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Polymer segregation under confinement: Free energy calculations and segregation dynamics simulations

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(Dated: 20 August 2014)

Monte Carlo simulations are used to study the behavior of two polymers under confinement in a cylindrical tube. Each polymer is modeled as a chain of hard spheres. We measure the free energy of the system, F , as a function of the distance between the centers of mass of the polymers, λ , and examine the effects on the free energy functions of varying the channel diameter D and length L , as well as the polymer length N and bending rigidity κ . For infinitely long cylinders, F is a maximum at $\lambda = 0$, and decreases with λ until the polymers are no longer in contact. For flexible chains ($\kappa = 0$), the polymers overlap along the cylinder for low λ , while above some critical value of λ they are longitudinally compressed and non-overlapping while still in contact. We find that the free energy barrier height, $\Delta F \equiv F(0) - F(\infty)$, scales as $\Delta F/k_B T \sim ND^{-1.93 \pm 0.01}$, for $N \leq 200$ and $D \leq 9\sigma$, where σ is the monomer diameter. In addition, the overlap free energy appears to scale as $F/k_B T = Nf(\lambda/N; D)$ for sufficiently large N , where f is a function parameterized by the cylinder diameter D . For channels of finite length, the free energy barrier height increases with increasing confinement aspect ratio L/D at fixed volume fraction ϕ , and it decreases with increasing ϕ at fixed L/D . Increasing the polymer bending rigidity κ monotonically reduces the overlap free energy. For strongly confined systems, where the chain persistence length P satisfies $D \ll P$, F varies linearly with λ with a slope that scales as $F'(\lambda) \sim -k_B T D^{-\beta} P^{-\alpha}$, where $\beta \approx 2$ and $\alpha \approx 0.37$ for $N = 200$ chains. These exponent values deviate slightly from those predicted using a simple model, possibly due to insufficiently satisfying the conditions defining the Odijk regime. Finally, we use Monte Carlo dynamics simulations to examine polymer segregation dynamics for fully flexible chains and observe segregation rates that decrease with decreasing entropic force magnitude, $f \equiv |dF/d\lambda|$. For both infinite-length and finite-length channels, the polymers are not conformationally relaxed at later times during segregation.

I. INTRODUCTION

When two self-avoiding polymer chains overlap, each experiences a reduction in conformational entropy. The resulting increase in free energy at maximum overlap approaches a finite value with increasing polymer length, and the polymer coils experience a very soft effective potential that allows for a high degree of mutual penetration.^{1,2} When the polymers are confined to a cylindrical space, the overlap free energy can be significantly affected. Under the right confinement conditions, it can be sufficiently high to cause segregation of the polymers.^{3,4} Such entropy-driven demixing of confined polymers may be relevant for some biological processes. Notably, it has been proposed to be the dominant mechanism for chromosome separation in bacteria, with proteins identified as segregation factors serving mainly to create the right conditions for entropy-driven segregation.⁴⁻⁶ While several recent studies have challenged this view,⁷⁻¹¹ an understanding of bacterial chromosome separation remains elusive and the importance of entropy as a driving force is currently not clear.^{12,13}

Computer simulation studies have provided insight into the segregation of polymers under confinement.^{4,14-24} Most studies have considered systems comprised of flexible linear polymers,^{4,14-18,20,21,23} though some have examined segregation of ring polymers,^{19,22,24} as well as the effects of bending rigidity²³ and molecular crowding.²⁴ In the case of

linear polymers, the role of cylindrical confinement in modulating the entropic repulsion has been investigated by examining the dependence of the polymer miscibility and intrachain ordering statistics on the confinement dimensions and chain density.^{18,20} It was found that chains demix even outside the de Gennes linear ordering scaling regime. In addition, it was observed that the degree of separation increases with increasing asymmetry of the confinement space (i.e. more elongated cylinders) and decreases with increasing volume fraction of the monomers. The variation of the chain miscibility with the confinement dimensions was used to predict the corresponding behavior for ring polymers using a scaling of the cylinder diameter $D \rightarrow D/\sqrt{2}$,¹⁹ and the analysis suggests that *E. coli* chromosomes are linearly ordered and lie in the spontaneous segregation regime.^{19,20}

The miscibility of confined polymers is determined by the form of the variation of the free energy with the degree of polymer overlap. In principle, this can be calculated using probability distributions obtained directly from simulations. Jung *et al.* measured such distributions for the distance between the polymer centers of mass for flexible chains and found that they were sharply peaked at wide separations for sufficiently large L/D but were significantly broader for more symmetric confinement.²⁰ The latter result is consistent with the prediction that there is no entropic cost for segregating chains in a spherical confining cavity.¹⁵ The results are indicative of a free energy function with a deep minimum

at large L/D that becomes more shallow as the confining space becomes more symmetric. Note that accurate estimates of the free energy far from a deep minimum are impeded by poor statistics if standard simulation methods are employed. A simple alternative is to employ analytic forms of the free energy function estimated using a de Gennes blob scaling analysis.^{15,16,21} Under the assumption that the polymer chain remains in conformational quasi-equilibrium, the free energy functions can be used to make quantitative predictions for the dynamics of polymer segregation. Arnold and Jun used such a simple model to study segregation in infinitely long cylinders and interpret results from Langevin simulations.¹⁶ Liu and Chakraborty employed an estimate of the free energy for a mean first-passage time analysis of the Fokker-Planck equation to study the dynamics of segregating chains in a 2-D system.²¹ In different limiting cases, the predictions yielded a scaling of the segregation time, τ , with polymer length that was consistent with results from Monte Carlo (MC) dynamics calculations. In addition, both theory and simulation yield a minimum in τ with confinement length. However, quantitative discrepancies were appreciable, pointing to the limitations of the simple analytical model employed to describe the free energy function.

In this study, we use MC simulations to calculate the free energy as a function of polymer separation for two polymer chains confined to a cylindrical tube. In order to obtain quantitatively accurate functions over a wide range of separations, we employ a technique²⁵ that we have previously used to calculate free energy functions for polymer translocation.^{26–28} We study the dependence of the free energy functions on the dimensions of the confining cylinder, the polymer length, the volume fraction and the polymer stiffness. To our knowledge, this is the first such systematic study of the overlap free energy for cylindrically confined systems. The calculated free energies are used to test predictions of simple analytical models used in other studies. We find that scaling arguments can account for the observed trends, though the measured scaling exponents differ somewhat from the predicted values. This is likely due to insufficiently satisfying the conditions defining the de Gennes regime for flexible polymers and the Odijk regime in the case of semi-flexible polymers. In addition, we carry out MC dynamics simulations to study the segregation dynamics and interpret the results using the free energy functions. In the early stages of segregation, the observed dynamics are in semi-quantitative agreement with the predictions. At longer times, the polymers are conformationally out of equilibrium, and the free energy functions are less useful for understanding the dynamics.

II. MODEL

We employ a minimal model of two polymer chains confined to a cylindrical tube. Each polymer is modeled

as a chain of N hard spheres, each with a diameter of σ . The pair potential for non-bonded monomers is thus

$$u_{\text{nb}}(r) = \begin{cases} \infty, & r \leq \sigma \\ 0, & r > \sigma, \end{cases} \quad (1)$$

where r is the distance between the centers of the monomers. Pairs of bonded monomers interact with a potential

$$u_{\text{b}}(r) = \begin{cases} 0, & 0.9\sigma < r < 1.1\sigma \\ \infty, & \text{otherwise.} \end{cases} \quad (2)$$

Thus, the bond length can fluctuate slightly about its average value, which is equal to the monomer diameter.

The polymers are confined to a hard cylindrical tube. The monomers interact with the wall of the tube with a potential:

$$u_{\text{w}}(r) = \begin{cases} 0, & r < D \\ \infty, & r > D, \end{cases} \quad (3)$$

where r is the distance of a monomer from the central axis of the cylinder. Thus, the tube itself has a diameter of $D + \sigma$, and D is defined to be the diameter of the cylindrical volume accessible to the centers of the monomers. For confining tubes of finite length, each end of the cylinder is capped with a hemisphere whose diameter is equal to that of the cylinder. The length, L , of the capped tube is defined to be that of the cylindrical portion of the volume. This is illustrated in Fig. 1.

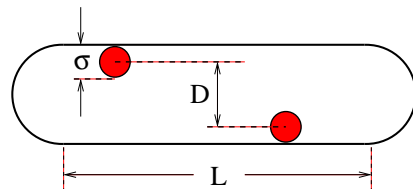


FIG. 1. Illustration of the definition of the tube diameter, D , and length, L , for a finite length confining tube. The two filled red circles are monomers in contact with the tube wall on opposite sides of the cylinder.

Most of the simulations in this study employ fully flexible polymer chains. However, in some cases we consider the effects of bending stiffness on the free energy functions. To do this, we employ a bending potential associated with each consecutive triplet of monomers. The potential has the form:

$$u_{\text{bend}}(\theta) = \kappa(1 - \cos \theta). \quad (4)$$

The angle θ is defined at monomer i such that $\cos \theta_i \equiv \hat{u}_i \cdot \hat{u}_{i+1}$, where \hat{u}_i is a normalized bond vector pointing from monomer $i-1$ to monomer i . The bending constant κ determines the stiffness of the polymer and is related to the persistence length P by $\kappa/k_{\text{B}}T = P/\langle l_{\text{bond}} \rangle$, where $\langle l_{\text{bond}} \rangle$ is the mean bond length.

III. METHODS

Monte Carlo simulations employing the Metropolis algorithm and the self-consistent histogram (SCH) method²⁵ were used to calculate the free energy functions for the polymer-nanopore model described in Section II. The SCH method provides an efficient means to calculate the equilibrium probability distribution $P(\lambda)$, and thus its corresponding free energy function, $F(\lambda) = -k_B T \ln P(\lambda)$, where k_B is Boltzmann's constant and T is temperature. The method circumvents the problem of poor statistics that would otherwise occur when the variation in F with respect to λ exceeds a few $k_B T$. This is an important consideration in the present study, where large overlap free energy barriers are observed. The method is similar to that used by Narros *et al.* to calculate effective potentials between overlapping polymers.^{29,30}

To implement the SCH method, we carry out many independent simulations, each of which employs a unique “window potential” of a chosen functional form. The form of this potential is given by:

$$W_i(\lambda) = \begin{cases} \infty, & \lambda < \lambda_i^{\min} \\ 0, & \lambda_i^{\min} < \lambda < \lambda_i^{\max} \\ \infty, & \lambda > \lambda_i^{\max} \end{cases} \quad (5)$$

where λ_i^{\min} and λ_i^{\max} are the limits that define the range of λ for the i -th window. Within each “window” of λ , a probability distribution $p_i(\lambda)$ is calculated in the simulation. The window potential width, $\Delta\lambda \equiv \lambda_i^{\max} - \lambda_i^{\min}$, is chosen to be sufficiently small that the variation in F does not exceed a few $k_B T$. Adjacent windows overlap, and the SCH algorithm uses the $p_i(\lambda)$ histograms to reconstruct the unbiased distribution, $P(\lambda)$. The details of the histogram reconstruction algorithm are given in Ref. 25, and a description for an application to a physical system comparable to that studied here is presented in Ref. 26.

Polymer configurations were generated using translational displacements of the monomers. For a given move, a monomer from either polymer was selected with equal probability and randomly displaced in each dimension. The displacement was chosen from a uniform distribution in the range $[-\Delta_{\max}, \Delta_{\max}]$. The trial moves were accepted with a probability $p_{\text{acc}} = \min(1, e^{-\Delta E/k_B T})$, where ΔE is the energy difference between the trial and current states. For the case of fully flexible polymers (i.e. $\kappa = 0$), this implies that the moves are accepted if the bonding constraints of Eq. (2) were satisfied, non-bonded particles do not overlap with each other, no monomer overlaps with the walls of the tube, and the distance between the centers of mass of the chains lie within the window defined in Eq. (5). The maximum displacement parameter was chosen to be $\Delta_{\max} = 0.22\sigma$, which yielded an acceptance probability of approximately 46%. In addition to translational monomer displacements, we also employed standard reptation moves in simulations of systems with finite bending rigidity.

The windows are chosen to overlap with half of the adjacent window, such that $\lambda_i^{\max} = \lambda_{i+2}^{\min}$. The window widths were typically $\Delta\lambda = \sigma$ or $\Delta\lambda = 2\sigma$. The number of windows (and, therefore, the number of independent simulations) was determined by the range of λ . The range was given by $\lambda \in [0, \lambda_{\max}]$. In the $L = \infty$ case, the value of λ_{\max} was determined by the condition that the polymers had negligible probability of contact. This corresponds to a region where the free energy is constant with respect to λ . As an illustration, for a system of polymers of length $N = 200$ in a cylinder of diameter $D = 4\sigma$, a value of $\lambda_{\max} = 120\sigma$ was used. This required simulations for 119 different window potentials for $\Delta\lambda = 2\sigma$. In the finite- L case, λ_{\max} is limited by monomer crowding near the caps of the cylinder, and values were chosen to account for this. For each simulation, individual probability histograms were constructed using the binning technique. We used 10 bins per histogram and so the sampling bin width was $\delta\lambda = 0.1\sigma$.

Initial polymer configurations were chosen as follows. For the $L = \infty$ case, the polymers were initially fully extended along the axis of the cylindrical tube, which we choose to be the z axis. The polymers were sufficiently spaced along the orthogonal x direction in order to avoid inter-chain monomer overlap. The relative separation of the centers of mass along the z axis were chosen to lie within the range allowed by Eq. (5) for a given window. The system was then relaxed using translational displacement of monomers for a sufficiently high number of moves, after which histogram sampling proceeded. For the case of finite- L tubes, it was necessary to initialize the system in a different manner. As before, the two chains were initially extended along the z axis and sufficiently separated along x to avoid overlap. However, the centers of mass of the polymers were initially set to $\lambda = 0$. In addition, the length of the tube was initially chosen to be just sufficiently large to contain the extended polymers. The polymer chains were then relaxed using translational MC moves. During this stage, the window potential was not applied. After each MC cycle (in which a move for each monomer is attempted once, on average) an attempt was made to shorten the tube by a fixed small amount. If this adjustment did not result in monomer overlap with the caps of the tube, the move was accepted. In this manner, the tube length was “ratcheted” down until it reached the desired length. Following this stage, a linear potential (i.e. a constant force) was applied to each monomer such that one polymer was driven in the $+z$ direction, and the other along $-z$. This proceeded until λ was within the allowed range for a given window potential given in Eq. (5). Subsequently, the system was relaxed with the window potential applied.

In addition to free energy calculations, Monte Carlo dynamics simulations were used to study the segregation dynamics of the two confined polymers. Polymer motion was generated solely through random monomer displacement, in which the coordinates of a randomly chosen monomer were displaced by an amount Δr_λ for

$\lambda = x, y, z$. Each coordinate displacement was randomly chosen from a uniform distribution $[-\Delta_{\max}, \Delta_{\max}]$. Unless otherwise stated, $\Delta_{\max} = 0.22\sigma$. A trial move was rejected if it led to overlap with another nonbonded monomer, violation of the bonding constraint, or overlap with the channel wall. The polymer configurations were initially chosen such that $\lambda = 0$. In the case of finite- L tubes, the polymer centers of mass were fixed near the center of the tube, as measured along the z axis. This was done by fixing the position of the center monomer of each polymer. Otherwise, initialization was carried out in the same manner as described above for the free energy simulations. Following equilibration, the segregation process was examined by measuring the time dependence of various quantities. We simulated typically 500 – 2000 segregation events to calculate averages of these time-dependent quantities.

The following quantities were measured in both the free energy simulations and the MC dynamics simulations: (1) λ , the distance between polymer centers of mass; (2) L_a , the overlap distance of the polymers along z ; (3) L_b , the average length of the non-overlapping portions of the chains, measured along z ; (4) $L_{\text{ext}} (= L_a + L_b)$, the average extension length of each polymer, measured along z . These quantities are illustrated in Fig. 2.

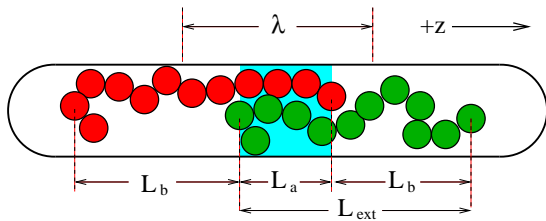


FIG. 2. Illustration of the definitions of the quantities measured in this study. All distances shown are measured along the z axis. Note that the instantaneous recorded value of L_b is the average of the two values illustrated here.

In the results presented below, lengths are measured in units of σ , the monomer diameter. In addition, time is measured in MC cycles, where 1 MC cycle corresponds to one attempted move per monomer, on average. For simulations of polymers with finite bending rigidity, the bending constant κ is measured in units of $k_B T$.

IV. RESULTS

A. Infinite length confinement cylinder

We consider first the case of fully flexible polymers (i.e. $\kappa = 0$) confined to cylindrical tubes of infinite length. Figure 3(a) shows a free energy function for a system of

polymers of length $N = 200$ confined to a tube of diameter $D = 4$. As expected, the free energy increases as the overlap of the polymer chains increases, and reaches a maximum when $\lambda = 0$. This is due to the reduction in conformational entropy of overlapping chains. There are four distinguishable regions, each of which are labeled in the figure: (I) In the region $0 < \lambda \lesssim 5$, F is approximately constant. (II) For $5 \lesssim \lambda \lesssim 51$, F decreases roughly linearly with λ , though the curve does have a slightly negative curvature in this region. (III) For $51 \lesssim \lambda \lesssim 90$, F continues to decrease with λ , though the curve has clearly positive curvature. (IV) For $\lambda \gtrsim 90$, F is constant. The general shape of the function in this figure is also observed for different values of N and R , though the domain boundaries are dependent on these parameters.

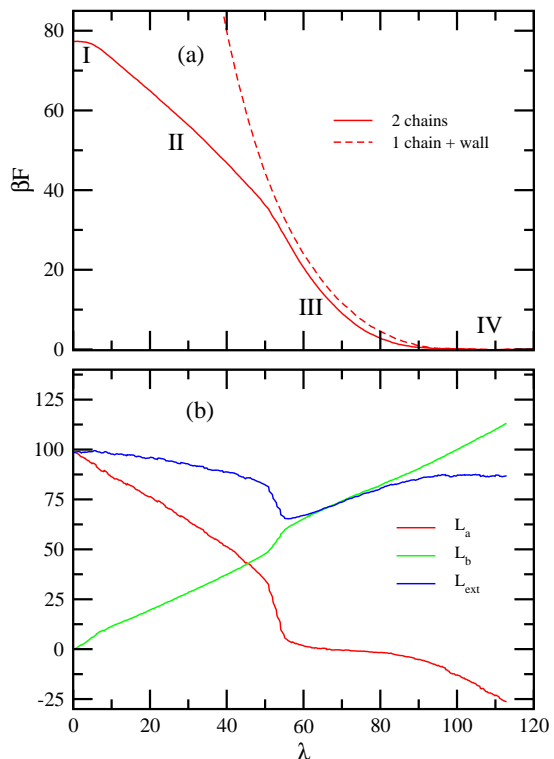


FIG. 3. (a) Free energy function for two chains of length $N = 200$ in an infinitely long cylinder of diameter $D = 4$. The dashed line shows an appropriately scaled free energy function for a single chain in a tube capped at one end with a flat wall, as described in the text. (b) Variation of L_a , L_b and L_{ext} with λ .

Region I is due to an effect exhibited for nearly overlapping centers of mass in which one polymer tends to extend farther on each side than the other, with the longer and shorter polymers periodically swapping identities. Only when λ is sufficiently large to prevent such “nesting” of chains will an increase in λ correspond to an increase in the actual overlap in the monomers and, thus, to a change in F . Such an effect has been observed previously for unconfined ring polymers.^{29,30} The significance

of the other domains is clear from the results shown in Fig. 3(b), which shows the average values of L_a , L_b , and L_{ext} as a function of λ . In region II, the polymers overlap, but the overlap distance L_a decreases as the polymer centers of mass become more widely separated. In a narrow region of $51 \lesssim \lambda \lesssim 55$, there are abrupt decreases in the polymer extension length L_{ext} as well as L_a , which falls to zero. Following this abrupt change, L_a remains close to zero, while L_{ext} and L_b increases with λ . Thus, region III corresponds to the case where the polymers do not overlap, but are longitudinally compressed. This compression decreases as the polymer centers of mass separate. For $L \gtrsim 90$ in region IV, we observe $L_a < 0$, and the value becomes increasingly negative with increasing polymer separation. This means that the polymers are no longer in contact and that the distance between the nearest pair monomers on each polymer is increasing. In addition, L_{ext} is constant in this region. Thus, the separation distance of non-interacting polymers does not affect their conformational state, and the free energy does not depend on the distance.

To further understand the variation of F in region III, we have carried out the following simulation. We measure the free energy of a single $N = 200$ chain in a $D = 4$ tube that is capped at one end with a flat wall, but which is open at the other end. We then measure F as a function of the distance between the center of mass of the polymer and its mirror image on the other side of the wall. This should approximate the behavior of two chains that are in contact, but do not overlap. For a quantitative comparison, the free energy is scaled by a factor of 2, to account for the presence of two chains in the original system. The scaled function is shown as a dashed curve in Fig. 3(a). The function follows that of the two-chain system very closely in region III, with the same positive curvature. Thus, in region III, the polymer chains interact as though the interface between them forms an impenetrable wall. There is a slight shift of the solid curve toward lower λ , which is likely due to the flexibility and slight penetrability of the interface in the two-chain system, in contrast to the case for a true hard wall. Note that the dashed curve diverges from the original two-chain function once the chains begin to overlap, as expected.

The effects of varying the polymer chain length, N , on the free energy functions are shown in Fig. 4. Results are shown for $D = 2$ and $D = 4$ in Figs. 4(a) and (b), respectively, and the data is scaled by $1/N$ on each axis. In each case, the scaled functions overlap to a considerable degree. The overlap is poorest for low N (notably so for $N = 10$). The curves appear to converge with increasing N , and convergence is evidently faster for $D = 2$ than for $D = 4$. Thus, the results suggest that $F/N = f(\lambda/N; D)$ for sufficiently large N , where f is a function parameterized by the tube diameter D . The deviations for short N are likely due to chain-end effects, which are expected to be more significant for wider confinement tubes where the chain is less stretched along z and more monomers

are close to the extrema positions of the polymer. Confirmation of this hypothesis requires simulations for appreciably greater N , which, unfortunately, is not computationally feasible at present. The height of the free energy barrier, $\Delta F \equiv F(0) - F(\infty)$, varies linearly with N , as is evident from the scaled curves as well as the inset of the figure. Slight deviations from linearity (not evident in the figure) occur at low N due to the finite-size effects. Note that the rate of increase of F with N is greater for the more confined system, as expected.

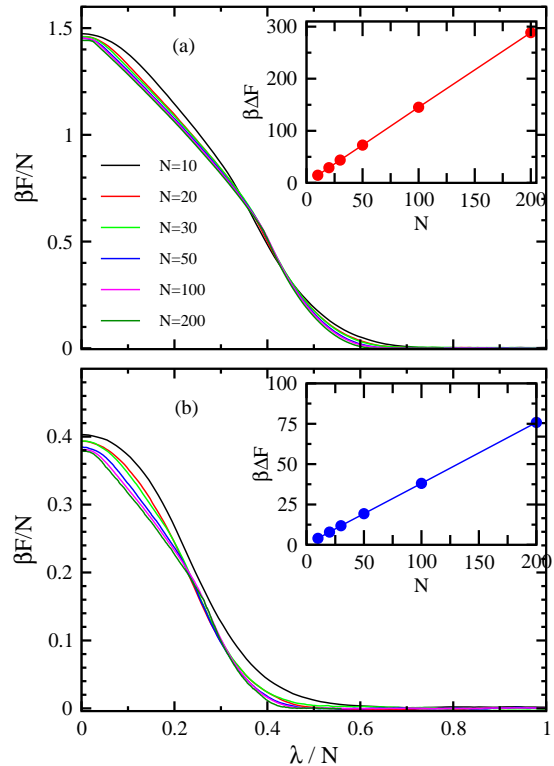


FIG. 4. (a) Scaled free energy functions for two polymer chains confined in an infinitely long cylindrical tube of diameter $D = 2$. Results are shown for several different values of polymer length, N . The inset shows the variation of $\Delta F \equiv F(0) - F(\infty)$ vs N . (b) As in (a), except for a tube diameter of $D = 4$.

A simple explanation for the apparent scaling of F with N is as follows. In regime II, it is plausible that $F \propto N_a$, the average number of monomers per polymer in the overlap region. This is consistent with the limiting case of maximum overlap at $\lambda = 0$, where $\Delta F \propto N$ was observed. Assuming that monomer densities are uniform (though distinct) in the overlapping and non-overlapping regions, it is easily shown that $N_a = Nu(\lambda/N; D)$, where u is a function parameterized by D , which controls the polymer subchain length per monomer in the overlapping and non-overlapping regions. Thus, $F/N = u(\lambda/N; D)$, where the proportionality constant has been absorbed into the function u . In regime III, the polymers do not overlap but are each compressed. We employ the

renormalized Flory theory of Jun *et al.*³¹ to estimate the variation of F with L_{ext} . Those authors note that the free energy for a polymer of extension length L_{ext} is $\beta F = AL_{\text{ext}}^2/(N/g)D^2 + BD(N/g)^2/L_{\text{ext}}$, where A and B are constants of order unity and $g \approx (D/\sigma)^{5/3}$ is the number of monomers in a compression blob of diameter D . From Fig. 3(b) we observe that $L_{\text{ext}} \approx c\lambda$ in this regime, where c is a D -dependent proportionality constant. It follows that $\beta F/N = w(\lambda/N; D)$, where $w(x; D) = (2Agc^2/D^2)x^2 + (2B/cg^2)x^{-1}$. This expression for F is expected to be valid in the regime where L_{ext} exceeds approximately half of its average length.³¹ Fig. 3(b) clearly shows that this condition is satisfied in regime III. Thus, in regimes II and III the observed scaling of F with N is predicted. The cross-over between the regimes occurs at λ^* determined by the condition $u(\lambda^*/N; D) = w(\lambda^*/N; D)$. Finally, the relative width of regime I is expected to vanish as $N \rightarrow \infty$, and F is of course invariant to λ in regime IV. Thus, we predict $F/N = f(\lambda/N; D)$ for sufficiently large N .

Figure 5 shows the effect on $F(\lambda)$ of variation in the confining tube diameter, D . Results are shown for polymers of length $N = 200$. As expected the polymer overlap free energy decreases with increasing diameter. This follows from the fact that an increase in D means the polymers have greater freedom in the transverse direction (i.e. x - y plane) and thus require less conformational distortion (i.e. reduction in entropy) in overlapping configurations. The variation of the free energy barrier height, ΔF , is shown in the inset of the figure on a log-log scale. Clearly, there is a power law relation between ΔF and D , and a fit to the data yields $\Delta F \sim D^{-1.93 \pm 0.01}$. A slight deviation from this scaling is evident for the widest tube considered ($D = 9$) and is most likely due to chain-end effects.

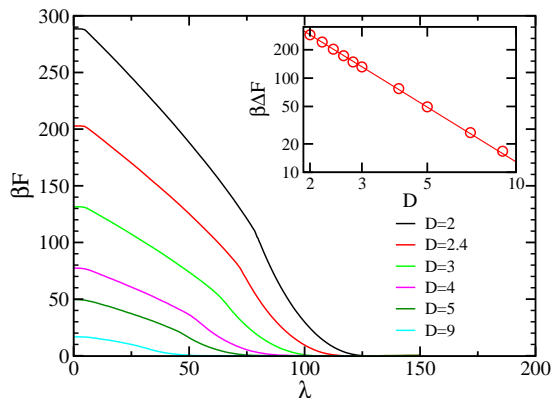


FIG. 5. Free energy functions for two polymer chains, each of length $N = 200$, confined in an infinitely long cylindrical tube. Results are shown for several different values of the cylinder diameter, D . The inset shows the variation of $\Delta F \equiv F(0) - F(\infty)$ vs channel diameter. A scaling of $\beta \Delta F \sim D^{-1.93 \pm 0.01}$ is observed.

To understand the observed dependence of ΔF on N and D , we consider an approach followed in Ref. 23,

which borrows from a previous treatment of a ring polymer in a confining channel.¹⁹ In Ref. 19, it was suggested that a ring polymer confined in a cylinder can be viewed as two overlapping chains, each with a length that is half of that of the ring. The latter picture corresponds to the present system with $\lambda = 0$. Polymers that overlap can be viewed as occupying an effective tube with half the cross-sectional area, i.e. with a reduced diameter of $D/\sqrt{2}$. In the context of the de Gennes blob model, it is known that the confinement free energy of a single chain in a tube of diameter D is given by $F_c(N, D) \sim k_B T N D^{-1/\nu}$, where the scaling exponent has the value $\nu \approx 0.588$ for good solvent conditions. Two non-interacting chains in the same tube have a free energy of confinement that is double this value. Thus, the predicted free energy difference between two confined polymers of length N in the non-overlapping (high λ) and completely overlapping ($\lambda = 0$) limits is thus, $\Delta F = 2F_c(N, D) - 2F_c(N, D/\sqrt{2})$, which yields $\Delta F \sim k_B T N D^{-\gamma}$, where $\gamma = 1/\nu \approx 1.7$. The predicted linear variation with respect to N is consistent with the results shown in Fig. 4. On the other hand, the exponent of $\gamma = 1.7$ differs from the value of 1.93 ± 0.01 obtained from the data in Fig. 5. This discrepancy may arise in part from the simplistic approach of using an effective reduced tube diameter to account for overlapping chains. More likely, it results from the use of the blob model outside the appropriate regime. Such discrepancies have been observed in other studies. For example, Kim *et al.* have noted that the scaling of the effective chain elasticity yields results consistent with the predictions of the blob model only for relatively large tube diameters ($D > 10$), while it yields unexpected scaling for smaller diameters, such as those employed in this study.³² More relevant to this work, Račko and Cifra measured the confinement free energy of single $N = 800$ chain of variable bending stiffness and observed a scaling exponent for the fully flexible case that clearly satisfies $\gamma > 1/\nu$ for tube diameters comparable those here (see Fig. 2 of Ref. 23).

Let us now consider the dynamics of segregation for polymers confined to infinite length cylinders. Figure 6(a) shows the variation of the average λ , L_a and L_{ext} with time, upon release from a state where the polymer centers of mass overlap (i.e. $\lambda = 0$). Results are shown for chains of length $N = 200$ in a cylinder of diameter $D = 4$. As expected, during segregation, λ increases and the overlap distance L_a decreases. Note that negative values of L_a correspond to the (negative) distance between nearest monomers on the chains after they no longer overlap. The polymer extension length L_{ext} initially decreases, which is followed by a slight, gradual increase. It is useful to consider the relation between the lengths L_a and L_{ext} , and the center of mass distance, λ , during segregation. Figure 6(b) shows this relation measured for the dynamics simulations and compares the values with those from the (equilibrium) free energy calculations. In the initial stages of segregation, the dynamics and equilibrium curves are in reasonably

good quantitative agreement. At a later stage there is a more pronounced discrepancy between the two sets of results for both L_a and L_{ext} . This occurs in region in the equilibrium case where the polymers are compressed and in contact, but not overlapping. During the segregation process in the dynamics simulation, the non-overlapping section of the polymer is not able to retract to its equilibrium length, and thus L_a and L_{ext} are both greater than the equilibrium values. This out-of-equilibrium behavior eventually ends at later times for separation distances, λ , corresponding to non-touching chains.

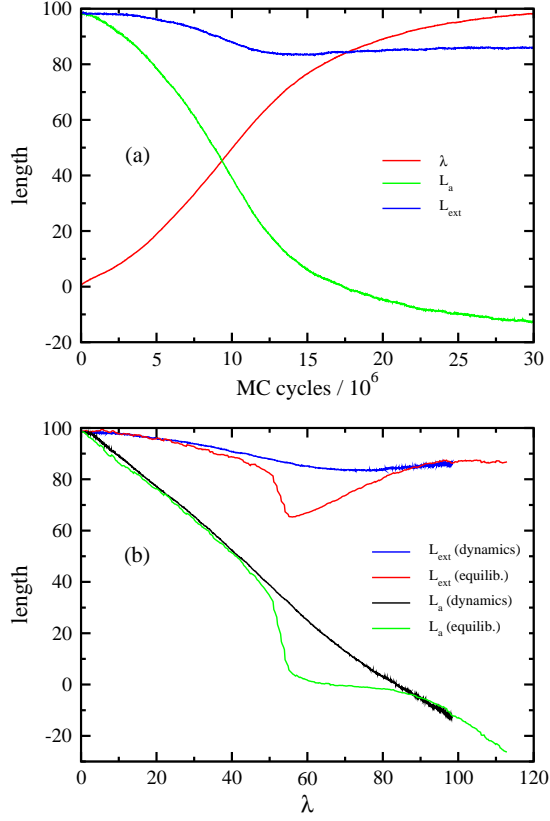


FIG. 6. (a) Variation of λ , L_a and L_{ext} with time during polymer segregation for a system with $N = 200$ and $D = 4$. The polymers start with $\lambda = 0$. (b) Variation of L_a and L_{ext} with λ . Results are shown for segregation dynamics simulations and for equilibrium simulations.

The discrepancy between the results for equilibrium and dynamics simulations shown in Fig. 6(b) was also observed for polymers of various lengths and cylinder diameters (data not shown). It is unlikely that this is a result of the model or MC dynamics method that we have employed. Thus, the out-of-equilibrium conformational behavior at later times for segregating polymers in open cylinders appears to be a general result. Thus, direct usage of the free energy functions, which are meaningful for a system in equilibrium, to provide quantitative predictions of polymer segregation dynamics is not appropriate. This applies, for example, to using $F(\lambda)$ in an analysis of

the Fokker-Planck equation to predict segregation times for large L systems.

In the early stages of segregation the polymers do remain conformationally relaxed. This corresponds to the regime where the polymers overlap (region II, as labeled in Fig. 3), and the free energy varies approximately linearly with λ for sufficiently long polymers. Thus, the magnitude of the effective force, $f \equiv |dF/d\lambda|$ is constant. The average relative velocity is approximately $v(\equiv d\lambda/dt) = 2f/\gamma$, where γ is the friction of each polymer and the factor of two accounts for the presence of two chains moving in opposite directions. We assume that the friction of the individual monomers is additive, $\gamma \approx \gamma_0 N$. Defining scaled variables $\lambda' \equiv \lambda/N$ and $t' \equiv t/N^2$, it follows that $d\lambda'/dt'$ should be constant and thus independent of N . From Fig. 4 the regime of validity is $0.03 \lesssim \lambda' \lesssim 0.4$ for $D = 2$. Figure 7 shows λ' vs t' for systems of various N for this tube diameter. The curves are approximately parallel to each other, with the higher N curves shifted to higher t' . To account for this shift, we use an approach similar to one employed in Ref. 16. We first note that F is approximately independent of λ in regime I ($\lambda' \lesssim 0.03$), within which polymer separation is governed by diffusion. The time required to reach the regime transition scales as $t_{\text{diff}} \sim (0.03 L_a^{(\text{max})})^2 / 2D_{\text{diff}} \sim N^3$, where $L_a^{(\text{max})}$ ($\sim N$) is the extension length of the two fully overlapping polymers, and D_{diff} ($\sim 1/N$) is the polymer diffusion coefficient. Thus, polymers are expected to cross into regime II at a scaled time $t' \sim N$, which is approximately consistent with the observed shift in the curves. In regime II, the functions are not linear but curved, which is due to the slight curvature in the free energy curves in Fig. 6(a) in this regime. As is evident from the inset of Fig. 7, the derivatives $d\lambda'/dt'$ are quantitatively comparable, though there is a slight reduction in the values with larger N . This is likely a consequence of the fact that scaled free energy functions in Fig. 4(a) have not quite converged over the range $N = 30$ –200. It may also be related to the very slight deviation from conformational equilibrium in regime II evident for L_a in Fig. 6. In spite of these discrepancies, the segregation dynamical behavior during the initial stages of the process is nevertheless reasonably consistent with predictions using the free energy functions.

B. Finite length confinement cylinder

Next we consider the case of flexible chains ($\kappa = 0$) confined to a cylindrical tube of finite length, L . Figure 8(a) shows the variation of F with λ for a system of chains with length $N = 200$ in a tube of diameter $D = 4$ and a length of $L = 90$. Figure 8(b) shows the variation in the mean values of L_a , L_b , and L_{ext} with λ . The general trends are similar to those of the infinite-length case shown in Fig. 3, except for a steep rise in F at high λ , which leads to a free energy minimum at

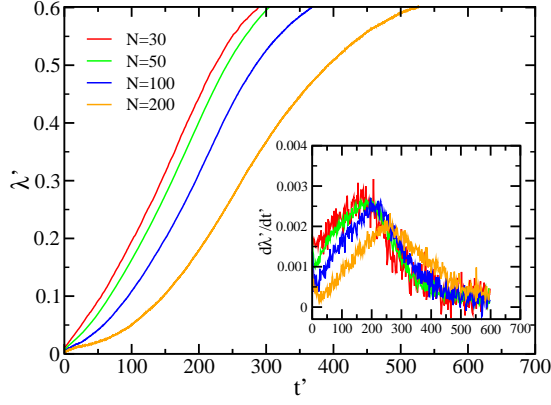


FIG. 7. Variation of $\lambda' \equiv \lambda/N$ vs $t' \equiv t/N^2$ for two polymers in an infinitely long cylinder of diameter $D = 2$. Results are shown for different N . The inset shows the derivative $d\lambda'/dt'$ vs t' for the same data.

$\lambda \approx 57$. This rapid rise is due to the presence of the hemispheric caps on the confining tube. When the polymer center of mass separation is sufficiently great, the chains press against the hemisphere walls, and the crowding of monomers reduces the conformational entropy of the chain. This crowding also leads to a reduction in the polymer extension L_{ext} at large λ .

Figure 9 shows free energy functions for $N=200$ chains in a tube of diameter $D=4$ for lengths ranging from $L=90$ to $L=\infty$. The curves have been shifted along the vertical axis so that $F = 0$ for complete overlap at $\lambda = 0$. The general features are similar for all of the finite- L curves: each curve rises steeply at high λ and exhibits a free energy minimum corresponding to the most probable polymer center of mass separation distance in equilibrium. The height of the free energy barrier, $\Delta F \equiv F(0) - F(\lambda_{\text{min}})$, and the location of the free energy minimum, λ_{min} , both increase with increasing L . As is evident from the corresponding data shown in Fig. 10, the ratio λ_{min}/L is nearly invariant with respect to tube length L . For larger L , where the polymers have negligible contact at distances where they are in contact with the end caps of the tube, the curves in Fig. 9 exhibit a broad flat minimum in F with a value equal to that for $L=\infty$ (data not shown).

Some quantitative aspects of the results in Fig. 9 can be understood by comparing the results with those of $L = \infty$ shown in Fig. 3. The free energy barrier height, ΔF , for finite L approaches that for $L=\infty$ at a tube length equal to the minimum cylinder length for which two polymers can fit inside without overlap or compression. This can be estimated from the relation $L + D = 2L_{\text{ext}}(\infty)$, where $L_{\text{ext}}(\infty)$ is average extension for a single polymer in an infinite cylinder. We note that $L_{\text{ext}}(\infty) \approx 88$ for $N = 200$ and $D = 4$ (see the curve for L_{ext} at large λ in Fig. 3(b)). Consequently, the critical tube length is predicted to be $L \approx 172$, which is approximately consistent with the results in the figure. Likewise, the convergence

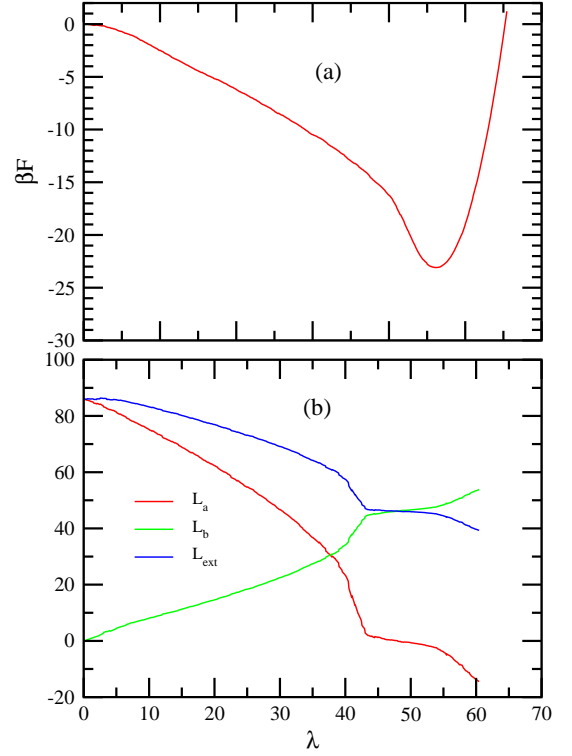


FIG. 8. (a) Free energy function for two chains of length $N = 200$ in a cylinder of diameter $D = 4$ and length $L = 90$. (b) Variation of L_a , L_b and L_{ext} with λ . Negative values of L_a correspond to the (negative) distance between the nearest ends of non-overlapping chains.

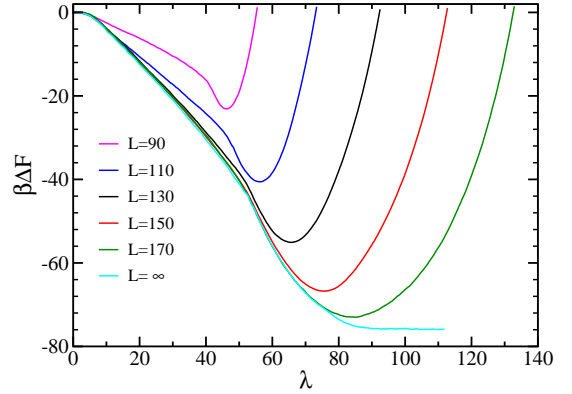


FIG. 9. Free energy functions for polymer chains of length $N = 200$, confined in a cylindrical tube of diameter $D = 4$. Results are shown for several different values of the cylinder length, L . The free energy curves are shifted such that $F = 0$ at $\lambda = 0$.

of F for finite L with that of $L = \infty$ in regime II up to $\lambda \approx 51$ for $L \gtrsim 130$ is also straightforward. At $\lambda = 51$, the combined average extension length of the overlapping chains for $L = \infty$ is $L_a + 2L_b \approx 130$ (using data from Fig. 3(b)). This corresponds to the minimum length of

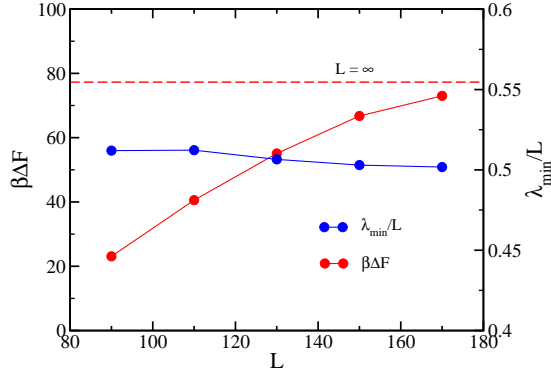


FIG. 10. Free energy barrier height, $\beta\Delta F$, and free energy minimum, λ_{\min} , vs channel length, L . Here, $N = 200$ and $D = 4$. The data correspond to the free energy functions shown in Fig. 9.

the confinement tube that can fit two polymers with this degree of overlap with no deformation from longitudinal confinement. More generally, the deviation of F from the $L = \infty$ curve is expected to occur at lower degrees of overlap, i.e. lower λ , as the confinement length is reduced. This trend is clearly evident in Fig. 9.

Figure 11 shows free energy functions for fixed monomer packing fraction, $\phi \equiv 2Nv/V$, where $v \equiv \pi\sigma^3/6$ is the volume per monomer and where V is the (fixed) confinement volume. Data is shown for $\phi = 0.1257$ for several values of the confinement space aspect ratio, L/D . Clearly, increasing the asymmetry of the tube increases the free energy barrier, ΔF , as well as the equilibrium separation, λ_{\min} . Figure 12(a) shows the variation of ΔF with L/D for three different packing fractions, and in each case ΔF increases with increasing L/D . It is also evident that the barrier height increases with decreasing ϕ . Such an increase in the free energy cost of overlapping chains leads to more effective demixing. Thus, our results are qualitatively consistent with the results of Jung *et al.* for a comparable model system, who found that polymer miscibility decreased (i.e. the tendency for chain demixing increased) with increasing L/D and decreasing ϕ .²⁰ As L/D becomes smaller, the barrier heights for different ϕ converge and tend toward zero. The trend is consistent with the prediction of negligible free energy cost for overlapping chains under spherical confinement.¹⁵ The results are also qualitatively consistent with results from a recent simulation study for the concentrated regime.¹⁷ Figure 12(b) shows the relative free energy minimum position λ_{\min}/L vs L/D . Over the range of L/D considered, λ_{\min}/L is independent of ϕ . In addition, the dependence of λ_{\min}/L on L/D is very weak, and has a value near $\lambda_{\min}/L \approx 0.51$. At low L/D , λ_{\min}/L increases slightly, an indication that the chains are becoming slightly more miscible. The trends for λ_{\min} are consistent with those for the positions of the peaks of the probability distribution shown in Fig. 2(a) of Ref. 20. (Note that the peak positions are shifted to

slightly lower values in that study since flat bounding surfaces were used to cap the cylinder, rather than the hemispheres used here.)

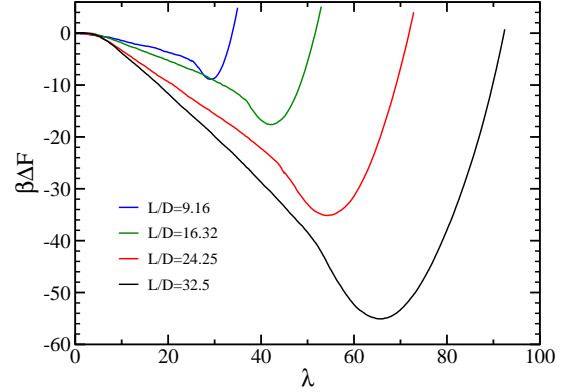


FIG. 11. Free energy functions for polymer chains of length $N = 200$, confined in a finite-length cylindrical tube with a total monomer density of $\phi = 0.1257$. Results are shown for several different values of the cylinder asymmetry ratio, L/D . The free energy curves are shifted such that $F = 0$ at $\lambda = 0$.

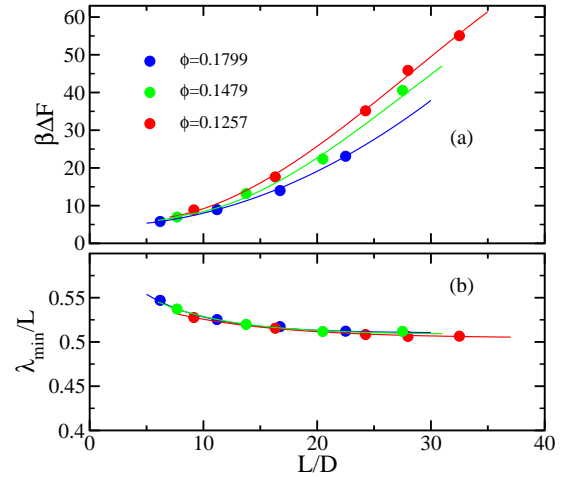


FIG. 12. (a) Free energy barrier height, $\beta\Delta F$, and (b) relative free energy minimum position, λ_{\min}/L , vs cylinder asymmetry, L/D . Data are shown for $N = 200$ for three densities. The solid lines are guides for the eye.

Figure 13 shows the time-dependence of L_a and λ during segregation for polymers of length $N = 200$ in a tube of diameter $D = 4$. Data are shown for the same values of L corresponding to the free energy functions in Fig. 9. Generally, the segregation rate increases monotonically with increasing L , though the rates are very close for $L \leq 130$ at short times. These trends are consistent with expectations based on the trends in Fig. 9 for the entropic force $f \equiv |dF/d\lambda|$, where we note that f increases with increasing L , though f converges for low λ for $L \lesssim 130$.

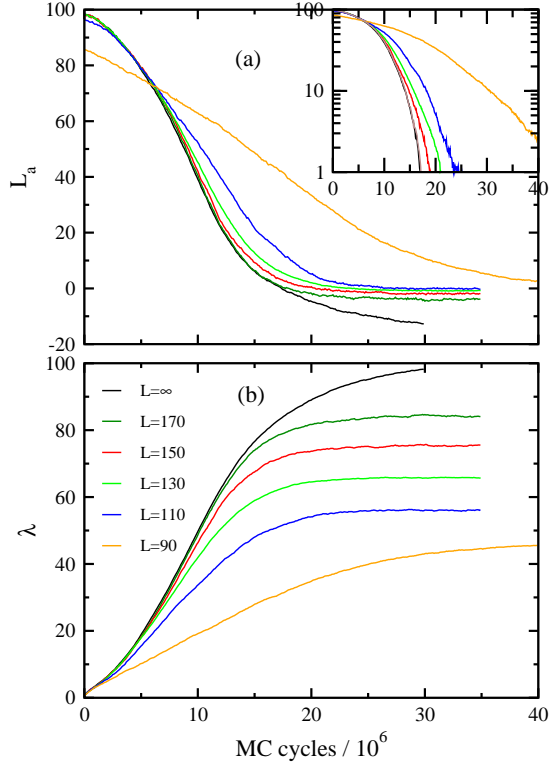


FIG. 13. (a) Time dependence of L_a during segregation for polymers of length $N = 200$ in a cylinder of diameter $D = 4$ and finite length. Results for several different cylinder lengths are shown. The inset shows the results plotted on a semi-log scale. (b) Time dependence of λ for the same system.

Figure 14 shows the relationship of L_a and L_{ext} with λ during segregation. The results are overlaid on those for a system in equilibrium acquired during the simulations used to obtain the free energy functions. The results follow a trend similar to that for $L = \infty$ evident in Fig. 6. During the first stage of segregation ($\lambda \lesssim 50$ and $t \leq 1.2 \times 10^7$) the polymer extension length L_{ext} is very close to the equilibrium values. The overlap length, L_a , is also close, though somewhat lower at very early times. As in the $L = \infty$ case, the rapid reduction in L_{ext} and L_a for the equilibrium system is not observed in the dynamics simulations. Thus, the system goes out of equilibrium during this stage, before reaching the free energy minimum at $\lambda \approx 66$.

C. Effects of bending rigidity

Finally, we consider the case of polymer chains of finite bending rigidity. Figure 15 shows several free energy functions for various values of the polymer stiffness constant, κ , for a system of chains of length $N = 200$ in an infinitely long confinement cylinder of diameter $D = 4$. As the chains become more rigid, the free energy barrier height, $\Delta F \equiv F(0) - F(\infty)$, decreases. As is evident from

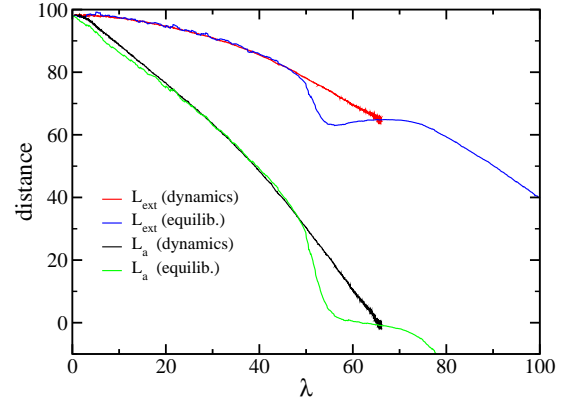


FIG. 14. Variation of L_a and L_{ext} with λ during polymer segregation for a system with $N = 200$, $D = 4$, and $L = 130$. Results are shown for segregation dynamics simulations and for equilibrium simulations.

the inset of the figure, ΔF appears to level off asymptotically to a finite value at large κ , in the limit where the polymers become stiff rods. In addition to this trend, the free energy functions become broader with increasing κ . This is due to an increase in the average extension length of the chains as they stiffen. As chains extend further along the cylinder, they can interact over greater distances. Thus, the reduction in conformational entropy (and increase in F) due to this interaction will occur at larger λ . For these $N = 200$ chains, it is expected that the maximum value for which $F > 0$ should asymptotically approach $\lambda = 200$, which is the maximum separation of rigid linear chains for which contact between the chains is possible. (This estimate neglects the fluctuations in the contour length due to the slight variability of the bond length.) This is consistent with the results in the figure.

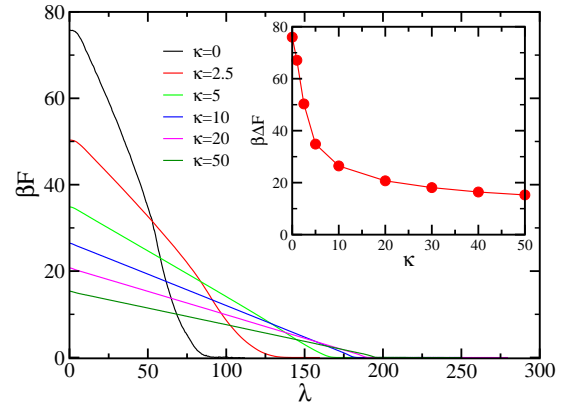


FIG. 15. Free energy functions for various degrees of bending rigidity, κ , for $N = 200$ and $D = 4$. The inset shows the variation of the free energy barrier height with κ .

The trends observed in Fig. 15 are helpful for under-

standing some results of the recent study by Račko and Cifra.²³ In that study, Langevin dynamics simulations were used to study the effects of bending rigidity on the segregation rate for polymers under cylindrical confinement. It was found that flexible chains segregate significantly faster than less flexible chains. They observed a fast-segregation regime for low persistence length P , for which the segregation rate decreased rapidly with increasing stiffness, and a slow-segregation regime at higher P , for which there was little variation of the rate with chain stiffness. For sufficiently high bending rigidity, the chains even failed to segregate over the time scale of the simulation. The transition between the regimes occurred when $P \sim D$. Fast segregation is expected to correspond to a large effective driving force magnitude, $f \equiv |dF/d\lambda|$, which our results show clearly decreases with κ (and, thus, P). In addition, the driving force is also closely correlated with the barrier height, ΔF , which, as the inset of the figure shows, decreases abruptly until $P \approx 5$. Note that $\kappa/k_B T = P/\langle l_{\text{bond}} \rangle$, where $\langle l_{\text{bond}} \rangle \approx \sigma = 1$ is the mean bond length. Thus, the transition occurs when $P \sim D$, and the trends in segregation rates predicted from the free energy results are consistent with those of the dynamics simulations.

Figure 16 shows the overlap distance L_a and extension length L_{ext} as a function of λ for various κ . These data were generated using the same free energy simulations used for Fig. 15. As expected, stiffening the chains leads to greater longitudinal extension of the polymers. This, in turn, leads to a greater degree of overlap for any given separation, λ . Another interesting trend is the gradual disappearance of regime III, in which $L_a \approx 0$ and the extension length L_{ext} first rapidly decreases due to polymer retraction and then slowly increases with λ . As κ is increased, the variation of L_a with λ becomes more uniformly linear. In addition, the “retraction dip” in L_{ext} disappears, and the difference in L_{ext} between the overlap and non-overlapping regions vanishes. As in Fig. 15, the cross-over between the regimes occurs when $P \sim D$.

Consider the case for chains of length $N = 200$ and bending stiffness $\kappa = 40$ in a $D = 4$ cylinder. Since $P \approx 40$ and the contour length of the chain, C , has a value $C \approx 200$, the condition for the Odijk regime, $D \ll P \ll C$ is marginally satisfied. Figure 17 shows the free energy function for this system. The curve is highly linear over the range $12 \lesssim \lambda \lesssim 188$, with slight deviations from linearity for $0 \leq \lambda \lesssim 12$ and $188 \lesssim \lambda \lesssim 195$. (The inset of the figure illustrates the deviation for the latter case.) These regions correspond to $L_b \lesssim 12$ and $L_a \lesssim 7$, respectively.

The trend where F varies linearly with λ , with only slight discrepancies near the edges of the regime where the chains overlap, is a generic feature of systems we have examined that marginally satisfy the Odijk condition. The derivative $F'(\lambda)$ in the linear domain was calculated for these systems by fitting $F(\lambda)$ in this region with a linear function. Figure 18(a) shows the variation of the magnitude of the derivative, $\beta|F'(\lambda)|$, vs P for

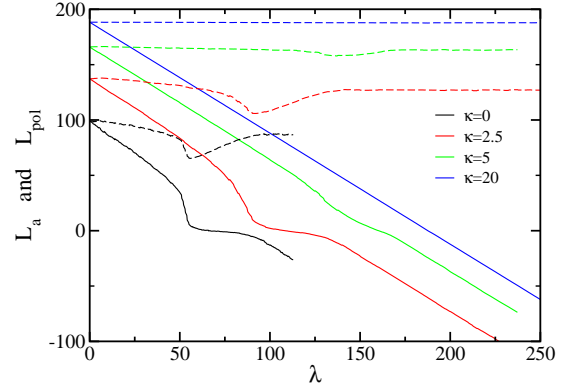


FIG. 16. Overlap length L_a (solid lines) and polymer extension length L_{ext} (dashed lines) vs λ for various degrees of bending rigidity, κ , for $N = 200$ and $D = 4$. The data were generated using the same simulations used for the results in Fig. 15.

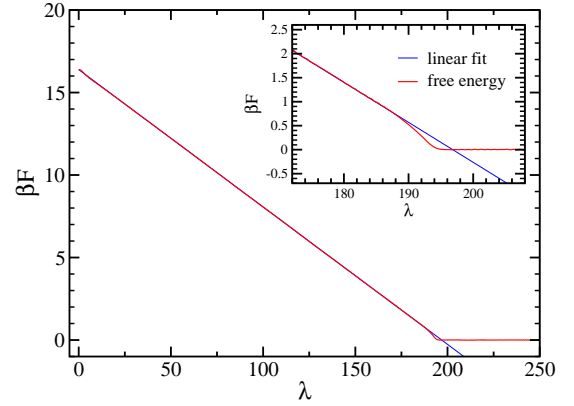


FIG. 17. Free energy function for polymer chains of length $N = 200$ and bending rigidity $\kappa = 40$ in an infinite tube of diameter $D = 4$. The blue curve shows a linear fit to most of the data. The inset shows a close up near the point past which the polymers no longer overlap.

four different cylinder diameters. For each D , a fit to the function $\beta|F'| \sim P^{-\alpha}$, yields exponents near $\alpha \approx 0.37$ in all cases. Figure 18(b) shows the same data, except with the derivatives scaled by a factor of $D^{2.03}$. This scaling factor was found to yield the best collapse of the data onto a single function. Thus, the results suggest that $\beta|F'| \sim D^{-\beta} P^{-\alpha}$ in the Odijk regime, where $\beta \approx 2$ and $\alpha \approx 0.37$.

A theoretical prediction for the scaling of $F'(\lambda)$ with respect to D and P in the Odijk regime can be derived as follows. First recall that the confinement free energy of a single chain, F_1 , can be approximated by assigning $k_B T$ for each deflection of the chain off of the walls of the confining cylinder. Thus, $F_1 \sim k_B T L_{\text{ext}}/l_{\text{def}}$, where the Odijk deflection length is given by $l_{\text{def}} \approx D^{2/3} P^{1/3}$.³³ The confinement free energy of a system of two overlap-

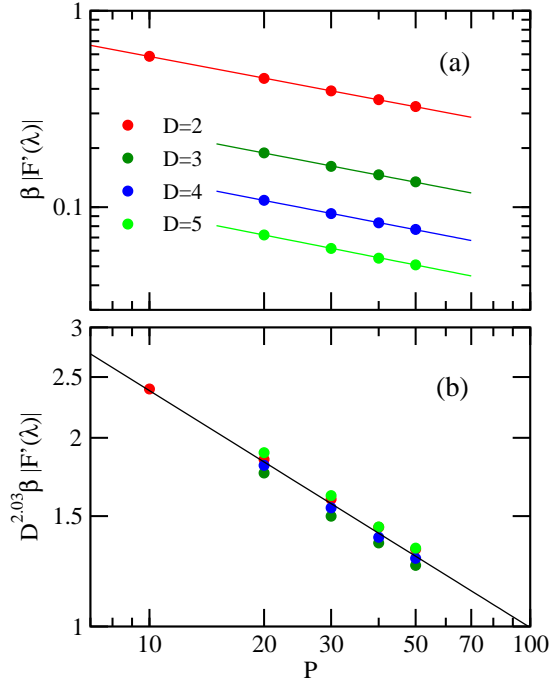


FIG. 18. (a) Magnitude of the free energy function derivative, $\beta|dF/d\lambda|$, vs polymer persistence length, P . The derivative is obtained from a fit to the linear region of $F(\lambda)$ for systems that marginally satisfy the condition for the Odijk regime. Data are shown for $N = 200$ chains for four cylinder diameters and are chosen to satisfy $4D \leq P \leq 4C$. The solid lines are power law fits of the four data sets. (b) Scaled free energy function derivatives, $D^{2.03}\beta|F'(\lambda)|$ vs P using the data in (a). The solid line is a power law fit to all of the data. The fit yielded $D^{2.03}\beta|F'(\lambda)| \sim P^{-0.37}$.

ping chains can be written, $F_c = 2F_1 + F^{(\text{int})}$, where $F^{(\text{int})}$ is the interaction free energy associated with the overlapping portions of the chains. This term can be estimated using an approximation of the free energy of a system of long, hard rigid rods. For that system, recall that the interaction free energy per particle, in the 2nd virial approximation, is given by $F^{(\text{int})}/Nk_B T = (l^2 \sigma N/V) \langle |\sin \gamma| \rangle$ for N rods of length l and diameter σ confined to a volume V , where γ is the angle between two rods.³⁴ For highly aligned systems, $\langle |\sin \gamma| \rangle \sim \sqrt{\langle \theta^2 \rangle}$, where θ is the angle between the rod and the alignment direction. To apply this result to the present system, we treat a deflection segment of length l_d as a rigid rod, and note that V corresponds to the volume over which intermolecular segments overlap. Thus, we substitute $l \rightarrow l_d \sim D^{2/3} P^{1/3}$, $N \rightarrow 2N_d \equiv 2L/l_d$, and $V \sim L_a D^2$. In addition, assuming that the alignment arises principally from the confinement, $\langle \theta^2 \rangle \sim (D/l_d)^2$. It follows that the overlap free energy is $\beta F \equiv \beta(F_c - 2F_1) \sim L_a \sigma D^{-5/3} P^{-1/3}$. Next, we note that $L_a \approx L_{\text{ext}} - \lambda$, where the extension length L_{ext} was confirmed to be constant with respect to λ (data not shown). This leads finally to the prediction that $d(\beta F)/d\lambda \sim -\sigma D^{-\beta} P^{-\alpha}$,

where $\beta = 5/3$ and $\alpha = 1/3$.

The predicted exponents are comparable to the measured exponents, though the differences between them are still significant. It is likely that the ratios P/D and C/P are not sufficiently large for some of the approximations to be completely valid. The deviations of this scaling from the form $\beta F'(\lambda) \sim D^{-\beta} P^{-\alpha}$, evident in the scatter of the data points about the best fit curve in Fig. 18(b), also suggest that the scaling regime has not been reached. We speculate that agreement with the predicted scaling would improve if the Odijk conditions were better satisfied. However, such verification requires using much longer polymer chains, which is not feasible for us at present.

V. CONCLUSIONS

In this study, we have used MC simulations to systematically study the overlap free energy function, $F(\lambda)$, for two linear polymers with center of mass separation, λ , confined in a cylindrical tube of diameter D and length L . As expected, F increases with decreasing polymer separation. In the case of flexible chains confined to tubes of infinite length, the functions are characterized by well defined domains. One unexpected result is the existence of a domain in which the polymers do not overlap, but are in contact and are compressed. This domain disappears when the polymers stiffen, with the cross-over at $P \sim D$, where P is the persistence length. We observe scaling laws for the free energy functions for both flexible and semi-flexible chain systems that are qualitatively consistent with theoretical predictions using scaling arguments. However, there are deviations observed between the measured and predicted values of the scaling exponents, which are most likely due to insufficiently satisfying the conditions defining the de Gennes and Odijk regimes. For confinement cylinders of finite L , the free energy barrier height increases with increasing confinement aspect ratio, L/D , at fixed packing fraction, ϕ , and decreases with increasing ϕ at fixed L/D . These results are consistent with previous measurements of polymer miscibility for a comparable model system.²⁰

While the main focus of this work is the characterization of the free energy functions, we also carried out simulations to study the dynamics of segregation. The goal here was to examine the relationship between the segregation rates and the free energy functions. One notable result is the deviation from conformational quasi-equilibrium observed at later times during polymer separation. This implies that the free energy functions cannot be used (e.g. in the Fokker-Plank equation) to make quantitatively accurate predictions for the segregation dynamics, since the $F(\lambda)$ characterizes a system in equilibrium. Nevertheless, we did observe the intuitively appealing qualitative trend that the rate of polymer segregation is generally faster when $|dF/d\lambda|$ increases. Furthermore, although we did not study the segregation

dynamics for chains of finite stiffness in this work, the observed effect of varying the chain rigidity on the free energy functions does qualitatively explain the observed trends in a recent Langevin dynamics simulation study.²³

This work has focused on the overlap free energy for systems of relatively short ($N \leq 200$) linear polymers. In future work, we will extend the present study in several ways. In order to make the results more applicable to chromosome separation in bacteria, we will examine the free energy functions of cylindrically confined ring polymers, as well as examine the role of crowding agents, as in Ref. 24. Preliminary calculations using ring polymers have thus far yielded trends comparable to those observed here. In addition, we will study systems of much longer chain lengths by employing more efficient Monte Carlo simulation methods. This will allow a more effective test of the scaling predictions described in this work. It will also enable us to examine the changes in the free energy as a system of semi-flexible polymers transitions from the Odijk to the de Gennes regimes upon increasing the confinement diameter.

ACKNOWLEDGMENTS

This work was supported by the Natural Sciences and Engineering Research Council of Canada (NSERC). We are grateful to the Atlantic Computational Excellence Network (ACEnet) for use of their computational resources.

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