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Heat Conduction across Monolayer and Few-Layer Graphenes

Yee Kan Koh,^{*,†,§} Myung-Ho Bae,[†] David G. Cahill,[†] and Eric Pop[‡]

[†]Department of Materials Science and Engineering and Frederick Seitz Materials Research Laboratory, University of Illinois, Urbana, Illinois 61801, United States, [‡]Department of Electrical & Computer Engineering, Micro and Nanotechnology Lab, University of Illinois, Urbana, Illinois 61801, United States, and [§]Department of Mechanical Engineering, National University of Singapore, Singapore

ABSTRACT We report the thermal conductance G of Au/Ti/graphene/SiO₂ interfaces (graphene layers $1 \leq n \leq 10$) typical of graphene transistor contacts. We find $G \approx 25 \text{ MW m}^{-2} \text{ K}^{-1}$ at room temperature, four times smaller than the thermal conductance of a Au/Ti/SiO₂ interface, even when $n = 1$. We attribute this reduction to the thermal resistance of Au/Ti/graphene and graphene/SiO₂ interfaces acting in series. The temperature dependence of G from $50 \leq T \leq 500 \text{ K}$ also indicates that heat is predominantly carried by phonons through these interfaces. Our findings suggest that metal contacts can limit not only electrical transport but also thermal dissipation from submicrometer graphene devices.

KEYWORDS Interfacial thermal conductance, few-layer graphene, metal contacts, acoustic phonons, heat dissipation, thermal management of graphene devices

Graphene, a monolayer or few layers of sp²-bonded carbon atoms, has attracted immense attention over the past few years partly due to the prospect of replacing III–V semiconductors as the workhorse of high-frequency electronics.¹ In addition to superior electrical properties (mobility $\sim 10000 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ at room temperature² on SiO₂ at practical carrier concentrations $\sim 10^{12} \text{ cm}^{-2}$), graphene also has exceptionally high in-plane thermal conductivity^{3,4} on the order $\sim 1000 \text{ W m}^{-1} \text{ K}^{-1}$, which is advantageous for thermal management. High in-plane thermal conductivity, however, implies that heat dissipation from graphenes is also affected by how heat flows across its interfaces.

In this Letter, we report the thermal conductance G of Au/Ti/graphene/SiO₂ interfaces which are typically found in graphene devices,⁵ for number of graphene layers $1 \leq n \leq 10$ and a temperature range of $50 \leq T \leq 500 \text{ K}$. We find $G \approx 25 \text{ MW m}^{-2} \text{ K}^{-1}$ irrespective of n at room temperature and that heat flow across the metal/graphene/SiO₂ interface is limited by G of the metal/graphene interface rather than the graphene/SiO₂ interface. Thus, the choice of metal contacts affects both electrical⁶ and thermal transport⁵ in graphene devices.

While in-plane heat transport in graphene can be attributed to acoustic vibrational modes called phonons,^{4,7} the dominant heat carriers across graphene interfaces in the cross-plane direction are not known. Even under the absence of an external electric field, graphene could have substantial carrier density⁶ on the order of 10^{13} cm^{-2} due to charge transfer

from metal contacts.⁸ Since the density of free carriers (electrons or holes) is high on both sides of the interface, heat transport across a metal/graphene interface could be facilitated by free carriers instead of phonons, analogous to heat transport by electrons across metal/metal interfaces.⁹ Moreover, since carriers in graphene are readily scattered by polar optical phonons (sometimes called remote interfacial phonons or surface-optical phonons) in the SiO₂ substrate,^{2,10} heat transport through graphene/SiO₂ interfaces could have a contribution from direct energy transfer¹¹ between free carriers in graphene and polar optical phonons in SiO₂.

To identify the dominant heat carriers across graphene/metal and graphene/SiO₂ interfaces, we measured the thermal conductance G of Au/Ti/graphene/SiO₂ interfaces over a temperature range of $50 \leq T \leq 500 \text{ K}$. We find that G of such interfaces depends only weakly on temperature above 100 K. The temperature dependence of G is expected to follow the temperature dependence of heat capacity for the excitations that are most responsible for heat conduction.¹² The heat capacity of the degenerate electrons in Au and the heat capacity of optical phonons in SiO₂ increase significantly between 100 and 500 K; the contribution of acoustic phonons to the heat capacity of Au, on the other hand, is essentially constant in this temperature range due to the low Debye temperature of Au. Therefore, we conclude that acoustic phonons are the dominant carriers of heat across these interfaces.

Even when an interface is atomically abrupt, heat transport by phonons across it is limited by the finite probability of phonon transmission; the resulting impedance to heat flow is characterized by a property of an individual interface called the Kapitza thermal conductance,¹² G_i . The total thermal conductance per unit area G of a thin film sand-

* Corresponding author. Email: mpekyk@nus.edu.sg.

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wiched between two solids can often be attributed to the series sum of contribution from two discrete interfaces and the bulk of the thin film.¹³ If this assumption were valid for the case of metal/graphene/SiO₂ interfaces, we could write

$$G^{-1} = (G_1^{-1})_{\text{metal}/n\text{-LG}} + (G_1^{-1})_{n\text{-LG}/\text{SiO}_2} + (h/\Lambda)_{n\text{-LG}} \quad (1)$$

where h and Λ are the thickness and the cross-plane thermal conductivity of n -layer graphene (n -LG), respectively, and h/Λ is the corresponding thermal resistance per unit area. Assuming $\Lambda > 1 \text{ W m}^{-1} \text{ K}^{-1}$, $h/\Lambda < 10^{-9} \text{ m}^2 \text{ K W}^{-1}$ and is negligible compared to G_1^{-1} .

When the film is sufficiently thin, however, phonons (especially long-wavelength phonons) could, in principle, traverse directly between the metal and SiO₂ without being scattered by the interfaces.¹⁴ In such cases, eq 1 is invalid, and we should treat the structure as one diffuse interface instead of two discrete interfaces. Factors dictating at what film thickness eq 1 breaks down are not yet established. However, from our measurements on G of Au/Ti/graphene/SiO₂ interfaces, we find that G remains unchanged for number of graphene layers of $1 \leq n \leq 10$ (equivalent to thickness of $0.4 \leq h \leq 4 \text{ nm}$). Moreover, the measured G is comparable to the G calculated using eq 1 over a temperature range of $50 \leq T \leq 500 \text{ K}$. Thus, our results suggest that, even when the graphene layer is only one atomic layer thick, heat transport across the metal/graphene/oxide interfaces is governed by the thermal conductance of two (metal/graphene and graphene/oxide) uncoupled interfaces. This indicates that heat conduction due to direct transmission of phonons between Au and SiO₂ is negligible.

Our test structures resemble typical metal contacts in graphene devices;⁵ see Figure 1a. Prior to deposition of graphene, we cleaned selected SiO₂/Si substrates by 10 min of sonication in acetone and/or heat treatment at 200 °C in ambient for 1 h; we noticed no difference in the measured G with or without precleaning. We deposited graphene on 104 nm SiO₂ on Si by micromechanical exfoliation¹⁵ from natural graphite. We then annealed the substrate in a chemical vapor deposition (CVD) furnace at 400 °C for 35 min in Ar/H₂ mixture gas to remove the adhesive residue from the tape. We patterned $\approx 100 \text{ nm}$ thick Au pads on selected graphene flakes by e-beam lithography, e-beam evaporation, and lift-off with $\approx 2 \text{ nm}$ Ti predeposited as the adhesion layer. E-beam evaporation was performed at a base-pressure of $7 \times 10^{-7} \text{ Torr}$, and the Au and Ti were deposited at rates of 2.5 and 0.5 Å/s, respectively. Due to low deposition rate of Ti, a significant amount of oxygen could be trapped in the Ti film. We note that even though the metal films were deposited in vacuum, water vapor that adsorbs on the substrate during the air exposure after the annealing step may still be present during the deposition of the Au/Ti contacts. We purposely deposited large metal pads

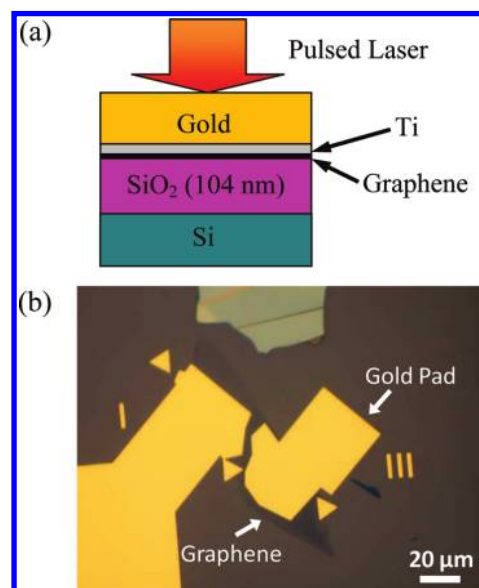


FIGURE 1. (a) Vertical cross section of the samples (not-to-scale). Au(100 nm)/Ti(2 nm) thin metal pads were patterned on graphene flakes on SiO₂ (104 nm) on Si substrate by e-beam lithography. (b) Example optical microscopy image of a graphene sample covered by metal pads.

on our samples such that the same metal pad covers both regions with and without graphene flakes; see Figure 1b. Time-domain thermoreflectance (TDTR) measurements, discussed below, were performed on both regions with and without graphene flakes covered by the same metal pads to derive G of Au/Ti/graphene/SiO₂ interfaces.

Our samples consist of graphenes with number of layers from $1 \leq n \leq 10$, denoted by n -LG (n layers of graphene) throughout this work. We employed a newly developed approach based on Raman spectroscopy¹⁶ to count the number of layers n of the graphene flakes. In this approach, n is determined from the ratio of the integrated intensity of Raman peak at $\sim 520 \text{ cm}^{-1}$ due to scattering by optical phonons in silicon, $I(\text{Si})$, and integrated intensity of G peak due to scattering by doubly degenerate in-plane optical phonons (iTO and LO) in graphene, $I(\text{G})$; see Figure 2a. We validated n derived using this approach by measuring the thickness of the graphenes by atomic force microscopy (AFM); a more complete description of this approach will be published in ref 16. We measure the Raman spectra of graphenes by a custom-built Raman spectrometer; a 488 nm laser beam excites the Raman spectra. We use laser powers of $\approx 1 \text{ mW}$ in our measurements and a $20\times$ objective lens with N.A. = 0.4 to focus the laser beam and collect Raman-scattered light in all polarizations. The full width half-maximum spectral resolution of our Raman setup is $\approx 6 \text{ cm}^{-1}$.

To verify that the graphene flakes are not damaged by deposition of Au/Ti, we coated a monolayer graphene (1-LG) sample with a semitransparent layer of Au (8 nm)/Ti (2 nm) and compared the Raman spectrum of the sample before and after metal deposition; see Figure 2b. We observe

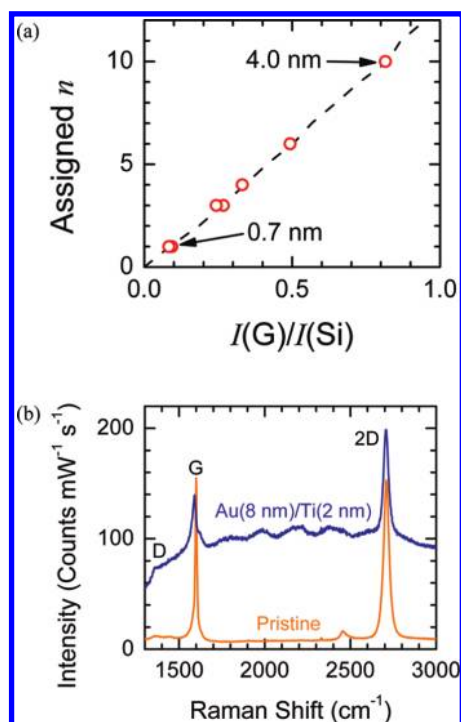


FIGURE 2. (a) Determining graphene layer number (n) from ratios of integrated intensity of the Raman peak due to scattering by optical phonons in silicon, $I(Si)$, and integrated intensity of graphene G peak, $I(G)$. The Raman spectra were acquired using a 488 nm laser. Raman measurements (open circles) are compared to average $I(G)/I(Si)$ values from ref 16 (dashed line) to determine the number of layers n . The thickness of two selected graphene flakes is measured by atomic force microscopy (AFM), as labeled. (b) Raman spectra of monolayer graphene before and after coverage with Au (8 nm)/Ti (2 nm). The spectrum of graphene after metal deposition is vertically down-shifted by 170 counts $mW^{-1} s^{-1}$ for clarity. D peaks (defect-mediated Raman scattering from iTO phonons near the Brillouin zone boundary) are weak in both spectra, indicating that metal deposition does not significantly damage the graphene structure. Metal deposition causes the G peak to split into two slightly broadened peaks centered at 1590 and 1622 cm^{-1} .

a distinct 2D peak (due to two iTO phonons near Brillouin zone boundary) at $2707 cm^{-1}$ with a fwhm of $35 cm^{-1}$ after the deposition of thin metal layers. This narrow 2D peak at $\sim 2700 cm^{-1}$ is a fingerprint¹⁷ of monolayer graphene and indicates that graphene was not significantly damaged by e-beam deposition of the metal film. The D peak (due to one iTO phonon near Brillouin zone boundary and defects) at $\sim 1350 cm^{-1}$ is weak after the metal deposition, suggesting that the density of graphene defects remains low. The G peak is slightly split and broadened after metal evaporation; see Figure 2b. This change of shape is inconsistent with a sharpened, red-shifted G peak due to Landau damping and stiffening of phonons by high carrier concentrations in graphene;¹⁸ we are unsure of the cause of these changes in the shape of the G peak but interactions between the G-band optical phonons in graphene and the electronic excitations of the metal may be playing a role.

We measure the thermal conductance G by time-domain thermoreflectance^{19,20} (TDTR). A schematic diagram of our

equipment is given in ref 20 and our method for data analysis is described in ref 21. In our TDTR measurements, a laser beam from a mode-locked Ti:sapphire laser is split into a pump beam and a probe beam with the relative optical path being adjusted via a mechanical delay stage. The pump beam is modulated at a frequency $f = 10$ MHz. Laser pulses of the pump beam of <1 nJ are absorbed by the Au pads, inducing a temperature oscillation of <10 K at the surface of the Au pads. Cooling of the surface after being heated by pump pulses is then monitored through changes in the intensity of the reflected probe beam using a Si photodiode and a lock-in amplifier. The radii of the laser beams used during the measurements are either 7.5 or $3.8 \mu m$ at the sample surface. We used total laser powers of <10 mW for laser spot size of $7.5 \mu m$ and <45 mW for laser spot size of $3.8 \mu m$, creating temperature rises of <10 K. The ratios of the power of the pump beam to the probe beam vary from 1:1 to 20:1; as expected, we did not observe any difference in the derived G using different power ratios.

To enhance the accuracy of G of Au/Ti/ n -LG/SiO₂ interfaces derived using TDTR, we performed TDTR measurements on adjacent regions with and without graphene flakes for every graphene flake we studied. We compared the ratio of in-phase and out-of-phase of the lock-in amplifier of both measurements to numerical solutions of a thermal model²¹ that takes into account changing of the radius of the pump beam at different relative delay times;²² see Figure 3a. We first take $G = 100 MW m^{-2} K^{-1}$ for Au/Ti/SiO₂ interfaces (this value of G was prior measured using a 500 nm SiO₂ coated with Au/Ti) and lump the uncertainty of TDTR measurements by deriving the thermal conductivity of SiO₂ thin films from initial measurements on regions without graphene flakes. Since the uncertainty should be similar for measurements on adjacent regions with graphene flakes, we then derived G of Au/Ti/ n -LG/SiO₂ interfaces by fitting the second TDTR measurements on regions with graphene flakes using the thermal conductivity of SiO₂ previously derived. The uncertainty of G for Au/Ti/ n -LG/SiO₂ interfaces derived using this approach is $\approx 20\%$. The main contributor to this is the uncertainty ($\approx 35\%$) in G of the Au/Ti/SiO₂ interfaces, which contributes $\approx 12\%$ to the total uncertainty.

We plot G of Au/Ti/ n -LG/SiO₂ interfaces as a function of number of graphene layer n in Figure 3b. We find that at room temperature $20 < G < 30 MW m^{-2} K^{-1}$ for Au/Ti/ n -LG/SiO₂ interfaces, irrespective of n ; this value of G is a factor of 4 smaller than $G = 100 MW m^{-2} K^{-1}$ directly measured on our control Au/Ti/SiO₂ interfaces; see Figure 3b. Similar values of thermal conductance were reported for Au/SAM/GaAs interfaces,²³ in which a self-assembled monolayer (SAM) of alkanedithiols is sandwiched between Au and GaAs.

We note that this relatively high value of G for Au/Ti/ n -LG/SiO₂ interfaces implies that graphene capped with metals cannot be partially suspended between asperities of SiO₂ substrate, which is generally perceived to be the case for uncapped graphenes supported on SiO₂.^{24,25} If the capped

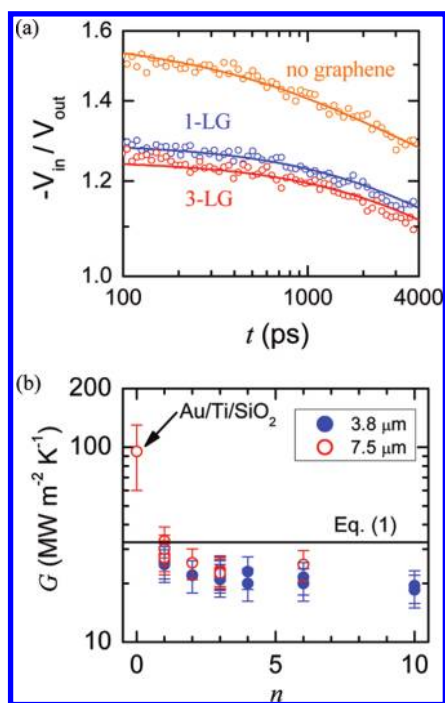


FIGURE 3. (a) Ratios of in-phase and out-of-phase signals (open circles) measured by the lock-in amplifier as a function of delay time t between pump and probe pulses. Measurements on Au/Ti/SiO₂/Si (no graphene), Au/Ti/1-LG/SiO₂/Si, and Au/Ti/3-LG/SiO₂/Si are labeled as “no graphene”, “1-LG”, and “3-LG”, respectively. The monolayer (1-LG) and trilayer (3-LG) graphenes are deposited on the same substrate and covered with metal pads under the same conditions, as shown in Figure 1b. The solid lines are calculations of a thermal model. (b) Thermal conductance G per unit area of Au/Ti- n -LG/SiO₂ measured by TDTR using laser beams with $1/e^2$ spot size of $7.5 \mu\text{m}$ (open circles) and $3.8 \mu\text{m}$ (solid circles) as a function of number of layers n ; $n = 0$ corresponds to G of the Au/Ti/SiO₂ interface. The solid line is a calculation using eq 1. The uncertainty of measurements is $\approx 20\%$.

graphene were suspended between asperities of SiO₂, the contact area between graphene and SiO₂ would be small and the thermal conductance of graphene/SiO₂ interfaces extremely low. For example, if graphenes in our measurements were partially suspended across voids with a contact area of $<10\%$, our measurements indicate that the real thermal conductance of the metal/graphene/oxide is $>250 \text{ MW m}^{-2} \text{K}^{-1}$, inconsistent with our measurement of G of an Au/Ti/SiO₂ interface and prior measurements of $G \approx 85 \text{ MW m}^{-2} \text{K}^{-1}$ for the 1-LG/SiO₂ interfaces²⁶ and $G < 120 \text{ MW m}^{-2} \text{K}^{-1}$ for the metal/graphite interfaces.²⁷ Thus, our results indicate that either the capped graphene conforms²⁸ to the SiO₂ substrate or the voids are filled with water or hydrocarbons that can carry heat across the gap.

Our assertion that the encased graphenes conform to the substrate is reinforced by our time-domain pump-beam-deflection²⁹ (TD-PBD) measurements of the acoustic waves reflected by interfaces with and without graphenes. We find that the shape and amplitude of the acoustic reflections are comparable with and without graphenes. Since voids with zero acoustic impedance should vastly enhance the acoustic reflection, our findings suggest that the area occupied by voids is a small fraction of the total area.

Our values for G of graphene contacts suggest that heat dissipation from graphene field-effect transistors (GFETs) with dimensions $L < 600 \text{ nm}$ will often be affected by the thermal conductance of graphene interfaces. To estimate the importance of graphene interfaces in the thermal management of GFETs supported on SiO₂/Si, we assume that heat is generated at the center of the GFET and can dissipate to the surroundings either through metal contacts or the SiO₂ substrate. The dominant path of heat dissipation is governed by a characteristic length called the thermal healing length^{30,31}

$$l_h = \sqrt{h\Lambda/G} \quad (2)$$

where $h = 0.35 \text{ nm}$ and $\Lambda \approx 1000 \text{ W m}^{-1} \text{K}^{-1}$ are the thickness and in-plane thermal conductivity of monolayer graphene and $1/G = 1/G_{\text{1-LG/SiO}_2} + h_{\text{SiO}_2}/\Lambda_{\text{SiO}_2}$. For monolayer graphene supported on $h_{\text{SiO}_2} = 100$ and 300 nm , $l_h \approx 180$ and 290 nm , respectively. For $L < 2l_h$, heat dissipates from the graphene mainly through the metal contacts; while for $L > 2l_h$, heat dissipates mainly through the SiO₂ substrate. Although most current graphene devices have $L > 2l_h$, the characteristic dimensions of future graphene devices will be reduced $< 2l_h$ leading to heat dissipation mainly through the metal contacts.

To estimate the importance of G compared to other thermal resistances of a GFET, we consider a hypothetical device of length $L = 100 \text{ nm}$ between contacts, width $W = 400 \text{ nm}$, on $h_{\text{SiO}_2} = 100 \text{ nm}$, and $100 \times 400 \text{ nm}^2$ metal contact area. The estimated heat flow resistances through one contact, along the graphene, and through the SiO₂ are $R_C \approx 10^6 \text{ K W}^{-1}$, $R_G \approx 7.1 \times 10^5 \text{ K W}^{-1}$, and $R_{\text{SiO}_2} \approx 2.2 \times 10^6 \text{ K W}^{-1}$, respectively. While heat dissipation from GFETs will depend on the realistic three-dimensional geometry of the device, this simple estimate reveals the heat flow path through the metal contacts could in fact be significant for thermal management of future graphene devices.

To further enhance our understanding of heat conduction across graphene, we measured G of Au/Ti/ n -LG/SiO₂ interfaces over a wide temperature range of $50 \leq T \leq 500 \text{ K}$; see Figure 4. As introduced above, the lack of temperature dependence of G for $T > 100 \text{ K}$ as in Figure 4 supports our assertion that the dominant heat carriers across Au/Ti/ n -LG and n -LG/SiO₂ interfaces are acoustic phonons and not free carriers⁹ or direct coupling¹¹ of free carriers in graphene and optical phonons in SiO₂. Our conclusion that free carriers are not responsible for heat conduction across graphene interfaces is also consistent with an estimate using the interface form of the Wiedemann–Franz law.⁹ For a graphene/metal contact area $A = 100 \mu\text{m}^2$ with an electrical resistance³² $R_e \approx 10 \Omega$, the thermal conductance at room temperature is $G_e \approx LT/(AR_e) \approx 10 \text{ kW m}^{-2} \text{K}^{-1}$ (Lorenz number $L = 2.45 \times 10^{-8} \Omega \text{ W K}^{-2}$), a factor of 1000 lower than the measured lattice thermal conductance of $>10 \text{ MW m}^{-2} \text{K}^{-1}$. In other words, except for superb electrical contacts that are yet to be discovered, heat transport across metal/graphene is predominantly carried by phonons.

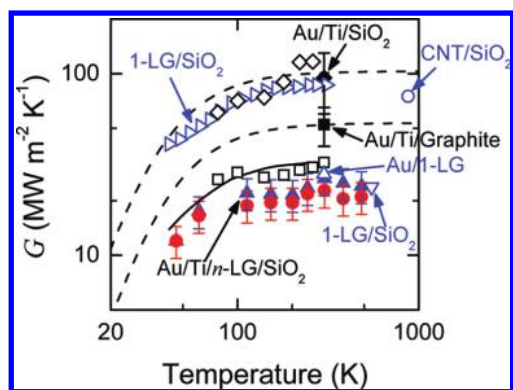


FIGURE 4. Temperature dependence of thermal conductance G of Au/Ti/1-LG/SiO₂ (solid triangles) and Au/Ti/3-LG/SiO₂ (solid circles) interfaces. Thermal conductance of Au/Ti/SiO₂ (solid diamond, this work), Au/Ti/graphite (solid square, this work), 1-LG/SiO₂ from Chen et al. (open right triangles, ref 26) and Freitag et al. (open triangle down, ref 11), Au/1-LG (open triangle up, Cai et al., ref 37), SWCNT/SiO₂ (open circle, Pop et al., ref 31), Au/graphite (open squares, ref 27), and Ti/graphite (open diamonds, ref 27) are included for comparison. SWCNT denotes single-wall carbon nanotube. The dashed lines are diffuse mismatch model¹² (DMM) calculations for G of Au/Ti/SiO₂ (top) and Au/Ti/graphite (bottom) interfaces. The solid line is the prediction of eq 1 using DMM calculations of $G_{\text{Au/Ti/graphite}}$ and measurements of $G_{1\text{-LG/SiO}_2}$ from ref 26. Equation 1 agrees with measurements of Au/Ti/ n -LG/SiO₂ over the entire temperature range.

The reduction of thermal conductance due to the presence of atomic graphitic layers that we observe in Figure 3b could be explained by weaker coupling³³ between metal and oxide. Under this explanation, the metal/graphene/oxide structure is treated as a perturbation that alters the probability for phonons to transmit between metal and oxide, instead of being treated as two discrete interfaces. We argue, however, that this explanation is inadequate especially for thick graphenes of $n = 10$ with layer thickness of ~ 4 nm. Since most heat is carried by phonons with wavelength < 1 nm at room temperature, a 4 nm layer is too thick to be considered a diffuse interface. Moreover, most phonon modes in metal and oxide have relatively low energy (the highest energy of acoustic phonons is 18 and 62 meV in Au and amorphous SiO₂, respectively), but the density of low-energy modes in graphene is small. To give an idea of the density of low-energy modes available in these materials, the ratio of heat capacity of Au, graphite, and SiO₂ at 30 K is 22:1:2.6. Consequently, phonons cannot traverse directly and coherently between metal and oxide.

Instead, we attribute the lower thermal conductance of Au/Ti/ n -LG/SiO₂ interfaces to Kapitza thermal resistance¹² of Au/Ti/ n -LG and n -LG/SiO₂ interfaces acting in series. To test this hypothesis, we compare our measurements to G calculated using eq 1; see the solid line in Figure 3b. In the calculation, we use a prior measurement²⁶ of G of a 1-LG/SiO₂ interface for $G_{1\text{-LG/SiO}_2}$ and approximate $G_{\text{metal/1-LG}}$ from our measurement of G of Au/Ti/graphite interfaces. We find that the calculation of eq 1 is in reasonable agreement with our measurements of G of Au/Ti/ n -LG/SiO₂ interfaces. Our finding suggests that even when graphene is only one atomic

layer thick, heat is carried across the metal/graphene/oxide interfaces by two-stage transmission of acoustic phonons across metal/graphene and graphene/oxide interfaces.

To further support our assertion that heat transport across the interface is dominated by the Kapitza thermal resistance of two graphene interfaces, we compare our G measurements over a wide temperature range to G calculated using eq 1 in Figure 4. In the calculations, we use prior measurements²⁶ of a 1-LG/SiO₂ interface for $G_{1\text{-LG/SiO}_2}$ over the similar temperature range. Since the temperature dependence of G of Au/Ti/graphene is not available, we approximate $G_{\text{metal/1-LG}}$ from G of Au/Ti/graphite interfaces calculated using the diffuse mismatch model (DMM).¹² Our implementation of the DMM calculations is slightly different from the approach described in ref 12, which is derived for G at low temperatures. Following a previous approach to calculations of thermal conductivity²² at high temperatures, we assume a linear dispersion for phonons in Au and set cutoff frequencies using the frequencies of longitudinal and transverse acoustic phonons at the Brillouin zone boundary in the [100] direction; the cutoff frequencies for longitudinal and transverse phonons in Au are 4.4 and 2.8 THz, respectively. We assume that scattering at the interfaces is elastic and allow mode conversion at the interfaces as long as the energy is conserved. We follow ref 12 and approximate the transmission coefficient α of phonons from Au to SiO₂ using

$$\alpha = \frac{I_{\text{SiO}_2}}{I_{\text{SiO}_2} + I_{\text{Au}}} = \frac{(\sum v_j^{-2})_{\text{SiO}_2}}{(\sum v_j^{-2})_{\text{SiO}_2} + (\sum v_j^{-2})_{\text{Au}}} \quad (3)$$

where $I_{\text{Au}} = (\sum v_j^{-2})_{\text{Au}}$ is the sum of v_j^{-2} of all phonon modes j available in the Au side and v_j is the speed of sound of phonons with mode j . We note that I_{Au} depends on the phonon frequency ν due to the cutoff frequencies that we impose. For Au to SiO₂, $\alpha = 0.10$ when $\nu < 2.8$ THz and $\alpha = 0.65$ when $\nu > 2.8$ THz. However, the transmission coefficient of phonons from Au to graphite could not be estimated using eq 3 since graphite is highly anisotropic. We therefore derive the effective $I_{\text{graphite}} = 6.25 \times 10^{-8} \text{ s}^2 \text{ m}^{-2}$ by fitting the calculations to a measurement of $G = 52 \text{ MW m}^{-2} \text{ K}^{-1}$ for an Au/Ti/graphite interface at room temperature; see Figure 4. The derived α for Au to graphite is then $\alpha = 0.04$ when $\nu < 2.8$ THz and $\alpha = 0.40$ when $\nu > 2.8$ THz. Our approach of deriving α from fitting is compatible to the approach by ref 34, which estimates α from the two-dimensional density of states in graphite.

Our measurements of G agree well with the calculations using eq 1 over the entire temperature range, see Figure 4, indicating that heat flow across graphene is governed by the Kapitza thermal conductance of the two interfaces acting in series. Our finding that the bulk of graphene does not significantly contribute to total thermal resistance of graphene in the cross-plane direction is consistent with similar conclu-

sions reached for heat flow across carbon nanotubes,^{31,35} SAMs,²³ and molecular chains,³⁶ which are also limited by interfaces and thus are insensitive to the size of the nanotubes, SAMs, or the molecular chains. Similar results are observed in graphene; see Figure 3b.

In conclusion, we find that heat conduction across metal/graphene/oxide interfaces is limited by finite transmission of phonons between metal and graphene. Thus, for thermal management of graphene devices, metals with high Debye temperature (e.g., Cr, Ni, Ti, Al) could be better choices of metal thermal contacts because of better energy match between phonon modes in these metals and in graphene. Our results enhance the microscopic understanding on heat transport across a single layer of crystalline atoms.

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