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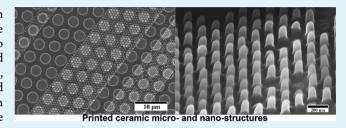
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## 1 Printed Sub-100 nm Polymer-Derived Ceramic Structures

- <sup>2</sup> Binh Duong,<sup>†</sup> Palash Gangopadhyay,<sup>‡</sup> Josh Brent,<sup>‡</sup> Supapan Seraphin,<sup>§</sup> Raouf O. Loutfy,<sup>#</sup>
- 3 Nasser Peyghambarian, and Jayan Thomas\*\*,†,||
- <sup>4</sup> NanoScience Technology Center, University of Central Florida, Orlando, Florida 32826, United States
- s <sup>‡</sup>College of Optical Sciences, The University of Arizona, Tucson, Arizona 85721, United States
- 6 \$Department of Materials Science & Engineering, The University of Arizona, Tucson, Arizona 85721, United States
- 7 \*Materials and Electrochemical Research Corporation, 7960 S. Kolb Road, Tucson, Arizona 85706, United States
- 8 "CREOL, College of Optics and Photonics and Department of Material Science and Engineering, University of Central Florida,
- 9 Orlando, Florida 32826, United States

**ABSTRACT:** We proposed an unconventional fabrication technique called spin-on nanoprinting (SNAP) to generate and transfer sub-100 nm preceramic polymer patterns onto flexible and rigid substrates. The dimensions of printed nanostructures are almost the same as those of the mold, since the ceramic precursor used is a liquid. The printed patterns can be used as a replica for printing second-generation structures using other polymeric materials or they can be further converted to desirable ceramic structures, which are



very attractive for high-temperature and harsh environment applications. SNAP is an inexpensive parallel process and requires no special equipment for operation.

21 KEYWORDS: nanostructured ceramics, nanoimprinting, sub-100 nm ceramic structures, polymer-derived ceramics, SNAP technique,

22 polyureasilazane

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#### 1. INTRODUCTION

23 Production of novel multifunctional inorganic materials with a 24 tailor-made, nanoscale structure is of considerable interest in 25 semiconductor, 1-4 electronic, 5 and photonic applications. 6-8 26 Modern technologies have created a need for the development 27 of new materials and patterning technologies that can provide 28 sub-100 nm resolution, high pattern fidelity, improved 29 reproducibility, and high throughput at low costs. 9,10 30 Furthermore, the increasing miniaturization of components 31 calls for new process technologies that allow the reliable, large-32 scale production of materials at nanometer scale in a very cost-33 efficient manner. In order to achieve this ambitious goal, 34 inorganic-organic hybrid materials, as well as amorphous and 35 polycrystalline ceramics, which are the materials of choice for 36 many of these applications, should be mass-produced using 37 techniques as simple as nanoimprinting. Possible applications 38 for nanoceramic materials are key technologies of the 21st 39 century including electronics, photonics, and information 40 technology, as well as microelectromechanical or nano-41 electromechanical systems. 11-14

Advanced ceramics are very attractive for electronic applications, because they can operate at high power, at high temperatures, and in harsh environments. They exhibit combinations of properties, such as electrical insulation and magnetism, that are not possible in other materials. Although scientifically interesting, possible fields of practical applications are enabled only if the ability to fabricate ceramics into nanoscale structures can be achieved via some simple

techniques. Conventionally, ceramic structures are mechanically 50 shaped using methods such as surface micromachining, 51 pressing, or powder injection molding. However, the smallest 52 reported feature created by these techniques was 0.1 mm in 53 size.<sup>19</sup> In addition, they are time-consuming and expensive to 54 manufacture, and they require intensive effort to produce 55 precise microparts. These drawbacks were resolved with the 56 successful transformation of polymers such as polysilazane, 57 polysiloxanes, and polycarbosilanes into ceramics by thermal 58 pyrolysis, known as polymer-derived ceramics (PDCs).<sup>20</sup> The 59 preceramic polymers offer the ease of fabrication and high 60 tailorability of chemical composition on a molecular level.<sup>21,22</sup> 61 It should be noted that the polymer precursor can easily be 62 converted to SiO<sub>2</sub>, SiC, or Si<sub>3</sub>N<sub>4</sub> by changing pyrolysis 63 environments at a higher temperature. 23 For example, heating 64 in the presence of ammonia and nitrogen can convert 65 polysilazane to  $Si_3N_4^{23}$  while exposing the precursor to steam 66 can produce SiO<sub>2</sub>.

The two main routes to fabricate ceramic structures from 68 polymer precursor are (i) photolithographic techniques<sup>25</sup> and 69 (ii) nonphotolithographic methods (such as microtransfer 70 molding ( $\mu$ TM),<sup>26</sup> micromolding in capillaries (MIMIC), and 71 nanoimprint lithography (NIL)<sup>27</sup>). In standard photolithog-72 raphy, desired patterns are created by exposing a ceramic 73

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74 precursor to an energetic radiation source such as ultraviolet 75 (UV), ion-beam, or electron-beam radiation. It has been 76 reported that, using UV lithography, the smallest defect-free 77  $\mathrm{Si_3N_4}$  structures (with a diameter of <50  $\mu\mathrm{m}$  and a thickness of 78 20  $\mu\mathrm{m}$ ) could be obtained after pyrolysis. Although a 79 technique such as electron-beam (e-beam) lithography is 80 capable of making features at the sub-20 nm level, this direct 81 structuring approach is not economically viable for high-volume 82 production, because of the high capital and operating costs that 83 are involved.

The conceptual novelty and technical capabilities of 85 nonlithographical methods have been greatly adopted in 86 fabricating various microscaled and nanoscaled devices. In the 87 nonphotolithography category, NIL clearly stands out as the 88 most promising technique that can provide sub-100 nm 89 resolution, high fidelity, and high-throughput at a low cost.<sup>29</sup> 90 However, there are critical processing factors limiting the use of 91 this approach in the fabrication of PDC nanostructures.<sup>30</sup> In 92 thermal-NIL (T-NIL), the mold is usually made of silicon with 93 desired structures fabricated by e-beam lithography. A high-94 molecular-weight (high-M<sub>w</sub>), solid thermoplastic polymer film 95 that has been cast on a substrate is heated above the glass-96 transition temperature  $(T_{\sigma})$  to reach a viscous flow state<sup>31</sup> and 97 the hard mold is pressed into the substrate under high pressure 98 (~50-100 bar). This is followed by cooling the patterned 99 polymer below its  $T_g$  before the mold is released. Although low- $100~M_{\rm w}$  polymers can be used in T-NIL, printed structures are often 101 brittle, possibly causing fractured structures during the 102 demolding step. T-NIL of preceramic polymers presents 103 additional challenges, because they are thermosetting materials. 104 A prior study reported that it was impossible to obtain direct 105 replication of PDC microstructures from a silicon master mold, 106 because of cracking and fragmentation during cross-linking. 107 UV-NIL is an alternative method to print structures that 108 prevent the use of the high temperatures and pressures required 109 in T-NIL by using liquid precursors, which can be cross-linked 110 at room temperature under UV light. However, this process 111 requires the mold or substrate to be transparent to UV light. To 112 the best of our knowledge, UV-NIL was used to produce only 113 ceramic precursor nanostructures, 33 but was never successfully 114 converted to ceramics. Here, we demonstrate the spin-on 115 <u>nanoprinting</u> (SNAP) technique, which is an easy but prudent 116 technique to print nanostructures from preceramic polymer and 117 convert them to ceramics. It is a benchtop procedure that can 118 be undertaken by any unskilled personnel in the art.

#### 2. EXPERIMENTAL SECTION

Materials and Fabrication of PDC Structures. Because of the 120 high thermosetting temperature of polyureasilazane (PUS, commer-121 cially known as Ceraset, Kion Corp.), ~400 °C, a thermal initiator— 122 dicumyl peroxide—was added to lower the curing temperature to 123 150-200 °C. The chemical structure of the precursor is shown in 124 Figure 1. The mixture was then filtered (using a 0.2- $\mu$ m filter) and 125 degassed for an hour before use, to prevent bubble formation during 126 thermal cross-linking. Figure 2 illustrates the printing process. The 127 silicon master mold was first wetted with a commercially available 128 antiadhesive agent (Rain-X). Rain-X is isopropanol-based cocktail of 129 quaternary ammonium and fatty acid siloxanes<sup>34</sup> and imparts a good 130 degree of hydrophobicity on SiO on silicon or SiO<sub>2</sub> surfaces.<sup>35</sup> This 131 hydrophobic coating is antiadhesive in nature and helps lower the 132 surface energy to efficiently spread and fill the nanostructured 133 features.<sup>36</sup> Then, the precursor solution was dropcast onto the mold, 134 which was preheated on a hot plate at 190 °C. The substrate was 135 placed on top of the mold after PUS was cured for ~30 s. A longer

$$\begin{bmatrix} Me & H \\ -Si & N \end{bmatrix}_{0.20} = \begin{bmatrix} Me & H \\ -Si & N \end{bmatrix}_{0.79} = \begin{bmatrix} Me & Ph & O & H \\ -Si & N & -C & N \end{bmatrix}_{0.01}$$

$$R = -H \text{ or -vinyl}$$

## Polyureasilazane

Figure 1. Chemical structure of polyureasilazane (PUS).<sup>23</sup>

curing time would result in a thicker film. A small pressure was applied 136 to remove excess material between the two substrates. The compact 137 structure was allowed to cool before the mold was separated from the 138 substrate with the nanostructures. In this study, we used four different 139 substrates: glass, silicon, tungsten foil, and carbon cloth. Thick 140 freestanding preceramic films (millimeter scale) were also prepared by 141 carefully removing the films right after the precursor solidified. To 142 obtain thin freestanding films, we used a sacrificial layer (polyvinyl 143 alcohol, PVA) or gelatin<sup>37</sup> coated on top of the substrates (silicon/ 144 glass), followed by steps 1 and 2 shown in Figure 2. Substrates with a 145 sacrificial layer and printed PUS were then immersed in boiled water 146 to dissolve the sacrificial layers. These aforementioned steps were 147 carried out in air. To convert the cross-linked samples to ceramics, 148 typical PDC pyrolysis was carried out. The samples (films on silicon 149 substrates, carbon cloth, and freestanding films) were pyrolyzed in an 150 argon atmosphere with a heating rate of 1 °C/min from room 151 temperature to 600 °C, then 3 °C/min to 1100 °C with a holding time 152 of 2 h at each stage.

Characterization of Printed Ceramic Structures. Scanning 154 electron microscopy (SEM, H-4800) was used to characterize the 155 morphology of the microstructures and nanostructures. An SEM 156 microscope system coupled with energy-dispersive X-ray spectroscopy 157 (EDS) was utilized to determine the elemental composition of the 158 sample. Fourier transform infrared (FTIR) and Raman spectroscopy 159 were employed to characterize structural changes. To collect infrared 160 (IR) spectra, a thin layer of the liquid PUS was obtained by placing a 161 drop of the liquid PUS between the two KBr plates. For the solid 162 samples (cross-linked PUS and pyrolyzed PUS), they were ground 163 into fine powders. The mixture of ~1% powder and KBr powder 164 (Sigma-Aldrich, FTIR grade) was ground again. A small amount of 165 the mixture was placed in a die and pressed to form a pellet. KBr 166 pellets were prepared for IR spectra collection. Raman spectroscopy 167 (Structural and Chemical Analyzer (SCA), SEM-SCA, Renishaw, 168 U.K.) has a wavelength of 514 nm, energy of 2.41 eV, power of 50 169 mW, and a beam diameter of  $\sim 1~\mu m$ . Crystallization behavior of the 170 cross-linked and pyrolyzed samples was monitored by X-ray diffraction 171 using monochromatic Cu Kα (Scintag XDS 2000 PTS Diffractom- 172 eter).

#### 3. RESULTS AND DISCUSSION

To demonstrate the capability of our nanoimprinting 174 technique, preceramic nanostructures with different aspect 175 ratios were fabricated as shown in Figure 3. We have 176 f3 successfully transferred the defect-free precursor films onto 177 both rigid substrates (glass and silicon) and flexible substrates 178 (tungsten foil and carbon cloth), as well as freestanding 179 preceramic films. All the printed preceramic structures were 180 stable on the substrates, even after a year. It is worth pointing 181 out that the master mold was not damaged, even after more 182 than 20 repetitive printings. Moreover, this technique can be 183 used to fabricate both amorphous and crystalline silicon-based 184 ceramic device structures. In order to demonstrate that it can 185 be used to print any versatile structure, we have printed a 186 photonic crystal-type structure and converted it to a ceramic, as 187 shown in Figure 4. According to the supplier, the mass 188 f4 conversion of polymer to ceramic, as measured by thermogravi- 189

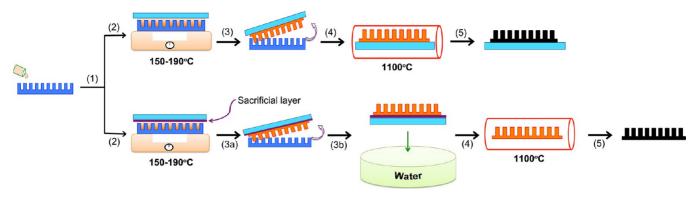


Figure 2. Schematic illustrating the steps involved in the PDC printing process. (1) First, the silicon mold is wetted with a commercially available antiadhesive agent. The solution of polyureasilazane (PUS) mixed with 1 wt % dicumyl peroxide is cast onto the preheated mold. The preceramic polymer is partially cured for  $\sim$ 1 min before a substrate is placed on top of the mold. (2) The compact structure is further cured at 190 °C before cooling it to room temperature. Steps 1 and 2 are carried out in air. (3) The transferred substrate is carefully separated from the mold. (4) The printed sample is converted to an amorphous ceramic by heating it to 1100 °C in an argon atmosphere. (5)  $SiO_xC_yN_z$  is obtained. Similar procedure is followed to prepare freestanding ceramic films. However, the substrate is first coated with a sacrificial layer before use. After step 3a, this layer is removed by soaking the sample into hot water.

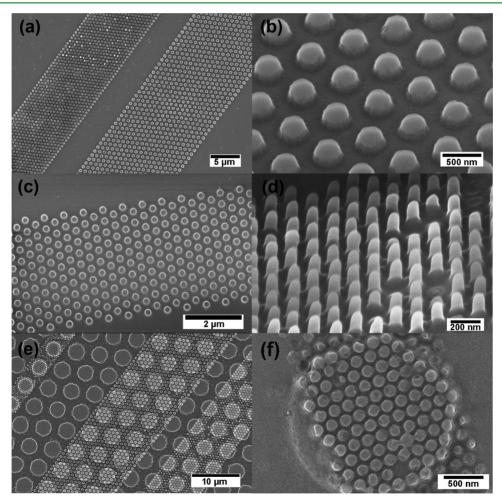


Figure 3. (a) Arrays of nanopillars with diameters of 300 and 500 nm. (b) Higher-magnification view of the 300-nm features. (c) Micrograph showing the top view of the 80-nm-diameter nanopillars. (d) Micrograph showing the  $45^{\circ}$ -angle view of the 80-nm-diameter nanopillars. (e) Nanopillars printed on and near micropillars. (f) Higher-magnification view of the 80-nm-diameter nanopillars printed on  $2-\mu$ m micropillars.

 $_{190}$  metric analysis (TGA), is ~20 wt %, and the volumetric  $_{191}$  shrinkage is often more than 60%. It should be noted that  $_{192}$  microcracks were found on samples having a thickness of more  $_{193}$  than 2  $\mu$ m, because of the release of gaseous byproducts during  $_{194}$  pyrolysis.  $_{38}$  After pyrolysis, cracks were observed on the films

prepared on silicon substrates and carbon cloths, even though  $_{195}$  the thickness of the films was <500 nm, because of the large  $_{196}$  differences in expansion coefficients between the precursor and  $_{197}$  the substrates during heating and cooling. Meanwhile, defect-  $_{198}$  free ceramics were obtained on the printed freestanding films.  $_{199}$ 

**Figure 4.** (a) SEM image showing the  $SiO_xC_yN_z$  photonic structures after being pyrolyzed at 1100 °C. (b) Higher-magnification micrographs of the ceramic photonic structure indicated in panel (a).

The conversion of preceramic polymers to amorphous ceramic nanostructures was confirmed by different analytical techniques, as shown in Figure 5. Chemical changes during pyrolysis were revealed by FTIR analysis. Significant reduction in intensities of all bands was observed after PUS was cross-linked at 190 °C (Figure 5a). Moreover, the disappearance of indicates that complete cross-linking took place after curing the sample at 190 °C. After pyrolysis, several overlapped bands are observed between 600 cm<sup>-1</sup> and 1200 cm<sup>-1</sup>, which can be attributed to the Si–O, Si–C, and Si–N bondings. X-ray photoelectron spectroscopy (XPS) shows the presence of Si, C, N, and O in both samples before and after pyrolysis (see Figure 13 Sb). The binding energies of all elements were found to be 214 ~0.6 eV lower than those measured before pyrolysis. Results

collected from four different samples suggest the existence of 215 Si-C, Si-N, and Si-O networks. The atomic concentration 216 collected from these samples (after pyrolysis) also shows 217 consistent compositions of ~13% Si, 55.2% C, 5.2% N, and 218 26.6% O. Since the silazane precursor was prepared and cured 219 in air, a high amount of oxygen contamination in the final 220 ceramics is expected. Both FTIR and XPS results confirm that 221 the composition of the product is  $SiO_xC_yN_z$  ceramics. It has 222 been reported that the structure of pyrolytic products are 223 sensitive to the cross-linking processing and pyrolysis 224 conditions. To learn more about the structure of the produced 225 ceramics, we carried out XRD analysis of the cross-linked and 226 pyrolyzed samples. XRD patterns shown in Figure 5c detected a 227 clear reflection at  $2\theta = 26.6^{\circ}$  in the pyrolyzed samples, revealing 228 the presence of graphite in the ceramic products. The Raman 229 spectra shown in Figure 5d reveals the signal of vinyl group at 230 3050 cm<sup>-1</sup>, which is an indication of polymerization reactions 231 that caused the liquid precursor to solidify. The visible rising of 232 the C=C band at ~1500 cm<sup>-1</sup> in the pyrolyzed PUS confirms 233 the existence of the carbon bonds in the pyrolyzed sample.

Previously, we have shown the influence of viscosity on the 235 efficacy of the printing process, particularly when printing 236 multiple nanofeatures over a landscape of micropatterns. The 237 low-viscosity (0.05–0.2 Pa s) PUS that has been used in this 238 report enables efficient low-pressure filling over a broad range 239 of nanodimensions with a relatively high aspect ratio. The 240 direct molding of high-aspect-ratio ceramic structures has never 241

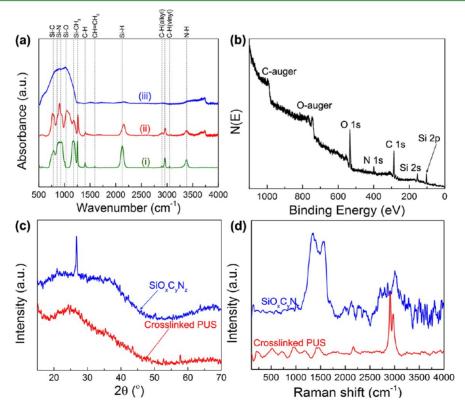


Figure 5. Different characterization techniques were employed to evaluate the samples before and after pyrolysis. (a) FTIR spectra depict significant changes in chemical structures of (i) the starting PUS sample, (ii) cross-linked PUS and  $SiO_xC_yN_z$ . After pyrolysis, most of the absorption bands disappear except for several overlapped broad bands between 600 cm<sup>-1</sup> and 1200 cm<sup>-1</sup>, which attribute to the Si–O, Si–C, and Si–N bondings. (b) The XPS data are in good agreement with FTIR results. XPS analysis suggests the existence of Si–C, Si–O, and Si–N networks in the samples after pyrolysis. Consistent compositions of ~13% Si, 55.2% C, 5.2% N, and 26.6% O were obtained from four different samples. (c) XRD patterns showing a clear reflection at  $2\theta = 26.6^{\circ}$  in the pyrolyzed samples, revealing the presence of graphite in the ceramic products. (d) Raman analysis shows the evolution of characteristic carbon (C=C) structures in the pyrolyzed sample.

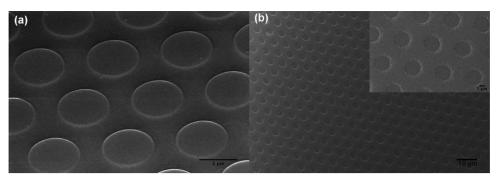


Figure 6. (a) SEM image of the printed PUS microstructures on a silicon substrate. (b) SEM image of microholes printed on the PMMA film using the mold shown in panel (a). The inset in panel (b) shows a higher-magnification image of the microhole arrays.

242 been demonstrated, to the best of our knowledge, particularly 243 in features ~100 nm in size. In addition, feature sizes in 244 ceramics are ideally free from any fundamental size limitation, such as in polymers, due to the relatively large molecular size of 246 polymer resists. Metallic glasses and ceramics have the potential to be able to replicate atomic-level features. However, structure 248 replication and printing within the size range from atomic to ~100 nm is generally dominated by strong capillary forces and wettability of the printing medium on the mold. The strong capillary forces and poor wettability can result in high molding pressure preventing faithful replication of high-aspect-ratio ceramic structures, particularly when the size range approaches 254 100 nm or smaller. Modified Hagen-Poisseuille's relationship 255 developed in ref 36 combines viscous and capillary contribu-256 tions at elevated temperatures for polymers for an accurate 257 description of printing pressure on nanometer length scales. 258 However, for such a low-viscosity medium, the printing 259 pressure is predominantly determined by the contact angle and printing length scales, both of which are intimately related and can be described as  $P = (4\gamma/d)\cos\theta \times (\chi - 1)$ , where  $\chi =$  $(8m^2\gamma\eta_T/t\cos\theta)\times d$ , which is  $\ll 1$ . Here,  $\eta_T$  is the viscosity at temperature T,  $\gamma$  the ceramic precursor-vacuum interfacial energy ( $\sim$ 1 N m<sup>-1</sup>),  $\theta$  the dynamic contact angle between the printing medium and nanostructure mold, t the filling time ( $\sim$ 1 266 s), m the aspect ratio, and d the diameter of the nanoasperities 267 to be filled. Within the wetting regime  $(\theta < \pi/2)$ , for a viscosity of 0.2 Pa s, one can safely assume that  $P(Pa) \approx -(\cos \theta/D)$ , 269 which offers a negative imprinting pressure and indicates 270 spontaneous self-filling of the nanoasperities.

The key advantage of using a ceramic precursor as the 272 printing medium is that the printed structure can be transferred 273 to ceramics with essentially the same dimensions but an 274 inverted structure. The conversion of the precursor to ceramic 275 will allow the fabrication of a second-generation mold with essentially the same material but with different wetting properties. This allows the imprinting process to be further extended to the nanometer scale with printing media otherwise 279 not printable because of poor wetting properties on silicon 280 molds. Modification of the contact angle with different 281 nanostructures is well-established in the literature, 39 and it 282 can be derived from energy arguments as  $\cos \theta = (1 - \varphi_s)(r - \varphi_s)$ 283  $\varphi_s$ ), where  $\varphi_s$  is the nonwetted solid fraction  $(\varphi_s = (\pi d^2/4p^2))$ and r is the ratio of the real surface area to the horizontal projection of the surface area  $(r = 1 + (\pi dh/p^2))$ , with h being 286 the height (or depth) of the nanoasperities and p being the 287 center-to-center pitch). Figure 3 shows printed preceramic 288 structures with different dimensions offering a unique

possibility of tuning contact angles for second- and third- 289 generation printed molds.

A current challenge facing NIL is the ability to completely 291 remove polymers from the mold surface after each printing, 292 which can be achieved either by applying a releasing agent or 293 lowering the surface adhesion of the mold. We found that the 294 second-generation pattern can easily be removed from the PUS 295 mold without any surface modification, even after more than 10 296 consecutive printings. Figure 6a shows the top view of the PUS 297 f6 printed micropillars. This replica served as a mold to print the 298 poly(methyl methacrylate) (PMMA) microholes, using a 299 nanoimprint by melt processing (NIMP) technique, 36 as 300 shown in Figure 6b. To investigate the releasing behavior of 301 the printed PUS mold, we measured contact angles of a silicon 302 substrate in comparison to printed PUS structures before and 303 after converting them to ceramic. Our results show that the 304 contact angle of water on a silicon substrate is 47°, while it is 305 98° and 77° on printed PUS before and after pyrolysis, 306 respectively. A smaller contact angle for the sample after heat 307 treatment is expected, because of the removal (burning) of the 308 organic side chains and functional groups present in PUS. Note 309 that the contact angle reported in the manuscript is measured 310 on a flat sample and is expected to decrease further, once 311 nanostructured. 36 The contact angle of the cured preceramic 312 polymer is comparable to the reported value of poly- 313 (dimethylsiloxane) (PDMS,  $90^{\circ}-120^{\circ}$ ).<sup>40</sup> The softness of an 314 elastomer such as PDMS limits the aspect ratio of relief features 315 in soft lithography between 0.2 and 2.<sup>41</sup> This drawback can be 316 substantially improved by using a preceramic polymer, because 317 an ultrahigh aspect ratio of ~20:1 microsized preceramic 318 structures can be achieved.<sup>42</sup> In addition, cured PDMS can be 319 swelled in many nonpolar organic solvents, 43 while cured PUS 320 is highly resistant to numerous solvents, water, and even dilute 321 acids and bases.<sup>23</sup> Furthermore, the cured preceramic polymer 322 is optically transparent down to 300 nm;<sup>23</sup> hence, it is suitable 323 for printing/molding UV-curable polymers. These results 324 indicated that the PUS mold is a potential candidate as a 325 mold material for NIL as well as soft lithography applications, 326 because it simultaneously solves many current technical 327 problems that exist in both techniques.

### 4. CONCLUSION

In summary, we have proposed a new printing method called 329 spin-on nanoprinting (SNAP) lithography and demonstrated 330 its feasibility of fabricating sub-100 nm ceramic patterns. 331 Moreover, no damage was observed on the silicon master mold, 332 even after more than 20 repetitive printing. Reproduction of 333 fine structures on a large-area printing (5 cm  $\times$  5 cm) is also 334

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335 viable by SNAP lithography within <5 min, which also set a 336 processing time benchmark against other conventional and 337 unconventional lithography. The printed preceramic structures 338 can serve as the molds for printing second-generation patterns 339 of various polymeric materials. We believe the simplicity, 340 versatility, short processing time, and high-fidelity replica make 341 our technique highly favorable for developing nanodevices.

#### AUTHOR INFORMATION

#### 343 Corresponding Author

344 \*E-mail: Jayan.Thomas@ucf.edu.

#### 345 Author Contributions

346 The manuscript was written through contributions of all 347 authors. All authors have given approval to the final version of 348 the manuscript. J.T. was responsible for administering the 349 project, project planning, and project execution.

#### 350 Notes

351 The authors declare no competing financial interest.

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