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# Temperature-Dependent Phonon Conduction and Nanotube Engagement in Metalized Single Wall Carbon Nanotube Films

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**ABSTRACT** Interfaces dominate the thermal resistances in aligned carbon nanotube arrays. This work uses nanosecond thermoreflectance thermometry to separate interface and volume resistances for 10  $\mu\text{m}$  thick aligned SWNT films coated with Al, Ti, Pd, Pt, and Ni. We interpret the data by defining the nanotube-metal engagement factor, which governs the interface resistance and is extracted using the measured film heat capacity. The metal–SWNT and SWNT–substrate resistances range between 3.8 and 9.2  $\text{mm}^2\text{K/W}$  and 33–46  $\text{mm}^2\text{K/W}$ , respectively. The temperature dependency of the heat capacity data, measured between 125 and 300 K, is in good agreement with theoretical predictions. The temperature dependence demonstrated by the metal–SWNT interface resistance data suggests inelastic phonon transmission.

**KEYWORDS** Carbon Nanotube, thermal boundary resistance, phonon, heat capacity

Aligned arrays of single and multiwall carbon nanotubes (SWNT, MWNT) films are promising materials for thermal management<sup>1–4</sup> and electronics applications such as field emission devices,<sup>5</sup> flexible electronics,<sup>5</sup> transistors,<sup>6</sup> sensors,<sup>7</sup> tough interfaces,<sup>8</sup> and energy storage materials.<sup>9</sup> They potentially offer the unique combination of low thermal resistance and controllable elastic modulus due to the high thermal conductivity ( $>3000 \text{ W m}^{-1} \text{ K}^{-1}$ )<sup>10,11</sup> and flexibility of individual nanotubes.<sup>12,13</sup> However, integrating these materials into devices and structures creates additional interfaces often with metals that inhibit heat conduction.

Measurements with various nanotube-substrate interface combinations such as pressed metal and dielectric interfaces,<sup>1,2,4</sup> growth interfaces,<sup>3,4,14,15</sup> and physically deposited metals,<sup>3,15</sup> yield large nanotube-substrate thermal interface resistances in the range of 0.3–50  $\text{mm}^2 \text{K/W}$ . These large resistances are due to incomplete nanotube-substrate contact amplifying the nanoscale conduction resistances of individual nanotube-substrate interfaces.<sup>3,15</sup> Such individual nanoscale metal–tube interfaces often dominate the conduction resistances for film thicknesses below  $\sim 50 \mu\text{m}$ . The nanoscale features of the contact further complicate the interface resistance by modifying the phonon transport physics for which there are no established models.<sup>16</sup> The structure of these interfaces at the

nanoscale is highly dependent on the interaction, adhesion, and wettability of the CNT and substrate materials. Previous data yield no clear relation between interface resistance and interface structure. Better understanding the contribution of the interface materials on the conduction physics and effective nanotube contact area at the interface are necessary to improve the thermal performance of nanotube films. This work directly measures the contribution of interface metalization on the SWNT engagement efficiency and thermal interface resistances via the composition dependence of the interface resistances and effective heat capacities of metal-coated SWNT films using nanosecond thermoreflectance thermometry. The temperature dependence of these properties provides a means to study phonon transmission at the interface.

The details of the alcohol-chemical vapor deposition (CVD) SWNT growth process used in this work can be found in Murakami et al.<sup>17</sup> Dip-coating a Si substrate into a Co–Mo acetate solution forms a dispersed monolayer of catalyst particles ( $\sim 1.3 \times 10^{17} \text{ m}^{-2}$ ). Annealing in air at 400 °C converts the acetates to metal oxides, followed by an Ar/H<sub>2</sub> reducing flow to retrieve the catalytic activity. The SWNTs are grown using alcohol-CVD at 800 °C<sup>17</sup> to yield an aligned SWNT film 10  $\mu\text{m}$  thick and a SWNT density of  $\sim 2\text{--}3\%$ , which was measured using a precision microbalance to compare the weight of the substrate before and after removing the SWNT film. Since the individual samples are derived from the same growth batch, the variation in the density among the samples is less than 20%. Raman data yield an average SWNT diameter of 1.9 nm and a D/G ratio of 0.012

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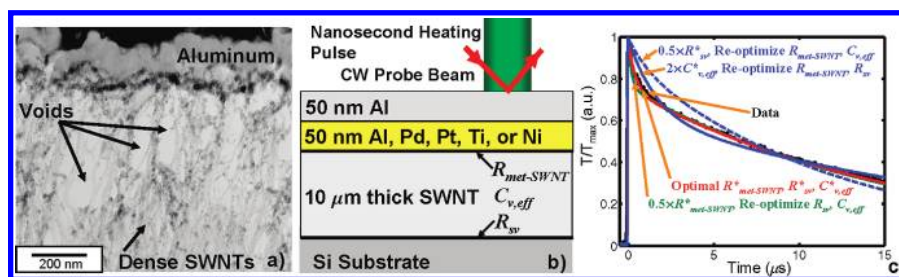


FIGURE 1. (a) Representative TEM of SWNT–metal contact showing voids and incomplete contact near the metal interface. (b) Schematic of sample geometry used in the measurements and for the thermal model. (c) Representative thermal trace data for the 100 nm Al-coated sample (black) along with optimal fit (solid red) yielding the optimal parameter set  $R_{\text{met-SWNT}}^*$ ,  $R_{\text{sv}}^*$ , and  $C_{v,\text{eff}}^*$ . The blue and green traces illustrate the data extraction sensitivity, showing the results of varying one of the fit parameters from its optimal value and reoptimizing the fit of the remaining two free parameters to the data.

with a D-band full-width half-maximum of  $20 \text{ cm}^{-1}$ , suggesting high purity films. TEM images reveal that the SWNT films consist of SWNT bundles with  $\sim 10$  or fewer nanotubes per bundle and a median of 6 SWNTs per bundle.<sup>18</sup> The resolution limits of the TEM place a lower bound of  $\sim 10\%$  on the number of bundles that consist of individual tubes; however, the actual number may be much larger. SEM images of the individual samples were used to measure the local SWNT thicknesses and showed thickness variations less than  $1.0 \mu\text{m}$ . Aligned SWNT films are individually metalized by e-beam giving a 50 nm coating of either Al, Pt, Pd, Ti, or Ni at a substrate temperature of  $\sim 300 \text{ K}$ . Following an air break, 50 nm of Al was e-beam evaporated onto the samples to improve the surface reflectivity and uniformity for the thermoreflectance measurement. Duong et al.<sup>19</sup> present a detailed SEM analysis of the dependence of the metal–SWNT morphology on material and deposition conditions. The microstructure of the interface is illustrated by a representative TEM cross-section of an Al(160 nm)/Pd(20 nm)–SWNT interface from previous work<sup>3</sup> in Figure 1a, showing many voids and a lower SWNT density near the interface compared to deeper within the sample. This incomplete contact leads to partial engagement between the SWNTs and the metal, increasing thermal conduction resistances.

This study uses nanosecond thermoreflectance thermometry to measure the interface resistances and heat capacity of the metalized SWNT films, the details of which can be found in previous work.<sup>3</sup> In brief, a 3 mm diameter, 532 nm wavelength, 6 ns pulse from a Nd:YAG laser heats the surface of the metal film at a rep-rate of 10 Hz. A 10 mW, 658 nm continuous wave probe laser is focused on the metal in the middle of the pump beam to a diameter of  $\sim 20 \mu\text{m}$ . A 650 MHz photodiode and oscilloscope capture the reflected intensity of the probe laser with submicrosecond temporal resolution. The reflected probe intensity linearly tracks the relative changes in metal surface temperature, yielding the normalized thermal response. Lateral heat conduction is negligible since the pump beam diameter is much larger than the maximum thermal diffusion distance during the measurement.

A least-squares algorithm fits the data to a solution of the heat diffusion equation for a multilayered stack model of the structure (Figure 1b) using three parameters,<sup>3</sup> the metal–SWNT interface resistance,  $R_{\text{met-SWNT}}$ , the effective volumetric heat capacity of the SWNT film apparent at the measurement time scales,  $C_{v,\text{eff}}$ , and a resistance,  $R_{\text{sv}} = R_{\text{SWNT-sub}} + R_{\text{SWNT,vol}}$ , which captures the combined resistance of the SWNT–substrate interface resistance ( $R_{\text{SWNT-sub}}$ ) and the residual volumetric resistance of the SWNT film ( $R_{\text{SWNT,vol}}$ ). The parameter extraction of the measurement for these particular samples is sensitive only to  $R_{\text{sv}}$  and neither  $R_{\text{SWNT-sub}}$  nor  $R_{\text{SWNT,vol}}$  individually. The unique impact of  $R_{\text{met-SWNT}}$ ,  $C_{v,\text{eff}}$ , and  $R_{\text{sv}}$  on the shape of the thermal response at different time scales permits their isolation.<sup>3</sup> Figure 1c presents sample thermal trace data, the optimal fit of the solution of the heat diffusion equation, and an illustration of the parameter extraction sensitivity by varying one parameter from its optimal value and reoptimizing the remaining two free parameters. The effective SWNT volume fraction contributing to the heat capacity during the time scales of the measurement can be estimated by  $\phi = C_{v,\text{eff}}/C_{v,\text{ind}}$ , where  $C_{v,\text{ind}} \sim 1.5 \text{ MJ/m}^3 \text{ K}^{-1}$  is the volumetric heat capacity of an individual SWNT.<sup>3</sup> Experimental studies report a wide range of values for the conductivity of individual SWNTs and MWNTs with values falling in the range of  $\sim 50\text{--}3600 \text{ Wm}^{-1} \text{ K}^{-1}$ .<sup>10,20,21</sup> In fitting the data, we assume an effective SWNT conductivity of  $k_{\text{cnt,eff}} = \phi \times k_{\text{SWNT}}$ , where  $k_{\text{SWNT}} = 3600 \text{ Wm}^{-1} \text{ K}^{-1}$  is the individual SWNT thermal conductivity of high quality SWNTs.<sup>10</sup> A reduced SWNT conductivity will appear as an additional contribution to  $R_{\text{sv}}$ . We neglect the metal–metal interface resistance since it is typically much less than  $R_{\text{met-SWNT}}$ , and since the thermalization time of the metals is less than the temporal resolution of the system.

The apparent effective heat capacity can deviate from the heat capacity based on the nominal density if there is poor SWNT–metal contact and if large intertube thermal resistances cause the partial intertube thermalization of the SWNTs during the time scales of the measurement.<sup>3</sup> A detailed model of intertube heat transfer within the array at the nanoscale developed in previous work<sup>3</sup> suggests that

intertube thermal transfer within the array is weak during the time scales of the measurement due to the large intertube thermal resistances. These results also suggest that the effective volume fraction contributing to the heat capacity is a reasonable measure for the volume fraction that makes good thermal contact with the metal film.<sup>3</sup> These results are supported with simple thermalization time scale arguments. Assuming a conductance of 3–50 pW/K for crossed SWNTs in intimate contact,<sup>22–24</sup> the thermalization time of a 10  $\mu\text{m}$  long SWNT in such cross-contact is  $\sim 0.5\text{--}1\ \mu\text{s}$ . Such values are a reasonable lower bound since the weak intertube van der Waals interactions make intimate contact unlikely and can lead to large intertube contact resistances.<sup>24</sup> For bundle–bundle contact, the thermalization time scales are likely longer since the thermal mass of the bundle can scale faster than the bundle–bundle contact area. The extraction of the heat capacity and the metal–SWNT interface resistances sensitivity are most strongly weighted by the thermal response below 3  $\mu\text{s}$  for these films (Figure 1c). Consequently, the apparent heat capacity can measure a large fraction of nonthermalized SWNTs. However, the apparent heat capacity may potentially change over the longer time scales of the measurement, which can greatly complicate the analysis and interpretation.

Figure 2a plots  $R_{\text{met-SWNT}}$ ,  $R_{\text{sv}}$ , and their sum total,  $R_{\text{tot}}$ , versus the measured effective heat capacity volume fraction,  $\phi$ , for the five metallizations. The error bars capture the uncertainty due to variations in measurement data taken at four different locations on each sample, variations in film physical properties (e.g., film thickness), and the sensitivity to the uniqueness of the fit parameter combinations. While  $R_{\text{met-SWNT}}$  falls in the range of 3.5–9.2  $\text{mm}^2\ \text{K/W}$ ,  $R_{\text{sv}}$  is much larger, ranging between 33–46  $\text{mm}^2\ \text{K/W}$ . The larger values of  $R_{\text{sv}}$  compared to  $R_{\text{met-SWNT}}$  may be due to a variety of contributions including large SWNT–substrate interface resistances, large SWNT volumetric resistances, or an artifact of the effective heat capacity increasing over the longer time scales of the measurement ( $\sim 10\ \mu\text{s}$ ) for which  $R_{\text{sv}}$  is sensitive. Attributing these larger values of  $R_{\text{sv}}$  entirely to  $R_{\text{SWNT,vol}}$  would require a very low value of  $k_{\text{cnt,eff}} \approx 0.3\ \text{W m}^{-1}\ \text{K}^{-1}$ , which would yield an estimate of  $k_{\text{SWNT}} \approx 45\ \text{W m}^{-1}\ \text{K}^{-1}$  based on the effective SWNT volume fraction,  $\phi$ . Although the literature has reported values as low as  $\sim 50\ \text{W m}^{-1}\ \text{K}^{-1}$  for  $k_{\text{SWNT}}$ ,<sup>20</sup> we suggest that given the high quality of the SWNT tubes indicated by the Raman data, a more plausible explanation is that the large  $R_{\text{sv}}$  is dominated by  $R_{\text{SWNT-sub}}$  due to the weak adhesion of the catalyst particles resulting from the “dip-coating” technique. Measurements of similar films<sup>3</sup> that utilized PVD catalyst deposition showed similar values for  $R_{\text{met-SWNT}}$ , but much lower values of  $R_{\text{SWNT-sub}}$  at a lower  $\phi$ .

The observations that the effective SWNT volume fractions are much less (0.5–0.9%) than the nominal volume fraction of 3%, and the trend in the data of decreasing  $R_{\text{met-SWNT}}$  with increasing  $\phi$  suggest that the

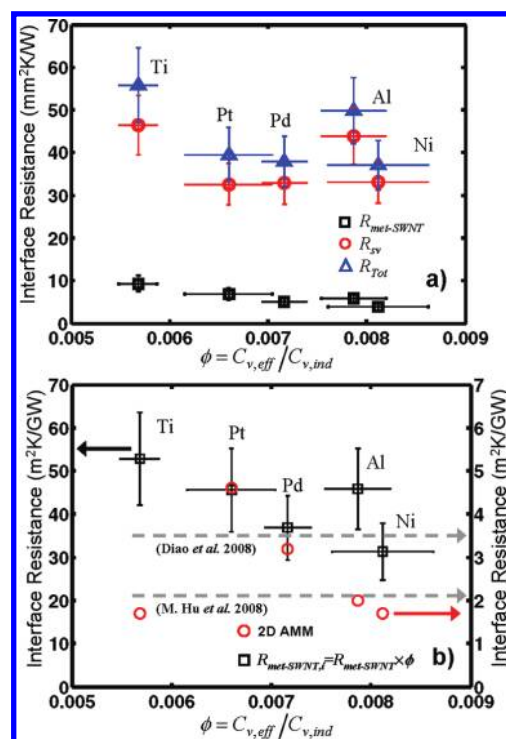


FIGURE 2. (a) Measured area-averaged metal–SWNT, SWNT–substrate, and total thermal resistance plotted as a function of the measured effective SWNT heat capacity volume fraction,  $\phi$ , calculated by dividing the measured effective SWNT volumetric heat capacity  $C_{v,\text{eff}}$  by the volumetric heat capacity of an individual SWNT,  $C_{v,\text{ind}}$ . (b) Estimated resistance of individual metal–SWNT contact extracted by multiplying the area-average metal–SWNT interface resistance by  $\phi$ . Data are compared to theoretical predictions of the individual SWNT interface resistance from molecular dynamics of SWNT–Si interfaces from Hu et al.<sup>25</sup> and Daio et al.<sup>26</sup> (gray dashed arrows) and from the AMM model modified for 2D–2D interfaces.<sup>3</sup> The theoretical values are shown on the right axis for clarity.

large interface resistance in SWNT arrays are due to a low SWNT engagement efficiency with the metal. Sample-dependent nanoscale surface morphologies and differences between the metals’ abilities to coat the SWNTs may explain their relative engagement efficiencies. Previous observations<sup>19,27</sup> showed that the metal–SWNT coating behavior can be strongly dependent on metal–SWNT interaction energies<sup>27</sup> with Ti, Ni, Pd, and Al demonstrating an increasing tendency to cluster on the individual SWNTs. Metals that effectively coat the SWNTs can show reduced engagement due to the lower tendency of the metal to form intertube clusters that can bridge multiple tubes and bundles. This effect can explain the low value of  $\phi$  for Ti compared to other metals since Ti has an excellent ability to coat SWNT and a low tendency to form clusters.

The thermal resistance of an individual SWNT–metal interface,  $R_{\text{met-SWNT,i}}$ , can be estimated from the relation  $R_{\text{met-SWNT,i}} = R_{\text{met-SWNT}} \times \phi$ .<sup>3</sup> Figure 2b shows the relation between  $R_{\text{met-SWNT,i}}$  and  $\phi$ , along with the results of molecular dynamics simulations for the resistance of an individual (10,10) SWNT–Si interface.<sup>25,26</sup> Figure 2b also shows theo-



retical predictions of individual metal–SWNT interface resistances based on a modification of the acoustic mismatch model (AMM) in an approximation treating the SWNT as a graphene–metal 2D–2D interfaces.<sup>3</sup> The AMM model predicts resistances similar to the molecular dynamics (MD) simulations of Si–SWNT interfaces and follows the general data trend with metallization.

The trend of decreasing  $R_{\text{met-SWNT},i}$  with increasing  $\phi$  suggests that the same physical properties that govern the interface resistance (e.g., interface adhesion energies, Debye temperatures, etc.) may be related to the mechanisms that govern the engagement of the metal with the SWNTs.  $R_{\text{met-SWNT},i}$  is about an order of magnitude larger than the theoretical predictions. Nonideal metal–SWNT interface geometries may explain this discrepancy. The bundle structure of the nanotubes can reduce the ratio of the metal–SWNT interface area to the SWNT volume and consequently increase the apparent individual metal–SWNT interface resistance. The models do not account for the likely formation of metal nanoclusters along the SWNTs which creates additional interfaces and modifies the local phonon density of states due to the effects of reduced and mismatched geometries.<sup>28–30</sup> However, the lower interface resistance values predicted by the MD simulations suggest that in addition to improving the engagement, there is the potential to significantly reduce the thermal resistance of SWNT films by reducing the individual metal–SWNT interface resistance.

Figure 3a,b is a plot of the temperature dependence of  $C_{v,\text{eff}}$  and the interface conductance per tube,  $(R_{\text{met-SWNT}} \times \phi)^{-1}$  and  $(R_{\text{sv}} \times \phi)^{-1}$ , between 125 and 300 K for a 10  $\mu\text{m}$  thick SWNT film coated with a 100 nm thick aluminum film. The temperature dependencies of these data can provide information about the phonon conduction physics. Optimal power law fits to the data yield temperature dependencies of  $C_{v,\text{eff}} \sim T^{0.97}$ ,  $(R_{\text{met-SWNT}})^{-1} \sim T^{1.08}$ , and  $(R_{\text{sv}})^{-1} \sim T^{0.85}$ . In considering the phonon properties, the bundling does not influence the temperature dependencies of  $C_{v,\text{eff}}$  since  $k_b T \gg E_{\text{dL}}$ , where  $E_{\text{dL}} \sim 5$  meV is the Debye energy of the intertube coupling modes and  $k_b$  is Boltzman's constant.<sup>31</sup> The SWNT thermal properties are well approximated by those of graphene since  $\theta_{\text{sub}} \ll T$  where  $\theta_{\text{sub}} \sim 10$  K is the characteristic temperature of the first optical sub-band of the SWNT estimated from calculations using the dynamical matrix of a classical potential field.<sup>31,32</sup> Figure 3a compares the measured data to theoretical calculations of the heat capacity of an individual 2 nm diameter SWNT tube using Bose–Einstein statistics based on the above dynamical matrix, and a calculation of the total heat capacity of the acoustic phonon modes in graphene using the band parameters in Prasher et al.<sup>33</sup> Figure 3a shows the individual contribution of the longitudinal acoustic (LA), transverse acoustic (TA), and out-of-plane bending modes (ZA) of graphene to its total heat capacity. Because of the porosity of the SWNT film, the theoretical calculations have been scaled by a factor of 0.006 so that the calculation of the heat capacity matches the

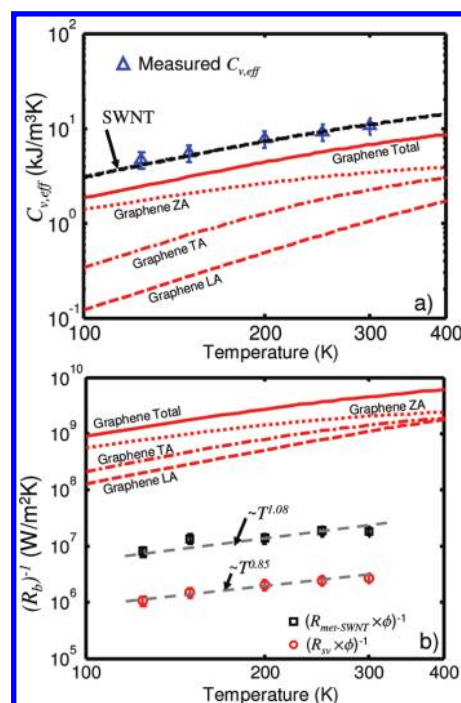


FIGURE 3. (a) Temperature dependence of the area-average metal–SWNT interface and effective  $C_{v,\text{eff}}$  for a 100 nm thick Al-coated SWNT film. The data are compared to theoretical calculation of the heat capacity of an individual SWNT based on Bose–Einstein statistics using a classical potential function<sup>32</sup> (black dashed) and a calculation of the heat capacity of graphene acoustic modes (solid red) based on graphene parameters in Prasher et al.<sup>33</sup> The theoretical predictions have been scaled by a factor of 0.006 so that the value of the data matches the SWNT theoretical results at 300 K. Also shown are the contributions of the graphene longitudinal (LA), transverse (TA), and out-of-plane bending (ZA) acoustic phonon bands to the total graphene heat capacity. (b) Temperature dependence of the conductance of individual SWNT interfaces,  $(R_{\text{met-SWNT}} \times \phi)^{-1}$  and  $(R_{\text{sv}} \times \phi)^{-1}$ . The gray dashed curves are optimal power law fits to the data. The solid red curve is the total theoretical upper bound for the interface conductance of a graphene–metal interface allowing for inelastic scattering. The broken red curves show the contributions from the individual acoustic phonon modes in graphene.

experimental data at 300 K. Note that, despite its empirical nature, the classical potential field<sup>32</sup> reproduces the overall features of the phonon dispersion to an extent sufficient for the current analysis.<sup>34</sup> The temperature dependency of the experimental data follows the theoretical predictions of the heat capacity calculation of the SWNT within the measurement uncertainty. The near identical temperature dependency of the acoustic mode heat capacity of graphene and that of the SWNT suggest that the thermal properties of the SWNT are well captured by phonon physics of graphene in the current temperature range. The calculations show that although the heat capacity is dominated by the ZA mode, the temperature dependency of the LA and TA modes is stronger in this temperature regime, resulting in a temperature scaling of the total heat capacity that is strongly influenced by all modes.

The temperature dependence of  $R_{\text{met-SWNT}}$  yields information about the metal–SWNT phonon interface transmit-

tance. Under the assumption of a small-temperature difference across the interface and isotropic phonon dispersion, the boundary resistance can be expressed as<sup>35,36</sup>

$$R_b^{-1} = \Gamma^{\text{inel}}(T) \sum_s \frac{1}{\Omega_d} \int_{\Omega_d^+} \int_0^{\omega_{\text{max},s}} \hbar \omega v_s(\omega) \cos(\theta) \frac{\partial n}{\partial T} g_s(\omega) d\omega d\Omega_d \quad (1)$$

where  $s$  is the mode branch,  $\omega$  is the phonon frequency,  $v_s(\omega)$  is the phonon velocity,  $n$  is the Bose–Einstein distribution,  $T$  is the temperature,  $g_s(\omega)$  is the phonon spectral density of states,  $\theta$  is the angle between  $\vec{k}$ , the phonon wave vector, and the interface normal,  $\Omega_d$  is the solid angle for  $d$ -dimensional space.  $\Gamma^{\text{inel}}(T)$  is the net phonon transmittance, which allows for implicit inelastic phonon scattering at the interface.<sup>36</sup> The integral is taken over the half space of phonons directed toward the interface ( $\Omega_d^+$ ). To predict the temperature dependency of the interface conductance of the SWNT, we evaluate eq 1 using the acoustic bands of graphene since the temperature dependency of the phonon heat capacity is well approximated by that of graphene for the temperature range in this work (Figure 3a). Evaluating eq 1 from the graphene (SWNT) side of the interface and equating  $\omega_{\text{max},s}$  to the Debye frequencies of the graphene acoustic modes (which are greater than those of Al) implicitly allows for inelastic phonon transmission.<sup>36</sup> Setting  $\Gamma^{\text{inel}}(T) = 1$  provides the upper limit to the total (inelastic and elastic) phonon conductance. Assuming a general dispersion relation of the form  $\omega_s = c_s k^\alpha$  and combining with eq 1 yields

$$R_b^{-1} = \Gamma^{\text{inel}}(T) \sum_s \frac{k_b}{(2\pi)^d} \left(\frac{1}{c_s}\right)^{d-1/\alpha} \left(\frac{k_b T}{\hbar}\right)^{d-1/\alpha+1} \int_{\Omega_d^+} \cos(\theta) d\Omega \times \int_0^{\hbar \omega_{\text{max},s}/k_b T} \frac{x^{d-1/\alpha+2} e^x dx}{(e^x - 1)^2} \quad (2)$$

where  $d$  is the dimension. Figure 3b shows the evaluation of eq 2 using the properties of graphene for the upper bound ( $\Gamma^{\text{inel}}(T) = 1$ ) of the total interface conductance and the individual contributions from the LA, TA, and ZA graphene modes. As with the heat capacity, the interface conductance is dominated by the ZA mode, but the temperature dependency of the LA and TA modes is stronger in this temperature regime, resulting in a temperature scaling of the interface conductance that is strongly influenced by all acoustic modes.

Figure 4 shows the temperature dependence of  $\Gamma^{\text{inel}}(T)$  extracted by dividing the experimental data for the per tube interface conductance by eq 2 evaluated with  $\Gamma^{\text{inel}}(T) = 1$ . A power law fit to the data yields  $\Gamma^{\text{inel}}(T) \sim T^{-n}$  where  $0.4 < n < 0.9$  with an optimal of  $n \sim 0.6$ . Since traditional AMM and

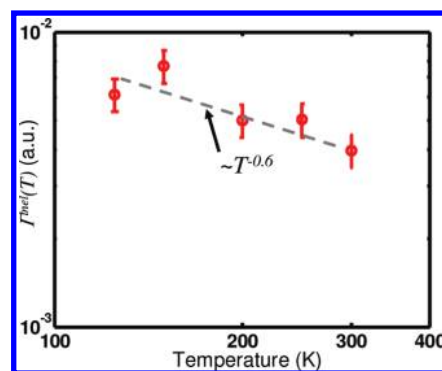


FIGURE 4. Temperature dependence of  $\Gamma^{\text{inel}}(T)$  along with the optimal power law fit (gray dashed). The temperature dependence suggests inelastic phonon scattering at the interface.

diffuse mismatch models (DMM) in the Debye approximation with elastic scattering<sup>37</sup> result in  $\Gamma^{\text{inel}}(T) \sim T^0$  with values on the order of unity, the data suggest that these simpler models do not fully capture the physics of the transport across metal–SWNT interfaces. The low values of  $\Gamma^{\text{inel}}$  may be due to nonideal interface geometry, multiple interfaces in series within the SWNT bundles, and metal clusters along the SWNT amplifying the interface resistance.

The temperature dependence of  $\Gamma^{\text{inel}}(T)$  suggests a spectral dependence of the individual phonon mode transmission coefficients. This dependency may be due to a combination of inelastic phonon scattering at the interface and density of states mismatch between the materials,<sup>38</sup> which can be complicated by the nanoscale geometry,<sup>28–30</sup> and interface disorder.<sup>39</sup> Inelastic interface scattering becomes more important as the temperature approaches the lower Debye temperature of the two materials. Previous measurements of the boundary resistances of Al/sapphire,<sup>40,41</sup> Pb/diamond,<sup>42</sup> and Au/diamond<sup>36,43</sup> all reported near-linear trends in the boundary conductance over similar temperature ranges, which were attributed to inelastic scattering. Hopkins et al.<sup>36</sup> reported a decreasing  $\Gamma^{\text{inel}}(T)$  with increasing temperature due to inelastic scattering. These similar trends in the temperature dependency of  $R_{\text{met-SWNT}}$  and  $\Gamma^{\text{inel}}(T)$  indicates that inelastic scattering may be important at metal–SWNT interfaces.

In summary, we find that the large thermal interface resistances in SWNT films are related to the degree of engagement of the SWNT films and the interface resistances of individual contacts at the nanoscale. The metallization dependence of the SWNT engagement suggest that engineering the CNT interfaces contacts offers a possible approach to reduce the total thermal resistance of CNT films, potentially below 1 mm<sup>2</sup> K/W.

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