## GENERAL RESEARCH

# Vapor-Liquid Equilibria and Excess Properties of Cyclohexane-1,1-Dimethylpropyl Methyl Ether (TAME) Mixtures

Armando del Río,† Baudilio Coto,‡ Concepción Pando,† and Juan A. R. Renuncio\*,†

Departamento de Química Fisica I, Universidad Complutense, E-28040 Madrid, Spain, and ESCET, Universidad Rey Juan Carlos, E-28933 Móstoles, Madrid, Spain

Vapor—liquid equilibrium (VLE) data are reported for the binary mixtures formed by cyclohexane and the branched ether 1,1-dimethylpropyl methyl ether (*tert*-amyl methyl ether or TAME). A Gibbs—Van Ness type apparatus was used to obtain total vapor pressure measurements for cyclohexane—TAME mixtures as a function of composition at 298.15, 308.15, 318.15, and 328.15 K. These data are analyzed together with isothermal VLE data previously obtained at 313.15 K and excess enthalpies and volumes previously determined at 298.15 K for these mixtures. The Peng—Robinson equation of state and the Wong—Sandler mixing rule, the lattice-fluid (LF) model, the Flory theory, the UNIQUAC model, and the modified UNIFAC (Dortmund) model are used to correlate or predict the VLE data and excess properties of cyclohexane—TAME mixtures.

#### Introduction

Branched ethers have been the subject of numerous investigations in recent years because of their use as additives in lead-free gasoline. The development of reliable models to describe the so-called "oxi-gasoline" requires an accurate knowledge of the thermodynamic properties for the involved mixtures. This is the reason for the increasing interest in the study of the phase equilibrium and other thermodynamic properties of the binary hydrocarbon-branched ether mixtures. Marsh et al. have recently published a review paper on the thermophysical properties for the mixtures formed by branched ethers and nonpolar solvents. 1,1-Dimethylethyl methyl ether (tert-butyl methyl ether or MTBE) is the primary oxygenated compound being used, but it dissolves easily in water, and the health risks caused by the contamination of drinking water with MTBE in California make this compound a controversial gasoline additive. This problem increases the importance of 1,1dimethylpropyl methyl ether (tert-amyl methyl ether or TAME), which is already one of the most widely used branched ethers.

The purpose of this paper is to report experimental VLE data for the cyclohexane—1,1-dimethylpropyl methyl ether system at 298.15, 308.15, 318.15, and 328.15 K and to discuss these data together with VLE data previously obtained by Chamorro et al.<sup>2</sup> at 313.15 K and other excess property data taken from the literature. Zhu et al.<sup>3</sup> have reported that the cyclohexane—TAME system exhibits moderately endothermic mixing at

298.15 K. Linek<sup>4</sup> and Witek et al.<sup>5</sup> reported positive excess volumes ( $V_{\rm m}^{\rm E}$ ) at 298.15 K. Both sets of data are in good agreement, and the  $V_{\rm m}^{\rm E}$  data obtained by Witek et al. will also be considered in this paper.

Several thermodynamic models will be used to analyze VLE,  $H_{\rm m}^{\rm E}$ , and  $V_{\rm m}^{\rm E}$  data for the cyclohexane—TAME mixtures: the Peng—Robinson (PR) equation of state (EOS)<sup>6</sup> and the Wong—Sandler mixing rule,<sup>7</sup> the lattice-fluid (LF) model,<sup>8,9</sup> the Flory theory,<sup>10</sup> the UNIQUAC model,<sup>11</sup> and the modified UNIFAC (Dortmund) model.<sup>12</sup>

## **Experimental Section**

Cyclohexane was purchased from Carlo Erba (RPEACS), with a purity higher than 99.5%. TAME (Fluka, 97% purity) was fractionally distilled over 0.3-nm molecular sieves for several hours. The middle distillate used in the present work (approximately 50% of the initial amount) had a purity better than 99.6%, as determined by a gas chromatographic analysis. Chemicals were handled under a dry nitrogen atmosphere and were degassed by reflux distillation for several hours following a procedure described elsewhere. <sup>13</sup>

VLE data were measured using a Gibbs–Van Ness type static apparatus.  $^{14}$  Binary liquid solutions of known composition were prepared in a test cell by volumetric injection of degassed liquids using calibrated pistons. The accuracy of the mole fraction is estimated to be about 0.0001 in the dilute region and about 0.0003 in the middle of the concentration range. Cell and piston injectors were immersed in a water bath whose temperature was controlled to within  $\pm 0.002$  K. The temperature was measured with a quartz thermometer, Testo 781, with an accuracy of 0.01 K. The total vapor pressure was measured when phase equilibrium was reached using a differential MKS Baratron pressure gauge with a resolution of 0.08% of the reading. The pressure accuracy is estimated to be 0.01 kPa.

<sup>\*</sup> Send correspondence to: J. A. Rodríguez Renuncio, Departamento de Química Física I, Universidad Complutense, E-28040 Madrid (Spain). Phone: 34 91394-4120. Fax: 34 91394-4135. E-mail: renuncio@eucmax.sim.ucm.es

<sup>†</sup> Universidad Complutense.

<sup>&</sup>lt;sup>‡</sup> Universidad Rey Juan Carlos.

Table 1. Properties of Pure Components Used in This Study

	T(K)	$V_{ m m} \ ({ m cm}^3\ { m mol}^{-1})$	$\kappa_{ m T} imes 10^9 \ ({ m Pa}^{-1})$	$\begin{array}{c} \alpha \times 10^4 \\ \text{(K$^{-1}$)} \end{array}$	p (kPa)	literature values range $p$ (kPa)
cyclohexane	298.15	108.70 <sup>a</sup>	$1.12^{b}$	$12.15^{c}$	13.03	$12.67-13.05^d$
3	308.15	$110.04^{a}$	$1.22^{b}$	$12.15^{c}$	20.15	$20.03 - 20.11^d$
	318.15	$111.43^{a}$	$1.33^{b}$	$12.15^{c}$	29.87	$29.81 - 30.22^{d,e}$
	328.15	$112.89^{a}$	$1.46^{b}$	$12.15^{c}$	43.37	$43.51 - 44.15^d$
TAME	298.15	$133.44^{f}$	$1.26^f$	$9.71^{f}$	10.04	$10.01 - 10.10^{g-i}$
	308.15	$134.65^{f}$	$1.53^f$	$9.62^f$	15.99	$15.79 - 15.88^{h-j}$
	318.15	$135.86^{f}$	$1.80^{f}$	$9.52^f$	24.04	$23.99 - 24.13^{h-j}$
	328.15	$136.85^{f}$	$2.07^f$	$9.43^{f}$	35.58	$35.36 - 35.57^{h-j}$

<sup>a</sup> Reference 15. <sup>b</sup> Reference 16. <sup>c</sup> Reference 17. <sup>d</sup> Reference 18. <sup>e</sup> Reference 19. <sup>f</sup> Reference 20. <sup>g</sup> Reference 21. <sup>h</sup> Reference 22. <sup>i</sup> Reference 23. <sup>*j*</sup> Reference 24.

Table 1 lists values for the molar volumes, isothermal compressibilities, thermal expansion coefficients, and vapor pressures of cyclohexane and TAME at the temperatures studied. Pure-component vapor pressure values obtained in this work are compared to those previously reported. The sources for the pure-component properties are also given in Table 1. The vapor pressures measured in this work are in good agreement with literature values, and this is considered an indication of the chemicals' purity.

#### **Results and Discussion**

**VLE Measurements.** VLE measurements for cyclohexane-TAME were carried out at 298.15, 308.15, 318.15, and 328.15 K. Results were analyzed using a modified Barker's method and the maximum likelihood principle. 25 The temperature, T, and the amount of substance for components 1 and 2 were considered to be the independent variables in the data reduction. Equations of material balance were included to take into account the amounts of substances present in the vapor

The excess Gibbs energy,  $\textit{G}_{m}^{E}$ , of the liquid phase was assumed to be described by an (m/n) Padé approximant and is given by

$$\frac{G_{\rm m}^{\rm E}}{RT} = x_1(1 - x_1) \frac{\sum_{i=0}^{m} P_i (2x_1 - 1)^i}{1 + \sum_{j=1}^{n} Q_j (2x_1 - 1)^j}$$
(1)

where  $P_i$  and  $Q_i$  are adjustable parameters and  $x_1$  is the mole fraction of cyclohexane. Data for the cyclohexane-TAME mixtures at the four temperatures studied are adequately described by (3/0) Padé approximants. This makes eq 1 equivalent to a Redlich-Kister equation. The vapor phase is described using the virial equation. Values for the second virial coefficients of the pure components and the cross virial coefficients were calculated by means of the Hayden and O'Connell method.<sup>26</sup>

Table 2 lists values for the cyclohexane liquid composition,  $x_1$ , and the total pressure, p, at the four temperatures studied, together with the calculated total pressure,  $p_{\text{calc}}$ ; the hydrocarbon vapor composition,  $y_1$ ; the excess Gibbs energy,  $G_{\rm m}^{\rm E}$ ; the activity coefficients,  $\ln \gamma_1$  and  $\ln \gamma_2$ , for cyclohexane and TAME, respectively; the Padé coefficients,  $P_i$ , for the representation of  $G_{\rm m}^{\rm E}$  in eq 1 and their uncertainties; and the standard deviations between experimental and calculated values of  $x_1$ ,  $\sigma_x$ , p, and  $\sigma_p$ . Figure 1 shows plots of the total pressure versus liquid and vapor compositions for the

temperatures studied. Deviations from Raoult's law are very small and a positive azeotrope is present in the region  $x_1 > 0.92$  at all of the temperatures. Figure 2 shows plots of vapor composition versus liquid composition obtained in this study together with literature values<sup>2</sup> available at 313.15 K. As can be observed, there is nearly no temperature effect on the vapor composi-

Values for the excess Gibbs energy of the cyclohexane-TAME system are positive, with maxima ranging from 205 J  $\mathring{\text{mol}}^{-1}$  at 298.15 K to 106 J  $\mathring{\text{mol}}^{-1}$  at 328.15 K. These maxima appear at approximately the same mole fraction  $(x_1 \approx 0.5)$  for all of the temperatures studied. Figure 3 shows plots of  $G_{\rm m}^{\rm E}$  values versus  $x_1$  for

the four temperatures studied. **VLE**,  $H_{\mathbf{m}}^{\mathbf{E}}$ , and  $V_{\mathbf{m}}^{\mathbf{E}}$  **Data Correlation.** The UNI-QUAC model<sup>11</sup> was used to correlate the isothermal VLE data. The experimental data previously reported<sup>2</sup> at 313.15 K are in good agreement with the VLE data reported in this paper and were also included in the correlation. The interaction parameters of this model,  $A_{ji}$ , were considered to vary linearly with temperature according to

$$A_{ii} = A_{ii.1} + A_{ii.2}(T - 298.15)$$
 (2)

The values for  $A_{ji,1}$  and  $A_{ji,2}$  were obtained by simultaneous correlation of the  $H_{\rm m}^{\rm E}$  and VLE data. The resulting values are  $A_{12,1} = -37.09$  K,  $A_{12,2} = -0.7484$ ,  $A_{21,1}$ = 58.45 K, and  $A_{21.2}$  = 0.7339. Values for the standard deviations between experimental and calculated excess enthalpies,  $\sigma_H$ , using the UNIQUAC model are given in Table 3. Values for the percent ratio of  $\sigma_H$  and the maximum values of the excess enthalpy,  $\sigma_H(\%)$  are also listed. Values for the standard deviations between experimental and calculated vapor pressures,  $\sigma_p$ , using the UNIQUAC model are given in Table 4. Values for the percent ratio of  $\sigma_p$  and the maximum value of vapor pressure,  $\sigma_p$ (%), are also listed. Values for the standard deviations indicate that such a correlation procedure leads to a simultaneous and very accurate description of VLE and  $H_{\rm m}^{\rm E}$  data; values for  $\sigma_p(\%)$  are always lower than 1% and the value of  $\sigma_H$ (%) is 0.3%.

The free-volume theory of Flory<sup>10</sup> has been recently recommended to predict  $H^{E}$  data for mixtures involving an hydrocarbon and a branched ether.<sup>27</sup> In this work, the theory of Flory is used to describe VLE,  $H_{\rm m}^{\rm E}$  and  $V_{\rm m}^{\rm E}$ data for the cyclohexane-TAME system. Each fluid is characterized by three characteristic magnitudes,  $p^*$ ,  $v^*$ , and  $T^*$ , which are evaluated from volumetric properties (molar volumes, cubic expansion coefficients, and isothermal compressibilities). The mixing rules introduce a binary parameter for the energy interaction,  $X_{AB}$ . An entropic correction parameter,  $Q_{AB}$ , is introduced into

Table 2. Vapor-Liquid Equilibrium Data and Coefficients and Standard Deviations for  $G^E$  Representation by Eq 1 for Cyclohexane (1)-TAME (2) at 298.15, 308.15, 318.15, and 328.15 K

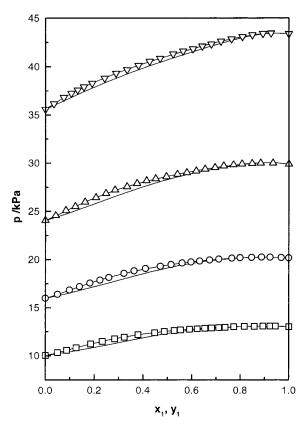
<del> </del>	ycionexane (1)—1AME (2) at 230.13, 310.13, and 320.13 K												
<i>X</i> <sub>1</sub>	p (kPa)	p <sub>calc</sub> (kPa)	<i>y</i> <sub>1</sub>	$G_{\mathrm{m}}^{\mathrm{E}}$ (J mol <sup>-1</sup> )	$\ln \gamma_1$	$\ln \gamma_2$	<i>X</i> <sub>1</sub>	p (kPa)	p <sub>calc</sub> (kPa)	<i>y</i> <sub>1</sub>	$G_{\mathrm{m}}^{\mathrm{E}}$ (J mol <sup>-1</sup> )	$\ln \gamma_1$	$\ln \gamma_2$
	cyclohexane (1)-TAME (2), $T = 298.15 \text{ K}$							cycle	ohexane	(1)-TAM	E (2), $T = 3$	18.15 K	
0.0000	10.04	10.04	0.0000	0	0.0000	0.0000	0.0000	24.04	24.04	0.0000	0	0.0000	0.0000
0.0495	10.33	10.33	0.0771	23	0.2130	-0.0012	0.0419	24.55	24.54	0.0614	20	0.1883	-0.0003
0.0868	10.57	10.57	0.1349	44	0.2338	-0.0027	0.0839	25.09	25.06	0.1209	41	0.1919	-0.0005
0.1262	10.84	10.84	0.1929	68	0.2421	-0.0036	0.1223	25.49	25.52	0.1721	61	0.1872	0.0001
0.1853	11.24	11.22	0.2718	104	0.2352	-0.0022	0.1617	25.95	25.97	0.2215	80	0.1769	0.0018
0.2333	11.50	11.50	0.3283	131	0.2182	0.0024	0.2066	26.41	26.44	0.2735	99	0.1610	0.0054
0.2832	11.76	11.76	0.3805	155	0.1941	0.0108	0.2473	26.85	26.84	0.3173	115	0.1444	0.0103
0.3231	11.93	11.95	0.4184	172	0.1725	0.0202	0.2845	27.19	27.17	0.3552	127	0.1287	0.0160
0.3793	12.17	12.17	0.4675	190	0.1415	0.0370	0.3336	27.54	27.56	0.4024	140	0.1086	0.0250
0.4479	12.39	12.40	0.5231	203	0.1060	0.0620	0.3748	27.88	27.86	0.4405	148	0.0930	0.0335
0.4877	12.52	12.51	0.5544	205	0.0878	0.0781	0.4139	28.16	28.12	0.4757	153	0.0799	0.0420
0.5277	12.61	12.61	0.5856	205	0.0715	0.0948	0.4511	28.35	28.34	0.5088	155	0.0689	0.0504
0.5538	12.67	12.67	0.6059	202	0.0622	0.1058	0.4947	28.58	28.59	0.5473	156	0.0581	0.0601
0.5909	12.75	12.75	0.6352	197	0.0504	0.1215	0.5406	28.82	28.83	0.5877	155	0.0488	0.0700
0.6231 $0.6536$	12.81 12.85	12.81 12.86	$0.6609 \\ 0.6856$	191 183	0.0417 $0.0346$	0.1350 0.1476	$0.5793 \\ 0.6180$	28.99 29.17	29.02 29.20	0.6218 $0.6558$	152 148	0.0424 $0.0371$	$0.0782 \\ 0.0862$
0.6813	12.89	12.80	0.0830	174	0.0340	0.1476	0.6545	29.17	29.20	0.6338	146	0.0371	0.0802
0.7108	12.93	12.94	0.7331	164	0.0238	0.1705	0.6953	29.51	29.51	0.7237	135	0.0327	0.0338
0.7377	12.97	12.97	0.7559	154	0.0238	0.1703	0.7312	29.68	29.64	0.7550	127	0.0245	0.1124
0.7727	13.01	13.00	0.7861	139	0.0153	0.1952	0.7714	29.79	29.77	0.7899	117	0.0203	0.1151
0.8169	13.04	13.04	0.8250	118	0.0105	0.2136	0.8066	29.89	29.86	0.8202	106	0.0165	0.1394
0.8575	13.06	13.06	0.8614	97	0.0069	0.2323	0.8481	29.94	29.95	0.8560	92	0.0119	0.1616
0.8935	13.07	13.07	0.8945	76	0.0042	0.2512	0.8836	29.98	29.99	0.8871	76	0.0080	0.1868
0.9231	13.08	13.07	0.9225	57	0.0024	0.2692	0.9348	29.98	30.01	0.9335	48	0.0031	0.2370
0.9443	13.07	13.07	0.9429	42	0.0013	0.2840	1.0000	29.87	29.87	1.0000	0	0.0000	0.0000
1.0000	13.03	13.03	1.0000	0	0.0000	0.0000	$P_0$	= 0.236	$\pm \ 0.001$	$P_1 = -0.$	$009 \pm 0.005$	$P_2 = 0.0$	$17 \pm$
$P_0 =$	= 0.3314 :	$\pm \ 0.0008$	$P_1 = -0$	$.001 \pm 0.003$	$P_2 = -0$	$.085~\pm$					$\sigma_x = 0.00000$		
				$\sigma_{x} = 0.0000$				,		(4) 55.43.6	T (0) T 0	20.45.17	
	1	. 1	(1) TAM	E (0) T 0(	00 15 17		0.0000				E(2), T=3		0.0000
0.0000				E(2), T=30		0.0000	0.0000	35.58	35.58	0.0000	0	0.0000	0.0000
$0.0000 \\ 0.0496$	15.99 16.38	15.99 16.38	$0.0000 \\ 0.0729$	0 21	$0.0000 \\ 0.1825$	$0.0000 \\ -0.0009$	0.0347 $0.0749$	36.15 36.81	36.17 36.80	0.0497 $0.1031$	18 37	0.1832 $0.1594$	$0.0004 \\ 0.0018$
0.0490	16.83	16.81	0.0729	45	0.1823	-0.0003	0.0749	37.24	37.23	0.1031	49	0.1394 $0.1426$	0.0018
0.0367	17.18	17.18	0.1442	67	0.2010	-0.0023	0.1030	37.59	37.23	0.1413	59	0.1420	0.0054 $0.0052$
0.1337	17.54	17.55	0.2556	90	0.1980	-0.0027	0.1568	37.90	37.89	0.2012	67	0.1234	0.0032
0.2237	17.86	17.87	0.3034	110	0.1864	0.0015	0.1909	38.28	38.29	0.2389	76	0.1028	0.0103
0.2603	18.13	18.14	0.3431	126	0.1728	0.0058	0.2420	38.80	38.83	0.2932	87	0.0841	0.0154
0.3220	18.55	18.55	0.4044	150	0.1463	0.0168	0.2886	39.30	39.29	0.3409	95	0.0703	0.0204
0.3635	18.82	18.79	0.4425	162	0.1278	0.0265	0.3335	39.67	39.71	0.3858	100	0.0596	0.0252
0.4099	19.06	19.03	0.4830	172	0.1076	0.0392	0.3802	40.12	40.11	0.4318	104	0.0509	0.0300
0.4709	19.29	19.30	0.5341	180	0.0836	0.0580	0.4264	40.52	40.49	0.4766	105	0.0443	0.0345
0.5153	19.47	19.47	0.5707	181	0.0684	0.0728	0.4689	40.83	40.83	0.5175	106	0.0397	0.0382
0.5606	19.62	19.63	0.6078	179	0.0551	0.0883	0.5229	41.28	41.24	0.5688	106	0.0352	0.0426
0.5970	19.73	19.74	0.6378	174	0.0459	0.1010	0.5635	41.59	41.54	0.6070	104	0.0324	0.0459
0.6331	19.83	19.84	0.6677	168	0.0380	0.1135	0.6044	41.81	41.83	0.6449	103	0.0298	0.0495
0.6738	19.93	19.94	0.7018	159	0.0304	0.1278	0.6432	42.08	42.10	0.6804	100	0.0274	0.0536
0.7119	20.03	20.02	0.7341	149	0.0244	0.1413	0.6803	42.30	42.34	0.7139	97	0.0249	0.0585
0.7654	20.12	20.12	0.7800	131	0.0173	0.1614	0.7195	42.59	42.59	0.7486	93	0.0219	0.0654
0.7990	20.17	20.16	0.8094	118	0.0135	0.1751	0.7631	42.83	42.83	0.7866	87	0.0182	0.0760
0.8468	20.21	20.21	0.8518	96	0.0087	0.1974	0.8085	43.04	43.06	0.8257	79	0.0140	0.0917
0.8878	20.23	20.23	0.8890	75	0.0052	0.2205	0.8492	43.23	43.22	0.8605	69	0.0100	0.1111
0.9232	20.23	20.23	0.9222	55	0.0027	0.2446	0.8931	43.38	43.36	0.8986	55	0.0059	0.1394
0.9691	20.19	20.20	0.9674	24	0.0005	0.2838	0.9262	43.43	43.42	0.9282	42	0.0031	0.1672
1.0000	20.15	20.15	1.0000	0	0.0000	0.0000	1.0000	43.37	43.37	1.0000	0	0.0000	0.0000
				$12 \pm 0.004$ ; $I_{\alpha} = 0.0001$							$008 \pm 0.004$		
$0.005; P_3 = 0.076 \pm 0.009; \sigma_x = 0.00001; \sigma_p = 12 \text{ Pa}$ $0.004; P_3 = 0.032 \pm 0.009; \sigma_x = 0.00001; \sigma_p = 24 \text{ Pa}$										ra			

the expression for the chemical potential. A value of 15.76 J cm<sup>-3</sup> was obtained for the energy interaction parameter,  $X_{\rm AB}$ , from the  $H_{\rm m}^{\rm E}$  data. The value for the  $Q_{\rm AB}$  parameter obtained from the VLE data was 0.020 J cm<sup>-3</sup>. Tables 3 and 4 summarize results for the correlation of the  $H_{\rm m}^{\rm E}$  and VLE data by means of the Flory theory. Calculated excess enthalpies are very accurate; a value of 1% was obtained for  $\sigma_H$ (%). Vapor pressure values calculated using Flory's theory are very accurate; the value of  $\sigma_p$ (%) compares favorably with those also reported in Table 4 for the other correlation procedures.

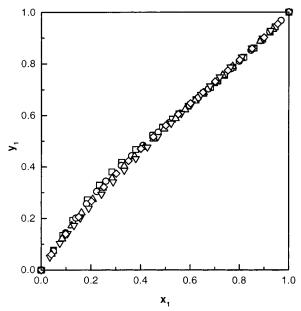
Although the theory of Flory does not include any volumetric parameter, in principle this model can be

used to predict  $V_{\rm m}^{\rm E}$  data. Figure 4 shows plots of the experimental  $H_{\rm m}^{\rm E}$  and  $V_{\rm m}^{\rm E}$  data and the values calculated by means of Flory's theory for the cyclohexane—TAME system at 298.15 K. As indicated by the arrows,  $H_{\rm m}^{\rm E}$  data are represented on the left axis and  $V_{\rm m}^{\rm E}$  data on the right axis. The  $H_{\rm m}^{\rm E}$  data are correctly described by the model. However, calculated excess volumes are only a poor estimation of the experimental  $V_{\rm m}^{\rm E}$  values. This could be due to the polarity of the ether molecule.

Correlations using the Peng–Robinson equation of state<sup>6</sup> and the Wong–Sandler mixing rule<sup>7</sup> were also carried out. In this rule, the composition dependence is based on the use of the excess Helmholtz energy,  $A_{\rm m}^{\rm E}$ ,



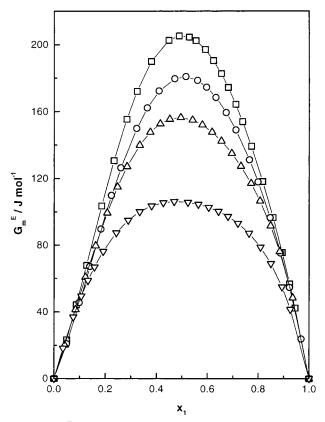
**Figure 1.** VLE data for the cyclohexane (1)—TAME (2) system: □, 298.15 K; ○, 308.15 K; △, 318.15 K; ▽, 328.15 K; and calculated values.



**Figure 2.**  $y_1$  versus  $x_1$  values for the cyclohexane (1)-TAME (2) system: □, 298.15 K; ○, 308.15 K; ◊, 313.15 K; △, 318.15 K; and ♥, 328.15 K. Data at 313.15 K are taken from Chamorro et al.2

to combine the EOS and an activity coefficient model. Because the Helmholtz and Gibbs excess energy terms are indistinguishable at low pressures, the abovementioned UNIQUAC model is used to evaluate  $G_{\mathrm{m}}^{\mathrm{E}}$ . As usual when an EOS is used, a cross term appears, which, in this case, is a cross virial coefficient

$$\left(b - \frac{a}{RT}\right)_{ij} = \frac{1}{2} \left[ \left(b_i - \frac{a_i}{RT}\right) + \left(b_j - \frac{a_j}{RT}\right) \right] (1 - k_{ij}) \quad (3)$$



**Figure 3.**  $G_{\rm m}^{\rm E}$  versus  $x_1$  values for the cyclohexane (1)-TAME (2) system: □, 298.15 K; ○, 308.15 K; △, 318.15 K; and ▽, 328.15 K.

Table 3. Excess Enthalpies for Cyclohexane (1)-TAME (2) at 298.15 K: Standard Deviations between Experimental and Calculated  $H_{\rm m}^{\rm E}$ ,  $\sigma_{H_0}$  and Percent Ratio of  $\sigma_H$  and the Maximum Value of the Excess Enthalpy,  $\sigma_H$ (%), for Correlations Using the UNIQUAC, Flory, and LF Models and Predictions Using the Modified UNIFAC (Dortmund) Model

	UNIQUAC	Flory	LF	mod UNIFAC (Dortmund)
$\sigma_{\rm H}$ (J mol <sup>-1</sup> )	1	3	11	40
$\sigma_{\rm H}(\%)$	0.3	1	3	10

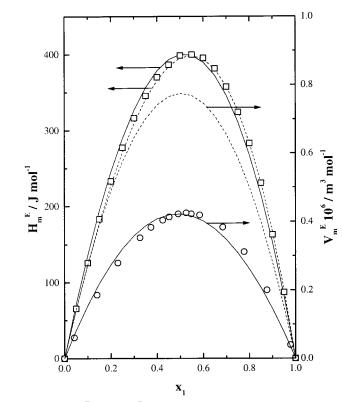
where a and b are the cubic EOS parameters and  $k_{ij}$  is a binary interaction parameter. The Wong-Sandler mixing rule requires the parameters  $k_{ij} = k_{ji}$  (considered to be temperature-independent) and the parameters of the excess Gibbs energy model,  $A_{ji}$ , (considered to be temperature-dependent according to eq 2). Values for these parameters were obtained by correlation of VLE data. The resulting values are  $A_{12,1} = -26.11$  K,  $A_{12,2} = 2.326$ ,  $A_{21,1} = -43.15$  K,  $A_{21,2} = -2.488$ , and  $k_{12} = 0.348$ . Values for  $\sigma_p$  and  $\sigma_p$ (%) obtained using the PR EOS are given in Table 4. Values for the standard deviations indicate that the PR EOS provides a VLE correlation of accuracy similar to that of the UNIQUAC model, being slightly less accurate than the UNIQUAC correlation at the lowest temperature but slightly more accurate at the highest one. Experimental vapor pressures and those calculated using the PR EOS are plotted in Figure 5 for the five temperatures studied.

The Peng-Robinson EOS could also be used to calculate volumetric properties. However, values for the excess volume predicted for cyclohexane-TAME by means of the PR EOS and the parameters obtained from the VLE correlation are negative, and for this reason, they are not shown in Figure 4. This points out the

Table 4. Correlation and Prediction of VLE Data for Cyclohexane (1)-TAME (2) Using the PR Equation of State, the UNIQUAC, Flory, LF, and Modified UNIFAC (Dortmund) Models: Standard Deviations between Experimental and Calculated Vapor Pressures,  $\sigma_p$ , and Percent Ratio of  $\sigma_p$  and the Maximum Value of the Vapor Pressure,  $\sigma_p(\%)$ 

	298.15 K <sup>a</sup>		308.15 K <sup>a</sup>		313.15 K <sup>b</sup>		318.15 K <sup>a</sup>		328.15 K <sup>a</sup>	
	$\sigma_p$ (kPa)	$\sigma_p(\%)$								
				VLE	correlation					
UNIQUAC	0.11	0.8	0.18	0.9	0.13	0.5	0.08	0.3	0.42	1.0
Flory	0.18	1.4	0.18	0.9	0.03	0.1	0.16	0.5	0.30	0.7
PR <sup>°</sup>	0.14	1.1	0.15	0.7	0.16	0.6	0.14	0.5	0.33	0.8
LF	0.11	0.8	0.08	0.4	0.13	0.5	0.06	0.2	0.52	1.2
				VLE	prediction					
mod UNIFAC (Dortmund)	0.15	1.2	0.25	1.2	0.70	2.8	0.76	2.5	1.47	3.4

<sup>&</sup>lt;sup>a</sup> Present work. <sup>b</sup> Reference 2.



**Figure 4.**  $H_{\rm m}^{\rm E}(\square)$  and  $V_{\rm m}^{\rm E}(\bigcirc)$  data for the cyclohexane (1)—TAME (2) system at 298.15 K: symbols, experimental data taken from Zhu et al.³ and Witeck et al.;⁵ —, correlated using the LF model; and - - -, calculated using the Flory theory.

difficulty of using these models to predict a property different from that used to calculate the interaction parameters.

VLE,  $H_{\rm m}^{\rm E}$ , and  $V_{\rm m}^{\rm E}$  data for the cyclohexane-TAME system were also correlated using the physical interaction model proposed by Sanchez and Lacombe: the lattice-fluid theory (LF).<sup>8,9</sup> In the LF model, each fluid is characterized by the number of segments of the molecule, r, and two scaling constants, the closed-packed volume,  $v^*$ , and the characteristic temperature,  $T^*$ . Values for the cyclohexane and TAME parameters were taken from Lacombe and Sanchez<sup>8</sup> and Coto et al., <sup>18</sup> respectively. The mixing rules include two binary parameters, the energy interaction parameter,  $\zeta_{AB}$ , and the volume interaction parameter,  $\xi_{AB}$ . These two parameters adopt values close to unity and should be calculated from excess enthalpy data and volumetric properties, respectively. For reasons similar to those of Flory's theory, an entropic correction parameter,  $q_{AB}$ , is introduced in the expression for the chemical poten-

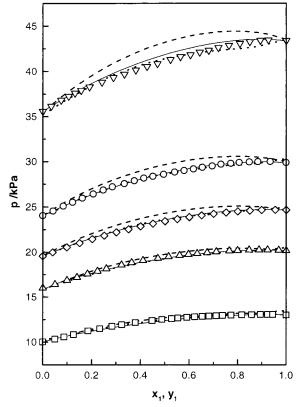


Figure 5. VLE data for cyclohexane (1)-TAME (2): □, 298.15 K;  $\bigcirc$ , 308.15 K;  $\Diamond$ , 313.15 K;  $\triangle$ , 318.15 K;  $\nabla$ , 328.15 K;  $\neg$ , correlated using the LF model; · · ·, correlated using the PR EOS; – predicted using the modified UNIFAC (Dortmund) model. VLE data at 313.15 K are taken from Chamorro et al.2

tial. All of these binary parameters are assumed to be temperature-independent. The resulting values for these parameters are  $\xi_{AB} = 0.9834$ ,  $\xi_{AB} = 1.0023$ , and  $q_{AB} =$ 

Tables 3 and 4 summarize results for the correlation of the  $H_{\rm m}^{\rm E}$  and VLE data by means of the LF model. Values for  $\sigma_H$ ,  $\sigma_H$ (%),  $\sigma_p$ , and  $\sigma_p$ (%) are listed in Tables 3 and 4. Calculated excess enthalpies can be considered accurate, as a value of 3% was obtained for  $\sigma_H(\%)$ . Calculated excess volumes are also accurate, as a value of 1.8  $\times$   $10^{-6}\ m^3\ mol^{-1}$  was obtained for the standard deviation between experimental and calculated excess volumes,  $\sigma_V$ , which corresponds to a value of 4% for  $\sigma_V$ (%), the percent ratio of  $\sigma_V$  and the maximum value for the excess volume. Figure 4 shows plots of  $H_{
m m}^{
m E}$  and  $V_{
m m}^{
m E}$ data calculated by means of the LF model. Both properties are correctly described by means of the LF model. Vapor pressure values calculated by means of the LF

**VLE and H\_{m}^{E} Data Prediction.** Predictions of VLE data from pure-component data and the model parameters available in the literature are of great industrial interest and were carried out using the modified UNI-FAC (Dortmund)<sup>12,29</sup> model. For comparison purposes,  $H_{\rm m}^{\rm E}$  data were also predicted by means of this model. Values for  $\sigma_H$  and  $\sigma_H$ (%) are listed in Table 3. The predicted excess enthalpies cannot be considered accurate. Values for  $\sigma_p$  and  $\sigma_p$ (%) are listed in Table 4. As could be expected, predicted values are less precise than those correlated by means of the PR EOS or the UNIQUAC, LF, or Flory models. Experimental vapor pressures and those calculated by means of the modified UNIFAC (Dortmund) model are plotted in Figure 5, which clearly shows that this model overestimates deviations from ideal behavior. This effect is more important at the higher temperatures. However, in a previous study on the prediction of phase equilibria for binary and ternary mixtures involving MTBE and TAME,<sup>30</sup> we found that the modified UNIFAC (Dortmund) model leads to very accurate predictions for mixtures formed by a branched ether and a linear hydrocarbon. A better agreement with experiment could be attained by introducing more groups to distinguish between -CH<sub>2</sub>- groups in linear and in cyclic molecules, but increasing the number of groups might lead to a less useful group-contribution method.

## Conclusions

Vapor pressure measurements were carried out for cyclohexane—TAME mixtures at 298.15, 308.15, 318.15, and 328.15 K. The system exhibits a nearly ideal behavior, but an azeotrope is found in the cyclohexane—rich region. There is no temperature effect on the vapor composition in the 298.15—328.15 K range.

Experimental VLE data reported here, and VLE data at 313.15 K, and  $H_{\rm m}^{\rm E}$  and  $V_{\rm m}^{\rm E}$  data at 298.15 K previously available for the cyclohexane—TAME mixtures are analyzed in terms of the Peng—Robinson equation of state and the Wong—Sandler mixing rule, the UNI-QUAC, Flory, and lattice-fluid models, and the well-known UNIFAC (Dortmund) group-contribution model.

Because the temperature effect on  $G^E$  appears to be very regular, a simultaneous description of VLE and  $H_{\rm m}^E$  data using the UNIQUAC model was successfully obtained. Both properties can be described by a unique set of four parameters.

The  $V_{\rm m}^{\rm E}$  data are well correlated by means of the LF model. However, prediction of  $V_{\rm m}^{\rm E}$  data using the PR EOS or the Flory theory is not possible. The  $H_{\rm m}^{\rm E}$  data are accurately correlated by means of the UNIQUAC, Flory, and LF models.

Several models provide a good correlation of VLE data. For VLE predictions, the modified UNIFAC (Dortmund) model is shown to lead to accurate predictions at the five temperatures studied.

Although a single binary mixture cannot be used to judge the applicability of different models, it should finally be noted that only the LF model is able to correlate simultaneously the VLE,  $H_{\rm m}^{\rm E}$ , and  $V_{\rm m}^{\rm E}$  data available for the cyclohexane—TAME mixtures. This successful correlation is attained using three adjustable temperature-independent parameters.

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#### **Nomenclature**

Latin Letters

A = Helmholtz energy

 $A_{ii}$  = UNIQUAC model interaction parameters

a =equation of state parameter

b =equation of state parameter

G = Gibbs energy

H = enthalpy

J = Joule

K = Kelvin

k = equation of state interaction parameter

 $kPa = 10^3 Pascal$ 

 $P_i$  = Padé approximant parameter

p = vapor pressure

 $Q_i$  = Padé approximant parameter

 $\vec{Q}_{AB}$  = entropic correction parameter, Flory's theory

 $q_{AB}=$  entropic correction parameter, lattice-fluid theory

R = gas constant

T = temperature

V = volume

 $X_{AB}$  = energy interaction parameter (Flory theory)

x = mole fraction in the liquid phase

y = mole fraction in the vapor phase

## Greek Symbols

 $\alpha$  = thermal expansion coefficient

 $\gamma = activity coefficient$ 

 $\zeta_{AB}$  = energy interaction parameter (lattice-fluid model)

 $\kappa$  = isothermal compressibility

 $\xi_{AB}$  = volume interaction parameter (lattice-fluid model)

 $\sigma =$  standard deviation

 $\sigma$ (%) = percent ratio of the standard deviation and the maximum value of a magnitude

#### Superscripts

\* = characteristic magnitud for a fluid

E = excess property

#### Subscripts

calc = calculated

i, j = components of binary systems

H =excess enthalpy

m = molar property

max = maximum

p = vapor pressure

V = excess volume

x = liquid composition of component 1

## Abbreviations

EOS = equation of state

LF = lattice-fluid

MTBE = 1,1-dimethylethyl methyl ether (*tert*-butyl methyl ether)

PR = Peng-Robinson

TAME = 1,1-dimethylpropyl methyl ether (*tert*-amyl methyl ether)

VLE = vapor-liquid equilibrium

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