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Theoretical investigations on phase stability, elastic constants and electronic structures of $D0_{22}$ - and $L1_2$ -Al₃Ti under high pressure

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ABSTRACT

Phase stability, elastic and thermodynamic properties, and electronic structure of titanium trialuminide (Al_3Ti) with Ll_2 and $D0_{22}$ structures under pressure up to 40 GPa have been investigated using first-principles calculations. The equilibrium structure and formation energy show that $L1_2$ - Al_3Ti is stable when the pressure is higher enough, approximately above than 20–30 GPa. The elastic constants, anisotropy index and Debye temperature of both phases increase with the pressure going up, and $L1_2$ - Al_3Ti has better ductility, smaller anisotropy and lower Debye temperature than $D0_{22}$ - $A1_3Ti$. The pressure-induced Ti-3d delocalization can strengthen its orbital hybridization with Al(s,p), which leads to stronger atomic bonding, and subsequently makes the $L1_2$ - Al_3Ti more stable under high pressure.

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1. Introduction

Titanium trialuminide (Al₃Ti) has many attractive characteristics, such as low density (\sim 3.3 g/cm³), high melting temperature (~1623 K), good oxidation resistance, high hardness, and large elastic modulus [1,2]. Although this intermetallic has these promising characteristics, actually, bulky Al₃Ti is hardly used as structural material, which mainly caused by its poor ductility and toughness, and this is commonly ascribed to its insufficient slip systems in its tetragonal D0₂₂ structure (space group I4/mmm) [1,3-6]. Recently, many experimental and theoretical studies have been undertaken in attempts to fulfil the structure transition from tetragonal D0₂₂-Al₃Ti to cubic L1₂-Al₃Ti for the purpose of increasing its slip systems. According to the literatures, adding ternary elements, especially transition metals, such as Fe, [7-10] Mn, [1,9-11] Cr, [1,7,9,10,12,13] Co, [9,10] Ni, [8-10] Cu, [8,9] Zn, [14] Zr, [15] V, [7] and La [16], is suggested as a possible route to the structure transformation, and consequently improve the ductility of A1₃Ti-based alloys.

Although the phase stabilizing effect and the $L1_2$ structure transition by adding ternary element for Al_3Ti have been discussed extensively, in further consideration, the effect of high pressure on the phase stability should be discussed, and the influence of

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phase stability under high pressure can be investigated by performing first-principles calculations [17–20]. However, according to our knowledge, there is scarcely report about the pressure-induced structural transition for Al_3Ti up to now. In this paper, an investigation on phase stability, elastic properties and atomic bonding of Al_3Ti under high pressure was performed using first-principles calculations. The formation energy, elastic constants and electronic structure of $D0_{22}$ - and $L1_2$ - Al_3Ti under the pressure range of 0–40 GPa were calculated.

2. Computational methodology

The first-principles calculations presented in this paper were accomplished using the CASTEP code (Cambridge Sequential Total Energy Package) [21,22], which was based on density functional theory (DFT), a plane-wave basis set was employed for the electronic wave-function expansion [23,24]. The core-valence interactions were described as ultra-soft pseudo-potentials (USPPs) [25]. The exchange correlation energy was treated with three different functionals; generalized gradient approximation (GGA) functionals of PBE [26] and PW91 [27,28], and local density approximation (LDA) CAPZ functional of Ceperley and Perdew et al. [29,30]. The valence electron configurations of Al $3s^23p^1$ and Ti $3s^23p^63d^24s^2$ are considered. The kpoints were set as $25\times25\times25$ and $40\times40\times22$ for bulk fcc-Al and hcp-Ti, and $20 \times 20 \times 20$ and $20 \times 20 \times 10$ for bulk A1₃Ti with L1₂ and D0₂₂ structures respectively, which makes the separation of the reciprocal space around 0.01 ${\rm \AA}^{-1}$, the cutoff energy on the plane wave basis was set as 350 eV, and the self-consistent field (SCF) tolerance was set as 5×10^{-7} eV/atom. The convergence tests have been tested, and the above parameters are also accordance with the previous studies [31-33]. The crystal supercell geometries were fully optimized, and their ground states were obtained, in which the Broyden-Fletcher-Goldfarb-Shanno

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 $\begin{tabular}{ll} \textbf{Table 1} \\ \textbf{Crystallographic data, lattice constants of bulk Al, Ti and Al_3Ti.} \\ \end{tabular}$

Phase	Space group (#)	Pearson symbol	Strukturbericht designation	Lattice constants (Å)		
				Present Calc.	Expt.	
fcc-Al	Fm-3m(225)	cF4	A1	$a = 4.0484^{a}$ $a = 4.0510^{b}$ $a = 3.9674^{c}$	a = 4.049 [46]	
hcp-Ti	P6 ₃ /mmc(194)	hP2	A3	a = 2.9422, $c = 4.6563$ ^a a = 2.9374, $c = 4.6464$ ^b a = 2.8672, $c = 4.5397$ ^c	<i>a</i> = 2.944, <i>c</i> = 4.669 [46]	
Tetragonal Al ₃ Ti	I4/mmm(139)	tI8	D0 ₂₂	a = 3.8507, c = 8.6332 ^a a = 3.8497, c = 8.6325 ^b a = 3.7678, c = 8.4618 ^c	<i>a</i> = 3.8537, <i>c</i> = 8.5839 [47]	
Cubic Al₃Ti	Pm-3m(221)	cP4	L1 ₂	$a = 3.9854^{a}$ $a = 3.9842^{b}$ $a = 3.8997^{c}$	<i>a</i> = 3.967–4.05 [35]	

^a The calculations with GGA-PBE exchange correlation functional in this work.

minimization scheme [34] was used to minimize the total energy and interatomic force on each atom to the convergence level of 5×10^{-6} eV/atom and 0.01 eV/Å, respectively.

In the present study, the crystal structures of Al₃Ti were built based on the data of previous experiments and calculations [31,35,36]. After fully optimizations, the calculated equilibrium lattice constants and previous experimental data are listed in Table 1, the elastic constants and formation energy $\Delta E_f(Al_3Ti)$ are listed in Table 2. The lattice constants calculated with LDA-CAPZ potential is rather smaller than the results of GGA-PBE and GGA-PW91, which indicates the "over-binding effect" reported in other LDA calculations [37–41]. The equilibrium lattice constants calculated with GGA-PBE functional are most close to the previous experimental data in Table 1. In Table 2, the GGA-PBE results of elastic constants have better agreements with previous theoretical results [42-44] and experimental data [45] than the results calculated with GGA-PW91 and LDA-CAPZ functionals. For the DO22 structure, by comparing GGA-PBE calculated elastic constants with experimental data [45], it shows very good agreement (less than 5.2%) for the values of C_{13} , C_{33} and C_{44} . However, the deviation of C_{11} , C_{12} and C_{66} comparing with the experimental data are slightly larger, the errors are about 12.5%, 43.9% and 8.0%, respectively. Furthermore, it is worthy to note that the same tendency exists in the previous calculations [42-44].

3. Results and discussion

3.1. Phase stability and formation energy

The formation energy ΔE_f (Al₃Ti) per atom is defined by the following equation [52]:

Table 2 Elastic constants and formation energy
$$\Delta E_f$$
 (Al₃Ti) of $L1_2$ - and $D0_{22}$ -Al₃Ti.

$\Delta E_f(Al_3Ti) = \frac{1}{4} [E_{total}(Al_3Ti) - 3E_{bulk}(Al) - E_{bulk}(Ti)],$	(1)
--	-----

where Etotal(Al₃Ti) is the total energy per formula of equilibrium Al₃₋ Ti structure; $E_{\text{bulk}}(Al)$, and $E_{\text{bulk}}(Ti)$ are the total energy per atom of fully relaxed fcc-Al and hcp-Ti, respectively. After the structures fully optimized, the formation energy of both phases under zero temperature and various pressure ranging from 0 to 40 GPa have been calculated, the results are summarized in Table 3. The results calculated with GGA-PBE and PW91 are very similar (the max numerical error of formation energy is only 3% for Ll₂-Al₃Ti under 5 GPa), and their results agree well with previous calculations [35,43,48,49], however, the LDA results differs vastly with the GGA results (the max numerical error of formation energy is 60% for D0₂₂-A1₃Ti under 5 GPa). That suggests the numerical errors of formation energy strongly depends on the exchange-correlation functional [53]. And from Table 2, one can further find that the formation energies under 0 GPa calculated with GGA-PBE and GGA-PW91 are more close to the experimental data [50] (the deviations are about 2%), and LDA-CAPZ calculated result has the largest deviation of more than 4%. The large errors of LDA formation energy calculations are due to the overestimation of local density approximation method [51].

Phase	Elastic prop	Elastic properties (GPa)								
	C ₁₁	C ₁₂	C ₁₃	C ₃₃	C ₄₄	C ₆₆	B ₀			
D0 ₂₂ -Al ₃ Ti	190.39	83.05	43.14	214.68	92.24	125.85	103.69	-38.280 ^b		
	190.49	81.44	42.47	211.09	90.60	123.35	102.61	-38.378^{c}		
	210.85	92.43	46.28	240.61	104.74	143.73	114.60	-40.816^{d}		
	192.3	82.7	44.9	212.5	93.0	128.4	103.3	-38.895 [43] ^e		
	194.5	87.9	47.6	219.8	93.8	129.5	108.3 [42] ^e	-39.30 [35] ^e		
	192	84	49	216	94	122	107 [44] ^e	-39.505 [48] ^e		
	_	_	_	_	_	_	- ' '	-38.11 [49] ^e		
	217.7	57.7	45.5	217.5	92.0	116.5	105.6 [45] ^f	$-39.2 [50]^{f}$		
L12-Al3Ti	184.40	64.21	_	_	74.61	_	104.27	-35.499 ^b		
	184.32	62.41	_	_	72.89	_	103.05	−35.741 ^c		
	207.54	69.05	_	_	87.29	_	115.21	-38.609^{d}		
	183.9	62.6	_	_	73.5	_	103.6	-36.583 [43] ^e		
	190.2	67.5	_	_	77.0	_	108.4 [42] ^e	-35.651 [51] e		
	192	65	_	_	74	_	107 [44] ^e	-36.614 [48] ^e		
	_	_	_	_	_	_	- ' '	-35.35 [49] ^e		

- ^a For the calculation of formation energy, the reference states are fcc-Al and hcp-Ti under 0 K and 0 GPa.
- ^b Calculations with GGA-PBE functional in this work under 0 K and 0 GPa.
- $^{
 m c}$ Calculations with GGA-PW91 functional in this work under 0 K and 0 GPa.
- $^{\rm d}\,$ Calculations with LDA-CAPZ functional in this work under 0 K and 0 GPa.
- ^e Other first-principle calculation results at zero temperature.
- f Experimental results at ambient temperature and pressure.

^b The calculations with GGA-PW91 exchange correlation functional in this work.

^c The calculations with LDA-CAPZ exchange correlation functional in this work.

Table 3 The total energy E_{total} , formation energy ΔE_{f_0} lattice constants and equilibrium volume V_0 of $L1_2$ - and $D0_{22}$ -Al₃Ti under various pressures and temperature T = 0 K^a.

Pressure (GPa)	0	5	10	15	20	25	30	35	40
D0 ₂₂ -Al ₃ Ti									
a (Å)	3.8507	3.7959	3.7495	3.7092	3.6733	3.641	3.6116	3.5846	3.5596 ^b
	3.8497	3.7948	3.7482	3.7079	3.6720	3.6396	3.6102	3.5831	3.5579 ^c
	3.7678	3.7192	3.6770	3.6401	3.6069	3.5769	3.5494	3.5240	3.5005 ^d
c (Å)	8.6332	8.5012	8.3908	8.2953	8.2120	8.1376	8.0695	8.0077	7.9504 ^b
	8.6325	8.4978	8.3867	8.2906	8.2071	8.1322	8.0642	8.0026	7.9458 ^c
	8.4618	8.3437	8.2438	8.1563	8.0786	8.0087	7.9454	7.8870	7.8330 ^d
c/a	2.242	2.240	2.238	2.236	2.236	2.235	2.234	2.234	2.234 ^b
	2.242	2.239	2.238	2.236	2.235	2.234	2.234	2.233	2.233 ^c
	2.246	2.243	2.242	2.241	2.240	2.239	2.239	2.238	2.238 ^d
V_0 (Å 3 /atom)	16.002	15.311	14.746	14.266	13.851	13.485	13.157	12.862	12.592 ^b
	15.992	15.297	14.728	14.248	13.832	13.466	13.138	12.843	12.573 ^c
	15.016	14.426	13.932	13.509	13.138	12.808	12.512	12.244	11.997 ^d
ΔE_f (kJ/mol)	-38.280	8.800	54.000	97.636	139.932	181.068	221.151	260.300	298.600 ^b
	-38.377	8.659	53.811	97.392	139.630	180.699	220.723	259.812	298.053 ^c
	-40.816	3.456	44.910	86.184	126.269	165.304	203.399	240.650	277.126 ^d
L1 ₂ -Al ₃ Ti									
a (Å)	3.9854	3.9281	3.8792	3.8368	3.7992	3.7653	3.7345	3.7062	3.6801 ^b
	3.9842	3.9264	3.8773	3.8350	3.7972	3.7634	3.7326	3.7043	3.6782 ^c
	3.8997	3.8480	3.8038	3.7649	3.7301	3.6986	3.6698	3.6433	3.6186 ^d
V_0 (Å ³ /atom)	15.825	15.153	14.594	14.120	13.709	13.346	13.021	12.727	12.460 ^b
	15.812	15.132	14.573	14.100	13.688	13.325	13.001	12.708	12.441 ^c
	14.826	14.245	13.759	13.341	12.974	12.648	12.356	12.090	11.846 ^d
ΔE_f (kJ/mol)	-35.499	11.016	55.746	98.932	140.792	181.492	221.161	259.902	297.801 ^b
-	-35.741	10.694	55.358	98.481	140.276	180.914	220.518	259.198	297.039 ^c
	-38.609	5.100	46.025	86.782	126.367	164.913	202.531	239.310	275.326 ^d

- ^a For the calculation of formation energy, the reference states are fcc-Al and hcp-Ti under the pressure and zero temperature.
- ^b Calculations with GGA-PBE functional in this work.
- ^c Calculations with GGA-PW91 functional in this work.
- ^d Calculations with LDA-CAPZ functional in this work.

Although the exchange correlation functionals have an influence on the formation energy calculation, some valuable points can still be deduced. First, the formation energy will increase, while the lattice constants and volume will decrease along with the pressure increasing. Second, the formation energies of $D0_{22}$ -A1 $_3$ Ti are smaller than the ones of $L1_2$ -A1 $_3$ Ti when the pressure is below 20 GPa, while the opposite situation exists when the pressure is above 30 GPa. In the range of 20–30 GPa, the difference between the formation energies of both structures depends on the exchange correlation functionals. Which suggests the $L1_2$ -A1 $_3$ Ti will be more stable when the pressure is higher enough, approximately above than 20–30 GPa.

Actually, the Gibbs free energy should be used to compare the phase stability between the both structures, because all calculations in our work are performed under the temperature T=0 K, so the relative stability of different structures can be deduced from the pressure dependence on enthalpy [54,55]. The enthalpy difference per formula $H(L1_2)$ - $H(D0_{22})$ under various pressure are calculated and shown in Fig. 1. The pressure corresponding to $H(L1_2)$ - $H(D0_{22})$ approaching zero is the transition pressure, it shows that the $D0_{22}$ -Al $_3$ Ti will transform to the $L1_2$ structure when the pressure is over ~ 30 GPa, ~ 28 GPa, ~ 21 GPa calculated with functionals of GGA-PBE, GGA-PW91, LDA-CAPZ, respectively. It is consistent with the above conclusion deduced from the formation energies under various pressures. And there are volume drop per atom of $\Delta V/V = 1.0-1.2\%$ with the three different functionals as shown in Fig. 2.

3.2. Elastic constants and thermodynamic properties

The elastic constants of solids have a direct relation to their mechanical and thermodynamic properties. Commonly, the single crystal's elastic constants C_{ij} can be obtained by calculating the total energy as a function of appropriate strains [42–44]. To calculate the elastic constants, a serial of deformed cells (strain) are introduced and optimized to calculate the tensor of elastic constants.

The elastic strain energy U of a deformed crystal cell is given as [56]:

$$U = \frac{\Delta E}{V_0} = \frac{1}{2} \sum_{ij} C_{ij} e_i e_j \tag{2}$$

where ΔE is the energy difference of deformed cell relative to the unstrained cell, V_0 is the volume of the equilibrium cell without any deformation, C_{ij} s are the elastic constants, e_i and e_j are strain.

For the $L1_2$ structure, there are three independent elastic constants: $C_{11} = C_{22} = C_{33}$, $C_{12} = C_{13} = C_{23}$, $C_{44} = C_{55} = C_{66}$; for the $D0_{22}$ structure, there are six independent constants: $C_{11} = C_{22}$, C_{12} , $C_{13} = C_{23}$, C_{33} , $C_{34} = C_{55}$, C_{66} . The obtained monocystal quantities,

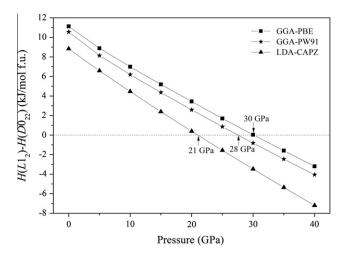


Fig. 1. Calculated enthalpy difference of $L1_2$ -Al $_3$ Ti relative to the $D0_{22}$ structure as a function of pressure, the structural transition point induced by pressure are marked by arrows.

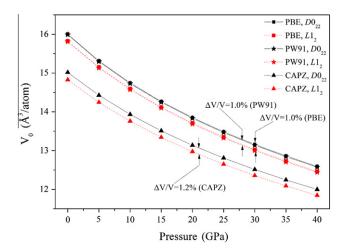


Fig. 2. Calculated volume–pressure relationship for $D0_{22^-}$ and $L1_2$ -Al₃Ti with different exchange correlation functionals.

such as these elastic constants, cannot accurately stand for the properties of polycrystalline materials, so they should be further calculated and rectified. The polycrystalline mechanical quantities, such as bulk modulus (B), shear modulus (G), Young's modulus (E), Poisson's ratio (v), can be calculated from these independent elastic constants.

There are three different algorithms corresponding to different bound to calculate these polycrystalline mechanical quantities: the Voigt bound is obtained by the average polycrystalline modules based on an assumption of uniform strain throughout a polycrystal, and it is the upper limit of the actual effective modules; while the Reuss bound is obtained by assuming a uniform stress, and it is the lower limit of the actual effective modules; the arithmetic average of Voigt and Reuss bounds is termed as the Voigt-Reuss-Hill approximation. The formula for calculating these mechanical quantities can be given as follows: (1) for the cubic $L1_2$ structures, $B_V = B_R = (C_{11} + 2C_{12})/3$, $G_V = (C_{11} - C_{12} + 3 C_{44}$ //5, $G_R = 5(C_{11} - C_{12})C_{44}/[4C_{44} + 3(C_{11} - C_{12})][57]$, (2) for the tetragonal $D0_{22}$ structures, $B_V = (1/9)[2(C_{11} + C_{12}) + C_{33} + 4C_{13}], B_R = C^2/M$, $G_V = \frac{(1/30)(M + 3C_{44} - 3C_{42} + ce:hsp - sp="0.25"/>12C_{44} + 6C_{66})}{(1/30)(M + 3C_{44} - 3C_{42} + ce:hsp - sp="0.25"/>12C_{44} + 6C_{66})}$ $G_R = 15[(18B_V/C^2) + [6/(C_{11} - C_{12})] + (6/C_{44}) + (3/C_{66})]^{-1}; M = C_{11} + C_{12}$ $\epsilon_{12} + 2\epsilon_{33} - 4\epsilon_{13}$, $\epsilon^2 = (\epsilon_{11} + \epsilon_{12})\epsilon_{33} - 2(\epsilon_{13})^2$ [58], and (3) for the Voigt-Reuss-Hill approximation, $B_H = (1/2)(B_V + B_R)$, $G_H = (1/2)(G_V + G_R)$, the sub letter of V, R and H denote Voigt, Reuss bound and Hill approximation, respectively. The B_H and G_H are adopted in this paper to calculate Young's modulus *E* and Poisson's ratio *v* by the following formulas: $E = \frac{9BG}{(3B + G)}$, $v = \frac{(3B - 2G)}{[2(3B + G)]}$ [59].

The elastic constants of $L1_2$ - and $D0_{22}$ -Al $_3$ Ti under 0 GPa are calculated with GGA-PBE, GGA-PW91 and LDA-CAPZ functionals, the results and other experimental and computational data are

presented in Table 2. As aforementioned, there are slightly large deviations between the experimental data [45] and our GGA-PBE calculated values of C_{11} , C_{12} and C_{66} for $D0_{22}$ -Al₃Ti, however, comparing with other theoretical calculations [42,44], the agreements of GGA-PBE results are reasonable and acceptable. Besides that, Al₃Ti lattice constants and elastic constants under 0 GPa calculated with GGA-PBE are more closer to the experimental data (refers Table 1). As the further step, the elastic constants under high pressure in the range of 5-40 GPa are also calculated with GGA-PBE functional, and the results are listed in Table 4. The elastic constants and mechanical moduli increase with the pressure increasing, which indicates the materials will be stiffer and more difficult to be compressed with pressure increasing. The hardness and brittleness of the compounds also have a relation to the B/G value: according to Pugh's criterion [60], the compound with larger B/G ratio (> \sim 1.75) usually is ductile, and with smaller *B*/*G* ratio ($<\sim$ 1.75) usually is brittle, thus, $L1_2$ -Al₃Ti should exhibit better ductility than DO₂₂-Al₃Ti, and both structures will have larger ductility under high pressure than ambient pressure.

Elastic anisotropy index A^U for crystal with any symmetry was proposed by Ranganathan and Ostoja-Starzewski [61],

$$A^{U} = 5\frac{G_{V}}{G_{R}} + \frac{B_{V}}{B_{R}} - 6 \geqslant 0 \tag{3}$$

Zero value of A^U denotes isotropic single crystals, and the deviation from zero defines the extent of this crystal's anisotropy. For cubic symmetry, the relationship between the commonly used Zener anisotropy ratio A and A^U can be defined as $A^U = (6/5)(\sqrt{A} - 1/\sqrt{A})^2$. The results of $L1_2$ - and $D0_{22}$ -Al₃Ti calculated as per the equation are listed in Table 4. It shows $L1_2$ -Al₃Ti has more isotropic features than $D0_{22}$ -Al₃Ti, and the both structures' isotropy decrease with the pressure increasing.

Debye temperature (Θ_D) is a fundamental parameter for the materials' thermodynamic properties, and it is correlated with many physical properties such as specific heat, elastic constants and melting temperature. The experimental value of a solid usually can be calculated from the sound velocity [62]. In this paper, Debye temperatures of $L1_2$ - and $D0_{22}$ -Al₃Ti under ambient and high pressure are estimated with the elastic constant data. Θ_D may be estimated from the averaged sound velocity by the following equation [62]:

$$\Theta_D = \frac{h}{k} \left[\frac{3n}{4\pi} \left(\frac{N_A \rho_0}{M} \right) \right]^{\frac{1}{3}} v_m \tag{4}$$

where h is the Planck's constant, k is Boltzmann's constant, N_A is the Avogadro constant, n is the atoms number per molecule, M is the molecular weight, and ρ_0 is the density, respectively. The average sound velocity v_m can be calculated as follows:

Table 4 Elastic constants C_{ij} , bulk modulus B, shear modulus G, Young's modulus E (all in GPa), Poisson's ratio and Elastic anisotropy index A^U of $L1_2$ - and $D0_{22}$ -Al₃Ti under various pressures.

Pressure (GPa)	$D0_{22}$ -Al ₃ Ti					$L1_2$ -Al $_3$ Ti				
	0	10	20	30	40	0	10	20	30	40
C11	190.4	241.8	287.8	330.5	370.6	184.4	240.9	292.1	339.8	385.6
C12	83.1	119.7	154.4	188.1	220.7	64.2	93.3	120.5	146.5	171.9
C13	43.1	69.2	94.2	118.4	142.3	_	_	_	_	_
C33	214.7	279.4	342.1	391.8	442.6	_	_	_	_	_
C44	92.2	118.8	142.3	163.6	183.4	74.6	102	126.8	149.4	170.6
C66	125.8	161.8	193.8	223.3	250.6	_	_	_	_	_
В	103.7	142.1	178.1	211.4	243.8	104.3	142.5	177.7	210.9	243.1
G	87.2	108.1	126.2	141.8	156.1	68.4	89.6	108.4	125.5	141.4
E	204.3	258.6	306.3	347.6	385.9	168.4	222.2	270.3	314.1	355.4
ν	0.17	0.2	0.21	0.23	0.24	0.23	0.24	0.25	0.25	0.26
B/G	1.19	1.31	1.41	1.49	1.56	1.52	1.59	1.64	1.68	1.72
A^U	0.39	0.53	0.66	0.77	0.88	0.06	0.13	0.19	0.23	0.27

Table 5 Debye temperature Θ_D of $L1_{2^-}$ and $D0_{22}$ -Al₃Ti under various pressures.

Pressure (GPa)	0	10	20	30	40
Θ_D of $D0_{22}$ -Al ₃ Ti (K)	664.2	731.4	783.6	824.5	859.9 ^a
	558.29	649.36	716.25 ^b	-	-
Θ_D of $L1_2$ -Al ₃ Ti (K)	591.0	668.0	727.7	776.7	819.0 ^a

- ^a Calculations with GGA-PBE elastic constants of this work.
- ^b Previous calculation of Ref. [49].

$$\upsilon_m = \left[\frac{1}{3}\left(\frac{2}{\upsilon_s^3} + \frac{1}{\upsilon_l^3}\right)\right]^{-1/3}, \text{ and } \upsilon_l = \left(\frac{3B + 4G}{3\rho_0}\right)^{1/2}, \upsilon_s = \left(\frac{G}{\rho_0}\right)^{1/2} \ \ \, (5)$$

where v_l and v_s are the longitudinal and shear sound velocities, respectively. The Debye temperatures of $L1_2$ - and $D0_{22}$ -Al $_3$ Ti are calculated from the aforementioned values of the lattice parameters, the bulk modulus and shear modulus, and the results are listed in Table 5

Nakamura and Kimura [45] calculated the Debye temperature of $D0_{22}$ -Al $_3$ Ti by measuring the velocity of ultrasonic waves at ambient pressure and temperature, and the value was 681 K. Because $L1_2$ -Al $_3$ Ti is metastable, its experimental Debye temperature can be hardly found in the literatures, Witczak et al. [63] measured the Θ_D of $L1_2$ Al $_5$ CrTi $_2$ with ultrasonic pulse-echo method, their experimental value was 588 K. Our results of Θ_D at ambient pressure are in good accordance with these experimental literatures [45,63]. Boulechfar et al. [49] calculated the Θ_D of $D0_{22}$ - and $L1_2$ -A1 $_3$ Ti under 0–20 GPa using first principles method, the results are listed in Table 5, and our results have acceptable agreements with their data.

In Debye theory, the Θ_D is the temperature of a crystal's highest normal mode of vibration, i.e., the highest temperature that can be achieved due to a single normal vibration. One can find that the Debye temperatures of both structures will increase with the pressure increasing, which indicates that the normal vibration of both crystals will enhance when the pressure increases. The $D0_{22}$ -Al₃Ti has higher Θ_D than $L1_2$ -Al₃Ti, and the gap of Θ_D between the both phases decrease with the pressure increasing.

3.3. Electronic structure and atomic bonding

For a deeper insight into the atomic bonding and electronic structure of $A1_3$ Ti under high temperature, the valence electron

density distribution, density of states (DOS) and partial density of states (PDOS) are investigated with GGA-PBE functional. Fig. 3a-d illustrate the valence electron distribution of $L1_2$ -A 1_3 Ti and $D0_{22}$ -A 1_3 Ti along (110) plane under 0 GPa and 40 GPa, respectively. The PDOS of $L1_2$ -A 1_3 Ti under 0 GPa and 40 GPa are presented in Fig. 4. The Γ point band composition of both phases under 0 GPa and 40 GPa are listed in Table 6.

The valence charge density distribution (Fig. 3) shows that both structures at 40 GPa have a strengthened valence electron interaction than at 0 GPa. The bonding charges of L_2 -A1₃Ti mainly locate at tetrahedral interstices along $\langle 111 \rangle$ directions, it is because the nearest-neighbor atoms of Ti-site leads to Ti-d hybridization around its local field [49,51,64]. And bonding charges of D_{22} -Al₃Ti mainly locate along its $\langle 112 \rangle$ directions caused by the d orbital hybridization [49,51,64].

The PDOS plots of Ll₂-A1₃Ti (Fig. 4) indicate that the left part of total DOS (below Fermi lever) is mainly contributed from Al atom, namely Al-3s and Al-3p, while the right part mainly comes from Ti atom, especially Ti-3d. Furthermore, the resonant peaks of PDOS plots can also confirm that the bonds of L1₂-Al₃Ti are mainly contributed from the electron orbitals hybridization of Ti-3d and Al(s,p) states [49,51,64]. By comparing DOS plots of $L1_2$ -A1₃Ti under 0 GPa and 40 GPa, one can easily find that the energy range of DOS under 40 GPa is widened, and has a shallower "valley" around Fermi level than the one under 0 GPa. Simultaneously, the PDOS of Al under 40 GPa shifts towards lower energy, while the PDOS of Ti under 40 GPa shifts towards higher energy, and the peak of Ti-3d around 2 eV under 40 GPa is lower than the one under 0 GPa. Considering the widened energy range, shallower "valley" and lower peak denote more non-localized features, and the wider bandwidth, especially the wider conduction band, denotes more "free electrons", one can know that the structure under 40 GPa has more metallic features than it at 0 GPa, thus, a better electrical conductivity of L1₂-Al₃Ti under high pressure will be anticipated.

Further, according to the Ti PDOS under 40 GPa shifts towards higher energy, and it has a lower peak than the one under 0 GPa, it is reasonable to conclude that pressure-induced delocalization of Ti electrons, especially Ti-3d, which strengthens the electron hybridization and atomic bonding between Ti and Al atoms. And subsequently, it improves the phase stability of $L1_2$ -Al₃Ti, even though the phase exhibits more metallic features with the pressure increasing.

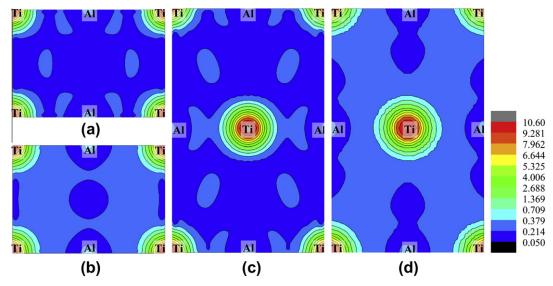


Fig. 3. Valence charge density $(e/Å^3)$ distribution of $L1_2$ - and $D0_{22}$ -Al₃Ti under 0 GPa and 40 GPa along (110) plane: (a) $L1_2$, 0 GPa; (b) $L1_2$, 40 GPa; (c) $D0_{22}$, 0 GPa, (d) $D0_{22}$, 40 GPa

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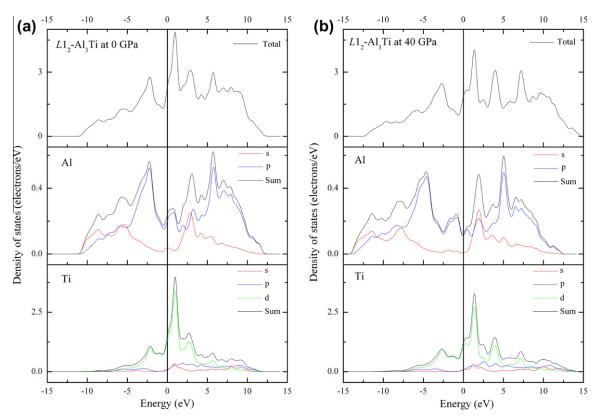


Fig. 4. Density of states (DOS) of L1₂-Al₃Ti under (a) 0 GPa and (b) 40 GPa.

From Table 6, the compositions for the lowest Γ point state of both structures are dominated by Al-s, and for $D0_{22}$ -A1₃Ti, it is specifically the s component of Al2. From the second to fourth lowest Γ point states of both structures, and the fifth Γ point states of $D0_{22}$ -A1₃Ti, they are dominated by the hybridization of Al-p and Ti-d. and the sixth Γ point states (the first unoccupied state) of $D0_{22}$ -A1₃Ti is mainly composed by Ti-d. The above

features are consistent with the previous calculation [51]. More important is that, except for the fourth lowest state of both structures, all Ti-d components at Γ point under 40 GPa increase comparing with 0 GPa, which indicates the quantity and the hybridization of Ti-3d will be improved and strengthened under high pressure, and the stronger atomic bonding can be anticipated.

Table 6 Band composition at Γ point for $D0_{22}$ - and $L1_2$ -Al₃Ti under 0 GPa and 40 GPa.

Band number	Energy (eV)	Al1	Al2	Ti
DO ₂₂ -Al ₃ Ti at 0 GPa				
1	-10.00	s 26.67%; p 2.42%	s 57.92%; p 5.39%	s 6.45%; p 1.11%; d 0.03%
2	-2.86	s 5.54%; p 20.53%	s 12.38%; p 35.67%	s 3.04%; p 8.08%; d 14.75%
3	-2.60	s 5.81%; p 19.07%	s 12.06%; p 34.79%	s 2.69%; p 8.47%; d 17.119
4	-1.37	s 2.77%; p 13.64%	s 3.51%; p 37.41%	s 1.34%; p 7.01%; d 34.32%
5	-0.93	s 2.13%; p 11.30%	s 1.94%; p 35.79%	s 0.95%; p 5.40%; d 42.49%
6	0.70	s 0.36%; p 6.79%	s 0.38%; p 10.47%	s 0.93%; p 1.90%; d 79.17%
D0 ₂₂ -Al ₃ Ti at 40 GPa		_	-	-
1	-11.27	s 29.36%; p 2.31%	s 62.49%; p 5.53%	s 0.21%; p 0.05%; d 0.04%
2	-3.08	s 3.56%; p 21.37%	s 11.81%; p 34.75%	s 2.65%; p 6.66%; d 19.20%
3	-2.87	s 4.81%; p 18.08%	s 11.88%; p 34.31%	s 2.25%; p 8.19%; d 20.48
4	-1.91	s 3.11%; p 13.37%	s 5.14%; p 37.86%	s 1.64%; p 9.83%; d 29.05
5	-0.81	s 2.10%; p 9.43%	s 1.26%; p 34.32%	s 1.11%; p 5.64%; d 46.14
6	0.79	s 0.22%; p 6.11%	s 0.05%; p 11.17%	s 0.37%; p 2.24%; d 79.84
Band number	Energy (eV)		Al	Ti
L1 ₂ -Al ₃ Ti at 0 GPa				
1	-10.70		s 85.92%; p 8.27%	s 5.51%; p 0.28%; d 0.02%
2	-3.06		s 9.90%; p 61.10%	s 1.36%; p 6.95%; d 20.67
3	-2.16		s 4.06%; p 56.85%	s 0.56%; p 2.76%; d 35.77
4	0.14		s 4.47%; p 26.55%	s 4.75%; p 4.12%; d 60.12%
L1 ₂ -Al ₃ Ti at 40 GPa			-	-
1	-12.14		s 91.79%; p 7.91%	s 0.22%; p 0.05%; d 0.02%
2	-3.66		s 9.16%; p 61.20%	s 0.64%; p 6.17%; d 22.83
3	-2.31		s 3.15%; p 57.02%	s 0.25%; p 1.32%; d 38.27
4	0.09		s 3.87%; p 27.68%	s 5.05%; p 4.56%; d 58.85

Note: for D022-Al₃Ti, Al1 refers to Al atoms in the same (001) plane with Ti atoms, and Al2 refers to Al atoms in the (001) plane occupied by themselves.

4. Summary

The structure, formation energy, elastic constants, Debye temperature and electronic structure of DO₂₂- and L1₂-Al₃Ti have been investigated with respect to external pressure by using first-principles calculations, and the pressure range is 0-40 GPa. The results show that (1) the L1₂-Al₃Ti will be stable when the pressure is around 20-30 GPa, the volume drop is about 1% along with the phase transition; (2) the elastic moduli, ductility, anisotropy index and Debye temperature of both phases increase with the pressure going up, and L1₂-Al₃Ti has better ductility, smaller anisotropy and lower Debye temperature than D0₂₂-Al₃Ti at the pressure range of 0-40 GPa; (3) the Ti-3d delocalization of Ll₂-A1₃Ti under high pressure will strengthen the hybridization between Ti-3d and Al(s,p), which leads to stronger atomic bonding, and subsequently makes the L₁₂-Al₃Ti more stable under high pressure.

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