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# Thermophysical and Thermodynamic Properties of 1-Butyl-3-methylimidazolium Tetrafluoroborate and 1-Butyl-3-methylimidazolium Hexafluorophosphate over an Extended Pressure Range

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The current study focuses on 1-butyl-3-methylimidazolium tetrafluoroborate, [bmim][BF<sub>4</sub>], and 1-butyl-3-methylimidazolium hexafluorophosphate, [bmim][PF<sub>6</sub>]. The objective is to study the influence of pressure as well as that of the anion on several properties of this type of ionic liquid. The speed of sound and densities in pure ionic liquids (ILs) as a function of temperature and pressure have been determined. Several other thermodynamic properties such as compressibilities, expansivities, and heat capacities have been obtained. To the best of our knowledge, this research comprises both the first speed of sound data and the first evaluation of heat capacities at high pressures for ILs. Speed of sound measurements have been carried out in broad ranges of temperature (283 < T/K < 323) and pressure (0.1 < p/MPa < 150), sometimes inside the metastable liquid region using a nonintrusive microcell. The T-P melting line of [bmim][PF<sub>6</sub>] has also been determined by an acoustic method. Density measurements have been performed for broad ranges of temperature (298 < T/K < 333) and pressure (0.1 < p/MPa < 60) using a vibrating tube densimeter. The pressure dependence of the heat capacities, which is generally mild, is found to be highly dependent on the curvature of the temperature dependence of the density.

### Introduction

Despite the fact that hexafluorophosphate,  $[PF_6]^-$ , and tetrafluoroborate,  $[BF_4]^-$ , based ILs can undergo hydrolysis producing HF in contact with water (mainly at high temperatures<sup>2</sup>), they are historically the most important and most commonly investigated. We have thus chosen these anions coupled with the much studied cation 1-butyl 3-methylimidazolium for our initial speed of sound studies.

Despite the increasing attention that room-temperature ionic liquids (RTILs) have recently received with respect to their thermophysical and thermodynamic properties, overall information is still scarce. Examples of very recent reviews and systematic studies can be found, for instance, in references 3–6 and references therein.

The speed of sound, u, is a property that can be experimentally determined with great precision over a broad range of temperature and pressure. Because u can be related to the first pressure partial derivative of density, accurate speed of sound data can be used to enhance the development of equations of state. Furthermore, it is a very useful source of information for computing values of other thermodynamic properties that are difficult to obtain at extreme experimental conditions, such as calorimetric data at high pressures. One possible method for deriving a wealth of thermodynamic properties consists of the measurement of the whole  $(p, \rho, T)$  and (p, u, T) surfaces to obtain by differentiation the derived properties of the

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investigated compound. This method has proven useful, for instance, in the calculation of derived properties of protonated and deuterated acetone. The Worden Properties of protonated as a more reliable method for deriving thermodynamic properties from speed of sound data is that which allows, by integration, the calculation of  $(p, \rho, T)$  and  $(p, C_p, T)$  surfaces from merely one isobar of both density and isobaric heat capacity. This method allows one to calculate other thermophysical properties such as isentropic  $(\kappa_S)$  and isothermal  $(\kappa_T)$  compressibilities, isobaric thermal expansivities  $(\alpha_p)$ , isobaric  $(C_p)$  and isochoric  $(C_v)$  heat capacities, and thermal pressure coefficients  $(\gamma_v)$  over the entire range of pressure of the speed of sound measurements. Whenever available, these values are compared with literature data obtained via other methods.

### **Experimental Section**

Acoustic Cell and Densimeter. Measurements of the speed of sound were performed in the temperature range of 283 < T/K < 323 and pressure range of 0.1 < P/MPa < 150. The speed of propagation of sound waves in liquids was determined using a nonintrusive method at an operational frequency of 0.5 MHz. We used the same experimental setup as previously described in great detail elsewhere. Pressure was measured using an Omega pressure transducer, which was calibrated against a high-accuracy Heise gauge. The pressure precision and accuracy are better than  $\pm 0.05\%$ . The acoustic cell was placed in a Hart Scientific calibration bath (stability  $\pm 0.001$  K), and temperature was measured by a four-wire platinum resistance thermometer (PRT) coupled to a Keithley digital multimeter (model DMM 199). The PRT was previously

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calibrated, thus allowing temperature measurements on the ITS-90 scale with an estimated uncertainty of better than  $\pm 0.01$  K. Typically, the uncertainty and repeatability of the speed of sound measurements are  $\pm 0.2\%$  and  $\pm 0.05\%$ , respectively. Likewise, densities were measured using an Anton Paar DMA 512P densimeter7 in the temperature range of 298 K to 333 K and the pressure range of 0.1 MPa to 60 MPa. The density overall uncertainty is estimated to be better than 0.02%. It should be noted that this value might increase slightly if one considers possible viscosity corrections. 13 These corrections rely on both the existence of viscosity data<sup>5</sup> and properly evaluated equations for the correlation between viscosity and signal damping. As for the first, to date there are no viscosity data for these ILs at pressures different from atmospheric. In the case of the latter, different corrections have been proposed<sup>13</sup> that basically depend on the instrument model and viscosity range. These issues are still under debate. In light of the above-mentioned caveats, we have not performed any viscosity corrections. Therefore, all of the results of the subsequent derived properties and their discussion are based on raw density data. Nonetheless, at atmospheric pressure, one should expect a downward density shift in the low-temperature range between 0.05% and 0.06% and 0.03% and 0.04% for [bmim][PF<sub>6</sub>] and [bmim][BF<sub>4</sub>], respectively, decreasing to about 0.02% for both ILs in the high-temperature range.

*Chemicals.* [bmim][PF<sub>6</sub>] was synthesized and purified at the QUILL Centre, Belfast, according to procedures found elsewhere. 14,15 It was washed several times with water to decrease the chloride content. It was determined that no precipitation (of AgCl) occurred by the addition of AgNO<sub>3</sub> to the wash water. [bmim][BF<sub>4</sub>] was purchased from Solvent Innovation (stated purity > 98%). The Cl<sup>-</sup> content, measured with a Cl<sup>-</sup>-specific electrode using the standard addition method, was 20 ppm and 100 ppm for [bmim][PF<sub>6</sub>] and [bmim][BF<sub>4</sub>], respectively. To reduce the water content and volatile compounds to negligible values, vacuum (0.1 Pa) and moderate temperature (60 °C) were applied to the [bmim][PF<sub>6</sub>] and [bmim][BF<sub>4</sub>] samples for several days always immediately prior to their use. The samples were analyzed by Karl Fisher titration and showed a mass % of water lower than 75 ppm ("Crison" Karl Fischer titration) and (70 ± 10) ppm (coulometric "Aquapal" Karl Fischer) for both [bmim][PF<sub>6</sub>] and [bmim][BF<sub>4</sub>].

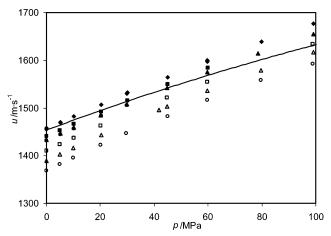
### **Results and Discussion**

**[bmim]**[**PF**<sub>6</sub>]. Speed of sound measurements have been carried out in a broad range of temperature (283 < T/K < 323) and pressure (0.1 < p/MPa < 150), sometimes inside the metastable, supercooled liquid region. Figure 1 and Table 1 report the speed of sound behavior as pressure and temperature change for [bmim][PF<sub>6</sub>]. For the sake of economy, data are presented at nominal temperatures that typically differ from the actual ones by no more than 0.01 K.

Original data have been fitted to a Pade 3  $\times$  3 equation of the form

$$(u/\text{m}\cdot\text{s}^{-1}) = \frac{\sum_{i=0}^{2} \sum_{j=0}^{2} a_{ij} (T/\text{K})^{i} (p/\text{MPa})^{j}}{\sum_{k=0}^{2} \sum_{l=0}^{2} b_{kl} (T/\text{K})^{k} (p/\text{MPa})^{l}}$$
(1)

The values of the coefficients were calculated by means of a least-squares analysis of the experimental results



**Figure 1.** Isotherms of the experimental speed of sound of [bmim]-[PF<sub>6</sub>]. The line represents the border between the stable and metastable, supercooled liquid. (See the text.) ◆, 283.16 K; ■, 291.15 K;  $\blacktriangle$ , 293.16 K;  $\Box$ , 303.16 K;  $\triangle$ , 313.16 K;  $\bigcirc$ , 323.15 K.

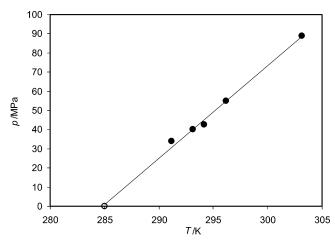
Table 1. Experimental Speed of Sound, u, Data for  $[bmim][PF_6]$  as a Function of Temperature, T, and Pressure, p

	P				
p/MPa	$u/\mathrm{m}\cdot\mathrm{s}^{-1}$	p/MPa	$u/\mathrm{m}\cdot\mathrm{s}^{-1}$	p/MPa	$u/\mathrm{m}\cdot\mathrm{s}^{-1}$
T = 28	3.16 K	T=29	93.16 K	98.921	1634.38
0.100	1455.52	0.100	1432.85		
0.100	1457.60	5.157	1446.45	T = 31	$3.16 \; { m K}$
5.088	1468.58	10.195	1459.01	0.100	1389.49
5.131	1470.64	20.215	1484.18	5.010	1402.83
10.263	1481.79	29.959	1507.92	10.043	1416.43
20.249	1506.72	44.757	1542.20	20.319	1443.30
29.954	1529.87	59.732	1574.70	41.702	1495.14
29.995	1532.46	78.627	1613.77	44.866	1502.87
44.961	1564.25	99.149	1654.46	59.754	1536.27
59.682	1596.68			79.721	1578.64
59.829	1599.61	T=29	94.16 K	99.097	1617.38
79.904	1638.64	0.100	1431.59	125.283	1662.16
99.077	1677.06	5.125	1444.54		
124.179	1724.36	10.105	1457.17	T = 32	$3.25~\mathrm{K}$
150.925	1772.61	20.357	1483.23	0.100	1367.98
		29.785	1506.04	5.061	1381.82
T = 29	1.15 K			9.942	1395.37
0.100	1440.19	T=30	03.16 K	20.234	1422.72
5.069	1453.26	0.100	1410.27	29.721	1446.75
10.166	1466.63	5.078	1423.48	44.935	1482.19
20.400	1492.36	10.204	1437.13	59.711	1515.95
30.019	1515.72	20.225	1462.82	79.553	1557.89
44.920	1549.95	44.714	1521.26	98.901	1592.52
59.912	1583.22	59.773	1554.58		

Table 2. Coefficients of Equation 1 for T/K, p/MPa, and  $u/m \cdot s^{-1}$  within the Interval (283 < T/K < 323, 0.1 < p/MPa < 100)

$a_{ij}$		j	
i	0	1	2
0 1 2	$\begin{array}{c} -2.98041 \times 10^{4} \\ -5.78316 \\ 4.03798 \times 10^{-1} \end{array}$	$\begin{array}{c} 6.35774 \times 10^{1} \\ 8.03545 \times 10^{-1} \\ -3.61889 \times 10^{-3} \end{array}$	$\begin{array}{c} -1.53934 \times 10^{-1} \\ 9.68016 \times 10^{-3} \\ -3.23951 \times 10^{-5} \end{array}$
$b_{kl}$		L	
$\overline{k}$	0	1	2
$\begin{matrix} 0 \\ 1 \\ 2 \end{matrix}$	$\begin{array}{c} 1.00000 \\ -1.56369 \times 10^{-1} \\ 5.47760 \times 10^{-4} \end{array}$	$\begin{array}{c} -1.66204\times 10^{-1} \\ 2.30593\times 10^{-3} \\ -6.07700\times 10^{-6} \end{array}$	$\begin{array}{c} 2.51840 \times 10^{-5} \\ 3.04219 \times 10^{-6} \\ -1.11069 \times 10^{-8} \end{array}$

(using the algorithm of Marquardt–Levenberg) and are given in Table 2. The standard deviation between the experimental and fitted values is found to be 0.07%. This fitting equation was screened for 40 isotherms within the experimental temperature range (283 < T/K < 323), thus in steps of 1 K, and for steps of 0.1 MPa within the



**Figure 2.** Melting line of [bmim][PF<sub>6</sub>]. ●, Acoustic determinations. O, Visual determination.

Table 3. T-p Melting-Line Data of [bmim][PF<sub>6</sub>]

T/K	p/MPa
285.00	0.1
291.15	34.0
293.15	40.2
294.16	42.5
296.15	55.0
303.15	88.9

experimental interval of pressure  $(0.1 \le p/\text{MPa} \le 100)$  for a total of 41 000 data points. No poles for this rational function were found. Also, neither the temperature nor the pressure derivatives of u(p,T) as described by eq 1 present any anomalies. Therefore, eq 1 can be safely used for interpolations. It is already well known that ILs are relatively easy to metastabilize, meaning that, on cooling, they may remain liquid below their equilibrium melting line (supercooling). A liquid is said to be supercooled when it is found as such either at temperatures lower than those of the melting line or at pressures above it (for positively sloped melting lines). In the case of [bmim][PF<sub>6</sub>], we have witnessed solidification several times in our isothermal runs intended to determine the speed of sound as a function of pressure. Because a crystalline phase cannot be superheated,16 whenever solidification occurred we decided to lower the pressure slowly until the liquid state was again restored. Thus, we were able to detect several points of the melting line of [bmim][PF<sub>6</sub>], since the difference between the speed of sound in this IL between the two states (solid versus liquid) is significant ( $u_{\rm sol}-u_{\rm liq}\approx 1000~{\rm ms^{-1}}$ ). Figure 2 and Table 3 present the solid/liquid phase transition line. Within the experimental uncertainty ( $\pm 0.1 \text{ K}$ ,  $\pm 10 \text{ bar}$ ), the p-T melting line shows linear behavior between coordinates (285.0 K, 0.1 MPa) and (303.15 K, 89.6 MPa), evolving with a slope of  $dp/dT = 4.87 \text{ MPa} \cdot \text{K}^{-1}$ . The first coordinate corresponds to our visual determination of melting at atmospheric pressure obtained in a sealed glass vessel by multiple cycles of slow temperature change. It agrees reasonably well with two values (283.15 K<sup>17</sup> and  $283.51 \text{ K}^{18}$ ) reported, but not with the one (276.43 K<sup>19</sup>) for water-free [bmim][PF<sub>6</sub>]. It disagrees with that reported (277.15 K<sup>17</sup>) for water-equilibrated [bmim][PF<sub>6</sub>]. The Clayperon equation can now be used to calculate the volume change on melting provided that one knows the corresponding enthalpy change. We note that literature values do not agree. Although Magee et al. 18 report a value of 19.6 kJ mol<sup>-1</sup>, Domanska and Marciniak<sup>19</sup> determined a value of 9.21 kJ mol<sup>-1</sup>. In our calculations, we have chosen the first value because their melting temperature agrees

Table 4. Coefficients of Second-Order Polynomial Fits, Y  $=A+B(T/K)+C(T/K)^2$ , to Atmospheric Isobars of  $Y=\rho$ or  $Y = C_p$ 

	$ ho/\mathrm{kg}\cdot\mathrm{m}^{-3}$	$C_p/\mathrm{J} ext{-}\mathrm{K}^{-1} ext{-}\mathrm{kg}^{-1}$
$\overline{A}$	1620.7039	-1641.9284
B	-0.87955633	17.750623
C	$8.4814007  imes 10^{-5}$	$-2.4889525  imes 10^{-2}$

reasonably well with ours. Solidification in [bmim][PF<sub>6</sub>] is accompanied by a contraction of about 7% ( $\Delta V_S = -14.1$ cm<sup>3</sup>·mol<sup>-1</sup>). This value is highly dependent on the standardization of the enthalpy of fusion.

The use of the speed of sound data to derive other thermodynamic properties requires a knowledge of one isobar of both density and heat capacity. There are already two sets of data available from different groups. 4,18,20 The choice of the isobars for the thermodynamic properties calculations was based on the comparison of both density and isobaric heat capacity data. The values presented by Magee et al. 18 seem more precise and are greater than those of Gu et al.<sup>20</sup> and Fredlake et al.<sup>4</sup> for both quantities (which may possibly be an indication of higher sample purity because it is quite uncommon to find typical impurities that are responsible for the increase in these properties). However, despite the fact that, in turn, these densities<sup>18</sup> are slightly lower than those presented by us<sup>3,21</sup> (for about 0.1%) and by Tokuda et al.<sup>5</sup> (for about 0.35%), that is the best set of combined data of densities and heat capacities along one isobar.

The atmospheric isobars of both density and heat capacity<sup>18</sup> were fitted with a second-order polynomial equation up to 330 K. The coefficients of the fittings are shown in Table 4. The method used to derive other thermodynamic properties is based on well-established thermodynamic relations. The speed of sound, u, is directly related to the pressure derivative of the density,  $\rho$ , through eq 2, in which the subscript S denotes the condition of constant entropy.

$$\left(\frac{\partial \rho}{\partial p}\right)_S = \frac{1}{u^2} \tag{2}$$

This derivative is related to the isothermal pressure derivative and the isobaric temperature derivative of the density through eq 3, where  $C_p$  is the specific heat capacity at constant pressure.

$$\left(\frac{\partial \rho}{\partial p}\right)_{S} = \left(\frac{\partial \rho}{\partial p}\right)_{T} - \frac{T}{\rho^{2}C_{p}} \left(\frac{\partial \rho}{\partial T}\right)_{p}^{2} \tag{3}$$

Rearranging the last equation and combining it with eq 2 creates eq 4, which also incorporates the definition of the thermal expansion coefficient,  $\alpha_p$ :

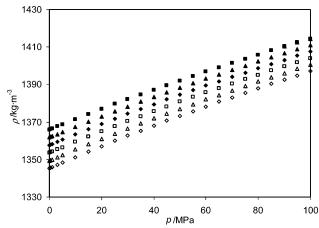
$$\left(\frac{\partial \rho}{\partial p}\right)_T = \frac{1}{\mu^2} + \frac{T}{C_p} \alpha_p^2 \tag{4}$$

$$\alpha_p = -\frac{1}{\rho} \left( \frac{\partial \rho}{\partial T} \right)_p \tag{5}$$

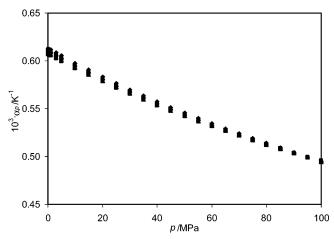
It can also be shown that the isothermal pressure partial derivative of the isobaric heat capacity can be calculated with eq 6:

$$\left(\frac{\partial C_p}{\partial p}\right)_T = -\frac{T}{\rho} \left[\alpha_p^2 + \left(\frac{\partial \alpha_p}{\partial T}\right)_p\right] \tag{6}$$

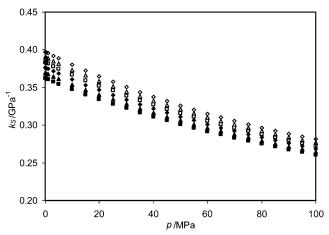
Thus, given an isobar of the density and of  $C_p$ , it is possible to integrate eqs 4 and 6 over pressure, 22 thus obtaining the  $(p, \rho, T)$  and  $(p, C_p, T)$  surfaces within the



**Figure 3.** Isotherms for the density of [bmim][PF<sub>6</sub>]. ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\spadesuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

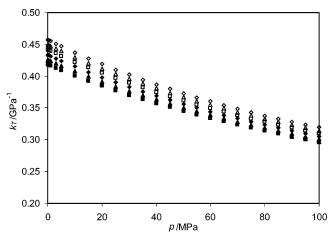


**Figure 4.** Isotherms for the isobaric expansivity of [bmim] [PF<sub>6</sub>]. ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

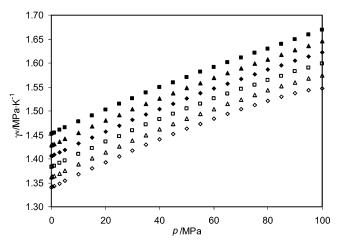


**Figure 5.** Isotherms for the isentropic compressibility of [bmim]- $[PF_6]$ . ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

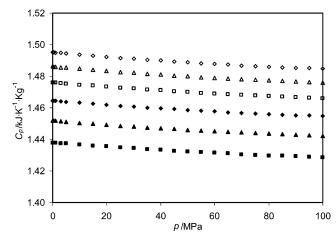
range of pressure and temperature of the experimental speed of sound data. The numerical integration procedure also allows one to calculate other properties, such as the isentropic compressibility,  $\kappa_S$ , isothermal compressibility,  $\kappa_T$ , isobaric thermal expansivity,  $\alpha_p$ , isochoric heat capacity  $C_v$ , and thermal pressure coefficient,  $\gamma_v$ . The estimated overall uncertainties (including sample impurities) are as follows: isentropic compressibility,  $\kappa_S$  (1%); isothermal compressibility,  $\kappa_T$  (2%); isobaric thermal expansivity,  $\alpha_p$ 



**Figure 6.** Isotherms for the isothermal compressibility of [bmim]- $[PF_6]$ . ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.



**Figure 7.** Isotherms for the thermal pressure coefficient of [bmim]- $[PF_6]$ . ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\spadesuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.



**Figure 8.** Isotherms for the isobaric heat capacity of [bmim] [PF<sub>6</sub>]. ■, 298.15 K; ▲, 303.15 K; ◆, 308.15 K; □, 313.15 K; △, 318.15 K; ◇, 323.15 K.

(4%); isobaric heat capacity,  $C_p$  (5%); isochoric heat capacity,  $C_v$  (8%); and thermal pressure coefficient,  $\gamma_v$  (6%). It should be noted that in the case of heat capacities the major contribution to the uncertainty lies in that of the original calorimetric data. The integration was carried out from atmospheric pressure up to 100 MPa. The results obtained for several thermodynamic properties are presented in Figures 3 to 9 and Tables 5 to 11.

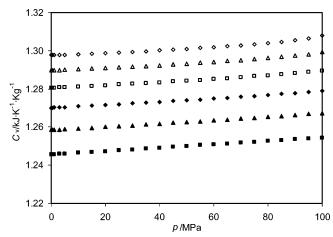


Figure 9. Isotherms for the isochoric heat capacity of [bmim]- $[PF_6]$ .  $\blacksquare$ , 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\square$ , 313.15 K;  $\triangle$ , 318.15 K; ♦, 323.15 K.

The isothermal compressibility results can be compared with those of Gu et al.20 showing deviations that go from

-1% at atmospheric pressure to +12% at 100 MPa and 298.2 K and from -9% to +13% at 323.2 K.

As for the heat capacities, results for both the isobaric and isochoric heat capacities reveal, in practice, pressure independence.

Although expansivities decrease markedly with pressure, according to Figure 4 and Table 8 they present a tendency to increase very mildly with increasing temperature at constant pressure. This trend agrees with that reported by Tokuda et al.<sup>5</sup> at atmospheric pressure. Nonetheless, within the typical experimental uncertainty of  $\alpha_n$  calculations (4%) the expansivities of [bmim][PF<sub>6</sub>] can, in practice, be considered almost temperature-independent. This behavior contradicts that which has been reported in other works<sup>18,20</sup> in which  $\alpha_p$  of [bmim][PF<sub>6</sub>] decreases as temperature rises. This contradiction underlies numerical difficulties in the data evaluation associated with very subtle effects and was previously noticed in different communications  $^{3,6,23}$ . The point is that a detailed evaluation of the raw data reveals that deviations from linearity in densitytemperature (or volume-temperature) plots are so mild that the determination of the temperature coefficient of  $\alpha_p$ 

Table 5. Calculated Values of Density,  $\rho$ , for [bmim][PF<sub>6</sub>]

	T/K									T	/K			
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	
$ ho$ /kg·m $^{-3}$								ρ/kg•m <sup>-3</sup>						
0.1	$1366.0_{0}$	$1361.8_{6}$	$1357.7_{2}$	$1353.5_{9}$	$1349.4_{6}$	$1345.3_{3}$	45	$1389.6_{4}$	$1385.8_{4}$	$1382.0_{4}$	$1378.2_{5}$	$1374.4_{6}$	$1370.6_{8}$	
0.5	$1366.2_{3}$	$1362.0_{9}$	$1357.9_{6}$	$1353.8_{3}$	$1349.7_{0}$	$1345.5_{8}$	50	$1392.0_{6}$	$1388.2_{9}$	$1384.5_{3}$	$1380.7_{7}$	$1377.0_{1}$	$1373.2_{6}$	
1	$1366.5_2$	$1362.3_{8}$	$1358.2_5$	$1354.1_2$	$1350.0_{0}$	$1345.8_{8}$	55	$1394.4_{5}$	$1390.7_1$	$1386.9_7$	$1383.2_5$	$1379.5_2$	$1375.8_{1}$	
3	$1367.6_{5}$	$1363.5_{3}$	$1359.4_2$	$1355.3_1$	$1351.2_{1}$	$1347.1_{1}$	60	$1396.8_{0}$	$1393.0_9$	$1389.3_{8}$	$1385.6_{9}$	$1381.9_9$	$1378.3_{1}$	
5	$1368.7_7$	$1364.6_{7}$	$1360.5_{8}$	$1356.4_{9}$	$1352.4_0$	$1348.3_2$	65	$1399.1_{1}$	$1395.4_{3}$	$1391.7_{6}$	$1388.0_9$	$1384.4_{3}$	$1380.7_7$	
10	$1371.5_{5}$	$1367.4_{9}$	$1363.4_{3}$	$1359.3_{9}$	$1355.3_{4}$	$1351.3_{0}$	70	$1401.4_{0}$	$1397.7_{4}$	$1394.1_{0}$	$1390.4_{6}$	$1386.8_{3}$	$1383.2_{0}$	
15	$1374.2_{7}$	$1370.2_{5}$	$1366.2_{4}$	$1362.2_{3}$	$1358.2_2$	$1354.2_2$	75	$1403.6_{5}$	$1400.0_{3}$	$1396.4_{1}$	$1392.8_{0}$	$1389.1_{9}$	$1385.5_{9}$	
20	$1376.9_{4}$	$1372.9_{6}$	$1368.9_9$	$1365.0_2$	$1361.0_{5}$	$1357.0_{9}$	80	$1405.8_{7}$	$1402.2_{8}$	$1398.6_{9}$	$1395.1_{0}$	$1391.5_2$	$1387.9_{5}$	
25	$1379.5_{7}$	$1375.6_{3}$	$1371.6_{9}$	$1367.7_{6}$	$1363.8_{3}$	$1359.9_{1}$	85	$1408.0_{7}$	$1404.5_0$	$1400.9_3$	$1397.3_{8}$	$1393.8_3$	$1390.2_{8}$	
30	$1382.1_{5}$	$1378.2_{4}$	$1374.3_{4}$	$1370.4_{5}$	$1366.5_{6}$	$1362.6_{7}$	90	$1410.2_{3}$	$1406.6_{9}$	$1403.1_{5}$	$1399.6_{2}$	$1396.1_0$	$1392.5_{8}$	
35	$1384.6_{9}$	$1380.8_{2}$	$1376.9_{5}$	$1373.0_{9}$	$1369.2_{4}$	$1365.3_{9}$	95	$1412.3_{7}$	$1408.8_{5}$	$1405.3_{4}$	$1401.8_{3}^{-}$	$1398.3_{4}$	$1394.8_{5}$	
40	$1387.1_{8}$	$1383.3_{5}$	$1379.5_{2}$	$1375.6_{9}$	$1371.8_{7}$	$1368.0_{6}$	100	$1414.4_{9}$	$1410.9_{9}$	$1407.5_{0}$	$1404.0_{2}$	$1400.5_{5}$	$1397.1_{0}$	

Table 6. Calculated Values of  $\kappa_T$  for [bmim][PF<sub>6</sub>]

								T/K					
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			κ <sub>T</sub> /G	Pa <sup>-1</sup>						κ <sub>T</sub> /G	$Pa^{-1}$		
0.1	$0.417_{9}$	$0.425_{6}$	$0.433_{5}$	$0.441_{4}$	$0.449_{3}$	$0.457_{3}$	45	$0.351_{0}$	$0.356_{7}$	$0.362_{4}$	$0.368_{1}$	$0.374_{0}$	$0.379_{8}$
0.5	$0.417_{1}$	$0.424_{9}$	$0.432_{7}$	$0.440_{6}$	$0.448_{5}$	$0.456_{4}$	50	$0.345_{1}$	$0.350_{6}$	$0.356_{1}$	$0.361_{7}$	$0.367_{3}$	$0.373_{0}$
1	$0.416_{2}$	$0.423_{9}$	$0.431_{7}$	$0.439_{6}$	$0.447_{4}$	$0.455_{4}$	55	$0.339_{5}$	$0.344_{8}$	$0.350_{1}$	$0.355_{5}$	$0.361_{0}$	$0.366_{5}$
3	$0.412_{6}$	$0.420_{2}$	$0.427_{9}$	$0.435_{6}$	$0.443_{4}$	$0.451_{2}$	60	$0.334_{0}$	$0.339_{1}$	$0.344_{3}$	$0.349_{6}$	$0.354_{9}$	$0.360_{3}$
5	$0.409_{1}^{\circ}$	$0.416_{6}^{-}$	$0.424_{1}$	$0.431_{7}$	$0.439_{4}$	$0.447_{1}^{-}$	65	$0.328_{8}$	$0.333_{8}$	$0.338_{8}$	$0.343_{9}$	$0.349_{1}$	$0.354_{3}$
10	$0.400_{6}$	$0.407_{8}$	$0.415_{1}$	$0.422_{4}$	$0.429_{7}$	$0.437_{2}$	70	$0.323_{7}$	$0.328_{6}$	$0.333_{5}$	$0.338_{4}$	$0.343_{5}$	$0.348_{6}$
15	$0.392_{5}$	$0.399_{4}$	$0.406_{4}$	$0.413_{5}$	$0.420_{6}$	$0.427_{7}$	75	$0.318_{9}$	$0.323_{6}$	$0.328_{4}$	$0.333_{2}$	$0.338_{1}$	$0.343_{1}$
20	$0.384_{8}$	$0.391_{5}$	$0.398_{2}$	$0.405_{0}$	$0.411_{9}$	$0.418_{8}$	80	$0.314_{2}$	$0.318_{8}$	$0.323_{4}$	$0.328_{1}$	$0.332_{9}$	$0.337_{8}$
25	$0.377_{4}$	$0.383_{9}$	$0.390_{4}$	$0.397_{0}$	$0.403_{6}$	$0.410_{2}$	85	$0.309_{7}$	$0.314_{1}$	$0.318_{6}$	$0.323_{2}$	$0.327_{9}$	$0.332_{8}$
30	$0.370_{3}$	$0.376_{6}$	$0.382_{9}$	$0.389_{3}$	$0.395_{7}$	$0.402_{1}$	90	$0.305_{4}$	$0.309_{7}$	$0.314_{0}$	$0.318_{5}$	$0.323_{2}$	$0.328_{0}$
35	$0.363_{6}$	$0.369_{7}$	$0.375_{8}$	$0.381_{9}$	$0.388_{1}$	$0.394_{3}$	95	$0.301_{1}$	$0.305_{3}$	$0.309_{5}$	$0.313_{9}$	$0.318_{6}$	$0.323_{5}$
40	$0.357_{2}$	$0.363_{0}$	$0.368_{9}$	$0.374_{9}$	$0.380_{9}$	$0.386_{9}$	100	$0.297_{1}$	$0.301_{0}$	$0.305_{1}$	$0.309_{5}$	$0.314_{2}$	$0.319_{5}$

Table 7. Calculated Values of  $\kappa_S$  for [bmim][PF<sub>6</sub>]

										T/	K		
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$\kappa_S/G$	Pa⁻¹						$\kappa_S/G$	Pa⁻¹		
0.1	$0.362_{0}$	$0.368_{9}$	$0.375_{9}$	$0.382_{9}$	$0.389_{9}$	$0.396_{9}$	45	$0.306_{1}$	$0.311_{2}$	$0.316_{3}$	$0.321_{4}$	$0.326_{5}$	$0.331_{7}$
0.5	$0.361_{3}$	$0.368_{3}$	$0.375_{3}$	$0.382_{3}$	$0.389_{2}$	$0.396_{2}$	50	$0.301_{2}$	$0.306_{1}$	$0.311_{1}$	$0.316_{0}$	$0.321_{0}$	$0.326_{0}$
1	$0.360_{6}$	$0.367_{5}$	$0.374_{5}$	$0.381_{4}$	$0.388_{4}$	$0.395_{3}$	55	$0.296_{4}$	$0.301_{2}$	$0.306_{0}$	$0.310_{8}$	$0.315_{7}$	$0.320_{5}$
3	$0.357_{6}$	$0.364_{4}$	$0.371_{3}$	$0.378_{1}$	$0.384_{9}$	$0.391_{8}$	60	$0.291_{9}$	$0.296_{5}$	$0.301_{2}$	$0.305_{9}$	$0.310_{6}$	$0.315_{3}$
5	$0.354_{6}$	$0.361_{4}$	$0.368_{1}$	$0.374_{8}$	$0.381_{6}$	$0.388_{3}$	65	$0.287_{5}$	$0.292_{0}$	$0.296_{5}$	$0.301_{1}$	$0.305_{7}$	$0.310_{3}$
10	$0.347_{5}$	$0.354_{0}$	$0.360_{5}$	$0.367_{0}$	$0.373_{5}$	$0.379_{9}$	70	$0.283_{3}$	$0.287_{7}$	$0.292_{1}$	$0.296_{5}$	$0.301_{0}$	$0.305_{5}$
15	$0.340_{8}$	$0.347_{0}$	$0.353_{3}$	$0.359_{5}$	$0.365_{8}$	$0.372_{0}$	75	$0.279_{2}$	$0.283_{5}$	$0.287_{8}$	$0.292_{1}$	$0.296_{4}$	$0.300_{9}$
20	$0.334_{3}$	$0.340_{3}$	$0.346_{4}$	$0.352_{4}$	$0.358_{4}$	$0.364_{5}$	80	$0.275_{3}$	$0.279_{4}$	$0.283_{6}$	$0.287_{8}$	$0.292_{1}$	$0.296_{5}$
25	$0.328_{2}$	$0.334_{0}$	$0.339_{8}$	$0.345_{6}$	$0.351_{5}$	$0.357_{3}$	85	$0.271_{5}$	$0.275_{5}$	$0.279_{6}$	$0.283_{7}$	$0.287_{9}$	$0.292_{2}$
30	$0.322_{3}$	$0.327_{9}$	$0.333_{5}$	$0.339_{2}$	$0.344_{8}$	$0.350_{4}$	90	$0.267_{9}$	$0.271_{8}$	$0.275_{7}$	$0.279_{8}$	$0.283_{9}$	$0.288_{3}$
35	$0.316_{7}$	$0.322_{1}$	$0.327_{5}$	$0.333_{0}$	$0.338_{4}$	$0.343_{9}$	95	$0.264_{3}$	$0.268_{1}$	$0.272_{0}$	$0.275_{9}$	$0.280_{1}$	$0.284_{6}$
40	$0.311_{3}$	$0.316_{5}$	$0.321_{8}$	$0.327_{1}$	$0.332_{4}$	$0.337_{6}$	100	$0.260_{8}$	$0.264_{5}$	$0.268_{2}$	$0.272_{2}$	$0.276_{6}$	$0.281_{5}$

Table 8. Calculated Values of  $\alpha_p$  for [bmim][PF<sub>6</sub>]

			T	′K									
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$10^3 \alpha_i$	$_{o}/{ m K}^{-1}$						$10^3\alpha$	$_{ m o}/{ m K}^{-1}$		
0.1	$0.606_{9}$	$0.608_{1}$	$0.609_{3}$	$0.610_{6}$	$0.611_{8}$	$0.613_{0}$	45	$0.547_{5}$	$0.548_{3}$	$0.549_{1}$	$0.549_{9}$	$0.550_{7}$	$0.551_{5}$
0.5	$0.606_{3}$	$0.607_{5}$	$0.608_{7}$	$0.609_{9}$	$0.611_{2}$	$0.612_{4}$	50	$0.542_{0}$	$0.542_{7}$	$0.543_{5}$	$0.544_{2}$	$0.544_{9}$	$0.545_{7}$
1	$0.605_{5}$	$0.606_{7}$	$0.607_{9}$	$0.609_{1}$	$0.610_{4}$	$0.611_{6}$	55	$0.536_{6}$	$0.537_{3}$	$0.538_{0}$	$0.538_{7}$	$0.539_{3}$	$0.540_{0}$
3	$0.602_{4}$	$0.603_{6}$	$0.604_{8}$	$0.606_{0}$	$0.607_{2}$	$0.608_{4}$	60	$0.531_{5}$	$0.532_{1}$	$0.532_{7}$	$0.533_{3}$	$0.533_{9}$	$0.534_{5}$
5	$0.599_{4}$	$0.600_{6}$	$0.601_{8}$	$0.602_{9}$	$0.604_{1}$	$0.605_{3}$	65	$0.526_{4}$	$0.527_{0}$	$0.527_{5}$	$0.528_{1}$	$0.528_{6}$	$0.529_{2}$
10	$0.592_{1}$	$0.593_{2}$	$0.594_{3}$	$0.595_{5}$	$0.596_{6}$	$0.597_{8}$	70	$0.521_{6}$	$0.522_{0}$	$0.522_{5}$	$0.523_{0}$	$0.523_{5}$	$0.524_{0}$
15	$0.585_{0}$	$0.586_{1}$	$0.587_{2}$	$0.588_{3}$	$0.589_{4}$	$0.590_{4}$	75	$0.516_{8}$	$0.517_{2}$	$0.517_{7}$	$0.518_{1}$	$0.518_{5}$	$0.518_{9}$
20	$0.578_{2}$	$0.579_{2}$	$0.580_{3}$	$0.581_{3}$	$0.582_{3}$	$0.583_{4}$	80	$0.512_{3}$	$0.512_{6}$	$0.512_{9}$	$0.513_{3}$	$0.513_{6}$	$0.513_{9}$
25	$0.571_{6}$	$0.572_{6}$	$0.573_{6}$	$0.574_{6}$	$0.575_{6}$	$0.576_{6}$	85	$0.507_{8}$	$0.508_{1}$	$0.508_{3}$	$0.508_{6}$	$0.508_{8}$	$0.509_{0}$
30	$0.565_{3}$	$0.566_{2}$	$0.567_{2}$	$0.568_{1}$	$0.569_{1}$	$0.570_{0}$	90	$0.503_{6}$	$0.503_{7}$	$0.503_{8}$	$0.503_{9}$	$0.504_{1}$	$0.504_{2}$
35	$0.559_{2}$	$0.560_{1}$	$0.561_{0}$	$0.561_{8}$	$0.562_{7}$	$0.563_{6}$	95	$0.499_{5}$	$0.499_{5}$	$0.499_{4}$	$0.499_{4}$	$0.499_{3}$	$0.499_{3}$
40	$0.553_{3}^{-}$	$0.554_{1}$	$0.554_{9}$	$0.555_{8}$	$0.556_{6}$	$0.557_{4}$	100	$0.495_{7}$	$0.495_{4}$	$0.495_{1}$	$0.494_{8}$	$0.494_{5}$	$0.494_{3}$

Table 9. Calculated Values of  $\gamma_v$  for [bmim][PF<sub>6</sub>]

	T/K												
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$\gamma_v/\mathrm{MF}$	Pa•K <sup>−1</sup>						$\gamma_v/MF$	Pa•K <sup>−1</sup>		
0.1	$1.45_{2}$	$1.42_{9}$	$1.40_{6}$	$1.38_{3}$	$1.36_{2}$	$1.34_{1}$	45	$1.56_{0}$	$1.53_{7}$	$1.51_{5}$	$1.49_{4}$	$1.47_{3}$	$1.45_{2}$
0.5	$1.45_{3}$	$1.43_{0}$	$1.40_{7}$	$1.38_{4}$	$1.36_{3}$	$1.34_{2}$	50	$1.57_{0}$	$1.54_{8}$	$1.52_{6}$	$1.50_{5}$	$1.48_{3}$	$1.46_{3}$
1	$1.45_{5}$	$1.43_{1}$	$1.40_{8}$	$1.38_{6}$	$1.36_{4}$	$1.34_{3}$	55	$1.58_{1}$	$1.55_{9}$	$1.53_{7}$	$1.51_{5}$	$1.49_{4}$	$1.47_{3}$
3	$1.46_{0}$	$1.43_{6}$	$1.41_{3}$	$1.39_{1}$	$1.37_{0}$	$1.34_{9}$	60	$1.59_{1}$	$1.56_{9}$	$1.54_{7}$	$1.52_{5}$	$1.50_{4}$	$1.48_{4}$
5	$1.46_{5}$	$1.44_{2}$	$1.41_{9}$	$1.39_{7}$	$1.37_{5}$	$1.35_{4}$	65	$1.60_{1}$	$1.57_{9}$	$1.55_{7}$	$1.53_{5}$	$1.51_{4}$	$1.49_{3}$
10	$1.47_{8}$	$1.45_{5}$	$1.43_{2}$	$1.41_{0}$	$1.38_{8}$	$1.36_{7}$	70	$1.61_{1}$	$1.58_{9}$	$1.56_{7}$	$1.54_{5}$	$1.52_{4}$	$1.50_{3}$
15	$1.49_{1}$	$1.46_{7}$	$1.44_{5}$	$1.42_{3}$	$1.40_{1}$	$1.38_{0}$	75	$1.62_{1}$	$1.59_{8}$	$1.57_{7}$	$1.55_{5}$	$1.53_{4}$	$1.51_{2}$
20	$1.50_{3}$	$1.48_{0}$	$1.45_{7}$	$1.43_{5}$	$1.41_{4}$	$1.39_{3}$	80	$1.63_{0}$	$1.60_{8}$	$1.58_{6}$	$1.56_{4}$	$1.54_{3}$	$1.52_{1}$
25	$1.51_{5}$	$1.49_{2}$	$1.46_{9}$	$1.44_{8}$	$1.42_{6}$	$1.40_{5}$	85	$1.64_{0}$	$1.61_{7}$	$1.59_{5}$	$1.57_{3}$	$1.55_{1}$	$1.53_{0}$
30	$1.52_{6}$	$1.50_{4}$	$1.48_{1}$	$1.45_{9}$	$1.43_{8}$	$1.41_{8}$	90	$1.64_{9}$	$1.62_{7}$	$1.60_{4}$	$1.58_{2}$	$1.56_{0}$	$1.53_{7}$
35	$1.53_{8}$	$1.51_{5}$	$1.49_{3}$	$1.47_{1}$	$1.45_{0}$	$1.42_{9}$	95	$1.65_{9}$	$1.63_{6}$	$1.61_{3}$	$1.59_{1}$	$1.56_{8}$	$1.54_{4}$
40	$1.54_{9}$	$1.52_{6}$	$1.50_{4}$	$1.48_{3}$	$1.46_{1}$	$1.44_{1}$	100	$1.66_{9}$	$1.64_{6}$	$1.62_{3}$	$1.59_{9}$	$1.57_{4}$	$1.54_{7}$

Table 10. Calculated Values of  $C_p$  for [bmim][PF<sub>6</sub>]

			T	/K									
$p/\mathrm{MPa}$	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$C_{p}/\mathrm{kJ}\cdot\mathrm{K}$	K <sup>-1</sup> •kg <sup>-1</sup>						$C_{p}/\mathrm{kJ}\cdot\mathrm{k}$	K <sup>-1</sup> •kg <sup>-1</sup>		
0.1	$1.43_{8}$	$1.45_{2}$	$1.46_{5}$	$1.\overline{47}_{6}$	$1.48_{6}$	$1.49_{5}$	45	$1.43_{3}$	$1.44_{7}$	$1.45_{9}$	$1.\overline{47}_{0}$	$1.48_{0}$	$1.48_{9}$
0.5	$1.43_{8}$	$1.45_{2}$	$1.46_{4}$	$1.47_{6}$	$1.48_{6}$	$1.49_{5}$	50	$1.43_{2}$	$1.44_{6}$	$1.45_{9}$	$1.47_{0}$	$1.48_{0}$	$1.48_{9}$
1	$1.43_{8}$	$1.45_{2}$	$1.46_{4}$	$1.47_{6}$	$1.48_{6}$	$1.49_{5}$	55	$1.43_{2}$	$1.44_{6}$	$1.45_{8}$	$1.46_{9}$	$1.47_{9}$	$1.48_{8}$
3	$1.43_{8}$	$1.45_{1}$	$1.46_{4}$	$1.47_{6}$	$1.48_{6}$	$1.49_{5}$	60	$1.43_{1}$	$1.44_{5}$	$1.45_{8}$	$1.46_{9}$	$1.47_{9}$	$1.48_{8}$
5	$1.43_{7}$	$1.45_{1}$	$1.46_{4}$	$1.47_{5}$	$1.48_{5}$	$1.49_{4}$	65	$1.43_{1}$	$1.44_{5}$	$1.45_{7}$	$1.46_{8}$	$1.47_{9}$	$1.48_{7}$
10	$1.43_{7}$	$1.45_{1}$	$1.46_{3}$	$1.47_{5}$	$1.48_{5}$	$1.49_{4}$	70	$1.43_{1}$	$1.44_{4}$	$1.45_{7}$	$1.46_{8}$	$1.47_{8}$	$1.48_{7}$
15	$1.43_{6}$	$1.45_{0}$	$1.46_{3}$	$1.47_{4}$	$1.48_{4}$	$1.49_{3}$	75	$1.43_{0}$	$1.44_{4}$	$1.45_{6}$	$1.46_{8}$	$1.47_{8}$	$1.48_{6}$
20	$1.43_{5}$	$1.44_{9}$	$1.46_{2}$	$1.47_{3}$	$1.48_{3}$	$1.49_{2}$	80	$1.43_{0}$	$1.44_{4}$	$1.45_{6}$	$1.46_{7}$	$1.47_{7}$	$1.48_{6}$
25	$1.43_{5}$	$1.44_{9}$	$1.46_{1}$	$1.47_{3}$	$1.48_{3}$	$1.49_{2}$	85	$1.42_{9}$	$1.44_{3}$	$1.45_{6}$	$1.46_{7}$	$1.47_{7}$	$1.48_{6}$
30	$1.43_{4}$	$1.44_{8}$	$1.46_{1}$	$1.47_{2}$	$1.48_{2}$	$1.49_{1}^{-}$	90	$1.42_{9}$	$1.44_{3}$	$1.45_{5}$	$1.46_{7}$	$1.47_{7}$	$1.48_{5}$
35	$1.43_{4}$	$1.44_{8}$	$1.46_{0}$	$1.47_{1}^{-}$	$1.48_{2}^{-}$	$1.49_{0}$	95	$1.42_{9}$	$1.44_{3}$	$1.45_{5}$	$1.46_{6}$	$1.47_{6}$	$1.48_{5}$
40	$1.43_{3}$	$1.44_{7}$	$1.46_{0}$	$1.47_{1}$	$1.48_{1}^{-}$	$1.49_{0}$	100	$1.42_{9}$	$1.44_{2}$	$1.45_{5}$	$1.46_{6}$	$1.47_{6}$	$1.48_{5}$

Table 11. Calculated Values of  $C_v$  for [bmim][PF<sub>6</sub>]

			T	/K						T	/K		
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$C_v/\mathrm{kJ}\cdot\mathrm{K}$	K <sup>-1</sup> •kg <sup>-1</sup>						$C_v/\mathrm{kJ}\cdot\mathrm{K}$	K <sup>-1</sup> •kg <sup>-1</sup>		
0.1	$1.24_{6}$	$1.25_{8}$	$1.27_{0}$	$1.28_{1}$	$1.29_{0}$	$1.29_{8}$	45	$1.24_{9}$	$1.26_{2}$	$1.27_{4}$	$1.\overline{28}_{4}$	$1.29_{3}$	$1.30_{1}$
0.5	$1.24_{6}$	$1.25_{8}$	$1.27_{0}$	$1.28_{1}$	$1.29_{0}$	$1.29_{8}$	50	$1.25_{0}$	$1.26_{3}$	$1.27_{4}$	$1.28_{4}$	$1.29_{3}$	$1.30_{1}$
1	$1.24_{6}$	$1.25_{9}$	$1.27_{0}$	$1.28_{1}$	$1.29_{0}$	$1.29_{8}$	55	$1.25_{0}$	$1.26_{3}$	$1.27_{4}$	$1.28_{5}$	$1.29_{4}$	$1.30_{1}$
3	$1.24_{6}$	$1.25_{9}$	$1.27_{0}$	$1.28_{1}$	$1.29_{0}$	$1.29_{8}$	60	$1.25_{1}$	$1.26_{3}$	$1.27_{5}$	$1.28_{5}$	$1.29_{4}$	$1.30_{2}$
5	$1.24_{6}$	$1.25_{9}$	$1.27_{0}$	$1.28_{1}$	$1.29_{0}$	$1.29_{8}$	65	$1.25_{1}$	$1.26_{4}$	$1.27_{5}$	$1.28_{6}$	$1.29_{5}$	$1.30_{2}^{-}$
10	$1.24_{6}$	$1.25_{9}$	$1.27_{1}$	$1.28_{1}$	$1.29_{0}$	$1.29_{8}$	70	$1.25_{2}$	$1.26_{4}$	$1.27_{6}$	$1.28_{6}$	$1.29_{5}$	$1.30_{3}$
15	$1.24_{7}$	$1.26_{0}$	$1.27_{1}$	$1.28_{2}$	$1.29_{1}$	$1.29_{8}$	75	$1.25_{2}$	$1.26_{5}$	$1.27_{6}$	$1.28_{7}$	$1.29_{6}$	$1.30_{3}$
20	$1.24_{7}$	$1.26_{0}$	$1.27_{2}$	$1.28_{2}$	$1.29_{1}$	$1.29_{9}$	80	$1.25_{3}$	$1.26_{5}$	$1.27_{7}$	$1.28_{7}$	$1.29_{6}$	$1.30_{4}$
25	$1.24_{8}$	$1.26_{0}$	$1.27_{2}$	$1.28_{2}$	$1.29_{1}$	$1.29_{9}$	85	$1.25_{3}$	$1.26_{6}$	$1.27_{7}$	$1.28_{8}$	$1.29_{7}$	$1.30_{5}$
30	$1.24_{8}$	$1.26_{1}$	$1.27_{2}^{-}$	$1.28_{3}^{-}$	$1.29_{2}$	$1.29_{9}$	90	$1.25_{4}$	$1.26_{6}$	$1.27_{8}$	$1.28_{8}$	$1.29_{7}$	$1.30_{5}$
35	$1.24_{9}$	$1.26_{1}$	$1.27_{3}^{-}$	$1.28_{3}$	$1.29_{2}^{-}$	$1.30_{0}$	95	$1.25_{4}$	$1.26_{7}$	$1.27_{8}$	$1.28_{9}$	$1.29_{8}$	$1.30_{6}$
40	$1.24_{9}$	$1.26_{2}$	$1.27_{3}$	$1.28_{3}$	$1.29_{2}^{-}$	$1.30_{0}$	100	$1.25_{4}$	$1.26_{7}$	$1.27_{9}$	$1.29_{0}$	$1.29_{9}$	$1.30_{8}$

is extremely dependent on the choice of the type of function to screen the data. For those situations where the statistical scatter of the raw data is large compared with an unambiguous determination of the curvature, we suggest the use of  $\ln \rho = f(T)$ . If this function proves to be linear,

then  $\ln V = f(T)$  is as well, and  $\alpha_p$  is constant (temperature-independent). Moreover, the choice of a logarithmic function avoids the existence of a mathematical violation that arises if one considers that both  $\rho - T$  and V - T plots are linear.

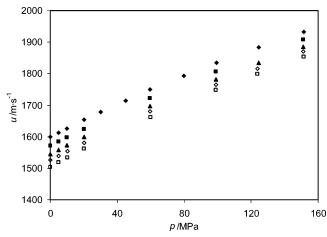


Figure 10. Isotherms for the experimental speed of sound in [bmim][BF<sub>4</sub>].  $\blacklozenge$ , 283.15 K;  $\blacksquare$ , 293.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 313.15 K; □, 323.15 K.

Table 12. Experimental Speed of Sound, u, Data for [bmim][BF<sub>4</sub>] as a Function of Temperature, T, and

, <b>p</b>				
$u/\mathrm{m}\cdot\mathrm{s}^{-1}$	p/MPa	$u/\mathrm{m}\cdot\mathrm{s}^{-1}$	p/MPa	$u/\mathrm{m}\cdot\mathrm{s}^{-1}$
33.15 K	20.080	1624.43	10.185	1554.04
1599.51	59.673	1721.05	20.070	1580.96
1612.54	98.994	1806.08	59.719	1679.35
1626.20	151.068	1907.30	99.014	1765.79
1653.13			123.975	1816.59
1678.26	T = 30	$3.15 \; { m K}$	151.204	1869.96
1714.66	0.100	1544.88		
1749.05	5.080	1558.60	T = 32	$3.15 \mathrm{K}$
1793.04	10.091	1572.45	0.100	1503.36
1833.62	20.063	1599.53	4.999	1517.83
1882.86	59.767	1697.00	10.202	1533.40
1932.20	99.007	1782.61	20.046	1561.37
	124.609	1834.02	59.977	1662.08
3.15 K			99.014	1748.81
1570.23	T = 31	3.15 K	123.945	1798.92
1583.99	0.100	1525.22	151.374	1853.24
1597.70	5.091	1539.35		
	u/m·s <sup>-1</sup> 3.15 K 1599.51 1612.54 1626.20 1653.13 1678.26 1714.66 1749.05 1793.04 1833.62 1882.86 1932.20 3.15 K 1570.23 1583.99	$u/\text{m} \cdot \text{s}^{-1}$ $p/\text{MPa}$ $13.15 \text{ K}$ $20.080$ $1599.51$ $59.673$ $1612.54$ $98.994$ $1626.20$ $151.068$ $1653.13$ $1678.26$ $T = 30$ $1714.66$ $0.100$ $1749.05$ $5.080$ $1793.04$ $10.091$ $1833.62$ $20.063$ $1882.86$ $59.767$ $1932.20$ $99.007$ $124.609$ $13.15 \text{ K}$ $1570.23$ $T = 31$ $1583.99$ $0.100$	$u/\text{m} \cdot \text{s}^{-1}$ $p/\text{MPa}$ $u/\text{m} \cdot \text{s}^{-1}$ $13.15 \text{ K}$ $20.080$ $1624.43$ $1599.51$ $59.673$ $1721.05$ $1612.54$ $98.994$ $1806.08$ $1626.20$ $151.068$ $1907.30$ $1653.13$ $1678.26$ $T = 303.15 \text{ K}$ $1714.66$ $0.100$ $1544.88$ $1749.05$ $5.080$ $1558.60$ $1793.04$ $10.091$ $1572.45$ $1833.62$ $20.063$ $1599.53$ $1882.86$ $59.767$ $1697.00$ $1932.20$ $99.007$ $1782.61$ $124.609$ $1834.02$ $13.15 \text{ K}$ $1570.23$ $T = 313.15 \text{ K}$ $1583.99$ $0.100$ $1525.22$	$u/\text{m} \cdot \text{s}^{-1}$ $p/\text{MPa}$ $u/\text{m} \cdot \text{s}^{-1}$ $p/\text{MPa}$ $13.15 \text{ K}$ $20.080$ $1624.43$ $10.185$ $1599.51$ $59.673$ $1721.05$ $20.070$ $1612.54$ $98.994$ $1806.08$ $59.719$ $1626.20$ $151.068$ $1907.30$ $99.014$ $1653.13$ $123.975$ $157.206$ $1678.26$ $T = 303.15 \text{ K}$ $151.204$ $1714.66$ $0.100$ $1544.88$ $1749.05$ $5.080$ $1558.60$ $T = 32$ $1793.04$ $10.091$ $1572.45$ $0.100$ $1833.62$ $20.063$ $1599.53$ $4.999$ $1882.86$ $59.767$ $1697.00$ $10.202$ $1932.20$ $99.007$ $1782.61$ $20.046$ $124.609$ $1834.02$ $59.977$ $13.15 \text{ K}$ $123.945$ $1583.99$ $0.100$ $1525.22$ $151.374$

Table 13. Coefficients of Equation 1 for T/K, p/MPa, and  $u/\text{m}\cdot\text{s}^{-1}$  within the Interval (283 < T/K < 323, 0.1 < p/MPa< 100)

	-/		
$a_{ij}$		j	
$\frac{a_{ij}}{i}$	0	1	2
0	$1.11539 \times 10^{3}$	$1.16241\times10^{1}$	$-1.85200  imes 10^{-2}$
1	$-1.03226  imes 10^{1}$	$-8.64584  imes 10^{-2}$	$1.23988  imes 10^{-4}$
2	$2.10054  imes 10^{-2}$	$1.55385  imes 10^{-4}$	$-2.03876  imes 10^{-7}$
$b_{kl}$		L	
$\overline{k}$	0	1	2
0	1.00000	$5.81502  imes 10^{-3}$	$-1.49739  imes 10^{-5}$
1	$-8.43584  imes 10^{-3}$	$-4.13259  imes 10^{-5}$	$9.95819  imes 10^{-8}$
2	$1.63578  imes 10^{-5}$	$7.19818  imes 10^{-8}$	$-1.63623  imes 10^{-10}$

 $[bmim][BF_4]$ . Speed of sound measurements have been carried out at broad ranges of temperature (283 < T/K < 323) and pressure (0.1  $\leq$  p/MPa  $\leq$  160). Figure 10 and Table 12 show the speed of sound behavior with pressure and temperature for [bmim][BF<sub>4</sub>]. Equation 1 was used to fit the experimental data, and all of the tests proved the nonexistence of poles in the (p, u, T) surface considered. The values of the fitting coefficients are provided in Table 13. The standard deviation between the experimental and fitted values is found to be 0.04%.

Density measurements have been carried out at broad ranges of temperature (298 < T/K < 333) and pressure (0.1

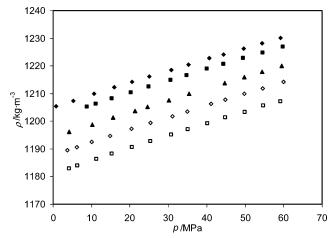


Figure 11. Isotherms for the experimental density of [bmim]-[BF<sub>4</sub>].  $\spadesuit$ , 298.34 K;  $\blacksquare$ , 303.23 K;  $\blacktriangle$ , 313.01 K;  $\diamondsuit$ , 322.85 K;  $\Box$ , 332.73

Table 14. Experimental Density,  $\rho$ , Data for [bmim][BF<sub>4</sub>] as a Function of Temperature, T, and Pressure, p

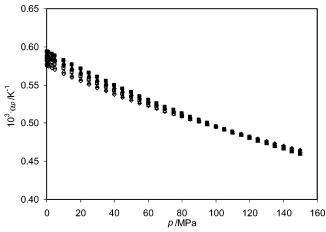
as a r ar	iculon of ic	imper ava	ic, i, and	i i cosui c,	· P
p/MPa	$ ho/{ m kg}\cdot{ m m}^{-3}$	p/MPa	$ ho/\mathrm{kg}\cdot\mathrm{m}^{-3}$	p/MPa	$ ho/\mathrm{kg}\cdot\mathrm{m}^{-3}$
T = 2	298.34 K	44.31	1220.61	25.40	1199.38
0.1	1205.03	49.50	1222.73	31.09	1201.87
0.70	1205.32	54.49	1224.75	34.85	1203.51
5.28	1207.44	59.82	1226.85	41.13	1206.23
10.60	1209.87			44.88	1207.85
15.92	1212.24	T = 3	13.01 K	49.83	1209.95
20.54	1214.26	0.1	1194.59	54.52	1211.91
25.00	1216.18	4.13	1196.19	59.92	1214.20
30.71	1218.62	10.18	1198.82		
35.19	1220.47	15.65	1201.26	T=3	32.73  K
40.66	1222.73	21.30	1203.75	0.1	1181.05
44.37	1224.21	24.58	1205.19	4.13	1182.92
49.66	1226.32	30.11	1207.62	6.35	1183.98
54.34	1228.16	35.39	1209.88	11.21	1186.30
59.23	1230.05	44.70	1213.84	15.22	1188.15
		49.72	1215.92	20.54	1190.55
T=3	803.23 K	54.43	1217.91	25.28	1192.70
0.1	1201.29	59.45	1219.95	30.76	1195.16
8.78	1205.30			35.08	1197.05
11.17	1206.40	T = 3	$22.85 \; \mathrm{K}$	40.11	1199.23
15.23	1208.22	0.1	1187.85	44.86	1201.24
20.27	1210.43	3.73	1189.50	49.84	1203.35
24.89	1212.44	6.22	1190.68	54.76	1205.70
30.67	1214.92	10.02	1192.47	59.13	1207.20
34.77	1216.66	14.87	1194.68		
40.02	1218.85	20.45	1197.20		

Table 15. Coefficients of Second-Order Polynomial Fits,  $Y=A+B(T/K)+C(T/K)^2$ , to Atmospheric Isobars of Y=
hoor  $Y = C_p$ 

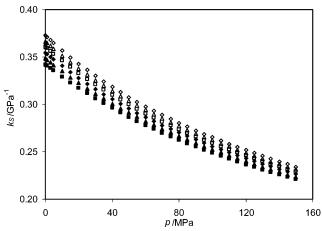
	$ ho/\mathrm{kg}\cdot\mathrm{m}^{-3}$	$C_p/\mathrm{J}\!\cdot\!\mathrm{K}^{-1}\!\cdot\!\mathrm{kg}^{-1}$
A	1476.2773	2056.7965
$\boldsymbol{B}$	-1.1035102	-5.2008507
C	$6.5020339  imes 10^{-4}$	$1.2456247  imes 10^{-2}$

< p/MPa < 60). The experimental data are presented both in Figure 11 and Table 14.

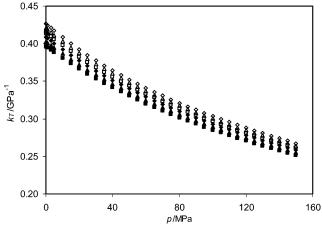
The derived thermodynamic properties were calculated by the integration method using isobaric density data of this current work and heat capacities taken from literature data<sup>23</sup> at 0.1 MPa. The atmospheric isobars of both density and heat capacity were fitted with a second-order polynomial equation. The coefficients of the fittings are reported in Table 15. The integration was carried out from atmospheric pressure up to 150 MPa. The results obtained for several thermodynamic properties are presented in Figures 12 to 17 and Tables 16 to 21.



**Figure 12.** Isotherms for the isobaric expansivity of [bmim] [BF<sub>4</sub>]. 
■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

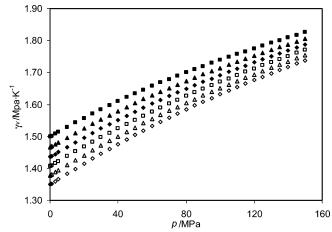


**Figure 13.** Isotherms for the isentropic compressibility of [bmim]-[BF<sub>4</sub>]. ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

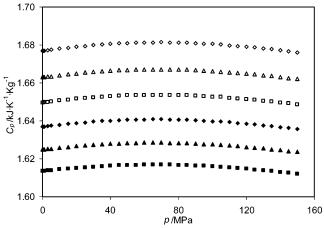


**Figure 14.** Isotherms for the isothermal compressibility of [bmim]-[BF<sub>4</sub>]. ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\diamondsuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

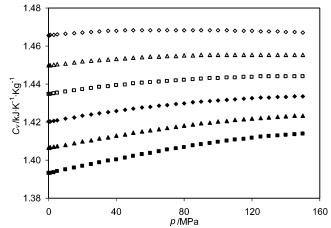
The comparison between the density data taken from the integration procedure and the experimental ones shows good agreement with a maximum deviation smaller than 0.1%, even at pressures as high as 60 MPa. This deviation is small and can be ascribed to the uncertainty of the speed of sound measurements because this quantity is responsible for about 85% of the calculated  $d\rho/dp$  in the integration process.



**Figure 15.** Isotherms for the thermal pressure coefficient of [bmim][BF<sub>4</sub>]. ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\spadesuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.



**Figure 16.** Isotherms for the isobaric heat capacity of [bmim]- $[BF_4]$ . ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\spadesuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.



**Figure 17.** Isotherms for the isochoric heat capacity of [bmim]- $[BF_4]$ . ■, 298.15 K;  $\blacktriangle$ , 303.15 K;  $\spadesuit$ , 308.15 K;  $\Box$ , 313.15 K;  $\triangle$ , 318.15 K;  $\diamondsuit$ , 323.15 K.

At atmospheric pressure, literature data show that whereas Huddleston et al. <sup>17</sup> report 1.12 g·cm<sup>-3</sup> and 1.17 g·cm<sup>-3</sup> (their ref 36), values found in the articles of Wang et al., <sup>24</sup> Seddon et al., <sup>25</sup> Fredlake et al., <sup>4</sup> and Tokuda et al. are quoted as 1.21105 g·cm<sup>-3</sup>, 1.2048 g·cm<sup>-3</sup>, 1.2037 g·cm<sup>-3</sup>, and 1.2035 g·cm<sup>-3</sup>, respectively. (In the latter two cases, a least-squares fit to their data was applied to make comparisons at the same nominal temperature of 298.15 K.)

Table 16. Calculated Values of  $\kappa_T$  for [bmim][BF<sub>4</sub>]

·			T	/K				T/K					
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$\kappa_T/G$	Pa <sup>-1</sup>				$\kappa_T$ /GPa $^{-1}$					
0.1	$0.396_{3}$	$0.402_{6}$	$0.408_{6}$	$0.414_{4}$	$0.420_{2}$	$0.426_{4}$	70	$0.310_{6}$	$0.315_{0}$	$0.319_{2}$	$0.323_{2}$	$0.327_{0}$	$0.330_{6}$
0.5	$0.395_{6}$	$0.401_{9}$	$0.407_{9}$	$0.413_{7}$	$0.419_{5}$	$0.425_{6}$	75	$0.306_{0}$	$0.310_{4}$	$0.314_{5}$	$0.318_{4}$	$0.322_{1}$	$0.325_{7}$
1	$0.394_{8}$	$0.401_{1}$	$0.407_{1}$	$0.412_{8}$	$0.418_{5}$	$0.424_{6}$	80	$0.301_{6}$	$0.305_{9}$	$0.309_{9}$	$0.313_{8}$	$0.317_{4}$	$0.321_{0}$
3	$0.391_{6}$	$0.397_{8}$	$0.403_{7}$	$0.409_{3}$	$0.415_{0}$	$0.420_{9}$	85	$0.297_{3}$	$0.301_{5}$	$0.305_{5}$	$0.309_{3}$	$0.312_{9}$	$0.316_{4}$
5	$0.388_{5}$	$0.394_{5}$	$0.400_{3}$	$0.405_{9}$	$0.411_{4}$	$0.417_{2}$	90	$0.293_{2}$	$0.297_{3}$	$0.301_{2}$	$0.304_{9}$	$0.308_{5}$	$0.312_{0}$
10	$0.380_{9}$	$0.386_{7}$	$0.392_{3}$	$0.397_{7}$	$0.403_{0}$	$0.408_{5}$	95	$0.289_{1}$	$0.293_{2}$	$0.297_{1}$	$0.300_{7}$	$0.304_{2}$	$0.307_{7}$
15	$0.373_{6}$	$0.379_{3}$	$0.384_{7}$	$0.389_{9}$	$0.394_{9}$	$0.400_{1}$	100	$0.285_{2}$	$0.289_{2}$	$0.293_{0}$	$0.296_{6}$	$0.300_{1}$	$0.303_{5}$
20	$0.366_{7}$	$0.372_{2}$	$0.377_{4}$	$0.382_{4}$	$0.387_{3}$	$0.392_{3}$	105	$0.281_{4}$	$0.285_{4}^{-}$	$0.289_{1}$	$0.292_{7}$	$0.296_{1}$	$0.299_{4}$
25	$0.360_{0}$	$0.365_{4}$	$0.370_{5}$	$0.375_{3}$	$0.380_{0}$	$0.384_{8}$	110	$0.277_{8}$	$0.281_{6}$	$0.285_{3}$	$0.288_{8}$	$0.292_{2}$	$0.295_{5}$
30	$0.353_{6}$	$0.358_{9}$	$0.363_{8}$	$0.368_{6}$	$0.373_{1}$	$0.377_{6}$	115	$0.274_{2}$	$0.278_{0}$	$0.281_{6}$	$0.285_{0}$	$0.288_{4}$	$0.291_{7}$
35	$0.347_{5}$	$0.352_{6}$	$0.357_{5}$	$0.362_{1}$	$0.366_{5}$	$0.370_{8}$	120	$0.270_{7}$	$0.274_{4}$	$0.278_{0}$	$0.281_{4}$	$0.284_{6}$	$0.287_{9}$
40	$0.341_{6}$	$0.346_{6}$	$0.351_{4}$	$0.355_{8}$	$0.360_{1}$	$0.364_{4}$	125	$0.267_{3}$	$0.271_{0}$	$0.274_{5}$	$0.277_{8}$	$0.281_{0}$	$0.284_{3}$
45	$0.336_{0}$	$0.340_{9}$	$0.345_{5}$	$0.349_{9}$	$0.354_{1}$	$0.358_{1}$	130	$0.264_{0}$	$0.267_{6}$	$0.271_{0}$	$0.274_{3}$	$0.277_{5}$	$0.280_{7}$
50	$0.330_{5}$	$0.335_{3}$	$0.339_{8}$	$0.344_{1}$	$0.348_{2}$	$0.352_{2}$	135	$0.260_{8}$	$0.264_{4}$	$0.267_{7}$	$0.270_{9}$	$0.274_{1}$	$0.277_{3}$
55	$0.325_{3}$	$0.330_{0}$	$0.334_{4}$	$0.338_{6}$	$0.342_{6}^{-}$	$0.346_{5}^{-}$	140	$0.257_{7}$	$0.261_{2}$	$0.264_{5}$	$0.267_{6}$	$0.270_{7}$	$0.273_{9}$
60	$0.320_{2}$	$0.324_{8}$	$0.329_{2}$	$0.333_{3}$	$0.337_{2}$	$0.341_{0}$	145	$0.254_{7}$	$0.258_{1}^{-}$	$0.261_{3}$	$0.264_{4}$	$0.267_{4}$	$0.270_{5}$
65	$0.315_{3}^{2}$	$0.319_{8}$	$0.324_{1}$	$0.328_{1}$	$0.332_{0}^{2}$	$0.335_{7}$	150	$0.251_7$	$0.255_{0}$	$0.258_{2}$	$0.261_{2}$	$0.264_{2}$	$0.267_{3}$

Table 17. Calculated Values of  $\kappa_S$  for [bmim][BF<sub>4</sub>]

			T/	K						$T_{i}$	K		
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$\kappa_S/G$	Pa⁻¹						κ <sub>S</sub> /G	Pa⁻¹		
0.1	$0.342_{2}$	$0.348_{5}$	$0.354_{5}$	$0.360_{4}$	$0.366_{3}$	$0.372_{6}$	70	$0.270_{0}$	$0.274_{1}$	$0.278_{0}$	$0.281_{7}$	$0.285_{3}$	$0.288_{8}$
0.5	$0.341_{6}$	$0.347_{9}$	$0.353_{9}$	$0.359_{8}$	$0.365_{7}$	$0.372_{0}$	75	$0.266_{1}$	$0.270_{2}$	$0.274_{0}$	$0.277_{6}$	$0.281_{1}$	$0.284_{5}$
1	$0.340_{9}$	$0.347_{2}$	$0.353_{2}$	$0.359_{0}$	$0.364_{9}$	$0.371_{1}$	80	$0.262_{5}$	$0.266_{4}$	$0.270_{1}$	$0.273_{7}$	$0.277_{1}$	$0.280_{4}$
3	$0.338_{2}$	$0.344_{4}$	$0.350_{3}$	$0.356_{0}$	$0.361_{8}$	$0.367_{9}$	85	$0.258_{9}$	$0.262_{7}$	$0.266_{4}$	$0.269_{8}$	$0.273_{1}$	$0.276_{4}$
5	$0.335_{6}$	$0.341_{6}$	$0.347_{4}$	$0.353_{1}$	$0.358_{7}$	$0.364_{7}$	90	$0.255_{4}$	$0.259_{2}$	$0.262_{7}$	$0.266_{1}$	$0.269_{4}$	$0.272_{5}$
10	$0.329_{1}$	$0.335_{0}$	$0.340_{6}$	$0.346_{0}$	$0.351_{4}$	$0.357_{0}$	95	$0.252_{1}$	$0.255_{7}$	$0.259_{2}$	$0.262_{5}$	$0.265_{7}$	$0.268_{8}$
15	$0.323_{0}$	$0.328_{6}$	$0.334_{0}$	$0.339_{2}$	$0.344_{4}$	$0.349_{7}$	100	$0.248_{8}$	$0.252_{4}$	$0.255_{8}$	$0.259_{0}$	$0.262_{1}$	$0.265_{2}$
20	$0.317_{1}$	$0.322_{6}$	$0.327_{8}$	$0.332_{8}$	$0.337_{7}$	$0.342_{8}$	105	$0.245_{6}$	$0.249_{1}$	$0.252_{5}$	$0.255_{6}$	$0.258_{7}$	$0.261_{7}$
25	$0.311_{5}$	$0.316_{8}$	$0.321_{8}$	$0.326_{7}$	$0.331_{4}$	$0.336_{2}$	110	$0.242_{6}$	$0.246_{0}$	$0.249_{2}$	$0.252_{3}$	$0.255_{3}$	$0.258_{3}$
30	$0.306_{1}$	$0.311_{2}$	$0.316_{1}$	$0.320_{8}$	$0.325_{4}$	$0.329_{9}$	115	$0.239_{6}$	$0.242_{9}$	$0.246_{1}$	$0.249_{1}$	$0.252_{0}$	$0.254_{9}$
35	$0.301_{0}$	$0.305_{9}$	$0.310_{7}$	$0.315_{2}$	$0.319_{6}$	$0.324_{0}$	120	$0.236_{7}$	$0.240_{0}$	$0.243_{0}$	$0.246_{0}$	$0.248_{8}$	$0.251_{7}$
40	$0.296_{0}$	$0.300_{8}$	$0.305_{4}$	$0.309_{8}$	$0.314_{1}$	$0.318_{3}$	125	$0.233_{9}$	$0.237_{1}$	$0.240_{1}$	$0.243_{0}$	$0.245_{7}$	$0.248_{6}$
45	$0.291_{2}$	$0.296_{0}$	$0.300_{4}$	$0.304_{7}$	$0.308_{8}$	$0.312_{8}$	130	$0.231_{1}$	$0.234_{2}$	$0.237_{2}$	$0.240_{0}$	$0.242_{7}$	$0.245_{5}$
50	$0.286_{7}$	$0.291_{3}$	$0.295_{6}$	$0.299_{7}$	$0.303_{7}$	$0.307_{6}$	135	$0.228_{4}$	$0.231_{5}$	$0.234_{3}$	$0.237_{1}$	$0.239_{8}$	$0.242_{5}$
55	$0.282_{3}$	$0.286_{7}$	$0.291_{0}$	$0.295_{0}$	$0.298_{8}$	$0.302_{6}$	140	$0.225_{8}$	$0.228_{8}$	$0.231_{6}$	$0.234_{3}$	$0.236_{9}$	$0.239_{6}$
60	$0.278_{0}$	$0.282_{4}$	$0.286_{5}$	$0.290_{4}$	$0.294_{2}$	$0.297_{8}$	145	$0.223_{3}$	$0.226_{2}$	$0.228_{9}$	$0.231_{5}$	$0.234_{1}$	$0.236_{8}$
65	$0.273_{9}$	$0.278_{2}$	$0.282_{2}$	$0.286_{0}$	$0.289_{7}$	$0.293_{2}$	150	$0.220_{8}$	$0.223_{6}$	$0.226_{3}$	$0.228_{8}$	$0.231_{3}$	$0.234_{0}$

Table 18. Calculated Values of  $\alpha_p$  for [bmim][BF<sub>4</sub>]

			$T_{\ell}$	K/				$T/\mathrm{K}$					
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$10^3\alpha$	$p/{ m K}^{-1}$						$10^3\alpha$	$p/K^{-1}$		
0.1	$0.594_{0}$	$0.590_{3}$	$0.586_{7}$	$0.582_{9}$	$0.579_{2}$	$0.575_{4}$	70	$0.521_{5}$	$0.520_{3}$	$0.519_{1}$	$0.517_{9}$	$0.516_{6}$	$0.515_{4}$
0.5	$0.593_{5}$	$0.589_{9}$	$0.586_{2}$	$0.582_{5}$	$0.578_{7}$	$0.574_{9}$	75	$0.517_{1}$	$0.516_{1}$	$0.515_{0}$	$0.514_{0}$	$0.513_{0}$	$0.511_{9}$
1	$0.592_{9}$	$0.589_{3}$	$0.585_{6}$	$0.581_{9}$	$0.578_{1}$	$0.574_{3}$	80	$0.512_{7}$	$0.511_{9}$	$0.511_{0}$	$0.510_{2}$	$0.509_{3}$	$0.508_{5}$
3	$0.590_{5}$	$0.586_{9}$	$0.583_{2}$	$0.579_{6}$	$0.575_{8}$	$0.572_{1}$	85	$0.508_{4}$	$0.507_{8}$	$0.507_{1}$	$0.506_{5}$	$0.505_{8}$	$0.505_{1}$
5	$0.588_{1}$	$0.584_{5}$	$0.580_{9}$	$0.577_{3}$	$0.573_{6}$	$0.569_{9}$	90	$0.504_{2}$	$0.503_{7}$	$0.503_{2}$	$0.502_{8}$	$0.502_{3}$	$0.501_{8}$
10	$0.582_{2}$	$0.578_{8}$	$0.575_{3}$	$0.571_{8}$	$0.568_{2}$	$0.564_{6}$	95	$0.500_{0}$	$0.499_{7}$	$0.499_{4}$	$0.499_{1}$	$0.498_{8}$	$0.498_{5}$
15	$0.576_{5}$	$0.573_{2}$	$0.569_{9}$	$0.566_{5}$	$0.563_{1}$	$0.559_{6}$	100	$0.496_{0}$	$0.495_{8}$	$0.495_{7}$	$0.495_{6}$	$0.495_{4}$	$0.495_{2}$
20	$0.571_{0}$	$0.567_{8}$	$0.564_{6}$	$0.561_{4}$	$0.558_{2}$	$0.554_{9}$	105	$0.492_{0}$	$0.492_{0}$	$0.492_{0}$	$0.492_{0}$	$0.492_{0}$	$0.492_{0}$
25	$0.565_{5}$	$0.562_{6}$	$0.559_{5}$	$0.556_{5}$	$0.553_{4}$	$0.550_{3}$	110	$0.488_{1}$	$0.488_{2}$	$0.488_{4}$	$0.488_{5}$	$0.488_{7}$	$0.488_{8}$
30	$0.560_{2}$	$0.557_{4}$	$0.554_{6}$	$0.551_{8}$	$0.548_{9}$	$0.546_{0}$	115	$0.484_{2}$	$0.484_{5}$	$0.484_{8}$	$0.485_{1}$	$0.485_{4}$	$0.485_{7}$
35	$0.555_{1}$	$0.552_{4}$	$0.549_{8}$	$0.547_{2}$	$0.544_{5}$	$0.541_{7}$	120	$0.480_{5}$	$0.480_{9}$	$0.481_{3}$	$0.481_{7}$	$0.482_{1}$	$0.482_{6}$
40	$0.550_{0}$	$0.547_{6}$	$0.545_{1}$	$0.542_{7}$	$0.540_{2}$	$0.537_{7}$	125	$0.476_{8}$	$0.477_{3}$	$0.477_{9}$	$0.478_{4}$	$0.478_{9}$	$0.479_{5}$
45	$0.545_{0}$	$0.542_{8}$	$0.540_{6}$	$0.538_{3}$	$0.536_{0}$	$0.533_{7}$	130	$0.473_{2}$	$0.473_{8}$	$0.474_{5}$	$0.475_{1}$	$0.475_{8}$	$0.476_{4}$
50	$0.540_{1}$	$0.538_{1}$	$0.536_{1}$	$0.534_{0}$	$0.532_{0}$	$0.529_{9}$	135	$0.469_{6}$	$0.470_{4}$	$0.471_{1}$	$0.471_{9}$	$0.472_{6}$	$0.473_{4}$
55	$0.535_{4}$	$0.533_{5}$	$0.531_{7}$	$0.529_{9}$	$0.528_{0}$	$0.526_{1}$	140	$0.466_{2}$	$0.467_{0}$	$0.467_{8}$	$0.468_{7}$	$0.469_{6}$	$0.470_{4}$
60	$0.530_{7}$	$0.529_{1}$	$0.527_{4}$	$0.525_{8}$	$0.524_{1}$	$0.522_{5}$	145	$0.462_{8}$	$0.463_{7}$	$0.464_{6}$	$0.465_{6}$	$0.466_{5}$	$0.467_{4}$
65	$0.526_{0}$	$0.524_{6}$	$0.523_{2}$	$0.521_{8}$	$0.520_{3}$	$0.518_{9}$	150	$0.459_{5}$	$0.460_{5}$	$0.461_{5}$	$0.462_{5}$	$0.463_{5}$	$0.464_{5}$

Our results agree reasonably well with those of Seddon et al., Fredlake et al., and Tokuda et al.

As for  $\alpha_p$ , although expansivities decrease sharply with pressure, they decrease mildly as temperature increases. This corroborates previously discussed<sup>23</sup> effects of the anions' size on the temperature coefficient of  $\alpha_p$  in which

by decreasing the anion's size one finds a tendency for that temperature coefficient to cross over from positive to negative values. In the latter case, the IL should present an "anomaly" (a minimum in the  $\alpha_p$  vs T plot at some higher temperature<sup>23</sup>). The differences obtained for the derived properties,  $\alpha_p$  and  $\kappa_T$ , when comparing the deriva-

Table 19. Calculated Values of  $\gamma_v$  for [bmim][BF<sub>4</sub>]

			T	K/K				T/K					
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$\gamma_v/\mathrm{MF}$	Pa•K <sup>−1</sup>				$\gamma_v/\mathrm{MPa}{\cdot}\mathrm{K}^{-1}$					
0.1	$1.49_{9}$	$1.46_{6}$	$1.43_{6}$	$1.40_{7}$	$1.37_{8}$	$1.34_{9}$	70	$1.67_{9}$	$1.65_{2}$	$1.62_{6}$	$1.60_{2}$	$1.58_{0}$	$1.55_{9}$
0.5	$1.50_{0}$	$1.46_{8}$	$1.43_{7}$	$1.40_{8}$	$1.38_{0}$	$1.35_{1}$	75	$1.69_{0}$	$1.66_{3}$	$1.63_{8}$	$1.61_{4}$	$1.59_{2}$	$1.57_{1}$
1	$1.50_{2}$	$1.46_{9}$	$1.43_{9}$	$1.40_{9}$	$1.38_{1}$	$1.35_{2}$	80	$1.70_{0}$	$1.67_{3}$	$1.64_{9}$	$1.62_{6}$	$1.60_{5}$	$1.58_{4}$
3	$1.50_{8}$	$1.47_{5}$	$1.44_{5}$	$1.41_{6}$	$1.38_{8}$	$1.35_{9}$	85	$1.71_{0}$	$1.68_{4}$	$1.66_{0}$	$1.63_{7}$	$1.61_{6}$	$1.59_{6}$
5	$1.51_{4}$	$1.48_{1}$	$1.45_{1}$	$1.42_{2}$	$1.39_{4}$	$1.36_{6}$	90	$1.72_{0}$	$1.69_{4}$	$1.67_{1}$	$1.64_{9}$	$1.62_{8}$	$1.60_{8}$
10	$1.52_{9}$	$1.49_{6}$	$1.46_{6}$	$1.43_{8}$	$1.41_{0}$	$1.38_{2}$	95	$1.72_{9}$	$1.70_{4}$	$1.68_{1}$	$1.66_{0}$	$1.64_{0}$	$1.62_{0}$
15	$1.54_{3}$	$1.51_{1}$	$1.48_{1}$	$1.45_{3}$	$1.42_{6}$	$1.39_{9}$	100	$1.73_{9}$	$1.71_{4}$	$1.69_{2}$	$1.67_{1}$	$1.65_{1}$	$1.63_{2}$
20	$1.55_{7}$	$1.52_{6}$	$1.49_{6}$	$1.46_{8}$	$1.44_{1}$	$1.41_{5}$	105	$1.74_{8}$	$1.72_{4}$	$1.70_{2}$	$1.68_{1}$	$1.66_{2}$	$1.64_{3}$
25	$1.57_{1}$	$1.54_{0}$	$1.51_{0}$	$1.48_{3}$	$1.45_{6}$	$1.43_{0}$	110	$1.75_{7}$	$1.73_{4}$	$1.71_{2}$	$1.69_{2}$	$1.67_{3}$	$1.65_{4}$
30	$1.58_{4}$	$1.55_{3}$	$1.52_{4}$	$1.49_{7}$	$1.47_{1}$	$1.44_{6}$	115	$1.76_{6}$	$1.74_{3}$	$1.72_{2}$	$1.70_{2}$	$1.68_{3}$	$1.66_{5}$
35	$1.59_{7}$	$1.56_{7}$	$1.53_{8}$	$1.51_{1}$	$1.48_{6}$	$1.46_{1}$	120	$1.77_{5}$	$1.75_{2}$	$1.73_{1}$	$1.71_{2}$	$1.69_{4}$	$1.67_{6}$
40	$1.61_{0}$	$1.58_{0}$	$1.55_{2}$	$1.52_{5}$	$1.50_{0}$	$1.47_{6}$	125	$1.78_{3}$	$1.76_{1}$	$1.74_{1}$	$1.72_{2}$	$1.70_{4}$	$1.68_{7}$
45	$1.62_{2}$	$1.59_{2}$	$1.56_{5}$	$1.53_{9}$	$1.51_{4}$	$1.49_{0}$	130	$1.79_{2}$	$1.77_{0}$	$1.75_{0}$	$1.73_{2}$	$1.71_{4}$	$1.69_{7}$
50	$1.63_{4}$	$1.60_{5}$	$1.57_{8}$	$1.55_{2}$	$1.52_{8}$	$1.50_{4}$	135	$1.80_{1}$	$1.77_{9}$	$1.76_{0}$	$1.74_{2}$	$1.72_{5}$	$1.70_{7}$
55	$1.64_{6}$	$1.61_{7}$	$1.59_{0}$	$1.56_{5}$	$1.54_{1}$	$1.51_{8}$	140	$1.80_{9}$	$1.78_{8}$	$1.76_{9}$	$1.75_{1}$	$1.73_{5}$	$1.71_{8}$
60	$1.65_{7}$	$1.62_{9}$	$1.60_{2}$	$1.57_{8}$	$1.55_{4}$	$1.53_{2}$	145	$1.81_{7}$	$1.79_{7}$	$1.77_{8}$	$1.76_{1}$	$1.74_{5}$	$1.72_{8}$
65	$1.66_{8}$	$1.64_{0}$	$1.61_{4}^{-}$	$1.59_{0}$	$1.56_{7}$	$1.54_{6}^{-}$	150	$1.82_{5}$	$1.80_{6}$	$1.78_{7}$	$1.77_{1}$	$1.75_{4}$	$1.73_{8}$

Table 20. Calculated Values of  $C_p$  for [bmim][BF<sub>4</sub>]

			T	/K				T/K					
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$C_p/\mathrm{kJ}\cdot\mathrm{I}$	$K^{-1}kg^{-1}$				$C_p$ /k $\mathbf{J}$ • $\mathbf{K}^{-1}$ k $\mathbf{g}^{-1}$					
0.1	$1.61_{3}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{3}$	$1.67_{7}$	70	$1.61_{7}$	$1.62_{8}$	$1.64_{1}$	$1.65_{4}$	$1.66_{7}$	$1.68_{1}$
0.5	$1.61_{3}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{3}$	$1.67_{7}$	75	$1.61_{7}$	$1.62_{8}$	$1.64_{1}$	$1.65_{4}$	$1.66_{7}$	$1.68_{1}$
1	$1.61_{4}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{3}$	$1.67_{7}$	80	$1.61_{7}$	$1.62_{8}$	$1.64_{1}$	$1.65_{4}$	$1.66_{7}$	$1.68_{1}$
3	$1.61_{4}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{3}$	$1.67_{7}$	85	$1.61_{7}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{7}$	$1.68_{1}$
5	$1.61_{4}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{4}$	$1.67_{7}$	90	$1.61_{6}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{7}$	$1.68_{1}$
10	$1.61_{4}$	$1.62_{6}$	$1.63_{8}$	$1.65_{1}$	$1.66_{4}$	$1.67_{8}$	95	$1.61_{6}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{7}$	$1.68_{1}$
15	$1.61_{5}$	$1.62_{6}$	$1.63_{8}$	$1.65_{1}$	$1.66_{5}$	$1.67_{9}$	100	$1.61_{6}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{6}$	$1.68_{0}$
20	$1.61_{5}$	$1.62_{7}$	$1.63_{9}$	$1.65_{2}$	$1.66_{5}$	$1.67_{9}$	105	$1.61_{6}$	$1.62_{7}$	$1.64_{0}$	$1.65_{2}$	$1.66_{6}$	$1.68_{0}$
25	$1.61_{5}$	$1.62_{7}$	$1.63_{9}$	$1.65_{2}$	$1.66_{5}$	$1.67_{9}$	110	$1.61_{5}$	$1.62_{7}$	$1.63_{9}$	$1.65_{2}$	$1.66_{6}$	$1.68_{0}$
30	$1.61_{6}$	$1.62_{7}$	$1.64_{0}$	$1.65_{2}$	$1.66_{6}$	$1.68_{0}$	115	$1.61_{5}$	$1.62_{7}$	$1.63_{9}$	$1.65_{2}$	$1.66_{5}$	$1.67_{9}$
35	$1.61_{6}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{6}$	$1.68_{0}$	120	$1.61_{5}$	$1.62_{6}$	$1.63_{9}$	$1.65_{1}$	$1.66_{5}$	$1.67_{9}$
40	$1.61_{6}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{6}$	$1.68_{1}$	125	$1.61_{4}$	$1.62_{6}$	$1.63_{8}$	$1.65_{1}$	$1.66_{4}$	$1.67_{9}$
45	$1.61_{7}$	$1.62_{8}$	$1.64_{0}$	$1.65_{3}$	$1.66_{7}$	$1.68_{1}$	130	$1.61_{4}$	$1.62_{5}$	$1.63_{8}$	$1.65_{1}$	$1.66_{4}$	$1.67_{8}$
50	$1.61_{7}$	$1.62_{8}$	$1.64_{1}$	$1.65_{3}$	$1.66_{7}$	$1.68_{1}$	135	$1.61_{3}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{4}$	$1.67_{8}$
55	$1.61_{7}$	$1.62_{8}$	$1.64_{1}$	$1.65_{4}$	$1.66_{7}$	$1.68_{1}$	140	$1.61_{3}$	$1.62_{5}$	$1.63_{7}$	$1.65_{0}$	$1.66_{3}$	$1.67_{7}$
60	$1.61_{7}$	$1.62_{8}$	$1.64_{1}$	$1.65_{4}$	$1.66_{7}$	$1.68_{1}$	145	$1.61_{2}$	$1.62_{4}$	$1.63_{6}$	$1.64_{9}$	$1.66_{3}$	$1.67_{7}$
65	$1.61_{7}$	$1.62_{9}$	$1.64_{1}$	$1.65_{4}$	$1.66_{7}$	$1.68_{1}$	150	$1.61_{2}$	$1.62_{4}$	$1.63_{6}$	$1.64_{9}$	$1.66_{2}$	$1.67_{6}$

Table 21. Calculated Values of  $C_v$  for [bmim][BF<sub>4</sub>]

			$T_{i}$	K/				T/K					
p/MPa	298.15	303.15	308.15	313.15	318.15	323.15	p/MPa	298.15	303.15	308.15	313.15	318.15	323.15
			$C_v/\mathrm{kJ}\cdot\mathrm{K}$	<sup>1</sup> -1•kg <sup>-1</sup>				$C_v$ /k $\mathbf{J}$ · $\mathbf{K}^{-1}$ · $\mathbf{k}\mathbf{g}^{-1}$					
0.1	$1.39_{3}$	$1.40_{6}$	$1.42_{0}$	$1.\overline{43}_{5}$	$1.45_{0}$	$1.46_{6}$	70	$1.40_{5}$	$1.41_{7}$	$1.42_{9}$	$1.\overline{44}_{2}$	$1.45_{5}$	$1.46_{8}$
0.5	$1.39_{3}$	$1.40_{7}$	$1.42_{0}$	$1.43_{5}$	$1.45_{0}$	$1.46_{6}$	75	$1.40_{6}$	$1.41_{8}$	$1.42_{9}$	$1.44_{2}$	$1.45_{5}$	$1.46_{8}$
1	$1.39_{3}$	$1.40_{7}$	$1.42_{0}$	$1.43_{5}$	$1.45_{0}$	$1.46_{6}$	80	$1.40_{7}$	$1.41_{8}$	$1.43_{0}$	$1.44_{2}$	$1.45_{5}$	$1.46_{8}$
3	$1.39_{4}$	$1.40_{7}$	$1.42_{1}$	$1.43_{5}$	$1.45_{0}$	$1.46_{6}$	85	$1.40_{8}$	$1.41_{9}$	$1.43_{0}$	$1.44_{2}$	$1.45_{5}$	$1.46_{8}$
5	$1.39_{4}$	$1.40_{7}$	$1.42_{1}$	$1.43_{5}$	$1.45_{0}$	$1.46_{6}$	90	$1.40_{8}$	$1.41_{9}$	$1.43_{1}$	$1.44_{3}$	$1.45_{5}$	$1.46_{8}$
10	$1.39_{5}$	$1.40_{8}$	$1.42_{2}$	$1.43_{6}$	$1.45_{1}$	$1.46_{7}$	95	$1.40_{9}$	$1.42_{0}$	$1.43_{1}$	$1.44_{3}$	$1.45_{5}$	$1.46_{8}$
15	$1.39_{6}$	$1.40_{9}$	$1.42_{3}$	$1.43_{7}$	$1.45_{1}$	$1.46_{7}$	100	$1.41_{0}$	$1.42_{0}$	$1.43_{1}$	$1.44_{3}$	$1.45_{5}$	$1.46_{8}$
20	$1.39_{7}$	$1.41_{0}$	$1.42_{3}$	$1.43_{7}$	$1.45_{2}$	$1.46_{7}$	105	$1.41_{0}$	$1.42_{1}$	$1.43_{2}$	$1.44_{3}$	$1.45_{5}$	$1.46_{8}$
25	$1.39_{8}$	$1.41_{1}$	$1.42_{4}$	$1.43_{8}$	$1.45_{2}$	$1.46_{7}$	110	$1.41_{1}$	$1.42_{1}$	$1.43_{2}$	$1.44_{3}$	$1.45_{5}$	$1.46_{8}$
30	$1.39_{9}$	$1.41_{1}$	$1.42_{5}$	$1.43_{8}$	$1.45_{3}$	$1.46_{8}$	115	$1.41_{1}$	$1.42_{2}$	$1.43_{2}$	$1.44_{4}$	$1.45_{6}$	$1.46_{8}$
35	$1.40_{0}$	$1.41_{2}$	$1.42_{5}$	$1.43_{9}$	$1.45_{3}$	$1.46_{8}$	120	$1.41_{2}$	$1.42_{2}$	$1.43_{3}$	$1.44_{4}$	$1.45_{6}$	$1.46_{8}$
40	$1.40_{0}$	$1.41_{3}$	$1.42_{6}$	$1.43_{9}$	$1.45_{3}$	$1.46_{8}$	125	$1.41_{2}$	$1.42_{2}$	$1.43_{3}$	$1.44_{4}$	$1.45_{6}$	$1.46_{8}$
45	$1.40_{1}$	$1.41_{4}$	$1.42_{6}$	$1.44_{0}$	$1.45_{4}$	$1.46_{8}$	130	$1.41_{3}$	$1.42_{3}$	$1.43_{3}$	$1.44_{4}$	$1.45_{6}$	$1.46_{8}$
50	$1.40_{2}$	$1.41_{4}$	$1.42_{7}$	$1.44_{0}$	$1.45_{4}$	$1.46_{8}$	135	$1.41_{3}$	$1.42_{3}$	$1.43_{3}$	$1.44_{4}$	$1.45_{5}$	$1.46_{8}$
55	$1.40_{3}$	$1.41_{5}$	$1.42_{8}$	$1.44_{1}$	$1.45_{4}$	$1.46_{8}$	140	$1.41_{3}$	$1.42_{3}$	$1.43_{3}$	$1.44_{4}$	$1.45_{5}$	$1.46_{7}$
60	$1.40_{4}$	$1.41_{6}$	$1.42_{8}$	$1.44_{1}$	$1.45_{4}$	$1.46_{8}$	145	$1.41_{4}$	$1.42_{3}$	$1.43_{3}$	$1.44_{4}$	$1.45_{5}$	$1.46_{7}$
65	$1.40_{5}$	$1.41_{6}$	$1.42_{9}$	$1.44_{1}$	$1.45_{5}$	$1.46_{8}$	150	$1.41_{4}$	$1.42_{4}$	$1.43_{4}$	$1.44_{4}$	$1.45_{5}$	$1.46_{7}$

tion of the measured densities with the integration method show average deviations of 4% and -4%, respectively. Although these values are within acceptable limits, they corroborate the strong dependence of the derivation method on the shape of the curves used to fit the experimental data and the necessity of collecting a large number of experimental points.

As for the heat capacities, the results for both the isobaric and isochoric heat capacities reveal, in practice, pressure independence.

### **Conclusions**

This work shows the usefulness of this method in deriving precise thermodynamic properties at high pres-

sures from speed of sound measurements. It maps the physical behavior of two important ionic liquids over wide pressure and temperature ranges.

As the anion increases in size ( $[BF_4]^- < [PF_6]^-$ ), the density increases accordingly, whereas the speed of sound shows the opposite trend. At first glance, this fact may seem counterintuitive because one tends to associate greater density with greater speed of sound. This line of thought mainly arises from comparisons (in density and speed of sound) made between the gas phase and the condensed phase. It is true that gases present smaller densities as well as speeds of propagation of sound waves than condensed phases, but this truism has little to do with density. The typical ratio between the densities of liquid to gas (far from the critical point) is on the order of thousands. However, the ratio (gas to liquid) of compressibilities is ca. 100 000. Therefore, compressibility is the factor that controls the speed of sound. It is also interesting that in these ILs (differing in the anion) if the mass density increases the molar volume also does. For instance, at atmospheric pressure and 298.15 K  $V_{\text{bmimPF}_6} - V_{\text{bmimBF}_4} =$  $20.3 \text{ cm}^3 \cdot \text{mol}^{-1}$ . This value can be attributed to the increase in the effective anion size<sup>3</sup> from 0.089 nm<sup>3</sup>/anion of BF<sub>4</sub><sup>-</sup> to 0.122 nm<sup>3</sup>/anion of PF<sub>6</sub><sup>-</sup>.

Generally, one can state that speed of sound values of ILs are not too dissimilar from those typically found in conventional solvents, tending to fall in the high-value side of the range. In contrast, both compressibilities and expansivities are ca. three times smaller than values typically found in those conventional solvents. This is probably a consequence of the fact that although critical temperatures,  $T_{\rm c}$ , are unknown for ILs, estimates of  $T_{\rm c}$  of ILs<sup>26</sup> show that their critical temperatures are certainly much higher (if it were possible to reach the liquid-gas critical point by avoiding the thermal decomposition of the IL) than those of molecular solvents. Therefore, in the case of ILs, roomtemperature conditions certainly correspond to very low reduced temperatures. It is well known that both compressibility and expansivity decrease drastically along the orthobaric line from an infinite value at the critical point to very modest values as temperature (and reduced temperature) decreases.

As for heat capacities, if comparisons are performed using molar quantities, for instance, at atmospheric pressure and 298.15 K, then  $C_{p,\mathrm{bmimPF_6}} - C_{p,\mathrm{bmimBF_4}} = 44.1$  $J \cdot mol^{-1} \cdot K^{-1}$ . The greater values presented by  $PF_6$  are mainly a consequence of the larger number of vibrational degrees of freedom of this anion compared with that of BF<sub>4</sub><sup>-</sup>. In other words, as the anion's structural complexity increases, one expects improved energy storage ability.

### Acknowledgment

We thank the QUILL group, Belfast, lead by Professor Kenneth Seddon for hosting some of us and helping with the synthesis and purification of [bmim][PF<sub>6</sub>].

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Received for review December 29, 2004. Accepted March 23, 2005. This work was financially supported by Fundação para a Ciência e Tecnologia, Portugal, under contract POCTI/EQU/35437/00. R.G.A., J.M.S.S.E., V.N.-V. and Z.P.V. are grateful to Fundação para a Ciência e Tecnologia for doctoral fellowships.

JE049534W