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## Experimental and Modeling Study on Phase Equilibria of Semiclathrate Hydrates of Tetra-n-butyl Ammonium Bromide + CH<sub>4</sub>, CO<sub>2</sub>, N<sub>2</sub>, or Gas Mixtures

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ABSTRACT: Tetra-n-butyl ammonium bromide (TBAB) is most-widely used as a hydrate promoter in the separation of flue gases and CO<sub>2</sub> sequestration. Because of the complicacy of semiclathrate hydrate formed by TBAB aqueous solution and gases, few researchers have investigated the thermodynamic modeling of phase equilibria of semiclathrate hydrates. In this work, the CH<sub>4</sub>-N<sub>2</sub> hydrate dissociation conditions were determined in TBAB solution first, and then a thermodynamic model for gas hydrate proposed by Chen and Guo was extended for semiclathrate hydrates of gas mixtures in TBAB aqueous solution. The Patel-Teja equation of state (PT EoS) was used for calculation of the fugacity of the gas phase. To evaluate the activity of water and activity coefficients of TBAB in TBAB aqueous solution, a correlation on the basis of existing osmotic coefficient and activity coefficient values is employed. For modeling the hydrate phase, parameters for sII hydrates proposed in the Chen-Guo hydrate model were used to calculate the fugacity of gases in hydrate phase, and parameters of TBAB were obtained from the correlation with the literature dissociation data for the pure gas + TBAB + water system. Then the presented model was used to predict dissociation data for the gas mixtures + TBAB + water system, and the results show acceptable agreement with other literature data and the experimental data for CH<sub>4</sub>-N<sub>2</sub> in this work.

#### 1. INTRODUCTION

Large amounts of greenhouse gases including methane, carbon dioxide, carbon monoxide, hydrogen sulfide, etc. are released into the atmosphere every year, which result in air pollution and global warming. Therefore, separation of the aforementioned gases from the corresponding gas flows is of industrial and environmental significance from the past century up to now. Cryogenic distillation, pressure swing adsorption (PSA), membranes, and absorption with liquids are the widely used techniques currently applied for this purpose. These approaches have their own limitations such as high energy requirement, high cost, corrosivity, solvent loss, or low capacity. A novel technology called the hydrate formation/dissociation method, which has been recently proposed, 1-6 has attracted much attention<sup>7–14</sup> and does have wide application prospects.<sup>15</sup>

Under favorable conditions of temperature and pressure, light gases will form hydrates with water, and different gases have different hydrates formation conditions. The difference in gas hydrate properties of various gases including the chemical affinity of the hydrate cages to enclathrate specific gases and the difference in the corresponding phase behaviors can determine the possibility of such separation processes. For instance, the hydrate phase can be enriched in component(s) of interest, while the concentration of other gas(s) can be increased in the gas phase at equilibrium.16

Tetra-n-butyl ammonium bromide (TBAB) forms semiclathrate hydrate with water such that it can reduce the gas hydrate formation pressures greatly.<sup>17</sup> In TBAB hydrate cavities, the TBA+ is encaged in tetrakaidecahedra and pentakaidecahedra (large) (50% of each), and the gaseous component, such as CH<sub>4</sub>, CO<sub>2</sub>, N<sub>2</sub>, and H<sub>2</sub>S, is trapped in dodecahedral small cages. <sup>18</sup> As a kind of semiclathrate hydrates, TBAB hydrates show great potential application in gas storage and transportation, separation of flue gases, and CO2 sequestration. 19-22 To design the efficient separation processes using hydrate formation technology, accurate and reliable phase equilibrium data should be obtained. Johnny Deschamps et al.<sup>23</sup> investigated phase equilibrium for TBAB semiclathrate hydrates of N<sub>2</sub>, CO<sub>2</sub>, N<sub>2</sub> + CO<sub>2</sub>, and CH<sub>4</sub> + CO<sub>2</sub>. Bahman Tohidi et al.<sup>24</sup> presented equilibrium data of H2, CH4, N2, CO2, and natural gas in semiclathrate hydrates of TBAB. Mohammadi et al. 16,25 reported experimental dissociation data for semiclathrate hydrates of TBAB + H<sub>2</sub>S, CH<sub>4</sub>, CO<sub>2</sub>, N<sub>2</sub>, or H<sub>2</sub>.

Unfortunately, modeling phase equilibria of semiclathrate hydrate systems has been rarely investigated in the literature. Joshi et al.<sup>26</sup> extended the hydrate model of Chen and Guo<sup>27</sup> for semiclathrate hydrate of CH<sub>4</sub>, CO<sub>2</sub>, and N<sub>2</sub> in aqueous solution of TBAB. It is observed that the Chen and Guo's model is simple, concise, and more flexible to apply not only for the clathrate system of pure gases and gas mixtures but also for hydrate systems in the presence of inhibitors.<sup>28</sup> Mohammadi and co-workers<sup>29</sup> used traditional van der Waals-Platteeuw (vdW-P) solid solution theory for modeling the hydrate phase and proposed a thermodynamic model for prediction of phase equilibria of semiclathrate hydrates of the CO<sub>2</sub>, CH<sub>4</sub>, or N<sub>2</sub> + TBAB aqueous solution. However, the thermodynamic modeling proposed in the above two examples of literature are the prediction of phase equilibria of TBAB and different pure gases, and models for phase equilibria of TBAB and gas

September 4, 2013 Received: Revised: December 4, 2013 Accepted: December 5, 2013 Published: December 5, 2013 mixtures systems have not yet been developed in open literature.

In this study, the CH<sub>4</sub> (37.52 mol %)-N<sub>2</sub> hydrate dissociation data in TBAB (10 wt %) solution are observed first. Then the calculation of sII hydrate of Chen and Guo's model<sup>27</sup> is modified for predicting phase equilibria of semiclathrate hydrate of gas mixtures in TBAB aqueous solution. In addition, parameters of TBAB in Chen and Guo' hydrate model<sup>27</sup> are obtained from the correlation with the literature<sup>16</sup> dissociation data. It is shown that the proposed modified model predicts the TBAB semiclathrate hydrate dissociation condition well.

#### 2. EXPERIMENTAL WORK

The composition of feed gas is prepared by Beijing AP Beifen Gas Industry Company. TBAB is prepared by Shanghai Sinopharm Chemical Reagent Company, and the purity of it is analytical pure. The experimental apparatus used in this study and the experimental procedures are the same as we proposed in our previous work. The method called "isochoric pressure search"  $^{4,5,15,30-33}$  is used to obtain the dissociation data of  $CH_4-N_2$  gas mixtures in TBAB aqueous solution.

#### 3. MODELING

**3.1. Development of the Thermodynamic Model.** For the traditional van der Waals-Platteuw (vdW-P) model, the liquid water—hydrate—gas/vapor equilibrium conditions are calculated by equating the fugacity of water in the aqueous  $(f_w^L)$  and in the hydrate  $(f_w^H)$  phases

$$f_w^L = f_w^H \tag{1}$$

where f is fugacity, subscript w denotes water, and superscripts L and H represent the liquid and hydrate phases, respectively.

According to Chen and Guo,<sup>27</sup> the equilibrium conditions are calculated by equating the fugacity of gas in the gas phase and in the hydrate phase:

$$f_i^G = f_i^H = x_i f_i^{H,0} (1 - \sum_j \theta_j)^{\alpha}$$
 (2)

However, for TBAB semiclathrate hydrates, both some small gases ( $N_2$ ,  $CO_2$ ,  $CH_4$ , etc.) and TBAB are involved in the formation of hydrate. Consequently eq 2 can be comprehended as the following equations:

$$f_j^G = f_j^H = x_j f_j^{H,0} (1 - \sum_j \theta_j)^{\alpha}$$
 for gases (3)

$$f_M^L = f_M^H = x_M f_M^{H,0} (1 - \sum_j \theta_j)^{\alpha} \text{ for TBAB}$$
 (4)

$$\sum_{i} x_i = x_M + \sum_{j} x_j = 1 \tag{5}$$

In this study, the model of Chen and Guo<sup>27</sup> is modified for predicting phase equilibria of semiclathrate hydrate of gas mixtures in TBAB aqueous solution, and the hydrate parameters of TBAB in the model are obtained by the correlation with dissociation data for pure gas + TBAB + water systems in the literature.<sup>16</sup>

The application of the two-step hydrate formation mechanism proposed by Chen and Guo<sup>27</sup> is described as follows:

First step: The formation of a stoichiometric basic hydrate through a quasi-chemical reaction between water and basic semiclathrate hydrate former. It should be pointed out that the gas species is assumed to be capable of forming a basic semiclathrate hydrate in this study, although the amount of them is small. The formation of a basic semiclathrate hydrate can be illustrated by the following quasi-chemical reaction equation

$$H_2O + \lambda_2 S = S_{\lambda_2} \bullet H_2O \tag{6}$$

where S represents TBAB and gas species;  $\lambda_2$  stands for the molecular number of S per water molecule in the basic semiclathrate hydrate. On the basis of the so far knowledge about the structures of the semiclathrate hydrates of TBAB, the hydration number is found to be 26 for type A and 38 for type B. Experimental study on crystal growth of semiclathrate hydrate of TBAB shows that each hydrate cell unit of the investigated semiclathrate is composed of 2 TBA+ and 2 Br along with 52 water molecules for type A and 76 for type B. The TBA+ cation is trapped in two large tetrakaidecahedra and pentakaidecahedra, respectively. It should be pointed out that a total of four similar large cavities are involved, and, hence,  $\lambda_2$  equals to 8/52 for type A and 8/76 for type B. During this step, the so-called linked cavities, the small cavities (5<sup>12</sup>), are formed automatically.

Second step: The adsorption of small size gas molecules (e.g.,  $N_2$ ,  $CO_2$ ,  $CH_4$ , etc.) into the empty linked cavities in basic semiclathrate hydrate and formation of the stable hydrate. The partial occupation of the linked cavities by help gas molecules will lower the chemical potential of the basic hydrate and results in the nonstoichiometric property of the final semiclathrate hydrates formed.

Based on the above stated two-step formation mechanism, the final modeling of the semiclathrate hydrate formed can be expressed as

$$f_{i} = f_{i}^{H} = x f_{i}^{H,0} (1 - \sum_{j} \theta_{j})^{\alpha}$$
(7)

$$\sum_{j} \theta_{j} = \frac{\sum_{j} f_{j}^{G} C_{j}}{1 + \sum_{j} f_{j}^{G} C_{j}}$$
(8)

$$\sum_{i} x_{i} = 1 \tag{9}$$

where  $\alpha = \lambda_1/\lambda_2$ ;  $\lambda_1$  is the number of linked cavities per water molecule in the basic semiclathrate hydrate. Each hydrate cell unit has 6 small cavities, and consequently  $\lambda_1$  equals to 6/52 for type A and 6/76 for type B.

It should be pointed out that  $f_i$  in eq 7 equals to  $f_j^G$  for gases and  $f_M^L$  (eq 15) for TBAB. In eq 7

$$f_i^{H,0} = f_i^{H,0}(T) f^{H,0}(P) f^{H,0}(a_w)$$
 (10)

where

$$f_i^{H,0}(T) = \exp\left(\frac{-\sum_j A_{jM}\theta_j}{T}\right) A' \exp\left(\frac{B'}{T - C'}\right)$$
(11)

$$f^{H,0}(P) = \exp\left(\frac{\beta P}{T}\right) \tag{12}$$

$$f^{H,0}(a_w) = a_w^{-1/\lambda_2} \tag{13}$$

 $\theta$  in eq 8 is the fraction of linked cavities ( $S^{12}$ ) occupied by small gas molecules ( $CO_2$ ,  $CH_4$ ,  $N_2$ , etc., no TBAB).  $f_j^G$  is the fugacity of gas. The fugacity of gas is calculated with Patel-Teja EOS.  $S^{35}$   $C_j$  is the so-called Langmuir constant of the guest gas molecules in the linked cavities and correlated as an Antoine-type equation:

$$C = X \exp\left(\frac{Y}{T - Z}\right) \tag{14}$$

The constants X, Y, and Z were determined against the rigorous Langmuir constants C calculated from the Lennard-Jones potential function. The fitted X, Y, and Z values for typical gas species are listed in Table 1.

Table 1. Antoine Constants for Calculating the Langmuir Constants in Eq 14

gas	$X \times 10^6/\text{bar}^{-1}$	Y/K	Z/K
$CH_4$	2.3048	2752.29	23.01
$CO_2$	1.6464	2799.66	15.9
$N_2$	4.3151	2472.37	0.64

In eq 11,  $A_{jM}$  are the binary interaction parameters specifying the guest—guest interaction between components j (small gas molecules) and M (TBAB).  $A_{jM} = A_{Mj}$  and  $A_{jj} = A_{MM} = 0$ . The  $A_{jM}$  values fitted from the common corresponding hydrate dissociation data for the pure gas + TBAB + water system <sup>16</sup> are given in Table 2. It should be pointed out that the semiclathrate

Table 2. Recommended Values for the Cross-Parameter  $A_{jM}$  (TBAB Semiclathrate Hydrate)

component	CO <sub>2</sub>	$CH_4$	$N_2$
5 wt % TBAB	410	220	80
10 wt % TBAB	380	110	70
25 wt % TBAB	50	-50	-100
50 wt % TBAB	-260	-150	-160

structure can be changed from type A to type  $B^{36}$  or vice versa. It leads to the change of the hydration number and semiclathrate structure parameters  $\beta$  with the varying TBAB concentrations. In this work, the semiclathrate structure parameter  $\beta$  is set to a const, and the change of the semiclathrate structure is corrected by the binary interaction parameters  $A_{iM}$ , which causes large changes in  $A_{iM}$ .

 $\beta$  in eq 12 is the hydrate structural parameter,  $\beta$  = 3.5 K/bar for type B TBAB sc hydrate, and  $\beta$  = 2.8 K/bar for type A. It is worth pointing out that several researchers<sup>18,37,38</sup>

It is worth pointing out that several researchers 16,5/,58 observed two types of TBAB semiclathrate hydrate structures, A and B, for varying TBAB concentrations. From the phase diagram of TBAB hydrate crystals (types A and B), it is observed that 18 wt % is a critical weight percentage. Type B has a higher melting point below 18 wt %, while above 18 wt %, type A has a higher melting point. Consequently, we indicate that the type of the semiclathrate hydrate is type B when the TBAB concentration is below 18 wt %, while above 18 wt %, the semiclathrate hydrate is type A.

Parameters A', B', and C' for TBAB are determined by fitting the hydrate equilibrium data for the pure gas + TBAB + water system. The regressed values of A', B', and C' for the gases and TBAB used in this work are listed in Table 3. Values of A', B', and C' for the gases are the same as sII hydrate in the model of Chen and Guo. The same are the same as sII hydrate in the model of Chen and Guo.

Table 3. Antoine Constants for Calculating  $f_i^0(T)$  in Eq 11

component	$A'/10^{23}$ bar	B'/K	C'/K
CO <sub>2</sub>	3.4474	-13470	6.79
$CH_4$	5.2602	-13088	4.08
$N_2$	6.8165	-12783	-1.10
TBAB type $A^a$	6.3491	-26596	-111
TBAB type B <sup>a</sup>	3.2498	-18620	5.43

<sup>a</sup>Values fitted in this work from dissociation data for the pure gas + TBAB + water system.

The same as in ref 29, fugacity of the hydrate promoter (TBAB) in the aqueous phase needs to be determined as well, and eq 12 can be applied for this purpose

$$f_{\rm M}^{\rm L} = x_{\rm M}^{\rm L} \gamma_{\rm M} P_{\rm M}^{\rm sat} \exp \left( \frac{\nu_{\rm M}^{\rm L} (P - P_{\rm M}^{\rm sat})}{RT} \right) \tag{15}$$

where  $\gamma_{\rm M}$  represents the activity coefficient of the hydrate promoter (TBAB) in the aqueous solution, and the subscript M stands for TBAB.

In TBAB aqueous solution, the activity coefficient of the TBAB salt is calculated through the corresponding values proposed by Lindenbaum and Boyd<sup>39</sup> and Amado and Blanco,<sup>40</sup> and the correlation was proposed by Ali Eslamimanesh<sup>29</sup> to calculate the activity coefficient of TBAB as follows:

$$\gamma_{\rm M} = -0.5057 w_{\rm M}^3 + 1.1603 w_{\rm M}^2 - 1.3689 w_{\rm M} + 0.7655$$
 (16)

The activity of water in the TBAB aqueous solution is also calculated through the corresponding values proposed by Lindenbaum and Boyd<sup>39</sup> and Amado and Blanco,<sup>40</sup> and the correlation was proposed in this work to calculate the activity of water as follows:

$$\ln a_{w} = -0.03321 w_{\rm M}^{2} - 0.09463 w_{\rm M} - 2.5874 \times 10^{-4}$$
(17)

Here,  $w_{\rm M}$  is the weight fraction of TBAB in solution.

The density  $(\rho)$  of the TBAB aqueous solution (and consequently the molar volume  $(\nu_{\rm M}^L)$ ) has been determined using the correlation of Söhnel and Novotny<sup>41</sup> with the recommended values by Belandria and co-workers<sup>42,43</sup>

$$\rho_{\rm M} = \rho_{\rm w} + B_1(100w_{\rm M}) + B_2(100w_{\rm M})^2 + B_3(100w_{\rm M})^3$$
(18)

where

$$B_{i} = q_{i} + r_{i}(T/K) + s_{i}(T/K)^{2}$$
(19)

where  $q_{ij}$   $r_{ij}$  and  $s_i$  are empirical constants, which are given in Table 4. In eq 18 and eq 19,  $\rho_{\rm M}$  is calculated in g/cm<sup>3</sup>.

**3.2. Calculation Procedure.** The calculation procedure for determining the semiclathrate hydrate formation conditions of a gas mixture with given composition is summarized in the schematic flow diagram shown in Figure 1. For simple gas hydrates (formed by pure gas), a similar procedure can be applied.

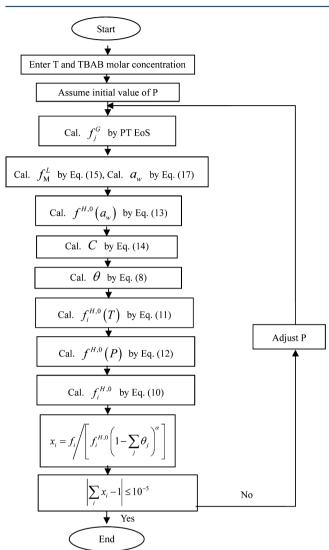
#### 4. RESULTS AND DISCUSSION

The measured dissociation conditions of semiclathrate hydrates of  $CH_4$  (37.52 mol %)- $N_2$  in the presence of 0.1 mass fraction of TBAB aqueous solution are reported in Table 5.

**4.1. Pure Gas + TBAB Systems.** The performance of the model for the prediction of the semiclathrate hydrate

Table 4. Constants in Eq 19



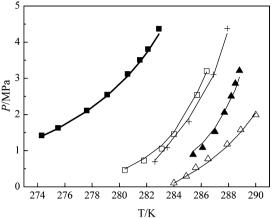


**Figure 1.** Flow diagram for calculating the formation pressure of semiclathrate hydrate at a given temperature.

Table 5. Dissociation Data of sc Hydrate of  $CH_4$ – $N_2$  in TBAB Aqueous Solution

parameter		value				
T/K	282.15	283.15	284.15	285.15	286.15	287.15
P/MPa	0.76	1.22	2.04	3.03	4.40	5.84

dissociation conditions for the  $\rm CO_2/CH_4/N_2+TBAB$  systems in the liquid solution-hydrate-vapor/gas equilibrium region has been first examined. The obtained results are shown in Figures 2–4. The experimental data on phase equilibria of the pure gas hydrate system for  $\rm CO_2$ ,  $\rm CH_4$ , and  $\rm N_2$  are also shown in Figures 2–4, respectively, for comparison. It is observed from Figures 2–4 that the model prediction results are in good agreement with the experimental data in all three cases. It is necessary to point out that the bold solid lines in Figures 2–4 are actually the predictions of Chen and Guo's model. <sup>27</sup>



**Figure 2.** Dissociation conditions of clathrate/semiclathrate hydrates for carbon dioxide + water/TBAB aqueous solution systems. Symbols stand for the experimental data, and curves refer to the predicted values using Chen and Guo's model or the modified model for TBAB sc hydrates in this work. ■, the CO<sub>2</sub> + water system (Adisasmito. S.; Sloan, E. D. et. al<sup>44</sup>); □, CO<sub>2</sub> in the presence of 0.05 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.<sup>16</sup>); ♠, CO<sub>2</sub> in the presence of 0.10 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.<sup>16</sup>); +, CO<sub>2</sub> in the presence of 0.50 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.<sup>16</sup>); +, CO<sub>2</sub> in the presence of 0.50 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.<sup>16</sup>); Bold solid curve, Chen and Guo's model predicted results for the CO<sub>2</sub> + water system (AARD = 1.5); Solid curves, modified model predicted results in this work (AARD = 5.4).

Equation 20 is used to calculate the error between the model results and experimental results

$$AARD = (100/N) \sum_{i}^{N} |P_{i,pred}^{diss} - P_{i,exp}^{diss}|/P_{i,exp}^{diss}$$
(20)

where N is the number of the experimental data points, and the subscript pred stands for the predicted values.

It should be pointed out again that parameters of TBAB were fitted from dissociation data for pure gas + TBAB + water systems and then used to predict results in Figure 5 for the mixture gas + TBAB + water system.

Several researchers 18,37,38 observed two types of TBAB

Several researchers observed two types of TBAB semiclathrate hydrate structures, A and B, for varying TBAB concentrations. From the phase diagram of TBAB hydrate crystals (type A and B), it is observed that 18 wt % is a critical weight percentage. Type B has a higher melting point below 18 wt %, while above 18 wt %, type A has a higher melting point. As a result, in Figures 2, 3, 4, and 5, it is indicated that the type of the semiclathrate hydrate is type B when TBAB concentration is below 18 wt %, while above 18 wt %, the semiclathrate hydrate is type A.

**4.2. Gas Mixtures + TBAB Systems.** The predicted phase equilibria of the gas mixtures + TBAB aqueous solution systems are sketched in Figure 5. It is observed from Figure 5 that predicted results show good agreement with the experimental and literature data.

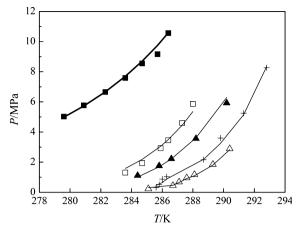


Figure 3. Dissociation conditions of clathrate/semiclathrate hydrates for methane + water/TBAB aqueous solution systems. Symbols stand for the experimental data, and curves refer to the predicted values using Chen and Guo's model or the modified model for TBAB sc hydrates in this work. ■, the CH<sub>4</sub> + water system (Adisasmito, S.; Sloan E. D. et. al.  $^{44}$ ); □, CH<sub>4</sub> in the presence of 0.05 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{25}$ ); ▲, CH<sub>4</sub> in the presence of 0.10 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ ); ⇒, CH<sub>4</sub> in the presence of 0.50 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ ); +, CH<sub>4</sub> in the presence of 0.50 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ ); Bold solid curve, Chen and Guo's model predicted results for the CH<sub>4</sub> + water system (AARD = 1.6); Solid curves, modified model predicted results in this work (AARD = 8.7).

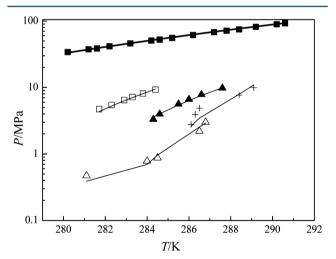


Figure 4. Dissociation conditions of clathrate/semiclathrate hydrates for nitrogen + water/TBAB aqueous solution systems. Symbols stand for the experimental data, and curves refer to the predicted values using Chen and Guo's model or the modified model for TBAB sc hydrates in this work.  $\blacksquare$ , the  $N_2$  + water system (van Cleeff, A.; Diepen, G. A. M.  $^{45}$ );  $\square$ , CH4 in the presence of 0.05 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ );  $\blacktriangle$ ,  $N_2$  in the presence of 0.10 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ ); +, +, N2 in the presence of 0.50 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ ); +, N2 in the presence of 0.50 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{16}$ ); Bold solid curve, Chen and Guo's model predicted results for the  $N_2$  + water system (AARD = 1.5); Solid curves, modified model predicted results in this work (AARD = 7.7).

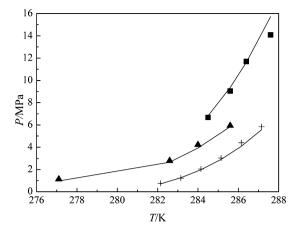


Figure 5. Dissociation conditions of clathrate/semiclathrate hydrates for gas mixtures + TBAB aqueous solution systems. Symbols stand for the experimental data, and curves refer to the predicted values using the modified model for TBAB sc hydrates in this work. ■, CO<sub>2</sub> (15.1 mol %) + N<sub>2</sub> in the presence of 0.05 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{46}$ ); ♠, CO<sub>2</sub> (39.9 mol %) + N<sub>2</sub> in the presence of 0.05 weight fraction TBAB aqueous solution (Mohammadi, A. H.; Richon, D. et al.  $^{46}$ ); +, CH<sub>4</sub> (37.52 mol %) + N<sub>2</sub> in the presence of 0.05 weight fraction TBAB aqueous solution in this work; Solid curve, modified model predicted results in this work (AARD = 5.4).

Many comprehensive researchers share a common outlook that the phase behavior of semiclathrate hydrates may be complicated and difficult to analyze. 1,36 There are at least five different structures in the system TBAB + water, with hydration numbers of 24, 26, 32, 36, and 38, but this has not been confirmed at this time. <sup>47</sup> In addition, some evidence has shown that there are some discrepancies even in the produce experimental data for the semiclathrate hydrate systems so far. For this reason, the selected dissociation data from the literature in this work were obtained by the same researchers. Because of the corresponding dissociation data selected from the literatures, it is worth pointing out the temperature range of the proposed model is 280-292 K. There will be big errors when the temperature is out of the range. The model is proposed by the experimental efforts for prediction of the phase equilibria of semiclathrate hydrates, especially for the gas mixtures + TBAB + water system. Unfortunately it could not predict the structure I and structure II hydrate.

#### 5. CONCLUSIONS

In this study, the hydrate dissociation data of CH<sub>4</sub>-N<sub>2</sub> gas mixtures in the presence of TBAB aqueous solution were first measured. In addition, a modified model based on the model of Chen and Guo was proposed to calculate/estimate the dissociation conditions of the semiclathrate hydrates of CO<sub>2</sub>/ CH<sub>4</sub>/N<sub>2</sub> or gas mixtures in the presence of TBAB aqueous solution. The model was developed on the basis of the calculation of structure II hydrate in Chen and Guo's model. The PT EoS was applied for calculation of fugacity of gas phase, and a correlation on the basis of existing osmotic coefficient and activity coefficient values is employed to estimate the activity of water and the activity coefficient of TBAB in TBAB aqueous solution. The optimal parameters of TBAB in the hydrate model were obtained minimizing the deviation of the calculated model results compared to the data of CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> + TBAB aqueous solution systems. The fitted parameters were

later used to predict the semiclathrate hydrate dissociation conditions of gas mixtures containing  $CO_2$ ,  $CH_4$ , and  $N_2$  in the presence of TBAB aqueous solution. The test model results indicate that the proposed model is adequate for engineering applications.

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#### Notes

The authors declare no competing financial interest.

#### ACKNOWLEDGMENTS

This study was supported by the National 973 Project of China (No. 2012CB215005).

#### NOMENCLATURE

A' =Antoine constants for calculating  $f_i^{H,0}(T)$  in eq 7

 $A_{ii}$  = cross interaction parameter

a = activity

B' =Antoine constants for calculating  $f_i^{H,0}(T)$  in eq 7

C =Langmuir constant

C' = Antoine constants for calculating  $f_i^{H,0}(T)$  in eq 7

f =fugacity of gas species and TBAB

 $f^0$  = fugacity of gas species and TBAB in equilibrium with the unfilled basic hydrate

S = species

P = pressure

T = temperature

w = weight fraction

X = Antoine constant for calculating Langmuir constant in eq. 10

x = mole fraction of basic hydrate

Y = Antoine constant for calculating Langmuir constant in eq

Z = Antoine constant for calculating Langmuir constant in eq 10

#### Greek letters

 $\alpha$  = structural parameter,  $\alpha = \lambda_1/\lambda_2$ 

 $\beta$  = structural parameter,  $\beta$  = 3.5 K/bar for type B TBAB hydrate and  $\beta$  = 2.8 K/bar for type A

 $\gamma$  = activity coefficient

 $\theta$  = fraction of the linked cavities occupied by guest molecules

 $\lambda_1$  = number of linked cavities per water molecule,  $\lambda_1$  = 6/78 for type B and  $\lambda_1$  = 6/52 for type A

 $\lambda_2$  = number of gas molecules per water molecule in basic hydrate,  $\lambda_2$  = 8/78 for type B and  $\lambda_2$  = 8/52 for type A

#### Subscripts

L = liquid

H = hydrate

G = gas

i = species i

j = species j, small gas components such as CH<sub>4</sub>, CO<sub>2</sub>, N<sub>2</sub> w = water

M = hydrate promoter TBAB

diss = dissociation

pred = prediction

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