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## Oxidation of Aromatic Sulfur Compounds Catalyzed by Organic Hexacyanoferrates in Ionic Liquids with a Low Concentration of H<sub>2</sub>O<sub>2</sub> as an Oxidant

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Supporting Information

ABSTRACT: A series of organic hexacyanoferrates were synthesized and employed as catalysts in ionic liquids (ILs) for catalytic oxidation of dibenzothiophene (DBT), benzothiophene (BT), and 4,6-dimethyldibenzothiophene (4,6-DMDBT). High activity was achieved using 1-butyl-3-methylimidazolium hexacyanoferrate ([C<sub>4</sub>mim]<sub>3</sub>Fe(CN)<sub>6</sub>) as a catalyst and 1-butyl-3methylimidazolium tetrafluoroborate ( $\lceil C_4 \text{mim} \rceil BF_4$ ) as an extractant in the presence of  $H_2O_2$  under mild conditions. It was interesting to find that the concentration of H<sub>2</sub>O<sub>2</sub> had a significant influence on desulfurization efficiency. The sulfur removal was 76.3% with 30 wt % H<sub>2</sub>O<sub>2</sub> as an oxidant, while it could reach 97.9% with 7.5 wt % H<sub>2</sub>O<sub>2</sub>. Electron spin resonance (ESR) spectroscopy measurements gave the evidence that the active oxygen species O2 - was generated in the catalytic oxidative desulfurization process, and gas chromatography-mass spectrometry (GC-MS) analysis indicated that the sulfur compounds were oxidized to the corresponding sulfones. The influence factors, such as reaction temperature, time, concentration, and dosage of H<sub>2</sub>O<sub>2</sub>, amount of catalyst, catalytic system recycling, and different sulfur-containing compounds, were investigated. The kinetic investigations showed that oxidation of sulfur compounds presented a pseudo-first-order kinetic. Under the optimal conditions, the catalytic system could be recycled at least 4 times without a remarkable decrease in activity.

### 1. INTRODUCTION

The sulfur compounds in fuels are known to have a negative impact on the environment because of SO<sub>x</sub> emissions from their combustion exhausts. Conventional hydrodesulfurization (HDS) is most widely used in refineries to remove aliphatic and acyclic sulfur compounds. However, it is less effective for treating some refractory sulfur compounds, such as benzothiophenes (BTs) and dibenzothiophenes (DBTs). 1-4 To achieve deep desulfurization, severe operating conditions, such as high temperature, high pressure, and high hydrogen consumption, are required, leading to high capital and operating costs. Therefore, it is essential to develop alternative non-HDS methods to produce clean diesel containing a low sulfur concentration. 5-9 Among them, oxidative desulfurization (ODS) is considered to be one of the most promising processes because of its high efficiency for removing refractory sulfur compounds under mild conditions. $^{10-17}$ 

Our previous work reported an ionic liquid (IL) extraction and catalytic oxidative desulfurization (ECODS) system, which could oxidize the sulfur compounds to their corresponding sulfones. 18-26 To date, some catalysts or ILs, such as FeCl<sub>3</sub>, tetramethylammonium tetrachloroferrate ([(CH<sub>3</sub>)<sub>4</sub>N]FeCl<sub>4</sub>),<sup>22</sup> 1-butyl-3-methylimidazolium tetrachloroferrate ([C₄mim]-FeCl<sub>4</sub>), 18 trioctylmethyl ammonium tetrachloroferrate  $([(C_8H_{17})_3CH_3N]FeCl_4)^{21}$  and triethylamine tetrachloroferrate  $([Et_3NH]FeCl_4)^{20}$  were developed by our group, and they all showed good performance in oxidative desulfurization. Then, other Fe-based ILs, e.g.,  $[C_4 \text{mim}] \text{FeCl}_3^{27}$  and  $[C_4^3 \text{MPy}]$ -

FeCl<sub>4</sub>, <sup>28</sup> were synthesized and used to investigate the oxidative removal of sulfur compounds from diesel fuels. The oxidant used in these desulfurization systems was hydrogen peroxide  $(H_2O_2)$ . Moreover,  $H_2O_2$  is the most common oxidant in other oxidative desulfurization fields, <sup>29–34</sup> partly because it is a commercial product often used at the industrial level and gives only water as a byproduct.<sup>35</sup> Although H<sub>2</sub>O<sub>2</sub> is one of the best candidates as an oxidant, a high concentration of H2O2 is a potentially explosive issue during transportation and may do harm to human health. However, it is hard to activate lowconcentration H<sub>2</sub>O<sub>2</sub> to oxidize DBTs in fuels, and few examples have been reported.<sup>36</sup> Therefore, the use of low-concentration H<sub>2</sub>O<sub>2</sub> in oxidative desulfurization will be an environmentally friendly and safe process.

Hexacyanoferrates are usually used as a redox couple in the electrochemical field.<sup>37</sup> However, there are very few examples of the application of hexacyanoferrates in catalysis, <sup>38</sup> especially in activation of low-concentration H2O2. Here, we first report the oxidation of DBT, BT, and 4,6- dimethyldibenzothiophene (4,6-DMDBT) with low-concentration H<sub>2</sub>O<sub>2</sub> using the ECODS system, with the organic hexacyanoferrates  $[C_n mim]_3 Fe(CN)_6$  (where n = 2, 4, and 8) as a catalyst and  $[C_4 \text{mim}]BF_4$  as an extractant. In this system,  $[C_4 \text{mim}]_3 Fe$ (CN)<sub>6</sub> exhibited the highest activity in the presence of 7.5 wt %

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Table 1. Sulfur Removal of Different Desulfurization Systems<sup>a</sup>

		sulfur removal (%)		
entry	desulfurization system	30 wt % H <sub>2</sub> O <sub>2</sub>	7.5 wt % H <sub>2</sub> O <sub>2</sub>	without H <sub>2</sub> O <sub>2</sub>
1	IL			23.2
2	$IL/H_2O_2$	21.7	19.0	
3	IL/catalyst I/H <sub>2</sub> O <sub>2</sub>	74.5	86.7	
4	IL/catalyst II/H <sub>2</sub> O <sub>2</sub>	76.3	97.9	
5	IL/catalyst III/H <sub>2</sub> O <sub>2</sub>	73.5	91.1	

"Experimental conditions: catalyst I,  $[C_2mim]_3Fe(CN)_6$ ; catalyst II,  $[C_4mim]_3Fe(CN)_6$ ; catalyst III,  $[C_8mim]_3Fe(CN)_6$ ; n(catalyst), 0.039 mmol; model oil, 5 mL; IL( $[C_4mim]BF_4$ ), 1 mL; O/S, 4; T, 40 °C; and t, 5 h.

 $\rm H_2O_2$  and the catalytic system could be recycled 4 times with a slight decrease in activity. Furthermore, the reaction mechanism was investigated by ultraviolet—visible (UV—vis), electron spin resonance (ESR) spin-trap technique, and gas chromatography—mass spectrometry (GC—MS) analysis.

### 2. EXPERIMENTAL SECTION

**2.1. Materials.** BT, DBT, and 4,6-DMDBT were purchased from Sigma-Aldrich. The ILs 1-butyl-3-methylimidazolium tetrafluoroborate ( $[C_4 \text{mim}]BF_4$ ), 1-n-octyl-3-methylimidazolium hexafluoroborate ( $[C_8 \text{mim}]BF_4$ ), 1-butyl-3-methylimidazolium hexafluorophosphate ( $[C_4 \text{mim}]PF_6$ ), and 1-n-octyl-3-methylimidazolium hexafluorophosphate ( $[C_8 \text{mim}]PF_6$ ) was purchased from Shanghai Chengjie Chemical Co., Ltd. Other materials were commercial-reagent-grade and were obtained from Shanghai Sinopharm Chemical Co., Ltd. Model oils were prepared by dissolving DBT and BT in n-octane to give solutions with a sulfur content of 500 and 250 ppm, respectively. In addition, tetradecane was added to the model oil as an internal standard. The  $H_2O_2$  concentration was measured by titration with potassium permanganate solution, which was determined by sodium oxalate.

**2.2. Instruments.** The Fourier transform infrared (FTIR) spectra of catalysts (KBr pellets) were tested with a Nicolet Nexus 470 FTIR instrument. Electrospray ionization—mass spectrometry (ESI—MS) spectra were collected on a LXQ linear ion trap mass spectrometer. UV—vis spectra were recorded on UV-2450 spectrophotometer (Shimadzu Corporation, Japan). Elementary analyses were carried out with CHN-O-Rapid (Heraeus Corporation). Sulfur compounds in IL phase were extracted by diethyl ether and determined by GC—MS (Agilent 7890A/5975C). X-band ESR spectra were recorded at room temperature on a JES FA200 spectrometer. The settings for the ESR spectrometer were as follows: center field, 336.496 mT; sweep width, 5 mT; microwave frequency, 9.5 GHz; modulation frequency, 100 kHz; and power, 0.998 mW.

**2.3.** Preparation of  $[C_n mim]_3 Fe(CN)_6$  (where n = 2, 4, and 8). A aqueous solution (50 mL) of  $K_3 Fe(CN)_6$  (3 mmol) and  $[C_n mim] BF_4$  (9 mmol) were mixed and stirred for 24 h at room temperature. The precipitate (KBF<sub>4</sub>) was filtered off, and the filtrate was concentrated by evaporating the solvent. Then, the resulting mixture was purified by methanol. After the solvent was removed under reduced pressure, the remaining solid was washed with diethyl ether and dried at 40 °C in a vacuum for 24 h to give the product as a yellow green powder.

Data for  $[C_2mim]_3Fe(CN)_6$ : IR (KBr, cm<sup>-1</sup>):  $\nu = 2115$  (C $\equiv$ N). ESI-MS: 111  $[C_2mim]_+^+$ , 651  $[C_2mim]_4Fe(CN)_6^+$ , 434  $[C_2mim]_2Fe(CN)_6^-$ . Elemental analysis calcd (%) for  $C_{30}FeH_{15}N_{12}$ : C, 52.85; H, 6.10; N, 30.82. Found: C, 52.58; H, 6.31; N, 30.90.

Data for  $[C_4 \text{mim}]_3 \text{Fe}(\text{CN})_6$ : IR (KBr, cm<sup>-1</sup>):  $\nu = 2115$ , 2107 (C $\equiv$  N). ESI-MS: 139  $[C_4 \text{mim}]^+$ , 768  $[C_4 \text{mim}]_4 \text{Fe}(\text{CN})_6^+$ , 490  $[C_4 \text{mim}]_2 \text{Fe}(\text{CN})_6^-$ . Elemental analysis calcd (%) for  $C_{30} \text{FeH}_{15} \text{N}_{12}$ : C, 57.23; H, 7.20; N, 26.70. Found: C, 57.34; H, 7.35; N, 26.70.

Data for  $[C_8 \text{mim}]_3 \text{Fe}(\text{CN})_6$ : IR (KBr, cm<sup>-1</sup>):  $\nu = 2115$ , 2106 (C $\equiv$  N). ESI-MS: 195  $[C_8 \text{mim}]^+$ , 993  $[C_8 \text{mim}]_4 \text{Fe}(\text{CN})_6^+$ , 602  $[C_8 \text{mim}]_2 \text{Fe}(\text{CN})_6^-$ . Elemental analysis calcd (%) for  $C_{30} \text{FeH}_{15} \text{N}_{12}$ : C, 63.22; H, 8.72; N, 21.06. Found: C, 63.35; H, 9.02; N, 20.94.

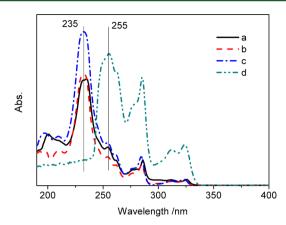
**2.4. Oxidative Desulfurization Procedure.** In a typical reaction run,  $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$  (24.6 mg, 0.039 mmol), IL  $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$  (24.6 mg, 0.039 mmol), IL  $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$  (24.6 mg, 0.039 mmol), IL  $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$  (1 mL), model oil (5 mL), and  $H_2O_2$  were added to a two-necked flask. Then, the mixture was stirred for 5 h at 40 °C under atmospheric pressure. After reaction, the model oil was separated by decantation for further analysis via gas chromatography—flame ionization detection (GC—FID, Agilent 7890A, HP-5 column, 30 m long × 0.32 mm inner diameter × 0.25  $\mu$ m film thickness; injector port temperature, 250 °C; detector temperature, 300 °C; and oven temperature, starting at 100 °C and rising to 200 °C at 15 °C/min for DBT and BT starting at 100 °C, rising to 160 °C at 20 °C/min, and then rising to 230 °C at 25 °C/min for 4,6-DMDBT). The sulfur removal was calculated as in eq 1, where  $C_0$  (ppm) is the initial sulfur concentration in the model oil and  $C_t$  (ppm) is the transient sulfur concentration at any time t (min).

sulfur removal (%) = 
$$(1 - C_t/C_0) \times 100$$
 (1)

### 3. RESULTS AND DISCUSSION

3.1. Investigation of Different Desulfurization Systems. DBT was selected as a representative sulfur compound in fuel because it was one of the main refractory sulfur compounds in the HDS treatment. The ionic liquid [C<sub>4</sub>mim]-BF4 was chosen as an extractant because of its remarkable selectivity of extraction sulfur compounds from model oil.<sup>39</sup> The conversion of DBT in model oil was used to calculate the removal of sulfur. The sulfur removal in different systems was listed in Table 1. When [C<sub>4</sub>mim]BF<sub>4</sub> was used as an extractant to remove DBT, the extractive desulfurization efficiency was only 23.2%. With the addition of 30 or 7.5 wt % H<sub>2</sub>O<sub>2</sub>, the sulfur removal decreased a little to 21.7 or 19.0%. The phenomena might be ascribed to the fact that the H<sub>2</sub>O<sub>2</sub> solution into the IL phase made some extracted DBT return to the oil phase. 40 The sulfur removal increased sharply to 74.5% for  $IL/[C_2mim]_3Fe(CN)_6/30$  wt %  $H_2O_2$  (entry 3 in Table 1), 76.3% for  $IL/[C_4mim]_3Fe(CN)_6/30$  wt %  $H_2O_2$ (entry 4 in Table 1), and 73.5% for  $IL/[C_8mim]_3Fe(CN)_6/30$ wt % H<sub>2</sub>O<sub>2</sub> (entry 5 in Table 1). The results showed the advantage of ECODS with the organic hexacyanoferrates over desulfurization by mere extraction or oxidation without catalysts. In comparison to 30 wt % H<sub>2</sub>O<sub>2</sub>, 7.5 wt % H<sub>2</sub>O<sub>2</sub> exhibited a higher oxidative performance. For example, the sulfur removal could reach 97.9% with [C<sub>4</sub>mim]<sub>3</sub>Fe(CN)<sub>6</sub> as a catalyst, 86.7% with [C<sub>2</sub>mim]<sub>3</sub>Fe(CN)<sub>6</sub> as a catalyst, and 91.1% with  $[C_8 \text{mim}]_3 \text{Fe}(CN)_6$  as a catalyst. The reason will be given in the following section. We also found that the catalytic activity was in the following order:  $[C_4 \text{mim}]_3 \text{Fe}(\text{CN})_6 > [C_8 \text{mim}]_3 \text{Fe}$  $(CN)_6 > [C_2 mim]_3 Fe(CN)_6$ . Therefore, deep desulfurization could be obtained with  $[C_4 \text{mim}]_3 \text{Fe}(CN)_6$  as a catalyst and 7.5 wt %  $H_2O_2$  as an oxidant in  $[C_4mim]BF_4$ .

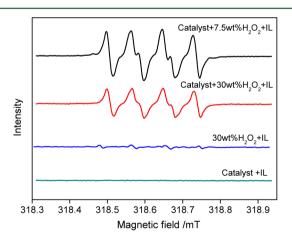
**3.2.** Reaction Mechanism of Oxidative Desulfurization. The ECODS reaction mechanism was investigated via UV—vis and ESR spin-trap technique. Figure 1 shows UV—vis



**Figure 1.** UV—vis spectra of (a) DBT in *n*-octane, (b) DBT extracted in  $CH_3OH$ , (c) DBT extracted in  $CH_3CN$ , and (d) DBT extracted in  $[C_4mim]BF_4$ .

spectra of DBT in n-octane and DBT extracted in solvents. An absorption band at 235 nm can be observed for DBT in n-octane. An absorption bands of DBT remained at about 235 nm. When DBT was extracted into  $[C_4 \text{mim}]BF_4$ , this band shifted to 255 nm, suggesting that the structure of DBT was distorted in  $[C_4 \text{mim}]BF_4$ . This might be attributed to the polarization of DBT by the fluorine ion. An addition, the oxidation of DBT in CH<sub>3</sub>OH and CH<sub>3</sub>CN was only 78.2 and 62.5% (see Table S1 of the Supporting Information), respectively, which was greatly lower than that in  $[C_4 \text{mim}]BF_4$  (94.3%). Therefore, the nature of the extractant had an important effect in the ECODS system, and the aromaticity of DBT might decrease in  $[C_4 \text{mim}]BF_4$ , which made DBT easier to be oxidized.

To further clarify the reaction mechanism, an ESR spin-trap technique was employed to probe the active oxygen species with DMPO as traps. As shown in Figure 2, no ESR signals



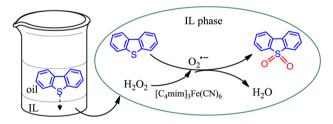
**Figure 2.** ESR spectra of the DMPO $-O_2^{\bullet -}$  adduct generated in the oxidative desulfurization process.

were observed when  $H_2O_2$  was absent. Very weak characteristic peaks of DMPO– $^{\bullet}$ OH signals could be obtained as the reaction was performed without catalyst, which may have resulted from the thermal decomposition of  $H_2O_2$  itself. However, the characteristic sextet peaks of the DMPO– $O_2$   $^{\bullet}$  – adduct were clearly observed in the presence of IL, catalyst, and 30 wt %  $H_2O_2$ .  $^{44-46}$  According to the ESR signals, we could conclude that  $O_2$   $^{\bullet}$  – was generated by  $[C_4 mim]_3 Fe(CN)_6$  upon

interaction with  $H_2O_2$  in IL. Interestingly, the ESR signal could be enhanced after the concentration of  $H_2O_2$  decreased from 30 to 7.5 wt %, indicating that more  $O_2^{\bullet}$  was produced. This result was consistent with the fact that the sulfur removal increased from 76.3 to 97.9% (Table 1). Thus, an obvious conclusion could be drawn that  $O_2^{\bullet}$  was the main active oxygen species on oxidation of DBT in this desulfurization system.

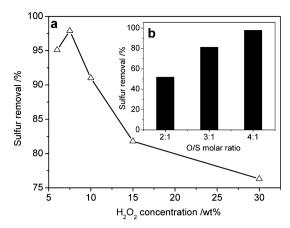
It is well-known that  $O_2^{\bullet -}$  is not stable in an aqueous environment. However, this stability issue could be addressed with [C<sub>4</sub>mim]<sub>3</sub>Fe(CN)<sub>6</sub> as a catalyst, because when the concentration of H<sub>2</sub>O<sub>2</sub> decreased while the O/S molar ratio remained constant, that is, more water was introduced to the reaction system, the amount of O2 odd not decrease but increased a lot (verified by Figure 2), which indicated that  $O_2^{\bullet}$  was stable in the  $[C_4 \text{mim}]_3 \text{Fe}(CN)_6 - [C_4 \text{mim}] BF_4$ system containing a certain amount of water. On the other hand, the utilization efficiency of H<sub>2</sub>O<sub>2</sub> increased remarkably. For instance, approximately 50% hydrogen peroxide was decomposed in our previous work<sup>22</sup> using [(CH<sub>3</sub>)<sub>4</sub>N]FeCl<sub>4</sub> as a catalyst, while 10.3% hydrogen peroxide was decomposed with  $[C_4mim]_3Fe(CN)_6$  as a catalyst (see Table S2 of the Supporting Information). The contrast provided direct evidence that [C<sub>4</sub>mim]<sub>3</sub>Fe(CN)<sub>6</sub> could stabilize O<sub>2</sub>• - in the desulfurization process. The oxidation products of the sulfur compounds were the corresponding sulfones and discussed at a later stage. Therefore, a plausible mechanism was proposed in Scheme 1. First, DBT in model oil was extracted into the IL

Scheme 1. Proposed Mechanism of the Oxidative Desulfurization Process



phase upon mixing model oil and IL. Then,  $O_2^{\bullet -}$  generated by the interaction between  $[C_4 \text{mim}]_3 \text{Fe}(\text{CN})_6$  and  $H_2 O_2$  in the IL phase can oxidize DBT to dibenzothiophene sulfones (DBTO<sub>2</sub>), which preferred to remain in the IL phase because of its higher polar. Therefore, a continuous decrease of the DBT concentration in model diesel was observed.

3.3. Influence of the Concentration and Dosage of H<sub>2</sub>O<sub>2</sub> on the Removal of DBT. To elucidate the influence of the concentration of H2O2 on the desulfurization, different concentrations of H<sub>2</sub>O<sub>2</sub> were applied under the experimental conditions of T = 40 °C, model oil (5 mL),  $[C_4 mim]BF_4$  (1 mL),  $H_2O_2$  (0.312 mmol), and  $[C_4mim]_3Fe(CN)_6$  (0.039 mmol). As seen in Figure 3a, when the concentration of H<sub>2</sub>O<sub>2</sub> decreased from 30 to 7.5 wt %, the sulfur removal increased from 76.3 to 97.9%. However, the sulfur removal dropped after the concentration of H<sub>2</sub>O<sub>2</sub> decreased to 6 wt %. Therefore, the influence of dosage of H2O2 was investigated using 7.5 wt %  $H_2O_2$  as an oxidant.  $H_2O_2/DBT$  (O/S) molar ratios of 2:1, 3:1, and 4:1 were plotted in Figure 3b. The sulfur removal increased from 51.8% at O/S = 2:1 to 97.9% at O/S = 4:1. According to the stoichiometric reaction, 2 mol of hydrogen peroxide is consumed for oxidation of 1 mol of DBT to DBT sulfone



**Figure 3.** Influence of the concentration and dosage of  $H_2O_2$  on the removal of DBT. Experimental conditions:  $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$ , 0.039 mmol; model oil, 5 mL;  $[C_4\text{mim}]\text{BF}_4$ , 1 mL; T, 40 °C; t, 5 h; (a) O/S, 4; and (b)  $[H_2O_2]$ , 7.5 wt %.

(DBTO<sub>2</sub>). However, it is well-known that there is a competition between the decomposition of hydrogen peroxide and the DBT oxidation reaction. <sup>22</sup> Therefore, O/S = 4 was the optimal dosage in the present study.

**3.4.** Influence of the Reaction Temperature and Time on the Removal of DBT. The sulfur removal with different reaction times at different temperatures is given in Figure 4. As

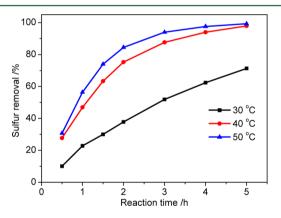
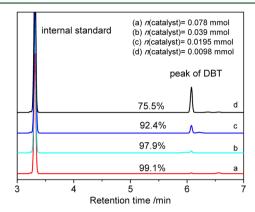


Figure 4. Influence of reaction temperature and time on sulfur removal. Experimental conditions:  $[C_4mim]_3Fe(CN)_6$ , 0.039 mmol; model oil, 5 mL;  $[C_4mim]BF_4$ , 1 mL; and O/S, 4.

expected, the conversion of DBT increased with the increasing reaction time. For example, 27.7% sulfur removal was obtained in 0.5 h at 40 °C, and the sulfur removal increased dramatically to 97.9% after 5 h. It can be found that the trend of sulfur removal was similar at 30 and 50 °C. However, the desulfurization efficiency at 30 °C was only 71.3% after 5 h. In combination of the 99.3% sulfur removal at 50 °C, it could be concluded that the reaction temperature profoundly enhanced the desulfurization rate. This trend was not in line with the result of our previous work  $^{18-22}$  with the Fe-based catalytic system, and the difference might be due to the different ligands to iron. From the practical point of view, 40 °C was chosen as an appropriate reaction temperature for the present ECODS process, because a higher temperature could result in higher operation cost and thermal decomposition of  $\rm H_2O_2$ .

**3.5.** Influence of the Amount of Catalyst on the Removal of DBT. The influence of the amount of catalyst on the desulfurization process was studied by varying the amount of  $[C_4mim]_3Fe(CN)_6$  from 0.0098 to 0.078 mmol. As shown in Figure 5, the DBT removal increased notably from 75.5 to

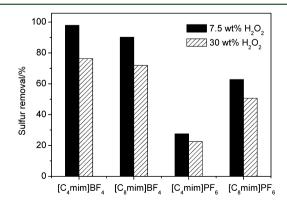


**Figure 5.** Influence of the amount of catalyst on the removal of DBT. Experimental conditions: T, 40 °C; model oil, 5 mL;  $[C_4mim]BF_4$ , 1 mL; O/S, 4; and t, 5 h.

97.9% as the amount of catalyst increased from 0.0098 to 0.039 mmol and then increased mildly when the mass of catalyst increased from 0.039 to 0.078 mmol. It was obvious that the excessive catalyst was not necessary and for an economical purpose. Thus, 0.039 mmol was chosen as the most suitable quantity in this experiment.

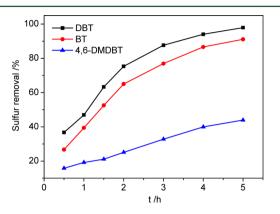
# **3.6.** Influence of Different ILs on the Removal of DBT. In the present ECODS process, ILs were deemed as a reacting phase and, thus, different ILs had a significant influence on the

sulfur removal performance. The tests with different ILs, such as  $[C_4 \text{mim}]BF_4$ , 1-n-octyl-3-methylimidazolium tetrafluoroborate ( $[C_8 \text{mim}]BF_4$ ), 1-butyl-3-methylimidazolium hexafluorophosphate ( $[C_4 \text{mim}]PF_6$ ), and 1-n-octyl-3-methylimidazolium hexafluorophosphate ( $[C_8 \text{mim}]PF_6$ ), were carried out in the presence of 7.5 and 30 wt %  $H_2O_2$ , respectively. The results in Figure 6 showed that DBT removal with 7.5 wt %  $H_2O_2$  was greater than that with 30 wt %  $H_2O_2$  in all of the ILs above. Furthermore, it was found that the difference in activity depended upon the nature of the ILs. In comparison to the ILs with  $PF_6$  anion, the ILs with  $BF_4$  anion were more beneficial to the sulfur removal.



**Figure 6.** Influence of different extractants on removal of DBT. Experimental conditions:  $[C_4 \text{mim}]_3 \text{Fe}(\text{CN})_6$ , 0.039 mmol; T, 40 °C; model oil, 5 mL; IL, 1 mL; O/S, 4; and t, 5 h.

**3.7.** Oxidation of Different Sulfur-Containing Compounds. The performance of catalyst  $[C_4 mim]_3 Fe(CN)_6$  for different sulfur-containing compounds, including DBT, BT, and 4,6-DMDBT, was evaluated in Figure 7. The sulfur removal was



**Figure 7.** Removal of different sulfur-containing compounds. Experimental conditions:  $[C_4 \text{mim}]_3 \text{Fe}(\text{CN})_6$ , 0.039 mmol; T, 40 °C; model oil, 5 mL;  $[C_4 \text{mim}] \text{BF}_4$ , 1 mL; O/S, 4; and t, 5 h.

increased with the increasing reaction time. Under the same conditions, the final desulfurization efficiency for DBT, BT, and 4,6-DMDBT was 97.1, 91.1, and 43.9%, respectively. The difference might be correlated with the electronic density of sulfur atoms and the steric hindrance effect. As calculated by Otsuki et al.,<sup>47</sup> the electron density on the S atom of BT (5.758) was lower than that of DBT (5.739), leading to a lower reactivity of BT. The lowest reactivity of 4,6-DMDBT may be attributed to the steric hindrance effect of the methyl groups, which was an obstacle for the approach of the sulfur atom to

the catalytic active species. <sup>19,48</sup> The results indicated that the steric hindrance gave a greater effect on oxidative desulfurization. However, the removal of 4,6-DMDBT could increase to 90.2% after optimization of the reaction condition ( $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$ , 0.078 mmol; T, 40 °C; model oil, 5 mL;  $\text{IL}([C_4\text{mim}]\text{BF}_4)$ , 1 mL; O/S, 12; and t, 5 h). Therefore, the organic hexacyanoferrates showed great potential for desulfurization of diesel fuel in the future.

The three sulfur-containing compounds mentioned above could be oxidized to their corresponding sulfones, which were determined by GC–MS analysis. After the reaction, the IL phase was separated and extracted with diethyl ether. The organic phase was collected and concentrated for GC–MS analysis. The sulfur oxidation products could not be detected in the oil phase, and all of the products existed in the IL phase because of the different chemical polarities between products and model oil. As shown in Figure 8a, the mass spectrum of the product showed the molecular ion peak at m/z 216.0 for DBT, which was assigned to DBTO<sub>2</sub>. Similar oxidation products of BT and 4,6-DMDBT were obtained, and the mass spectra in panels b and c of Figure 8 matched that of BTO<sub>2</sub> (166.0) and 4,6-DMDBTO<sub>2</sub> (246.0), respectively.

**3.8. Recycling of the Catalytic System.** The cycle property was an important factor and essential to be investigated. After the first reaction run, the upper layer was separated by decantation. The IL phase was distilled at 40 °C in vacuum for 12 h to evaporate the residual  $H_2O_2$ ,  $H_2O$ , and model oil. Then, fresh  $H_2O_2$  and model oil were added for the next cycle under the same conditions. The results in Figure 9 showed that the system could be recycled at least 4 times without a significant decrease in activity. However, the sufur removal decreased to 85.7% after 5 times. The decrease of

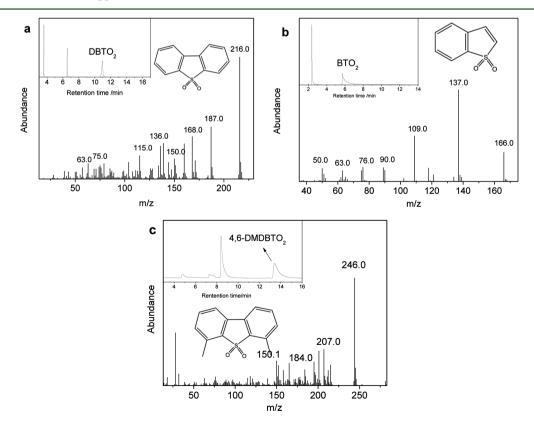
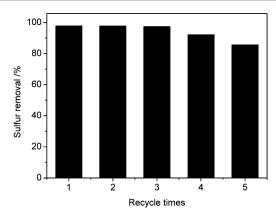


Figure 8. GC-MS of the oxidation products.



**Figure 9.** Recycling of the catalytic system containing  $[C_4\text{mim}]BF_4$  and  $[C_4\text{mim}]_3Fe(CN)_6$  on the removal of DBT. Experimental conditions:  $[C_4\text{mim}]_3Fe(CN)_6$ , 0.039 mmol; model oil, 5 mL;  $[C_4\text{mim}]BF_4$ , 1 mL; O/S, 4; and T, 40 °C.

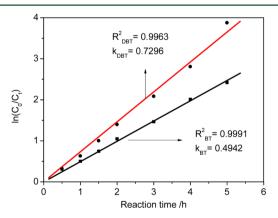
sulfur removal might be attributed to the increasing oxidation product  $DBTO_2$  that accumulated in the IL phase. <sup>19</sup>

**3.9.** Kinetics of the Catalytic Desulfurization of Model Oil. Reaction kinetics was a greatly important parameter to explain the oxidation of sulfur compounds. Experiments were performed with  $[C_4 \text{mim}]_3 \text{Fe}(CN)_6 / [C_4 \text{mim}] BF_4 / H_2O_2$  to obtain kinetic parameters of the oxidation of sulfur compounds. The rate constant for the apparent consumption of sulfur compound was obtained from the pseudo-first-order eqs 2 and 3 as follows:

$$-\mathrm{d}C_t/\mathrm{d}t = kC_t \tag{2}$$

$$ln(C_0/C_t) = kt$$
(3)

where  $C_0$  and  $C_t$  were the initial sulfur concentration and the sulfur concentration at time t, respectively.  $\ln(C_0/C_t)$  against the reaction time was plotted in Figure 10. The linear fit of



**Figure 10.** Pseudo-first-order kinetics for oxidation of DBT and BT. Experimental conditions:  $[C_4mim]_3Fe(CN)_6$ , 0.039 mmol; model oil, 5 mL;  $[C_4mim]BF_4$ , 1 mL; O/S, 4; and T, 40 °C.

 $\ln(C_t/C_0)$  against the the reaction time demonstrated the pseudo-first-order kinetics characteristics for oxidation of DBT and BT using catalyst  $[C_4\text{mim}]_3\text{Fe}(\text{CN})_6$  ( $R^2_{\text{DBT}} = 0.9963$ , and  $R^2_{\text{BT}} = 0.9991$ ). The apparent rate constants k of DBT and BT were 0.7296 and 0.4942 h<sup>-1</sup>, respectively.

### 4. CONCLUSION

A deep desulfurization process based on extraction using [C<sub>4</sub>mim]BF<sub>4</sub> and catalytic oxidation with a series of organic hexacyanoferrates catalyst  $[C_n mim]_3 Fe(CN)_6$  (where n = 2, 4,and 8) was developed. The sulfur removal could increase to 97.9, 91.1, and 43.9% for DBT, BT, and 4,6-DMDBT, respectively, with  $[C_4 mim]_3 Fe(CN)_6$  as a catalyst and 7.5 wt %  $H_2O_2$  as an oxidant. The catalyst could interact with  $H_2O_2$  in  $[C_4 mim]BF_4$  to generate  $O_2^{\bullet}$ , which could oxidize the sulfur compounds to the corresponding sulfones. Moreover, O2. could remain stable in the reaction process, and only 10.3% H<sub>2</sub>O<sub>2</sub> was decomposed. The sulfur conversion followed the pseudo-first-order kinetics, with the reaction rate constants of 0.7296 and 0.4942 h<sup>-1</sup> for DBT and BT, respectively. Moreover, the catalytic system could be recycled at least 4 times without a vital decrease in activity. Therefore, deep desulfurization has been obtained with low concentration of H<sub>2</sub>O<sub>2</sub> as oxidant. It provides a safer and more environmentally friendly way for the oxidative desulfurization of diesel oil.

### ASSOCIATED CONTENT

### S Supporting Information

FTIR of (a)  $[C_2mim]_3Fe(CN)_6$ , (b)  $[C_4mim]_3Fe(CN)_6$ , and (c)  $[C_8mim]_3Fe(CN)_6$  (Figure S1), ESI–MS of catalysts in CH<sub>3</sub>OH (Figure S2), oxidation of DBT in different extractants (Table S1), and decomposition of  $H_2O_2$  in the reaction process (Table S2). This material is available free of charge via the Internet at http://pubs.acs.org.

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### Notes

The authors declare no competing financial interest.

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