , as will be seen in the next section.

#### **IV. Discussions and Conclusions**

Before discussing the results, it is worthwhile to review here the approach usually employed to interpret the dependence of  $\tau(T)$  on T. It is known that  $\tau(T)$  is well accounted for by the WLF equation<sup>28</sup> within a temperature range from  $T_{\rm g}$  to ( $T_{\rm g}+100$  °C) while the Arrhenius equation<sup>16</sup> is suitable below  $T_{\rm g}$ . More general equations were obtained by Addam-Gibbs<sup>17</sup> (AG), when interpreting the relaxation process as the cooperative interaction due the packing of polymer segments as the temperature is decreased from above the glass transition, and by Tool-Narayanaswamy-Moynihan (TNM)<sup>29-33</sup> as a result of considering enthalpy relaxation in terms of a fictive temperature,  $T_{\rm f}$ , as a measure of departure from thermal equilibrium and accounting for the glass transition kinetic behavior. These concepts were reexamined by Hodge and Berens,34 resulting in the following equation, the Addam-Gibbs-Tool-Narayanaswamy-Moynihan (AG-TNM) equation, for the relaxation time temperature dependence:

$$\frac{\tau(T)}{\tau_{\rm g}} = \exp\left[-\frac{B}{T_{\rm g} - T_{\rm 0}} + \frac{B}{T_{\rm 0} - T_{\rm f}(T)}\right] \tag{4}$$

where  $\tau_g$  is the relaxation time measured at  $T_g$ , B is an activation temperature, BR, with R the universal gas constant, being an activation energy per mole, and  $T_0$ is the temperature at which the configurational entropy would be zero. For a process of a glass formation during a cooling process, at a constant cooling rate q from a temperature  $T_i$  above  $T_g$ , the fictive temperature can be determined by the following equation:<sup>34</sup>

$$T_{\rm f}(T) = T_{\rm i} + \int_{T_{\rm i}}^{T} \mathrm{d}T \left\{ 1 - \exp\left[ -\left(\frac{1}{q} \int_{T}^{T} \frac{\mathrm{d}T'}{\tau(T)}\right)^{b} \right] \right\}$$
 (5)

 $\tau(T)$  and b are the usual parameters in the KWW equation, and T and T' are the integration variables. Determination of  $T_f(T)$  requires a cumbersome procedure since b,  $\tau(T)$ , and the cooling/heating dynamics should be known in all temperature ranges. To circumvent such a difficulty, the  $\tau(T)$  dependence is habitually analyzed in two limit cases, since the exponential of eq

4 contains both the high- and the low-temperature behaviors of the WLF and Arrhenius equations, as follows:

(a) Limit Case—Above  $T_g$ . At the limit of high temperatures one has  $T_f \approx T$ , and eq 4 becomes:

$$\frac{\tau(T)}{\tau_{\rm g}} = \exp\left[-\frac{B}{T_{\rm g} - T_{\rm 0}} + \frac{B}{T - T_{\rm 0}}\right] \tag{6}$$

which is the Vogel-Fulcher-Tammann-Hesse<sup>35-37</sup> (VFTH) equation. It shows the same dependence of the WLF equation, given by:

$$\log\left(\frac{\tau(T)}{\tau_{\rm g}}\right) = -C_1^{\rm g} + \frac{C_1^{\rm g} C_2^{\rm g}}{T - T_0} \tag{7}$$

where  $C_1^g$  and  $C_2^g$  are constants. According to the free where  $C_1^a$  and  $C_2^a$  are constants. According to the free volume theory<sup>26</sup>  $C_1^g = b'/2.303f(T_g)$  and  $C_2^g = f(T_g)/\alpha_f$ - $(T_g)$ , where b' is a polymer dependent constant,  $f(T_g)$  is the free volume fraction, and  $\alpha(T_g)$  is the volumetric expansion coefficient both at  $T_g$ . It should be noted that as eq 7 is the logarithm form of eq 6, then  $B = 2.303 C_1^g C_2^g$  and  $T_0 = T_g - C_2^g .38$ (b) Limit Case—Below  $T_g$ . At the low-temperature limit the fictive temperature tends to a constant value

limit, the fictive temperature tends to a constant value,  $T_{\rm f} = T_{\rm f}'$ , and eq 4 becomes:

$$\frac{\tau(T)}{\tau_{\rm g}} \propto \exp\left[-\frac{B}{T\left(\frac{T_0}{T_{\rm f}'} - 1\right)}\right] \tag{8}$$

which has the same form as the Arrhenius equation.

Since the WLF behavior usually occurs above  $T_g$ , <sup>27</sup> one can infer that the  $C_1^g$  and  $C_2^g$  WLF parameters can be used in the AG-TNM equation. Such a parametrization has been successfully applied to polyimides functionalized with similar size NLO azo chromophres and allowed a complete relaxation description over more than 15 orders of magnitude in time.<sup>39</sup>

The fitting parameters of the experimental data, using the WLF equation (eq 7) for MMA-DR13(9 wt %) and MMA-DR13(43 wt %) copolymers, are displayed in Table 1. Results revealed that for both compositions the  $C_1^g$  parameters are basically the same and the  $C_2^g$ fall in the same range. Similar values of  $C_1^g$  means that a unique relaxation curve can be obtained if the relaxation time is plotted normalized to  $T_{\rm g}$ . In fact, eq 8 predicts this behavior if the final fictive temperature is set equal to  $T_{\rm g}$ . In this case, one obtains:<sup>40</sup>

$$\log \frac{\tau(T)}{\tau_{\sigma}} = C_1^{\rm g} \frac{T_{\rm g} - T}{T} \tag{9}$$

and normalization with respect to  $(T_{\rm g}-T)/T$  arises. The fitting curves obtained using the Arrhenius and VFTH functions are shown in Figure 7 by dashed and full lines, respectively, plotted as a function of  $(T_g - T)$ T. It should be noticed that eq 5 is expected to account

Table 1. Values of WLF Equation Parameters  $C_1^g$ ,  $C_2^g$ , and To Obtained from Fitting the Experimental Normalized Relaxation Times above  $T_{\rm g}$ 

MMA-DR13 (wt %)	$C_1^{\mathrm{g}}$	C <sub>2</sub> <sup>g</sup> (K)	$T_0$ (K)
9	$12\pm2$	$40\pm10$	$350\pm20$
43	$12\pm2$	$50\pm10$	$340\pm20$

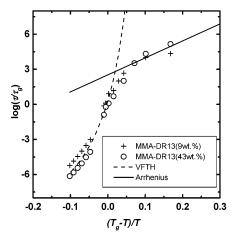
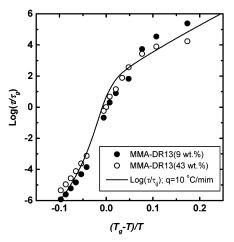


Figure 7. Plot of relaxation times (normalized to  $\tau_{g}$ ) as a function of the parameter  $(T_{\rm g}-T)/T$ , for both MMA–DR13-(9%) and MMA–DR13(43%) samples, and fitting curves to WLF and Arrhenius equations.



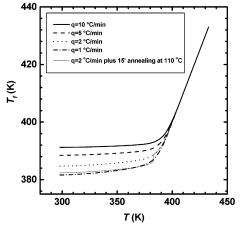
**Figure 8.** Result from fitting of experimental data to the AG-TNM equation for both MMA-DR13(9%) and MMA-DR13-(43%) samples.

for the kinetics of the glass formation for a particular cooling process, in such a way that when introduced into eq 8 one expects to fit the experimental data in the region near  $T_{\rm g}$ . This is shown by the full line in Figure 8, which is the curve obtained with the AG-TNM equation using  $C_1^g$  and  $C_2^g$  parameters listed in Table 1, a cooling rate of 10 °C/min, and the KWW b parameter equal to 0.5, which is the average value in the temperature range used in the experiments. Fitting results indicate that a good prediction of the orientational stability of NLO chromophores in MMA-DR13 copolymers can be achieved.

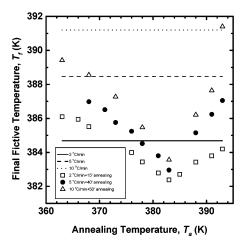
The orientational stability can be better understood using eq 8, as the B parameter is related to the Arrhenius activation energy,  $E_a$ , of the primary  $\alpha$ relaxation, responsible for randomization of the chromophore orientation. The expression for  $E_{\alpha}$  in terms of the final fictive temperature  $T_f$  follows from eq 8:

$$E_{\rm a}(T) = \frac{2.303 \, C_1^{\rm g} \, C_2^{\rm g}}{1 - \frac{T_0}{T_{\rm f}'}} \tag{10}$$

To finish this point, the analysis performed above is used to predict the thermal treatment process that leads to the lowest final fictive temperature  $T_f$  as close as



**Figure 9.** Fictive temperature,  $T_{\rm f}$ , temperature dependence, for different thermal treatments.



**Figure 10.** Final fictive temperature,  $T_f$ , vs annealing temperature,  $T_a$ , for several annealing times and cooling rates. The horizontal lines indicate the final fictive temperatures achieved for the cooling rates of 2, 5, and 10 °C/min.

possible to the  $T_0$  value. In Figure 9 the fictive temperature dependence on the cooling rate for MMA-DR13-(43 wt %), calculated from eq 5, using b = 0.5, is shown. As one can expect, the lower the cooling rate is, the lower the final fictive temperature is, and a more stable glass can be obtained. Low cooling rate requires a long time exposure of the sample to the corona discharge, leading to the surface sample deterioration. Previous results obtained for the MMA-DR13 copolymers indicated that the exposure of the sample to the corona discharge should not exceed much more than 60 min to minimize sample damage.<sup>4</sup> Consequently, cooling rates smaller than 2 °C/min should be avoided, as the exposure will exceeds the maximum allowed. Indeed, at a cooling rate of 2 °C/min, the cooling process will take about 45 min, which seems to be fine. However, further thermal stability of the copolymer can be achieved if one includes an annealing step during the cooling process at a given rate. The main concern here is to find the optimum annealing temperature for a given time interval, compatible with the advisable for maximum corona exposure of about 60 min. For this purpose the final fictive temperature has been calculated at chosen cooling rate for different annealing temperatures and times. The calculation follows from eq 5, which has to be modified to include an annealing step.<sup>39</sup> The plot of final fictive temperatures as a function of the annealing temperature is shown in Figure 10. The curves show a minimum around 110 °C, indicating that this value is the ideal one to perform the annealing. The lowest final fictive temperature is reached for a cooling rate of 2 °C/min and annealing at 110 °C for 15 min. The  $T_f$  value in this case is 109 °C, lower than that one achieved when cooling at 2 °C/min and close to the one achieved when cooling at 1 °C/min (Figure 9). The total time of exposure to the corona discharge process will be in this case of 65 min, which guarantees minor sample surface damage.

As a measure of the fragile characteristic of MMA-DR13, revealed in the plot of Figure 6, one can estimate the fragility index, defined in terms of the WLF equation as:41

$$m_{\text{WLF}} = \left[ \frac{\partial (\log(\tau/\tau_g))}{\partial (T_g/T)} \right]_{T=T_g}$$
 (11)

which according to eq 9 gives:

$$m_{\rm WLF} = \frac{C_1^{\rm g}}{C_2^{\rm g}} T_{\rm g} \tag{12}$$

From this equation, considering the values of  $C_1^g$  and  $C_2^g$  in Table 1 and those of  $T_g$ , one obtain the fragility indexes of 120  $\pm$  50 and 90  $\pm$  40 for MMA-DR13(43 wt %) and MMA-DR13(9 wt %), respectively. The large values confirm the fragile MMA-DR13 glass former is. The replacement of the (-COOCH<sub>3</sub>) group by the chromophore group in the side chain seems confer a less fragile behavior since the index is lower than that of PMMA, which is 145.41

The fragility of the glass former has been correlated with the KWW stretching b parameter.<sup>41</sup> The general trend is that a glass former presenting large values of b tend to present fragile behavior, i.e., a small fragility index. In this way one may expect larger values of b parameter for MMA-DR13 than that obtained for PMMA, although both polymeric systems have similar glass transition temperatures. The values of b at the glass transition temperature are claimed to be dominated by the numbers 0.43 and 0.6 respectively associated with long-range Coulombic interactions and shortrange interactions.<sup>13</sup> As a consequence, the expected values for long-chain polymeric systems would be of 0.43, accounting for long-range Coulombic intrachain interactions associated with the backbone relaxation. However, exceptions are known for polymeric chains having side groups that somehow actively participate in the relaxation process. Normally, side groups are known to increase the interchain interactions since they act as spacers or even add rotational mode to the interchain interaction.<sup>13</sup> In this situation  $b(T_g)$  is expected to be closer to the short-range forces limit, i.e., 0.6. This seems to be the case for MMA-DR13 copolymer with  $b(T_{\rm g})$  of 0.55  $\pm$  0.05. This effect should indeed be remarkable in MMA-DR13, since in PMMA  $b(T_g)$ falls in opposite side with a value of 0.34.41 This result is consistent with a strong contribution of the chromophore group for the primary  $\alpha$  relaxation.

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