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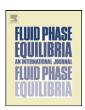
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## Measurement and modelling of solubility for calcium sulfate dihydrate and calcium hydroxide in NaOH/KOH solutions

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#### ABSTRACT

The solubility of calcium sulfate dihydrate ( $CaSO_4 \cdot 2H_2O$ ) and calcium hydroxide ( $Ca(OH)_2$ ) in alkali solutions is essential to understand their desilication behavior from Bayer liquor. In this work, solubilities of calcium sulfate dihydrate and calcium hydroxide for the ternary systems of  $CaSO_4 \cdot 2H_2O - NaOH - H_2O$ , CaSO $_4 \cdot 2H_2O - KOH - H_2O$ , and  $Ca(OH)_2 - NaOH - H_2O$  were measured by using the classic isothermal dissolution method over the temperature range of 25–75 °C. The Pitzer model embedded in Aspen Plus platform was used to model the experimental solubility data for these systems. The experimental solubility data was employed to obtain the new binary interaction parameters for  $Ca(OH)^* - OH^-$ ,  $Ca(OH)^* - Ca^{2*}$  and  $Ca(OH)^* - K^*$ , suggesting that the species  $Ca(OH)^*$  is a dominant species in simulated solubility for alkali systems. Validation of the parameters was performed by predicting the solubility for the ternary systems of  $Ca(OH)_2 - NaOH - H_2O$ ,  $CaSO_4 \cdot 2H_2O - NaOH - H_2O$  and  $CaSO_4 \cdot 2H_2O - KOH - H_2O$  with the overall average relatively deviation (ARD) of 2.12%, 0.75% and 1.63%, respectively.

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#### 1. Introduction

Bauxite, the major source of aluminium containing ore used in the production of alumina, includes several impurities, such as iron, titanium and silica components [1–3]. The presence of silica in bauxite can give rise to an appreciable loss of caustic soda and aluminum in forming desilication products (DSP), as well as cause scale build-up due to the re-precipitation of complex sodalite-type DSP on plant surfaces. Therefore, during the extraction of alumina from bauxite, the removal of silicate ions is necessary, especially when using diaspore bauxite containing high silica. The conventional method of removing silicates can be achieved by introducing chemicals, such as calcium oxide (CaO) and calcium hydroxide (Ca(OH)<sub>2</sub>) [4–6].

Previous experimental studies show that  $CaSO_4 \cdot 2H_2O$  also has high desilication capacity, and significant amounts of sulfate in liquor can be included into the DSP which became more stable desilication product [7]. The solubilities of calcium sulfate dihydrate in acid solutions have been extensively studied. However, limited work has been done about the solubility of calcium sulfate dihydrate in alkali solutions. Furthermore, we found that calcium sulfate dihydrate in sodium hydroxide solutions was unstable and

quickly transformed to calcium hydroxide at NaOH concentration more than  $0.10\,\text{mol}\,\text{L}^{-1}.$  In order to fully understand the desilication behavior of  $\text{CaSO}_4\cdot 2\text{H}_2\text{O}$  and  $\text{Ca}(\text{OH})_2$  in alkali solutions, it is necessary to investigate the solubility of  $\text{CaSO}_4\cdot 2\text{H}_2\text{O}$  and  $\text{Ca}(\text{OH})_2$  in alkali solutions.

A suitable thermodynamic model is very important for calculating the thermodynamic properties of mixed electrolyte solutions, and for evaluating the results of solubility data. Most of the previous studies have focused on the solubility of calcium sulfate dihydrate in acid solutions. Tanji [8] developed a computer program around a chemical model based on the formation of the ion pairs of CaSO<sub>4</sub><sup>0</sup>, MgSO<sub>4</sub><sup>0</sup>, and NaSO<sub>4</sub><sup>-</sup>. This model proved useful in dealing with the solubility of CaSO<sub>4</sub>·2H<sub>2</sub>O in dilute acid systems. Li and Demopoulos [9] used the Bromley-Zemaitis activity coefficient model to calculate the solubility of calcium sulfate in multi-component aqueous chloride solutions. Azimi et al. [10] applied the mixed solvent electrolyte (MSE) activity coefficient model to accurately model the solubility of CaSO<sub>4</sub>·2H<sub>2</sub>O and its scaling potential in sulfate systems. Barba et al. [11,12] successfully used their thermodynamic model based on the nonrandom two-liquid (NRTL) equation to investigate the behavior of calcium sulfate dihydrate solubility in aqueous solutions of Na<sub>2</sub>SO<sub>4</sub> and MgCl<sub>2</sub> on the basis of experimental solubility values at 40 °C. Pitzer's equations were also used by Meijer and Rosmalen [13] who proposed a computer program to calculate the solubility and supersaturation of CaSO<sub>4</sub> in seawater. Harvie and Weare [14] using Pitzer's framework developed a chemical model

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for predicting solubility of gypsum in NaCl solutions. However, the chemistry of calcium sulfate dihydrate systems has been rarely modelled in multi-component alkali solutions due to scarce solubility data. Pitzer equation has been successfully used to calculate solubility of  $\text{Ca}(\text{OH})_2$  in the NaOH solutions at 13, 20 and 40 °C [15], and the experimental solubility data can be well correlated by the model. Hence, the Pitzer model has shown the potential capability in predicting solubility data of salts for alkali systems. Furthermore, the Pitzer model has been rendered into AspenPlus<sup>TM</sup> commercial software and widely applied in industry. Consequently, we decided to choose the Pitzer model embedded in the AspenPlus platform to model the solubility of  $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$  and  $\text{Ca}(\text{OH})_2$  in alkali solutions in present study.

In this work, the solubility of  $CaSO_4 \cdot 2H_2O$  for the ternary systems of  $CaSO_4 - NaOH - H_2O$  and  $CaSO_4 - KOH - H_2O$  were presented at the temperature range of 35 - 75 °C and the alkali concentration range of  $0 - 0.09 \, \text{mol} \, L^{-1}$ . The solubility data of  $Ca(OH)_2$  for the ternary system  $Ca(OH)_2 - NaOH - H_2O$  were also measured at the temperature range of 25 - 75 °C and the NaOH concentration range of  $0 - 0.5 \, \text{mol} \, L^{-1}$ . The solubility data for above ternary systems were successfully modelled using the Pitzer model embedded in the AspenPlus platform. New interaction parameters for the associated hydroxyl calcium ion  $Ca(OH)^+$  with the other dominant species in alkali solutions were determined.

#### 2. Experimental

#### 2.1. Materials

All chemical reagents used in the experiments were analytical grade without further purification. The concentration of the solutions made with reagent grade NaOH and KOH was verified by titration with standardized  $H_2SO_4$ . The water used in all experimental work was double distilled water (conductivity < 0.1  $\mu$ S cm<sup>-1</sup>).

#### 2.2. Apparatus and procedure

The 200 mL of alkali solution of known composition was poured into a 250-mL polytetrafluoroethylene bottle, which were equipped with a magnetic stirrer and sealed with a polytetrafluoroethylene-lined cap. The bottles were then immersed in a temperature-controlled water bath, allowing the solution to stir continuously for about 0.5 h to establish the temperature equilibrium. The temperature was kept constant within 0.1 °C. Then, excess solid (4g) was quickly added to the solutions in bottles, which were tightly sealed again. The standard equilibration time used was 6 h, and the determination of equilibration time is explained in the next section. After the solid-liquid equilibrium was attained, stirring was stopped to allow solids to settle by 6 h. The supernatant solution was then taken with a pipette and immediately filtered by using 0.22 µm Whatman Puradisc syringe filters. The clear filtrate was added into a 25-mL volumetric flask which was kept in the water bath and then heated to bath temperature for measuring the density of saturated solution. The solubility of solids was determined by titration of Ca with EDTA. The solid phase was filtered and washed three times with water. The washed solids were dried at 50 °C for 12 h and then analyzed by X-ray powder diffraction to determine the final solid phase.

#### 2.3. Determination of equilibration time

The equilibration time in solubility measurements normally varies from several hours to several days depending on the dissolution rate of the solid phase and the applied conditions [16]. Li and Demopoulos reported that the equilibration time of solid and liquid

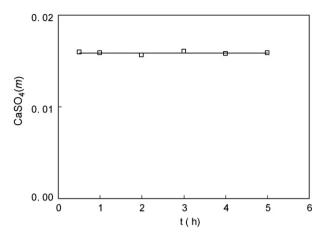


Fig. 1. Solubility of CaSO<sub>4</sub>·2H<sub>2</sub>O in NaOH solutions versus the equilibrium time.

can be reached within 0.5 h in determining the solubility of calcium sulfate dihydrate in HCl solution [17]. As can be seen from Fig. 1, after 30 min, the solubility of calcium sulfate dihydrate in sodium hydroxide solution stabilizes. In present work, a longer time of 6 h was selected to ensure solubility equilibrium.

#### 2.4. Reproducibility

The solubility of calcium hydroxide in pure water has been investigated by Cameron and Robinson [18]. Similar experiments were carried out by the authors to verify the reproducibility and accuracy of the adopted procedure in this work. The solubility of calcium hydroxide in water at  $25\,^{\circ}\text{C}$  was measured. The uncertainty of the determined solubility values was within  $\pm 0.00009\,\text{mol}\,\text{kg}\,\text{H}_2\text{O}^{-1}$  with a relative deviation of 0.4%. The results showed that the experimental procedure for measuring solubility was considered to be reliable and feasible.

#### 2.5. Solubility measurement

The XRD analysis of equilibrated solid phases showed calcium sulfate dihydrate in alkali solutions to be stable at the temperature range of  $35-75\,^{\circ}\text{C}$  and the alkali concentration range of  $0.01-0.09\,\text{mol}\,\text{L}^{-1}$ . The results of equilibrated solids characterization by XRD are listed in Table 1. It can be clearly seen that calcium sulfate dihydrate in alkali solutions is stable at the alkali concentration range of  $0.01-0.09\,\text{mol}\,\text{L}^{-1}$  while it was partially transformed to calcium hydroxide at alkali concentration of  $0.1\,\text{mol}\,\text{L}^{-1}$ .

The solubility data of calcium sulfate dihydrate for the ternary systems of CaSO<sub>4</sub>·2H<sub>2</sub>O–NaOH–H<sub>2</sub>O and CaSO<sub>4</sub>·2H<sub>2</sub>O–KOH–H<sub>2</sub>O over the temperature range from 35 to 75 °C are measured by using

 $\label{eq:table 1} \textbf{XRD } characterization of the equilibrated solids in the $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}-\text{NaOH-KOH-H}_2\text{O}$ systems.$ 

T(K)	c (mol L <sup>-1</sup> )	t (h)	Equilibrated solid phase(s)
308.15	0.01-0.09 (NaOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
318.15	0.01-0.09 (NaOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
328.15	0.01-0.09 (NaOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
338.15	0.01-0.09 (NaOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
348.15	0.01-0.09 (NaOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
308.15-348.15	0.1 (NaOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
308.15	0.01-0.09 (KOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
318.15	0.01-0.09 (KOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
328.15	0.01-0.09 (KOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
338.15	0.01-0.09 (KOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
348.15	0.01-0.09 (KOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O
308.15-348.15	0.1 (KOH)	6	CaSO <sub>4</sub> ·2H <sub>2</sub> O and Ca(OH) <sub>2</sub>

**Table 2** Solubility of CaSO<sub>4</sub>·2H<sub>2</sub>O (1) in NaOH (2)+H<sub>2</sub>O (3).

$M_2  (\mathrm{mol}  \mathrm{L}^{-1})$	$ ho_{ m s}$ (g mL $^{-1}$ )	$C_1 (g L^{-1})$	$m_1^{\mathrm{exp}}~(\mathrm{molkg^{-1}})$	$m_1^{\mathrm{cal}}~(\mathrm{molkg^{-1}})$	$(m_1^{\rm exp} - m_1^{\rm cal})/m_1^{\rm exp}~(\%)$
T=308.15 K					
0.00	0.9961	2.1044	0.01550	0.01541	0.60
0.01	0.9958	2.3281	0.01724	0.01720	0.24
0.03	0.9985	2.7347	0.02022	0.01979	2.12
0.05	1.0005	3.1097	0.02297	0.02303	-0.28
0.07	1.0004	2.7735	0.02050	0.02049	0.05
0.09	0.9984	2.5449	0.01886	0.01893	-0.40
T=318.15 K					
0.00	0.9923	2.0955	0.01539	0.01529	0.63
0.01	0.9912	2.3050	0.01715	0.01718	-0.20
0.03	0.9935	2.7111	0.02014	0.01991	1.14
0.05	0.9942	2.8216	0.02097	0.02118	-0.99
0.07	0.9957	2.6394	0.01960	0.01932	1.41
0.09	0.9964	2.4481	0.01817	0.01802	0.88
T=328.15 K					
0.00	0.9877	2.0535	0.01512	0.01503	0.57
0.01	0.9897	2.2612	0.01684	0.01704	-1.18
0.03	0.9903	2.6905	0.02006	0.02004	0.08
0.05	0.9899	2.6724	0.01995	0.02008	-0.68
0.07	0.9914	2.4432	0.01822	0.01820	0.12
0.09	0.9938	2.2964	0.01709	0.01715	-0.31
T=338.15 K					
0.00	0.9825	1.9860	0.01461	0.01457	0.26
0.01	0.9860	2.2103	0.01653	0.01672	-1.15
0.03	0.9863	2.6409	0.01977	0.02014	-1.87
0.05	0.9883	2.4620	0.01840	0.01858	-0.95
0.07	0.9875	2.2814	0.01708	0.01707	0.04
0.09	0.9908	2.1890	0.01634	0.01633	0.04
T=75 °C					
0.00	0.9767	1.8995	0.01395	0.01385	0.69
0.01	0.9842	2,1133	0.01583	0.01606	-1.44
0.03	0.9847	2.6253	0.01968	0.01983	-0.74
0.05	0.9856	2.2792	0.01708	0.01693	0.89
0.07	0.9856	2.1400	0.01605	0.01592	0.79
0.09	0.9865	2.0524	0.01539	0.01555	-1.05
			ADD (%) 0.72		
/ n			ARD (%) = 0.73		

$$ARD(m) = \left(\sum_{i=1}^{n} \left| m^{cal} - m^{exp} \right| / m^{exp} \right) / n.$$

above procedure and tabulated in Tables 2 and 3. The solubility data of calcium hydroxide for ternary system Ca(OH) $_2$ -NaOH-H $_2$ O at the temperature range of 25–75  $^{\circ}$ C are also determined and listed in Table 4 .

#### 3. Modelling approach

3.1. Thermodynamic equilibria of  $CaSO_4 \cdot 2H_2O$  (or  $Ca(OH)_2$ )-NaOH-KOH-H<sub>2</sub>O system

Eqs. (1)–(3) represent the common dissociation equilibria for all systems considered in this work.

$$CaSO_4 \cdot 2H_2O(s) \leftrightarrow Ca^{2+} + SO_4^{2-} + 2H_2O$$
 (1)

$$Ca(OH)_2(s) \leftrightarrow Ca(OH)^+ + OH^- \tag{2}$$

$$Ca(OH)^+ \leftrightarrow Ca^{2+} + OH^- \tag{3}$$

The thermodynamic equilibrium constants for the dissociation reactions (1)–(3) are:

$$K_{\text{CaSO}_4 \cdot 2\text{H}_2\text{O(S)}} = (m_{\text{Ca}^{2+}} \gamma_{\text{Ca}^{2+}}) (m_{\text{SO}_4^{2-}} \gamma_{\text{SO}_4^{2-}}) (\alpha_{\text{H}_2\text{O}})^2$$

$$= (m_{\text{Ca}^{2+}}) (m_{\text{SO}_4^{2-}}) \gamma_{\pm \text{CaSO}_4}^2 (\alpha_{\text{H}_2\text{O}})^2$$
(4)

$$K_{Ca(OH)_2(S)} = (m_{Ca(OH)^+} \gamma_{Ca(OH)^+})(m_{OH^-} \gamma_{OH^-})$$
 (5)

$$K_{\text{Ca(OH)}^{+}} = \frac{(m_{\text{Ca}^{2+}}\gamma_{\text{Ca}^{2+}})(m_{\text{OH}^{-}}\gamma_{\text{OH}^{-}})}{(m_{\text{Ca(OH)}^{+}}\gamma_{\text{Ca(OH)}^{+}})}$$
(6)

By re-arranging Eqs. (4)–(6), the molalities of the free calcium ion  $\text{Ca}_1^{2+}$  for the ternary system  $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$ –alkali– $\text{H}_2\text{O}$ , the free calcium ion  $\text{Ca}_2^{2+}$  for the ternary system  $\text{Ca}(\text{OH})_2$ –NaOH–H $_2\text{O}$ , and the hydroxyl calcium ion  $\text{Ca}(\text{OH})^+$  are:

$$m_{\text{Ca}_{1}^{2+}}^{2+} = \frac{K_{\text{CaSO}_{4} \cdot 2\text{H}_{2}\text{O(s)}}}{m_{\text{SO}_{4}^{-2}} \gamma_{\pm \text{CaSO}_{4}}^{2} (\alpha_{\text{H}_{2}\text{O}})^{2}}$$
(7)

$$m_{\text{Ca(OH)}^{+}} = \frac{K_{\text{Ca(OH)}_{2}(s)}}{\gamma_{\text{Ca(OH)}^{+}}(m_{\text{OH}^{-}}\gamma_{\text{OH}^{-}})}$$
(8)

$$m_{\text{Ca}_{2}^{2+}} = \frac{K_{\text{Ca}(\text{OH})^{+}}(m_{\text{Ca}(\text{OH})^{+}}\gamma_{\text{Ca}(\text{OH})^{+}})}{\gamma_{\text{Ca}^{2+}}(m_{\text{OH}^{-}}\gamma_{\text{OH}^{-}})}$$
(9)

The solubility of calcium sulfate dihydrate and calcium hydroxide is equal to the sum of molalities of the calcium containing species as follows:

$$s_{\text{CaSO}_4 \cdot 2\text{H}_2\text{O}} = m_{\text{Ca}_1^{2+}} + m_{\text{Ca}(\text{OH})^+}$$
 (10)

$$s_{\text{Ca(OH)}_2} = m_{\text{Ca}_2^{2+}} + m_{\text{Ca(OH)}^+}$$
 (11)

**Table 3** Solubility of  $CaSO_4 \cdot 2H_2O(1)$  in KOH (2)+ $H_2O(3)$ .

T=308.15 K 0.01 0.03 0.05	0.9954 1.0016 1.0021	2.3545 2.8455	0.01744	0.04500	
0.03	1.0016		0.01744	0.04700	
		2 8455		0.01722	1.29
0.05	1.0021	2.0 133	0.02098	0.01990	5.18
0.03		3.2190	0.02376	0.02315	2.59
0.07	1.0026	2.7444	0.02026	0.02047	-1.05
0.09	1.0027	2.5557	0.01888	0.01891	-0.16
T=318.15 K					
0.01	0.9915	2.3420	0.01742	0.01720	1.24
0.03	0.9947	2.8147	0.02090	0.02000	4.30
0.05	0.9956	2.9109	0.02162	0.02124	1.79
0.07	0.9967	2.6164	0.01943	0.01932	0.55
0.09	0.9988	2.4556	0.01822	0.01799	1.22
T=328.15 K					
0.01	0.9910	2.2958	0.01708	0.01707	0.08
0.03	0.9898	2.7925	0.02084	0.02013	3.42
0.05	0.9949	2.6616	0.01978	0.02008	-1.54
0.07	0.9960	2.4354	0.01810	0.01820	-0.56
0.09	0.9977	2.3401	0.01737	0.01713	1.39
T=338.15 K					
0.01	0.9873	2.1929	0.01638	0.01674	-2.20
0.03	0.9875	2.7148	0.02031	0.02041	-0.53
0.05	0.9942	2.4420	0.01816	0.01861	-2.48
0.07	0.9953	2.2715	0.01689	0.01708	-1.16
0.09	0.9968	2.1787	0.01619	0.01631	-0.78
T=348.15 K					
0.01	0.9871	2.1765	0.01626	0.01609	1.04
0.03	0.9877	2.6395	0.01974	0.01976	-0.12
0.05	0.9896	2.3382	0.01746	0.01703	2.51
0.07	0.9919	2.1928	0.01636	0.01597	2.37
0.09	0.9942	2.1177	0.01578	0.01555	1.41
			ARD (%) = 1.64		

In order to calculate the solubility of calcium sulfate dihydrate and calcium hydroxide in alkali solution, the solubility product  $K_{\text{CaSO}_4\cdot 2\text{H}_2\text{O}(s)}$  and  $K_{\text{Ca}(\text{OH})_2}(s)$ , and  $K_{\text{Ca}(\text{OH})^+}$  as well as the activity coefficients of relevant species need to be determined.

#### 3.2. Equilibrium constant

The equilibrium constant of a reaction can be evaluated from the Gibbs free energy relation:

$$K = \exp\left(-\frac{\Delta G_r^0}{RT}\right) = \exp\left(-\frac{\sum \nu_i \mu_i^0}{RT}\right)$$
 (12)

Unfortunately, the equilibrium constant for the SLE calculation in Eq. (12) determined from the standard chemical potential  $\mu^0$  of individual species is not always available or accurate. Therefore, this equilibrium constant is regressed from experimental measurements in the form of a temperature function:

$$\ln K(T) = k_1 + \frac{k_2}{T} + k_3 \ln T + k_4 T \tag{13}$$

 $k_1$  to  $k_4$  are determined in extrapolation or regression procedures from various types of electrolyte data. In present work, these equilibrium constants existing in the databank of Aspen Plus were directly used.

#### 3.3. The Pitzer activity coefficient model

The Pitzer model embedded in the Aspen Plus platform was employed for the studied systems. The model has been discussed in detail in many publications. Here, we give only the expression for the excess Gibbs free energy [19]:

$$\frac{G^{E}}{RT} = n_{w} \left[ f(I) + \sum_{i} \sum_{j} B_{ij} m_{i} m_{j} + \sum_{i} \sum_{j} \theta_{ij} m_{i} m_{j} + 1/2 \sum_{i} \sum_{j} \left( \sum_{k} m_{k} |z_{k}| \right) \right] \times C_{ij} m_{i} m_{j} + 1/6 \sum_{i} \sum_{j} \sum_{k} \psi_{ijk} m_{i} m_{j} m_{k}$$
(14)

The cation–anion parameters  $B_{ij}$  and  $C_{ij}$  are characteristic for an aqueous single-electrolyte system.  $B_{ij}$  is expressed as a function of  $\beta^0_{ij}$  and  $\beta^1_{ij}$  or  $\beta^0_{ij}$ ,  $\beta^2_{ij}$  and  $\beta^3_{ij}$ .  $\theta_{ij}$  and  $\psi_{ijk}$  are for the difference of interaction of unlike ions of the same sign from the mean of like ions.

These parameters  $B_{ij}$ ,  $C_{ij}$ ,  $\theta_{ij}$  and  $\psi_{ijk}$  follow the temperature dependency relation:

$$parameter(T) = a_1 + a_2(T - T^{ref}) + a_3\left(\frac{1}{T} - \frac{1}{T^{ref}}\right) + a_4 \ln\left(\frac{T}{T^{ref}}\right)$$
(15)

The activity coefficient is a parameter which accounts for the nonideality of electrolyte solutions, and is defined by the excess Gibbs free energy of the solution:

$$\ln \gamma_i = \left(\frac{\partial (G^E/RT)}{\partial n_i}\right)_{T,P,n_{i\neq j}} \tag{16}$$

#### 3.4. Compilation and reduction of experimental data

In order to use the Aspen regression property analysis, molality should be transformed to mole fraction. Therefore, the following

**Table 4** Solubility of Ca(OH)<sub>2</sub> (1) in NaOH (2)+ $H_2O$  (3).

7-298.15 K 000	$M_2$ (mol L <sup>-1</sup> )	$ ho_{ m s}$ (g mL $^{-1}$ )	$C_1 (g L^{-1})$	$m_1^{\mathrm{exp}}~(\mathrm{molkg^{-1}})$	$m_1^{\mathrm{cal}}~(\mathrm{molkg^{-1}})$	$(m_1^{\rm exp} - m_1^{\rm cal})/m_1^{\rm exp}$ (2)
0.01	T=298.15 K					
1,001	0.00	0.9990	1.5566	0.02109	0.02180	-3.36
1,001	0.01	1.0000	1.3955	0.01889	0.01822	3.58
0.05	0.03	1.0013		0.01334	0.01271	4.73
1,0030						
1,009						
1.15						
1,095						
1,000						
1.040						
1.50						
F-308.15   K						
1,000	).50	1.0204	0.0790	0.00107	0.00104	2.65
1,000	C= 308 15 K					
1.01		0.0058	1 /177	0.01927	0.02000	3 79
0.03         0.9961         0.7847         0.0106         0.01090         -2.19           0.05         0.9971         0.5552         0.00727         0.00739         -2.67           0.09         0.9987         0.2799         0.00379         0.00408         -7.59           0.15         1.0012         0.1943         0.00264         0.00264         0.12           1.20         1.0032         0.1463         0.00199         0.00201         -1.31           1.30         1.0065         0.0997         0.00135         0.00137         -1.77           1.50         1.0025         0.0783         0.00106         0.00138         -1.41           1.50         1.0055         0.0647         0.00089         0.00990         -1.37           1.50         1.0065         0.09937         0.0158         0.00108         -1.41           1.50         1.007         0.09937         1.130         0.01838         0.01907         -3.73           1.01         0.9937         1.1470         0.01562         0.01533         0.56           1.02         0.9937         1.1470         0.01562         0.01533         0.56           1.03         0.9948         0.7469						
0.05         0.9971         0.5352         0.00727         0.00747         -2.67           1.07         0.9976         0.3795         0.00516         0.00539         -4.60           0.19         0.9987         0.2790         0.00279         0.00408         -7.59           1.15         1.0012         0.1463         0.00199         0.00201         -1.31           1.30         1.0065         0.0937         0.00135         0.00137         -1.17           1.40         1.0125         0.0783         0.00106         0.00108         -1.41           1.40         1.0125         0.0783         0.00106         0.00108         -1.41           1.50         1.0065         0.0647         0.0008         0.0009         -1.37           1.51         1.0066         0.0647         0.0008         0.0009         -1.33           1.50         1.007         0.0937         1.1470         0.01562         0.01553         0.56           1.00         0.9939         1.1470         0.01562         0.01553         0.56           1.00         0.9948         0.7469         0.01017         0.01199         0.02           1.07         0.9955         0.4378						
0.976						
0.99						
1.15         1,0012         0.1943         0.00264         0.0264         0.12           1.20         1,0032         0.1463         0.00199         0.00201         113           1.30         1,0065         0.0997         0.00135         0.00137         -117           1.50         1,0065         0.0647         0.00089         0.00090         -137           1.50         1,0065         0.0647         0.00089         0.00090         -1.37           2.71         1,1065         0.0647         0.00089         0.00090         -1.37           2.72         1,1170         0.01632         0.0167         -3.73         0.00090         -1.37           2.72         1,1170         0.0152         0.01533         0.0160         0.9837         1.1470         0.01562         0.01533         0.056         0.0563         0.056         0.0563         0.056         0.0563         0.056         0.0563         0.056         0.0563         0.0560         0.158         0.056         0.0563         0.0563         0.0560         0.158         0.056         0.0563         0.0560         0.158         0.0660         1.158         0.0064         0.0073         0.00644         0.0073         0.0073						
1.002	0.09	0.9987	0.2790	0.00379	0.00408	-7.59
1.00	).15	1.0012	0.1943	0.00264	0.00264	0.12
1.0065						
1,41						
1.0065						
T=313.15 K 1.000						
0.00         0.9393         1.3502         0.01838         0.01907         -3.73         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.05         0.005         0.00590         0.00590         0.153         0.05         0.00590         0.158         0.007         0.00959         0.03478         0.00473         0.00494         -4.27         0.09         0.0971         0.2535         0.00345         0.00363         -5.22         0.0155         0.00363         -5.22         0.0155         0.0059         0.00277         0.066         0.0030         1.0017         0.1375         0.00187         0.00188         -0.40         0.0050         1.019         0.0050         0.00184         0.0019         -1.97         0.040         0.0119         -1.57         0.0184         0.0064         0.0004         0.0011         -0.57         0.05         1.0146         0.0621         0.00084         0.0004         0.0011         -0.57         0.05         0.01468         0.01468         0.01468         0.01468         0.01468         0.01468         0.01468         0.01468         0.01468         0.01468         0.034         0.050	0.50	1.0065	0.0647	0.00089	0.00090	-1.37
1,000	Γ=313.15 K					
0.01		0.9939	1 3502	0.01838	0.01907	-3 73
.033         0.948         0.7469         0.01017         0.01019         -0.26           .05         0.9955         0.4893         0.00679         0.00690         -1.58           .067         0.9999         0.3478         0.00473         0.00494         -4.27           .099         0.9971         0.2535         0.00345         0.00363         -5.22           .015         0.9997         0.1835         0.00250         0.00247         0.96           0.20         1.0041         0.0929         0.00127         0.00188         -0.40           0.30         1.0041         0.0929         0.00127         0.00129         -1.37           0.40         1.1015         0.0739         0.00100         0.00111         -0.57           0.50         1.0146         0.0621         0.00084         0.00084         0.37           7-318.15 K         0.00         0.9918         1.2827         0.01750         0.01843         -3.66           0.01         0.9918         1.2827         0.01750         0.01843         -3.7           0.01         0.9918         1.0760         0.01468         0.01463         0.37           0.02         0.9918         1.0760						
1.58						
0.007						
0.099         0.9971         0.2535         0.00345         0.00363         -5.22           0.15         0.9997         0.1835         0.00250         0.00247         0.96           0.20         1.0017         0.1375         0.00187         0.00188         -0.40           0.30         1.0041         0.0929         0.00100         0.00101         -0.57           0.50         1.0146         0.0621         0.00084         0.00084         0.37           0.50         1.0146         0.0621         0.00084         0.00084         0.37           0.50         1.0146         0.0621         0.00084         0.00084         0.37           0.50         1.0146         0.0621         0.00084         0.00084         0.37           0.50         1.0146         0.0621         0.00084         0.00084         0.37           0.00         0.9918         1.2827         0.01750         0.01814         -3.66           0.01         0.9918         1.0760         0.01488         0.01463         0.37           0.03         0.9934         0.4775         0.00651         0.00644         1.04           0.07         0.9942         0.3444         0.00435						
0.15         0.9997         0.1835         0.00250         0.00247         0.96           0.20         1.0017         0.1375         0.00187         0.00188         -0.40           0.30         1.0041         0.0929         0.00100         0.00101         -0.57           0.50         1.0146         0.0621         0.00084         0.00101         -0.57           0.55         1.0146         0.0621         0.00084         0.00101         -0.57           0.50         1.0146         0.0621         0.00084         0.00184         0.37           0.01         0.9918         1.2827         0.01750         0.01814         -3.66           0.01         0.9918         1.0760         0.01468         0.01463         0.37           0.03         0.9929         0.6965         0.00950         0.00945         0.50           0.05         0.9934         0.4775         0.00651         0.00648         0.33           0.09         0.9954         0.2464         0.00336         0.00350         0.433           0.09         0.9954         0.2464         0.00336         0.00350         0.433           0.102         0.9993         0.1221         0.00166						
1,001	0.09	0.9971	0.2535	0.00345	0.00363	-5.22
0.30         1,0041         0,0929         0,00127         0,00129         -1,97           0.40         1,0146         0,0621         0,00084         0,00084         0,37           7-318,15 K         0.00         0,9918         1,2827         0,01750         0,01814         -3,66           0.01         0,9918         1,0760         0,01468         0,01463         0,37           0.03         0,9929         0,6965         0,00950         0,00945         0,50           0.05         0,9934         0,4775         0,00651         0,00644         1,04           0.07         0,9942         0,3444         0,00470         0,00468         0,33           0.09         0,9954         0,2464         0,00336         0,00350         -4,33           0.15         0,9974         0,1622         0,00221         0,00223         -1,01           0.20         0,9993         0,1221         0,00166         0,0169         -1,84           0.30         1,0018         0,0844         0,00115         0,00119         -2,295           0.40         1,0079         0,0667         0,00011         0,00022         -1,46           0.50         1,0127         0,0546 <td>0.15</td> <td>0.9997</td> <td>0.1835</td> <td>0.00250</td> <td>0.00247</td> <td>0.96</td>	0.15	0.9997	0.1835	0.00250	0.00247	0.96
1.004	0.20	1.0017	0.1375	0.00187	0.00188	-0.40
0.00						
0.50         1,0146         0,0621         0,00084         0,00084         0,37           T=318,15 K         0.00         0,9918         1,2827         0,01750         0,01814         -3,66           0,01         0,9918         1,0760         0,01468         0,01463         0,37           0,03         0,9929         0,6965         0,00950         0,00044         1,04           0,07         0,9942         0,3444         0,00470         0,00468         0,33           0,09         0,9954         0,2464         0,00336         0,00350         -4,33           0,15         0,9974         0,1622         0,00221         0,00223         -1,01           0,20         0,9993         0,1221         0,00166         0,00169         -1,84           0,30         1,0018         0,0844         0,00115         0,00119         -2,95           0,40         1,0079         0,0667         0,0001         0,00076         -2,69           T=328,15 K         0         0         0,9871         1,1546         0,01583         0,01630         -3,02           0,01         0,9878         0,9540         0,01307         0,01285         1,66           0,03						
T=318.15 K  0.00						
0.00         0.9918         1.2827         0.01750         0.01814         -3.66           0.01         0.9918         1.0760         0.01468         0.01463         0.37           0.03         0.9929         0.6965         0.00950         0.00945         0.50           0.05         0.9934         0.4775         0.00651         0.00644         1.04           0.07         0.9954         0.2464         0.00336         0.00350         -4.33           0.15         0.9974         0.1622         0.00221         0.00223         -1.01           0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.0015         0.00119         -2.95           0.40         1.0079         0.0667         0.0091         0.00092         -1.46           0.50         1.0127         0.0546         0.00074         0.00076         -2.69           T=328.15 K         0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927	0.30	1.0146	0.0621	0.00084	0.00084	0.57
.000         0.9918         1.2827         0.01750         0.01814         -3.66           0.01         0.9918         1.0760         0.01468         0.01463         0.37           0.03         0.9929         0.6965         0.00950         0.00945         0.50           0.05         0.9934         0.4775         0.00651         0.00644         1.04           0.07         0.9954         0.2464         0.00336         0.00350         -4.33           0.15         0.9974         0.1622         0.00221         0.00223         -1.01           0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.00115         0.00119         -2.95           0.40         1.0079         0.0667         0.00091         0.00072         -1.46           0.50         1.0127         0.0346         0.00074         0.00076         -2.69           0.73         2.58         0.00074         0.00076         -2.69           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285	T=318.15 K					
.0.01         0.9918         1.0760         0.01468         0.01463         0.37           .003         0.9929         0.6965         0.00950         0.00945         0.50           0.05         0.9934         0.4775         0.00651         0.00644         1.04           0.07         0.9942         0.3444         0.00470         0.00468         0.33           0.09         0.9954         0.2464         0.00336         0.00350         -4.33           0.15         0.9974         0.1622         0.00221         0.00223         -1.01           0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.0015         0.00119         -2.95           0.40         1.0079         0.0667         0.0091         0.00092         -1.46           0.50         1.0127         0.0546         0.00074         0.00076         -2.69           V=328.15 K         0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927		0 9918	1 2827	0.01750	0.01814	-3.66
.0.03         0.9929         0.6965         0.00950         0.00945         0.50           .0.05         0.9934         0.4775         0.00651         0.00644         1.04           .0.07         0.9942         0.3444         0.00470         0.00468         0.33           .0.09         0.9954         0.2464         0.00336         0.00350         -4.33           .0.15         0.9974         0.1622         0.00221         0.00223         -1.01           .0.20         0.9993         0.1221         0.00166         0.00169         -1.84           .0.30         1.0018         0.0844         0.00115         0.00119         -2.95           .040         1.0079         0.0667         0.0091         0.00076         -2.69           .50         1.0127         0.0546         0.0074         0.00076         -2.69           .7=328.15 K						
.0.05         0.9934         0.4775         0.00651         0.00644         1.04           0.07         0.9942         0.3444         0.00470         0.00468         0.33           0.09         0.9954         0.2464         0.00336         0.00350         -4.33           0.15         0.9974         0.1622         0.00221         0.00223         -1.01           0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.00115         0.00119         -2.95           0.40         1.0079         0.0667         0.00091         0.00092         -1.46           0.50         1.0127         0.0546         0.00074         0.00092         -1.46           0.50         1.0127         0.0546         0.00074         0.00092         -2.69           0.6         1.0127         0.0546         0.00183         0.01630         -3.02           0.01         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.59927         0.0811						
0.07         0.9942         0.3444         0.00470         0.0468         0.33           0.09         0.9954         0.2464         0.00336         0.00350         -4.33           0.15         0.9974         0.1622         0.00221         0.0023         -1.01           0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.00115         0.00119         -2.95           0.40         1.0079         0.0667         0.00091         0.00092         -1.46           0.50         1.0127         0.0546         0.00074         0.00076         -2.69           T=328.15 K           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.0033         1.84           0.09         0.9919						
0.09         0.9954         0.2464         0.00336         0.00350         -4.33           0.15         0.9974         0.1622         0.00221         0.00223         -1.01           0.20         0.9993         0.1221         0.00166         0.0019         -1.84           0.30         1.0018         0.0844         0.00115         0.00119         -2.95           0.40         1.0079         0.0667         0.00091         0.00076         -2.69           T=328.15 K           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.0035         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.15         0.9935         0.1392         0.00143         0.00144         0.43           0.20         0.9952						
0.15         0.9974         0.1622         0.00221         0.00223         -1.01           0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.00115         0.00019         -2.95           0.40         1.0079         0.0667         0.00091         0.00076         -2.69           T=328.15 K           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.05         0.9919         0.2240         0.00366         0.00304         0.70           0.15         0.9935         0.1392         0.00145         0.00144         0.43           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.20         0.997						
0.20         0.9993         0.1221         0.00166         0.00169         -1.84           0.30         1.0018         0.0844         0.00115         0.00119         -2.95           0.50         1.0127         0.0546         0.00074         0.00076         -2.69           T=328.15 K           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.015         0.9935         0.1392         0.00190         0.0188         1.40           0.02         0.9952         0.1059         0.00145         0.00144         0.43           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.40         1.0030						
0.30         1.0018         0.0844         0.00115         0.00119         -2.95           0.40         1.0079         0.0667         0.00091         0.00092         -1.46           0.50         1.0127         0.0546         0.00074         0.00076         -2.69           T=328.15 K           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.15         0.9935         0.1392         0.00190         0.00188         1.40           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.30         0.9955         0.10749         0.00103         0.00101         1.44           0.40         1.003	0.15	0.9974	0.1622	0.00221	0.00223	
0.40       1.0079       0.0667       0.00091       0.00092       -1.46         0.50       1.0127       0.0546       0.00074       0.00076       -2.69         T=328.15 K         0.00       0.9871       1.1546       0.01583       0.01630       -3.02         0.01       0.9878       0.9540       0.01307       0.01285       1.66         0.03       0.9888       0.5927       0.00811       0.00799       1.49         0.05       0.9895       0.3991       0.00546       0.00535       2.00         0.07       0.9902       0.2922       0.00400       0.00393       1.84         0.09       0.9919       0.2240       0.00306       0.00304       0.70         0.15       0.9935       0.1392       0.00190       0.0188       1.40         0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.20       0.9955       0.0749       0.0013       0.00101       1.44         0.40       1.0030       0.0595       0.0081       0.0082       -0.59         0.50       1.0083       0.0505       0.0069       0.0068       1.83         T=338.15 K<	0.20	0.9993	0.1221	0.00166	0.00169	-1.84
0.40       1.0079       0.0667       0.00091       0.00092       -1.46         0.50       1.0127       0.0546       0.00074       0.00076       -2.69         T=328.15 K         0.00       0.9871       1.1546       0.01583       0.01630       -3.02         0.01       0.9878       0.9540       0.01307       0.01285       1.66         0.03       0.9888       0.5927       0.00811       0.00799       1.49         0.05       0.9895       0.3991       0.00546       0.00535       2.00         0.07       0.9902       0.2922       0.00400       0.00393       1.84         0.09       0.9919       0.2240       0.00306       0.00304       0.70         0.15       0.9935       0.1392       0.00190       0.0188       1.40         0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.20       0.9955       0.0749       0.0013       0.00101       1.44         0.40       1.0030       0.0595       0.0081       0.0082       -0.59         0.50       1.0083       0.0505       0.0069       0.0068       1.83         T=338.15 K<	0.30	1.0018	0.0844	0.00115	0.00119	-2.95
0.50         1.0127         0.0546         0.00074         0.00076         -2.69           T=328.15 K           0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.15         0.9935         0.1392         0.00190         0.00188         1.40           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.30         0.9975         0.0749         0.00103         0.00101         1.44           0.40         1.0030         0.0595         0.00081         0.00082         -0.59           0.50         1.0083         0.0505         0.00069         0.0068         1.83           ***T=338.15 K*****************	0.40	1.0079	0.0667	0.00091	0.00092	-1.46
T=328.15 K  0.00				0.00074	0.00076	
0.00         0.9871         1.1546         0.01583         0.01630         -3.02           0.01         0.9878         0.9540         0.01307         0.01285         1.66           0.03         0.9888         0.5927         0.00811         0.00799         1.49           0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.15         0.9935         0.1392         0.00190         0.0188         1.40           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.30         0.9975         0.0749         0.00103         0.00101         1.44           0.40         1.0030         0.0595         0.00081         0.00082         -0.59           0.50         1.0083         0.0505         0.00069         0.00068         1.83           F=338.15 K           0.01         0.9844         0.8446         0.01161         0.0116         3.85           0.02         0.9858 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
0.01     0.9878     0.9540     0.01307     0.01285     1.66       0.03     0.9888     0.5927     0.00811     0.00799     1.49       0.05     0.9895     0.3991     0.00546     0.00535     2.00       0.07     0.9902     0.2922     0.00400     0.00393     1.84       0.09     0.9919     0.2240     0.00306     0.00304     0.70       0.15     0.9935     0.1392     0.00190     0.00188     1.40       0.20     0.9952     0.1059     0.00145     0.00144     0.43       0.30     0.9975     0.0749     0.00103     0.00101     1.44       0.40     1.0030     0.0595     0.00081     0.00082     -0.59       0.50     1.0083     0.0505     0.00069     0.0068     1.83       T=338.15 K       0.00     0.9818     1.0355     0.01427     0.01454     -1.88       0.01     0.9844     0.8446     0.01161     0.01116     3.85       0.03     0.9858     0.5091     0.00699     0.00671     4.02       0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9887     0.1837     0.00252     0.00248     1.51 <td>T=328.15 K</td> <td></td> <td></td> <td></td> <td></td> <td></td>	T=328.15 K					
0.03       0.9888       0.5927       0.00811       0.00799       1.49         0.05       0.9895       0.3991       0.00546       0.00535       2.00         0.07       0.9902       0.2922       0.00400       0.00393       1.84         0.09       0.9919       0.2240       0.00306       0.00304       0.70         0.15       0.9935       0.1392       0.00190       0.00188       1.40         0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.30       0.9975       0.0749       0.00103       0.00101       1.44         0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.0068       1.83         T=338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.0041       2.78         0.07       0	0.00	0.9871	1.1546	0.01583	0.01630	-3.02
0.03       0.9888       0.5927       0.00811       0.00799       1.49         0.05       0.9895       0.3991       0.00546       0.00535       2.00         0.07       0.9902       0.2922       0.00400       0.00393       1.84         0.09       0.9919       0.2240       0.00306       0.00304       0.70         0.15       0.9935       0.1392       0.00190       0.00188       1.40         0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.30       0.9975       0.0749       0.00103       0.00101       1.44         0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.0068       1.83         T=338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.0041       2.78         0.07       0	0.01	0.9878	0.9540	0.01307	0.01285	1.66
0.05         0.9895         0.3991         0.00546         0.00535         2.00           0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.15         0.9935         0.1392         0.00190         0.00188         1.40           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.30         0.9975         0.0749         0.00103         0.00101         1.44           0.40         1.0030         0.0595         0.00081         0.00082         -0.59           0.50         1.0083         0.0505         0.00069         0.0068         1.83           T=338.15 K           0.00         0.9818         1.0355         0.01427         0.01454         -1.88           0.01         0.9844         0.8446         0.01161         0.01116         3.85           0.05         0.9864         0.3303         0.00454         0.0041         2.78           0.07         0.9870         0.2335         0.00321         0.00317         1.01           0.09         0.9887 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
0.07         0.9902         0.2922         0.00400         0.00393         1.84           0.09         0.9919         0.2240         0.00306         0.00304         0.70           0.15         0.9935         0.1392         0.00190         0.00188         1.40           0.20         0.9952         0.1059         0.00145         0.00144         0.43           0.30         0.9975         0.0749         0.00103         0.00101         1.44           0.40         1.0030         0.0595         0.00081         0.00082         -0.59           0.50         1.0083         0.0505         0.00069         0.0068         1.83           T=338.15 K           0.00         0.9818         1.0355         0.01427         0.01454         -1.88           0.01         0.9844         0.8446         0.01161         0.01166         3.85           0.03         0.9858         0.5091         0.00699         0.00671         4.02           0.05         0.9864         0.3303         0.00454         0.00441         2.78           0.07         0.9870         0.2335         0.00321         0.00317         1.01           0.09         0.9887 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
0.09       0.9919       0.2240       0.00306       0.00304       0.70         0.15       0.9935       0.1392       0.00190       0.00188       1.40         0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.30       0.9975       0.0749       0.00103       0.00101       1.44         0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.0068       1.83         T = 338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.00441       2.78         0.07       0.9870       0.2335       0.00321       0.00317       1.01         0.09       0.9887       0.1837       0.00252       0.00248       1.51         0.015       0.0906       0.1130       0.00155       0.00155       0.0313						
0.15       0.9935       0.1392       0.00190       0.00188       1.40         0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.30       0.9975       0.0749       0.00103       0.00101       1.44         0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.00068       1.83         T = 338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.00441       2.78         0.07       0.9870       0.2335       0.00321       0.00317       1.01         0.09       0.9887       0.1837       0.00252       0.00248       1.51         0.15       0.9906       0.1130       0.00155       0.00155       0.0315						
0.20       0.9952       0.1059       0.00145       0.00144       0.43         0.30       0.9975       0.0749       0.00103       0.00101       1.44         0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.00068       1.83         T=338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.00441       2.78         0.07       0.9870       0.2335       0.00321       0.00317       1.01         0.09       0.9887       0.1837       0.00252       0.00248       1.51         0.15       0.9906       0.1130       0.00155       0.00155       0.0315						
0.30       0.9975       0.0749       0.00103       0.00101       1.44         0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.00068       1.83         T=338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.00441       2.78         0.07       0.9870       0.2335       0.00321       0.00317       1.01         0.09       0.9887       0.1837       0.00252       0.00248       1.51         0.15       0.9906       0.1130       0.00155       0.00155       0.00155						
0.40       1.0030       0.0595       0.00081       0.00082       -0.59         0.50       1.0083       0.0505       0.00069       0.00068       1.83         T=338.15 K         0.00       0.9818       1.0355       0.01427       0.01454       -1.88         0.01       0.9844       0.8446       0.01161       0.01116       3.85         0.03       0.9858       0.5091       0.00699       0.00671       4.02         0.05       0.9864       0.3303       0.00454       0.00441       2.78         0.07       0.9870       0.2335       0.00321       0.00317       1.01         0.09       0.9887       0.1837       0.00252       0.00248       1.51         0.15       0.9906       0.1130       0.00155       0.00155       0.00155						
0.50     1.0083     0.0505     0.00069     0.00068     1.83       F=338.15 K       0.00     0.9818     1.0355     0.01427     0.01454     -1.88       0.01     0.9844     0.8446     0.01161     0.01116     3.85       0.03     0.9858     0.5091     0.00699     0.00671     4.02       0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.0155	0.30		0.0749	0.00103	0.00101	1.44
T=338.15 K 0.00 0.9818 1.0355 0.01427 0.01454 -1.88 0.01 0.9844 0.8446 0.01161 0.01116 3.85 0.03 0.9858 0.5091 0.00699 0.00671 4.02 0.05 0.9864 0.3303 0.00454 0.00441 2.78 0.07 0.9870 0.2335 0.00321 0.00317 1.01 0.09 0.9887 0.1837 0.00252 0.00248 1.51 0.15 0.9906 0.1130 0.00155 0.00155 0.13	0.40	1.0030	0.0595	0.00081	0.00082	-0.59
T=338.15 K  0.00	0.50	1.0083	0.0505	0.00069	0.00068	1.83
0.00     0.9818     1.0355     0.01427     0.01454     -1.88       0.01     0.9844     0.8446     0.01161     0.01116     3.85       0.03     0.9858     0.5091     0.00699     0.00671     4.02       0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.00155	T 220 45 W					
0.01     0.9844     0.8446     0.01161     0.01116     3.85       0.03     0.9858     0.5091     0.00699     0.00671     4.02       0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.00155						
0.03     0.9858     0.5091     0.00699     0.00671     4.02       0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.00155						
0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.00155	0.01	0.9844	0.8446	0.01161	0.01116	
0.05     0.9864     0.3303     0.00454     0.00441     2.78       0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.00155	0.03	0.9858	0.5091	0.00699	0.00671	4.02
0.07     0.9870     0.2335     0.00321     0.00317     1.01       0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.00155						
0.09     0.9887     0.1837     0.00252     0.00248     1.51       0.15     0.9906     0.1130     0.00155     0.00155     0.013						
0.15 0.9906 0.1130 0.00155 0.00155 0.13						
J.20 0.9923 0.0846 0.00116 0.00119 -2.24						
			0.0846	0.00116	0.00119	
0.30 0.9946 0.0614 0.00084 0.00085 -0.70	0.30	0.9946	0.0614	0.00084	0.00085	
0.40 0.9986 0.0492 0.00068 0.00068 -0.67	0.40	0.9986	0.0492	0.00068	0.00068	-0.67
0.50 1.0044 0.0444 0.00061 0.00060 2.08	0.50		0.0444	0.00061	0.00060	2.08

Table 4 (Continued)

$M_2  (\operatorname{mol} L^{-1})$	$ ho_{ m s}({ m gmL^{-1}})$	$C_1 (g L^{-1})$	$m_1^{\rm exp}~({ m molkg^{-1}})$	$m_1^{\mathrm{cal}}  (\mathrm{mol}  \mathrm{kg}^{-1})$	$(m_1^{\rm exp} - m_1^{\rm cal})/m_1^{\rm exp}$ (%)
T=348.15 K					
0.00	0.9760	0.9261	0.01283	0.01287	-0.30
0.01	0.9817	0.7254	0.01000	0.00957	4.30
0.03	0.9826	0.3960	0.00546	0.00538	1.43
0.05	0.9834	0.2523	0.00347	0.00344	0.91
0.07	0.9846	0.1779	0.00245	0.00248	-1.36
0.09	0.9860	0.1358	0.00187	0.00195	-4.12
0.15	0.9880	0.0921	0.00127	0.00127	-0.36
0.20	0.9901	0.0730	0.00101	0.00100	0.71
0.30	0.9920	0.0544	0.00075	0.00072	3.65
0.40	0.9958	0.0439	0.00060	0.00059	1.78
0.50	1.0006	0.0375	0.00051	0.00052	2.08
	ARD (%) = 2.15				

relation for aqueous multi-component solutions was used for the conversion:

$$x_{i} = \frac{m_{i}}{\sum_{j}^{n} \nu_{j} m_{j} + 55.508}$$
 (17)

Based on the maximum-likelihood principle [20], the following general objective function was used to optimize the solubility data:

OBF = Min 
$$\sum_{i} \left[ w_1 \left( \frac{T_i^{\text{exp}} - T_i^{\text{cal}}}{\sigma_T} \right)^2 + w_2 \left( \frac{P_i^{\text{exp}} - P_i^{\text{cal}}}{\sigma_P} \right)^2 + w_3 \left( \frac{x_i^{\text{exp}} - x_i^{\text{cal}}}{\sigma_X} \right)^2 \right]$$
 (18)

#### 4. Results and discussion

#### 4.1. Solubility results

Fig. 2 shows the solubility of calcium sulfate dihydrate as a function of NaOH concentration at various temperatures. It can be observed that the solubility of calcium sulfate dihydrate increases with increasing NaOH concentration. After passing a maximum, the solubility decreases at higher NaOH concentrations. The increase in the solubility can be explained by the association of Ca<sup>2+</sup> and OH<sup>-</sup> ions and formation of Ca(OH)<sup>+</sup> ion. However, the solubility decreases in concentrated NaOH solutions may be related to changes in the activity coefficient of the calcium, hydroxide and

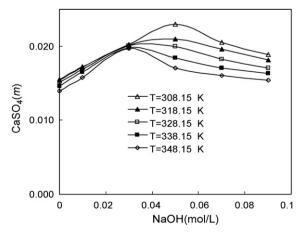


Fig. 2. The experimental solubility data of  $CaSO_4 \cdot 2H_2O$  as a function of NaOH concentration at different temperatures.

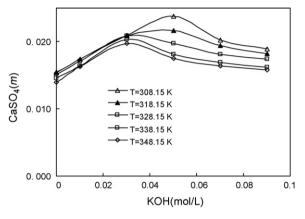


Fig. 3. The experimental solubility data of  $CaSO_4 \cdot 2H_2O$  as a function of KOH concentration at different temperatures.

hydroxyl calcium ions as well as the activity of water. At the NaOH concentration range of  $0-0.03 \, \mathrm{mol} \, L^{-1}$ , the solubility of  $\mathrm{CaSO_4 \cdot 2H_2O}$  slightly varies with the increasing temperature. Similar trends are observed for the solubility of calcium sulfate dihydrate in KOH solutions, although the solubilities are higher than those of  $\mathrm{CaSO_4 \cdot 2H_2O}$  at a given NaOH concentration. The m-T diagram for  $\mathrm{CaSO_4 \cdot 2H_2O}$ –KOH–H<sub>2</sub>O system is illustrated in Fig. 3.

Fig. 4 shows the experimental solubility data of calcium hydroxide in NaOH solutions at different temperatures. It can be seen from the figure that the solubility of Ca(OH)<sub>2</sub> decreases with increasing temperatures, and sharply decreases with the increment of alkali concentration due to the common ion effect of OH<sup>-</sup>.

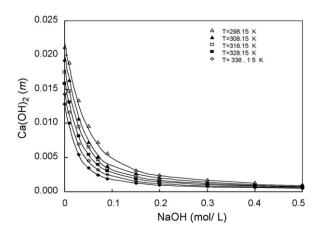


Fig. 4. The experimental solubility of  ${\rm Ca}({\rm OH})_2$  as a function of NaOH concentration at different temperatures.

Table 5 Pitzer model interaction parameters obtained by regressing solubility data for the binary  $Ca(OH)_2-H_2O$  system.

Component i	Component j	Paramo	eters	Value
Ca(OH) <sup>+</sup>	OH-	$eta_{ij}^0$	$a_1$ $a_2$	0.13618 0.03584
		$eta_{ij}^1$	$a_1$ $a_2$	-0.36923 $-0.06441$
		$C_{ij}$	$a_1$ $a_2$	-0.04982 $-0.05177$
Ca(OH) <sup>+</sup>	Ca <sup>2+</sup>	$ heta_{ij}$	$a_1$ $a_2$	$-10.0032 \\ 0.00014$

#### 4.2. Solubility evaluation with existing model parameters

In order to test the capability of predicting the solubility of CaSO<sub>4</sub>·2H<sub>2</sub>O or Ca(OH)<sub>2</sub> in alkali solution, the solubility of Ca(OH)<sub>2</sub> in water over the temperature range from 25 to 75 °C was calculated by using the Pitzer model with the Aspen Plus default database (version 2006) and compared with experimental data listed in Table 4. The overall average relative deviation (ARD) is 5.31% and the maximum relative deviation is 6.58%, indicating that the solubility of Ca(OH)<sub>2</sub> in water cannot be calculated accurately with the Aspen Plus default database. Koenigsberger et al. [21] reported that when they use thermodynamic quantities for calcium hydroxide from CODATA [22] they need to include an associated Ca(OH)<sup>+</sup> species in addition to the Ca<sup>2+</sup>-OH<sup>-</sup> interaction parameters to accurately calculate pure water calcium hydroxide solubility at 25 °C. Consequently, new interaction parameters for the associated hydroxyl calcium ion Ca(OH)+ with the other dominant species in alkali solutions should be regressed.

Similarly, in order to evaluate the interaction parameters between  $\text{Ca}^{2+}$  and  $\text{SO}_4{}^{2-}$  ions in the Aspen Plus default databank, the solubility of  $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$  in water listed in Table 2 was predicted using the Pitzer model with the maximum relatively deviation of 45.68%. The results show that Aspen Plus predictions are in poor agreement with the experimental data. Therefore, it is decided to perform an estimation of the parameters for  $\text{Ca}^{2+}\text{-SO}_4{}^{2-}$  using the solubility of  $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$  in water over the temperature range from 35 to 75 °C through the Aspen Plus built-in regression feature.

#### 4.3. Model parameterization

#### 4.3.1. $Ca(OH)_2-H_2O$ system

In order to improve Aspen Plus's prediction capacity, the new interaction parameters for  $Ca(OH)^+-OH^-$  and  $Ca(OH)^+-Ca^{2+}$  were obtained by regressing the solubility data of calcium hydroxide in water over temperature range from 25 to 75 °C, and listed in Table 5. Fig. 5 shows the comparison of the regressed and experimental solubility for  $Ca(OH)_2-H_2O$  system at different temperatures. As shown in Fig. 5, the calculated solubility data agree well with the experimental values with the ARD of 2.78% and the maximum relatively deviation is -3.78%.

#### 4.3.2. $CaSO_4 \cdot 2H_2O - NaOH - KOH - H_2O$ system

As was seen from the above, the current Pitzer model embedded in Aspen Plus cannot predict well the solubility data of calcium sulfate dihydrate in water. Therefore, we opted to determine the binary interaction parameter for  $\text{Ca}^{2+}\text{-SO}_4{}^2$  via regression of solubility data of  $\text{CaSO}_4 \cdot 2\text{H}_2\text{O}$  in water over the temperature range from 35 to 75 °C. The obtained model parameters are presented in Table 6. The correlated results can accurately mimic

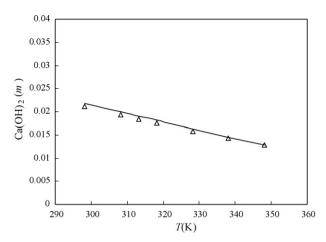


Fig. 5. Experimental and regressed solubility of  $Ca(OH)_2$  in  $H_2O$ . Legend:  $\Delta$ , experimental data from this work; –, regressed values.

**Table 6** Pitzer model interaction parameters obtained by regressing solubility data for the binary system  $CaSO_4 \cdot 2H_2O - H_2O$  and the ternary system  $CaSO_4 \cdot 2H_2O - NaOH - H_2O$ .

Component i	Component j	Paramete	ers Value
Ca <sup>2+</sup>	SO <sub>4</sub> <sup>2-</sup>	P 11	$a_1$ 13.1654 $a_2$ -0.13683
		r ii	$a_1$ -164.540 $a_2$ -2.13694
		P 11	$a_1$ -28.6004 $a_2$ 0.09130
		,	$a_1$ -192.276 $a_2$ 2.13099
OH-	SO <sub>4</sub> <sup>2-</sup>	9	$a_1$ 3.75756 $a_2$ -0.03263

the experimental data with the maximum relatively deviation of 0.68%.

The experimental solubility data of  $CaSO_4 \cdot 2H_2O$  for the ternary  $CaSO_4 \cdot 2H_2O - NaOH - H_2O$  system at 35 °C were used to regress the mixing parameter  $OH^- - SO_4^{2-}$  in order to allow a more precise estimation of the chemistry of this system. Fig. 6 shows the calculated and experimental solubility data of  $CaSO_4 \cdot 2H_2O$  in the ternary system as a function of the NaOH concentration. It is seen that the influence of temperature and NaOH concentration on the solubility of  $CaSO_4 \cdot 2H_2O$  can be well depicted by the model. For the ternary  $CaSO_4 \cdot 2H_2O - KOH - H_2O$  system, the mixing parameters.

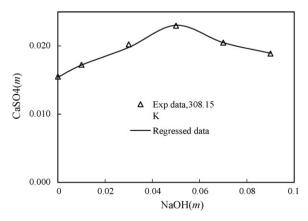


Fig. 6. Experimental and regressed solubility of  $CaSO_4 \cdot 2H_2O$  in NaOH solutions at 308.15 K.

**Table 7** Pitzer model interaction parameters obtained by regressing solubility data for the ternary system  $CaSO_4 \cdot 2H_2O$ -KOH- $H_2O$  at 35 °C.

Component i	Component j	Parameters	Value
Ca(OH)+	K <sup>+</sup>	$ heta_{ij} \qquad \qquad a_1 \ a_2 \qquad \qquad$	0.44779 0.00000
Ca <sup>2+</sup>	K <sup>+</sup>	$egin{array}{ccc}  heta_{ij} & a_1 \ a_2 \end{array}$	0.21223 0.00066

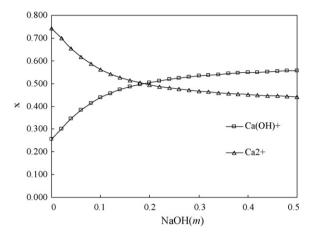


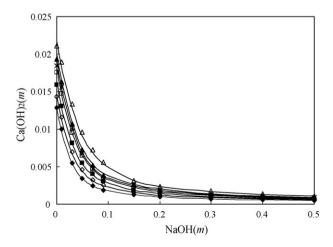
Fig. 7. The distribution of Ca-bearing species for the ternary system  $Ca(OH)_2-NaOH-H_2O$  at 313.15 K versus the NaOH concentration.

 $Ca(OH)^+$ – $K^+$  and  $Ca^{2^+}$ – $K^+$  in solution were regressed using the solubility of calcium sulfate dihydrate in KOH solutions at 35 °C. The overall ARD is 2.05% and the resulting interaction parameters are listed in Table 7.

#### 4.4. Model validation

#### 4.4.1. $Ca(OH)_2$ -NaOH- $H_2O$ system

In order to test whether the model parameters obtained from simple system perform equally well in multi-component solutions, the solubility data of calcium hydroxide in NaOH solutions at elevated temperatures were predicted without introducing any new parameters. Fig. 7 shows the distribution of Ca-bearing species in solutions versus the NaOH concentrations. It is apparent that the Ca(OH)<sup>+</sup> always increases with the increase in NaOH concentrations. Fig. 8 shows the comparison of the



**Fig. 8.** Experimental and predicted solubility of Ca(OH)<sub>2</sub> in NaOH solutions at different temperatures. Legend:  $\triangle$ , 298.15 K;  $\blacktriangle$ , 308.15 K;  $\times$ , 313.15 K;  $\square$ , 318.15 K;  $\blacksquare$ , 328.15 K;  $\diamondsuit$ , 338.15 K;  $\diamondsuit$ , 348.15 K; -, predicted results.

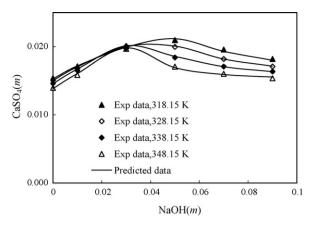


Fig. 9. Experimental and predicted solubility of  $CaSO_4 \cdot 2H_2O$  in NaOH solutions at different temperatures.

predicted and experimental solubility data for  $Ca(OH)_2$  in the  $Ca(OH)_2$ -NaOH-H<sub>2</sub>O system. As shown in Fig. 8, the experimental solubility data can be well predicted by the model with the overall ARD of 2.15%.

#### 4.4.2. CaSO<sub>4</sub>·2H<sub>2</sub>O-NaOH-KOH-H<sub>2</sub>O system

The solubility data of  $CaSO_4 \cdot 2H_2O$  in NaOH solutions over the temperature range from 45 to 75 °C are predicted with the new interaction parameters,  $Ca^{2+} - SO_4^{2-}$ ,  $Ca(OH)^+ - Ca^{2+}$  and  $OH^- - SO_4^{2-}$ . The predicted results obtained for the solubility of  $CaSO_4 \cdot 2H_2O$  versus NaOH concentrations are shown in Fig. 9 along with the experimental data. The model parameters closely reflect the experimental data with the overall ARD of 0.75% and the maximum relatively deviation of 2.12%.

Similarly, the solubility of CaSO $_4 \cdot 2H_2O$  in KOH solutions over the temperature range from 45 to 75 °C is predicted using the available interaction parameters, Ca<sup>2+</sup>–SO $_4$ <sup>2–</sup>, Ca(OH)<sup>+</sup>–Ca<sup>2+</sup>, OH<sup>–</sup>SO $_4$ <sup>2–</sup>, Ca(OH)<sup>+</sup>–K<sup>+</sup> and Ca<sup>2+</sup>–K<sup>+</sup>. To show the overall performance of the present model, the predicted and the experimental solubilities are compared and plotted in Fig. 10. The results indicate that the deviation is basically evenly occurred and no data points show a biased deviation from the diagonal. Although, the predicted results obtained for the solubility of CaSO $_4$  in KOH solutions are relatively accurate compared to the experimental data with the overall ARD of 1.53% and the maximum relatively deviation of 4.30%, the solubility prediction accuracy decreases with the increase of temperature.

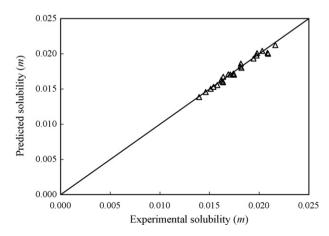


Fig. 10. Experimental and predicted solubility of  $CaSO_4 \cdot 2H_2O$  in KOH solutions at different temperatures.

#### 5. Conclusions

In this work, new experimental data for the solubility of CaSO<sub>4</sub>·2H<sub>2</sub>O were presented for the ternary systems CaSO<sub>4</sub>·2H<sub>2</sub>O-NaOH-H<sub>2</sub>O,  $CaSO_4 \cdot 2H_2O - KOH - H_2O$ , Ca(OH)<sub>2</sub>-NaOH-H<sub>2</sub>O over the temperature range from 25 to 75°C.

The thermodynamic equilibrium for the above ternary systems was modelled through the Pitzer model embedded in the Aspen Plus platform. The modelling involved the regression of binary solubility data and ternary solubility data. New interaction parameters for the associated hydroxyl calcium ion Ca(OH)+ with the other dominant species in alkali solutions were determined. It was shown that the speciation employed in binary systems, as well as the interaction parameters obtained by regressing solubilities is sufficient to represent the solubilities in ternary systems (not used in the regression state) very well. The developed Pitzer model proved to be an accurate model for describing the phase equilibria of calcium sulfate dihydrate and calcium hydroxide in alkali solutions.

#### List of symbols

number of data points n

the molality of species (mol kg  $H_2O^{-1}$ ) m mexp the experimental solubility (mol kg  $H_2O^{-1}$ )  $m^{cal}$ the calculated solubility (mol kg  $H_2O^{-1}$ )

temperature (K)

Tref 298.15 K

K the equilibrium constant

 $K_{CaSO_4 \cdot 2H_2O(s)}$  the solubility product constant of calcium sulfate

dihvdrate

 $K_{\text{Ca}(\text{OH})^+}$ the dissociation constant of hydroxyl calcium ion

 $\Delta G_r^0$ the standard Gibbs free energy of the reaction the stoichiometric coefficient of species i

the interaction parameters  $B_{ii}$ ,  $C_{ii}$ 

i, j and k cations and anions of the solution

the weight factor w

Р the pressure of system (kPa)

the solubility of electrolytes in terms of mole fractions x

the number of moles of the solution constituents  $n_i$ 

f(I)an electrostatic term as a function of ionic strength

#### Greek letters

the activity coefficient of component

 $\mu^0$ the standard chemical potential of individual species

the mixing parameters  $\theta_{ii}, \psi_{iik}$ the standard deviations

the mean activity coefficient of calcium sulfate  $\gamma_{\pm CaSO_4}$ 

the activity of water  $\alpha_{H_2O}$ 

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