

Application of a High-Throughput Analyzer in Evaluating Solid Adsorbents for Post-Combustion Carbon Capture via Multicomponent Adsorption of CO₂, N₂, and H₂O

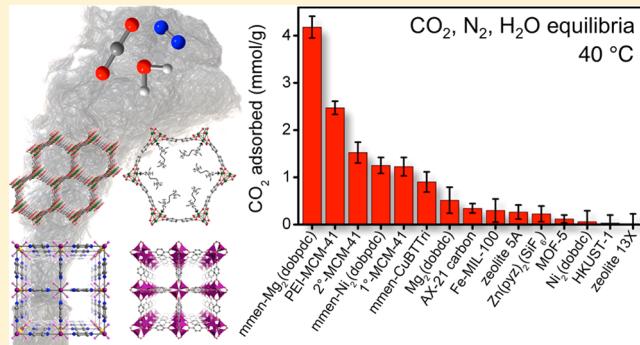
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Supporting Information

ABSTRACT: Despite the large number of metal–organic frameworks that have been studied in the context of post-combustion carbon capture, adsorption equilibria of gas mixtures including CO₂, N₂, and H₂O, which are the three biggest components of the flue gas emanating from a coal- or natural gas-fired power plant, have never been reported. Here, we disclose the design and validation of a high-throughput multicomponent adsorption instrument that can measure equilibrium adsorption isotherms for mixtures of gases at conditions that are representative of an actual flue gas from a power plant. This instrument is used to study 15 different metal–organic frameworks, zeolites, mesoporous silicas, and activated carbons representative of the broad range of solid adsorbents that have received attention for CO₂ capture. While the multicomponent results presented in this work provide many interesting fundamental insights, only adsorbents functionalized with alkylamines are shown to have any significant CO₂ capacity in the presence of N₂ and H₂O at equilibrium partial pressures similar to those expected in a carbon capture process. Most significantly, the amine-appended metal organic framework mmn-Mg₂(dobpdc) (mmn = *N,N'*-dimethylethylenediamine, dobpd⁴⁻ = 4,4'-dioxido-3,3'-biphenyldicarboxylate) exhibits a record CO₂ capacity of 4.2 ± 0.2 mmol/g (16 wt %) at 0.1 bar and 40 °C in the presence of a high partial pressure of H₂O.



INTRODUCTION

In 2012, coal- and natural gas-fired power plants released 11.1 Gt of carbon dioxide—nearly 30% of the total global emissions.^{1,2} While there are more than 68,000 power plants currently in operation, approximately 300 of these plants are directly responsible for an astonishing 10% of the world's CO₂ emissions. Capturing and permanently sequestering this CO₂ would have a significant and immediate impact on rising levels of CO₂ in the atmosphere.^{3,4} With little financial incentive to reduce CO₂ emissions in most countries, however, existing carbon capture technologies are simply too expensive to be practical at the scales required for large power plants that release upward of 40 tonnes of CO₂ per minute.^{4,5} Since the most expensive component of any carbon capture and sequestration process is the separation of CO₂ from the other gases present in the flue gas of a power plant, a large research effort has focused on developing new materials and processes to remove CO₂ from flue gas using as little energy as possible.^{6,7} While the exact composition of a flue gas depends on the design of the power plant and the source of natural gas or coal, a mixture of mostly N₂, CO₂, and H₂O is released at ambient

pressure and 40–80 °C (Table 1).⁸ The effects of potentially more reactive gases that are present in lower concentrations,

Table 1. Expected Range of Compositions for Flue Gas From a Coal- or Natural Gas-Fired Power Plant⁸

	coal	natural gas
CO ₂ (mbar)	120–150	30–50
N ₂ (mbar)	750–800	740–800
H ₂ O (mbar) ⁹	50–140	70–100

such as O₂, SO_x, NO_x, and CO, must also be considered, but, at a minimum, materials are needed that can selectively capture a large amount of CO₂ in the presence of N₂ and H₂O.

Taking advantage of the Lewis acidity of CO₂, Lewis basic aqueous amine solutions have been studied extensively for extracting CO₂ from gas mixtures and are currently used to remove CO₂ from many natural gas streams around the

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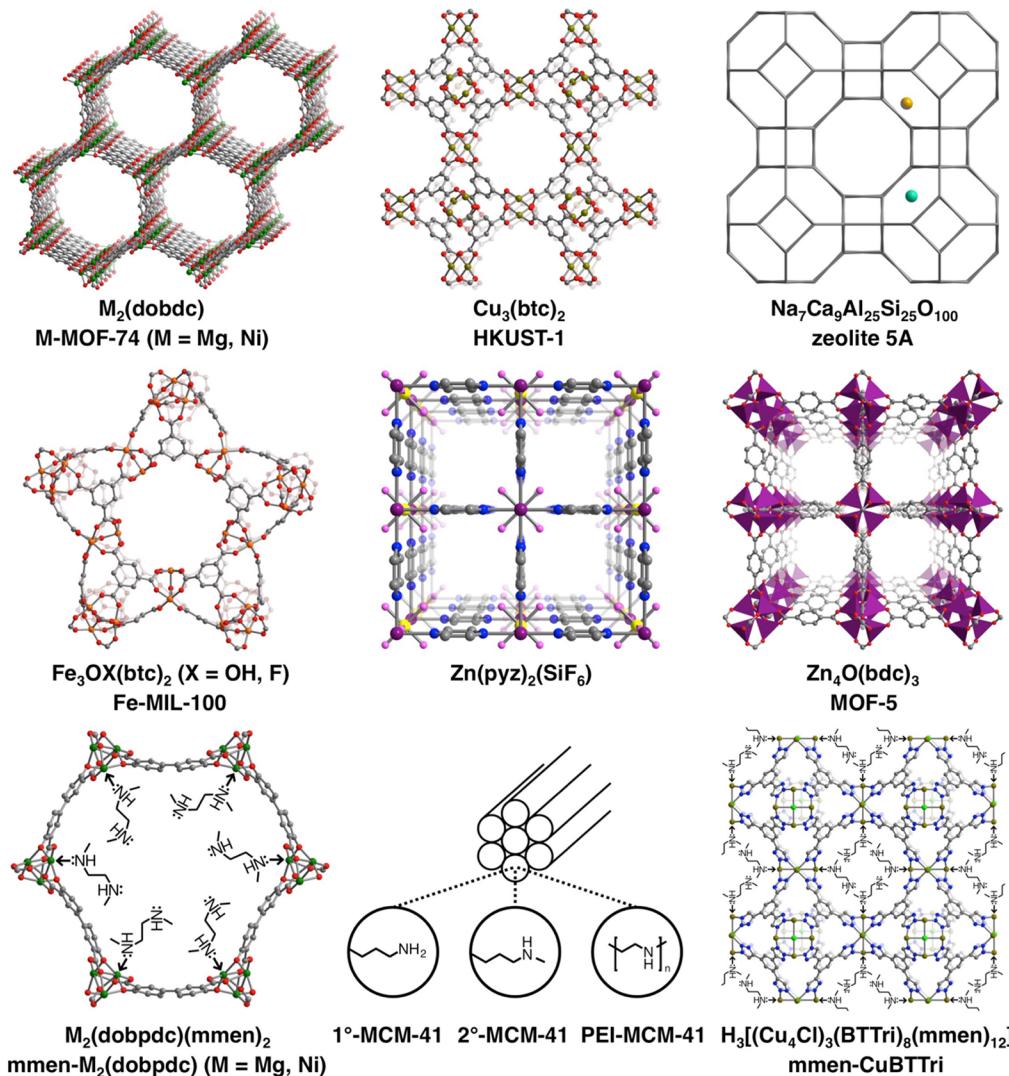


Figure 1. Multicomponent adsorption measurements were performed for mixtures of CO_2 , N_2 , and H_2O in all of the adsorbents shown above as well as zeolite 13X ($\text{Na}_{50}\text{Al}_{50}\text{Si}_{59}\text{O}_{218}$) and an activated carbon (AX-21) that are not pictured. For the metal–organic framework structures, gray, red, blue, dark-yellow, orange, purple, pink, yellow, and bright-green spheres represent C, O, N, Cu, Fe, Zn, F, Si, and Cl atoms, respectively; H atoms have been omitted for clarity. Purple tetrahedra represent Zn atoms, and dark-green spheres represent Mg or Ni atoms. For the zeolite structure (upper right), each vertex represents a tetrahedral SiO_4 or AlO_4 unit, while teal and dark-orange spheres represent typical positions for extra-framework Na and Ca cations, respectively.

world.¹⁰ Aqueous amine scrubbers can also be used to capture high-purity CO_2 from flue gas, but new materials with lower regeneration energy requirements could lead to a significantly lower overall cost for carbon capture.

To this end, solid adsorbents, including zeolites, activated carbons, silicas, and metal–organic frameworks, have received significant attention as alternatives to amine solutions, demonstrating high CO_2 capacities and high selectivities for CO_2 over N_2 , together with reduced regeneration energy penalties.¹¹ It is now well established that adsorbents must contain strong CO_2 binding sites in order to adsorb a significant amount of CO_2 at 50–150 mbar and to achieve the high CO_2 purities necessary for cost-effective sequestration.^{12,13} While many different classes of adsorbents have been studied for CO_2 capture, the most promising materials have typically featured exposed metal cations, exposed anions, or alkylamines, all of which can have strong interactions with CO_2 .¹¹ Despite the large number of adsorbents that have been reported in the context of CO_2 capture, the majority of studies

have relied exclusively on pure CO_2 and N_2 isotherms, which has made it challenging to identify the best materials for capturing CO_2 from an actual flue gas mixture that has a significant amount of H_2O . This is particularly true for metal–organic frameworks and has hindered progress in the field.¹⁴

There have been some noteworthy computational and experimental efforts to evaluate the stability and CO_2 capture performance of metal–organic frameworks under more realistic conditions,^{15,16} but to the best of our knowledge, there are no reports of multicomponent equilibrium adsorption isotherms for mixtures that include CO_2 , N_2 , and H_2O . In any gas separation application, mixed gas equilibrium adsorption data are critical for comparing the performances of different materials, for designing processes, and for validating theoretical models of mixture adsorption.¹⁷ While models such as ideal adsorbed solution theory (IAST) can be used to predict adsorption for simple gas mixtures such as CO_2 and N_2 with reasonable confidence,^{18,19} their accuracy is not well established for more complex mixtures such as CO_2 , N_2 , and H_2O .²⁰ More

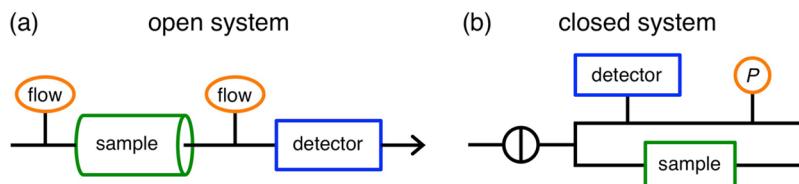


Figure 2. (a) In an open system multicomponent adsorption measurement, a mixture of gases is flowed over a packed bed of adsorbent. The flow rate and composition of the inlet and outlet gas streams are recorded until the composition of the outlet gas stream matches the inlet. (b) In a closed system multicomponent adsorption measurement, a mixture of gases is dosed to a sample and allowed to equilibrate. The amount of each component adsorbed is determined from the equilibrium gas-phase composition and either the equilibrium pressure in a volumetric measurement or the equilibrium weight in a gravimetric measurement.

importantly, all models that rely on single-component adsorption isotherms to predict mixed gas adsorption assume that the adsorbent is in the same thermodynamic state in the presence of each gas. For many adsorbents that exhibit structural or chemical changes specific to different gas molecules, this is most certainly not the case, and direct measurement of mixed gas adsorption is the only way to reliably evaluate gas separation performance.

In contrast to single-component adsorption measurements, which are now carried out routinely and with high accuracy using commercial instruments, mixed gas adsorption measurements are often time-consuming, requiring carefully designed custom equipment and complex data analysis.²¹ As a result, there is a significant lack of mixed gas equilibrium adsorption data reported in the literature.¹⁷ The limited mixed gas adsorption data available are mostly for two-component mixtures in zeolites, and equilibrium adsorption data for mixtures of more than two components are exceedingly rare, even though many industrial gas separations involve multi-component mixtures.^{17a,22}

More routinely, dynamic column breakthrough experiments are used to evaluate the separation performance of an adsorbent by flowing a mixture of gases through a packed bed and measuring the composition of the outlet gas stream as a function of time.²³ It is important to note that a typical breakthrough experiment does not yield equilibrium data, and the relationship between breakthrough results and equilibrium adsorption isotherms is not always clear.^{17c} For instance, nearly all adsorbents will show at least some capacity for capturing CO₂ in a standard breakthrough experiment with a mixture of CO₂, N₂, and H₂O, since the front of the bed will desiccate the incoming gas mixture, leaving just CO₂ and N₂ as the gas flows through the bed.^{24,25} This can lead to misleading conclusions about the intrinsic ability of a material to adsorb CO₂ at a specific partial pressure of H₂O, particularly when experiments are run on a small amount of sample. Indeed, many factors in addition to multicomponent adsorption capacities can influence experimental breakthrough curves, including column size, column shape, gas flow rates, adsorbent packing density, and extra-column effects.²⁶ Because breakthrough experiments mimic the dynamic conditions of a large-scale separation, they can be helpful in developing processes for CO₂ capture. However, multicomponent equilibrium experiments are better suited for comparing the properties of different materials under similar conditions, since the amount of each gas adsorbed is determined only by the partial pressure of each gas and the temperature. Moreover, these equilibrium data can be used to model any dynamic process using local equilibrium theory, where an equilibrium is assumed to exist between the gas and adsorbed phases at every cross-section of an adsorbent bed.

While this assumption is never entirely true, it is a reasonable approximation for many processes and relies on accurate multicomponent equilibrium data.²⁷

Here, we report the design and validation of a high-throughput instrument for the accurate measurement of multicomponent equilibrium adsorption at conditions relevant to post-combustion carbon capture. These measurements are used to compare the performance of 15 different metal–organic frameworks, activated carbons, zeolites, and amine-appended silicas that are representative of the wide range of adsorbents that have been studied for this application (Figure 1).

RESULTS AND DISCUSSION

Multicomponent Adsorption. Although multicomponent adsorption experiments are far less common than single-component experiments in the literature, there has still been significant progress toward developing improved methods for mixed gas measurements. Since it is usually not possible to measure directly the composition of the adsorbed phase, the main challenge in any multicomponent experiment is determining the composition, or relative partial pressures, of the gas phase at equilibrium.^{17,21} The composition of the adsorbed phase, as well as the amounts of each gas adsorbed, can then be calculated as the difference between the amount of each component added to the system and the amount that is still present in the gas phase at equilibrium. A variety of techniques have been developed for this purpose in both open and closed systems, but performing measurements with high enough accuracy to provide meaningful results is not trivial and likely explains the lack of published multicomponent data. Often, the adsorption capacities determined from a multicomponent measurement have such high errors that it is impossible to compare the properties of different materials.²¹ If done accurately, however, any open or closed system measurement should generate equivalent multicomponent adsorption data for a given set of equilibrium conditions. Methods for performing multicomponent measurements have been reviewed thoroughly in the literature,^{17a,b,21,22} but will be briefly summarized here in the context of choosing an appropriate technique for high-throughput multicomponent adsorption measurements of CO₂, N₂, and H₂O mixtures at conditions representative of a power plant flue gas.

In a typical open system experiment, a gas mixture is flowed over a packed bed of adsorbent until the composition of the outlet gas stream is the same as that of the inlet, with a mass spectrometer or gas chromatograph used to record the outlet gas composition (Figure 2a).²⁸ Determining the equilibrium amounts adsorbed of each gas requires the accurate measurement of both the inlet and outlet gas flow rates and compositions as well as appropriate corrections for extra-

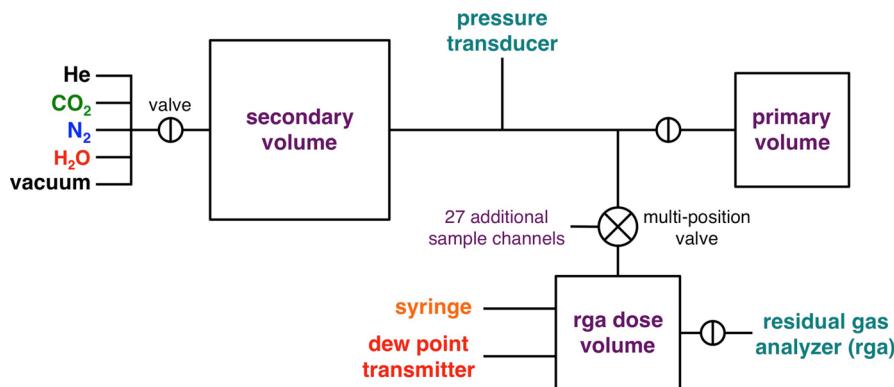


Figure 3. Simplified schematic of the high-throughput instrument used in this work to perform multicomponent adsorption measurements. Twenty-eight independent sample channels share a common gas-dosing manifold and are each connected to the residual gas analyzer (rga) dose volume via a multiposition valve. For multicomponent measurements, a mixture of gases is dosed into the secondary volume and rga dose volume, then expanded to the primary volume, which contains the activated adsorbent. The syringe is cycled multiple times, then the equilibrium pressure is recorded. For mixtures of CO_2 , N_2 , and H_2O , the dew point transmitter is used to record the partial pressure of H_2O , and the rga is used to measure the ratio of the partial pressures of CO_2 and N_2 .

column effects and ensuring that the column is isothermal at equilibrium.²¹ Because the equilibrium gas-phase composition is equivalent to the composition of the inlet gas stream, it is easy to compare the adsorption capacities of different materials under identical equilibrium conditions in an open system multicomponent experiment. Correcting for extra-column effects can, however, be extremely complicated. These corrections are critical to the accuracy of the results, particularly for small sample sizes where the dead volume of the system is not negligible.^{26a} Additionally, it can be challenging to measure the outlet flow rate with high accuracy since the calibration of most flow meters is dependent on the composition of the gas that is flowing through them.^{26b} As a result of these issues, open system measurements often require a large amount of sample in order to collect accurate data, and consequently are not very amenable to high-throughput screening.²¹

Closed system measurements, on the other hand, are typically more accurate, allowing multicomponent experiments to be performed on smaller quantities of sample.²¹ Still, there are significant experimental challenges to using closed systems to measure multicomponent equilibrium adsorption in a high-throughput manner. In a typical closed system experiment, a mixture of gases is dosed to an evacuated sample from a calibrated dosing volume, and the gas-phase composition is recorded once the sample has reached equilibrium (Figure 2b).²⁹ Since equilibration times can often be on the order of hours or even days, a circulation pump, or other gas-mixing device that does not alter the amount of gas inside the closed system, is typically needed.³⁰ Similar to open system measurements, a mass spectrometer or gas chromatograph can be used to measure the composition of the gas phase after equilibrium is reached, but now care must be taken to ensure that the equilibrium conditions are not altered when the gas is analyzed.²¹ The total amount adsorbed can be determined using standard volumetric or gravimetric techniques with calibrated volumes and a pressure transducer or with buoyancy corrections and a balance, respectively. Equilibrium amounts adsorbed can then be determined by material balance using the ideal gas law or an appropriate equation of state.

Unlike in open system measurements, it is often challenging to measure multicomponent adsorption consistently at a specific set of equilibrium conditions in a closed system since

the composition of the dosed gas mixture required to achieve a specific gas-phase composition at equilibrium is difficult to predict.²¹ In spite of this, closed systems are more amenable to automation and to comparing multicomponent adsorption for a large number of samples with high accuracy. More advanced versions of the open and closed multicomponent experiments described here have also been developed, including the zero length column technique,³¹ total desorption analysis,³² *in situ* infrared spectroscopy,³³ and the isotope exchange technique.³⁴ While each of these techniques has certain advantages and disadvantages, none are particularly well suited for high-throughput multicomponent measurements with mixtures of CO_2 , N_2 , and H_2O .

High-Throughput Multicomponent Adsorption Instrument. In this work, a closed system approach was used to develop a high-throughput adsorption instrument that can measure multicomponent adsorption for up to 28 samples at a time (Figure S13). The instrument, built by Wildcat Discovery Technologies Inc., has 28 independent sample channels that share a common gas-dosing manifold with inputs for up to 8 gases, including H_2O (Figure 3). Each sample channel has a calibrated volume ("secondary volume") and a 1000 torr pressure transducer (MKS Seta Model 730 absolute capacitance manometer; accuracy = 0.25% reading), which are contained inside a heated enclosure that is maintained at 40 °C to minimize temperature fluctuation. Each secondary volume is connected via 1/16" stainless steel tubing to a sample chamber ("primary volume"). The secondary volumes are each approximately 21 mL, while the primary volumes are each approximately 14 mL. The secondary volumes are also connected via 1/16" stainless steel tubing to two Valco multiposition valves, with the 28 channels split evenly between the two valves. The multiposition valves allow each of the 28 channels to be independently opened to the shared 14 mL "rga dose volume" (rga = residual gas analyzer), which contains a mass spectrometer (MKS Microvision 2), a dew point transmitter (Vaisala, accuracy = ± 3 °C), and a 170 mL gastight syringe. All gas lines, dosing volumes, and sample volumes can be heated above 40 °C, allowing H_2O dosing pressures of >70 mbar. Custom software allows multicomponent measurements to be performed in a fully automated manner with complete control over all test

parameters. To the best of our knowledge, this is the first instrument reported to be capable of performing high-throughput multicomponent adsorption measurements at equilibrium.

In order to accurately measure the sample mass, activated samples are loaded in tared 4 mL vials inside a glovebox under a N₂ atmosphere. The 4 mL vials are then inserted into aluminum sample assemblies that can each hold up to 7 vials and can be fully sealed while inside the glovebox, with a Schrader valve completing the seal above each sample. The sample assemblies are then transferred to the high-throughput adsorption instrument, and the headspace above each sample is fully evacuated. The instrument then actuates each Schrader valve, opening each sample channel to vacuum. Sample temperatures in the range of 25–150 °C are achieved using heating elements under the sample holders, and temperatures throughout the instrument are continuously recorded by eight thermocouples.

Pure-component adsorption isotherms up to a maximum pressure of 1.2 bar are measured using a standard volumetric technique. To ensure that all volume calibrations, pressure transducer calibrations, thermocouple readings, and adsorption calculations are accurate and that any leak rates are negligible, background adsorption isotherms were measured for empty sample holders on all 28 channels using He, N₂, CO₂, and H₂O (Figure S14). The magnitude of the background adsorption was always found to be <5 μmol. For a typical sample size of 50 mg, this corresponds to a maximum error of <0.1 mmol/g.

All multicomponent measurements in this work were performed for mixtures of CO₂, N₂, and H₂O at 25 or 40 °C. In a typical experiment, H₂O was first dosed repeatedly to each sample. Since the 40 °C saturation pressure of H₂O is just 73.8 mbar, several H₂O doses were needed to ensure a reasonable partial pressure of H₂O at equilibrium.³⁵ Once an adequate amount of H₂O was added, a CO₂ and N₂ mixture of known composition was dosed to each sample. Although it is usually difficult to target specific equilibrium conditions in closed system multicomponent measurements, very similar equilibrium partial pressures could be achieved for each sample by selecting appropriate gas dosing pressures and compositions.

After all gases were dosed, the gastight syringe was cycled at least 15 times over several hours to force the free gas above the sample to mix, ensuring that the entire system was at equilibrium with a uniform gas-phase composition. At equilibrium, a pressure transducer was used to record the total pressure, and the dew point transmitter was used to record the partial pressure of H₂O (Figure S15). Closing the valves between the secondary and primary volumes then isolated each sample, and the ratio of CO₂ to N₂ in the gas phase was determined by sampling from the secondary volume to the rga (Figures S16, S17). Since the rga operates under high vacuum and requires a low inlet pressure, the gas pressure must be lowered significantly prior to sampling. This was accomplished by expanding the gas into a series of large evacuated volumes in order to ensure that the gas-phase composition remained constant.

Before measuring any multicomponent data, empty sample holders were used to check the accuracy of the instrument by dosing known mixtures of CO₂, N₂, and H₂O, cycling the syringe, and using the pressure transducers, dew point transmitter, and rga to measure the partial pressures of CO₂, N₂, and H₂O in the gas phase, just as would be done in a real multicomponent experiment. The calculated partial pressures

were in very good agreement with the expected partial pressures over the full range of conditions targeted for the multicomponent experiments (Figure 4). A detailed error

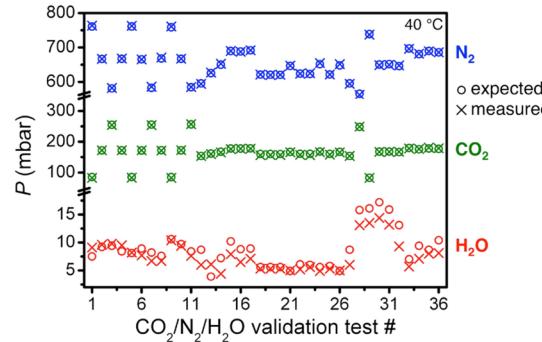


Figure 4. To validate the high-throughput multicomponent adsorption instrument, the experimentally measured partial pressures (crosses) of N₂ (blue), CO₂ (green), and H₂O (red) are compared to the expected partial pressures (circles) of standard gas mixtures dosed into empty sample holders at 40 °C.

analysis can be found in the Supporting Information, but it is worth emphasizing that for just 50 mg of sample, the errors in the amounts of CO₂ and N₂ adsorbed are <0.2 mmol/g at a 95% confidence interval, and the error in the amount of H₂O adsorbed is <0.3 mmol/g.

When drawing conclusions from multicomponent adsorption results, particularly with complex gas mixtures, it is always important to ensure that the system is truly at equilibrium when the amounts of each component adsorbed are determined.^{17a} In order to ensure that the gastight syringe used in this work was cycled enough times to drive the complete system to an equilibrium, multicomponent measurements were performed for two metal–organic frameworks, mmen-Mg₂(dobpdc) (mmen = N,N'-dimethylene diamine, dobpd⁴⁻ = 4,4'-dioxido-3,3'-biphenyldicarboxylate) and mmen-Ni₂(dobpdc), with 0, 5, 10, 15, or 20 syringe cycles and with the samples being fully regenerated between each measurement. The multicomponent results are discussed in detail later, but it is important to note here that the measured amounts of CO₂, N₂, and H₂O adsorbed did not vary within the error of the measurement once the syringe was cycled at least 5 times, demonstrating that the system had reached an equilibrium (Figure 5). As a result, we are confident that all multicomponent results presented in this work represent equilibrium amounts adsorbed, with the only exception being the amine-appended mesoporous silicas that exhibited exceedingly slow kinetics.

While single-component adsorption isotherms can be conveniently shown on two-dimensional plots since the amount adsorbed is only a function of total pressure, a complete description of the three-component adsorption isotherms measured here would require a four-dimensional plot since the amount adsorbed is a function of three partial pressures.²¹ To simplify the presentation of the multicomponent results reported in this work, the amount of CO₂ adsorbed from a mixture of CO₂, N₂, and H₂O is often plotted on the same two-dimensional plot as a single-component CO₂ adsorption isotherm. The single-component isotherm (green circles) effectively represents the amount of CO₂ that would be adsorbed at a given CO₂ partial pressure if N₂ and H₂O had no effect, positive or negative, on CO₂ adsorption. The amount of

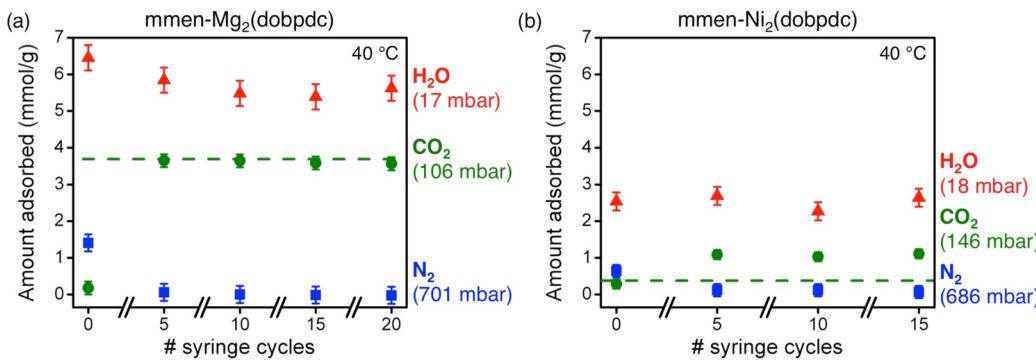


Figure 5. Amount of CO₂, N₂, and H₂O adsorbed for (a) mmn-Mg₂(dobpdc) and (b) mmn-Ni₂(dobpdc) is plotted as a function of the number of times the gastight syringe was cycled to mix the headspace gas during a multicomponent experiment. For each multicomponent measurement, the samples were fully regenerated by heating to 100 °C under vacuum, and all experimental parameters were identical with the exception of the number of syringe cycles. The dashed green lines represent the amount of pure CO₂ adsorbed from a single-component isotherm at the same CO₂ partial pressure as the multicomponent experiment.

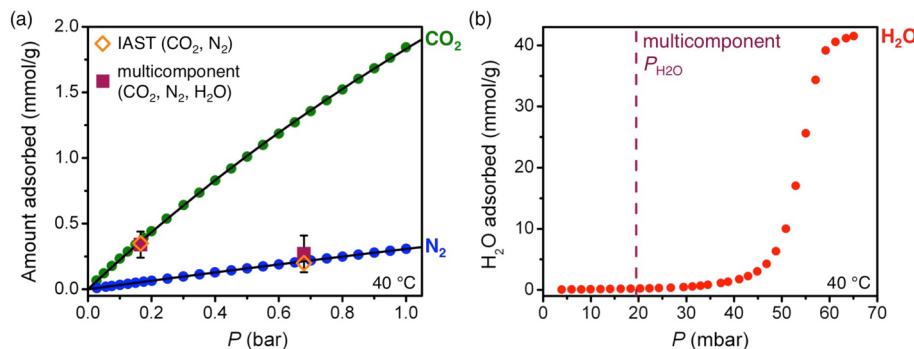


Figure 6. (a) Circles represent single-component CO₂ (green) and N₂ (blue) adsorption isotherms at 40 °C for the activated carbon AX-21. Black lines correspond to single-site Langmuir fits. Square data points represent the amount of CO₂ and N₂ adsorbed from a mixture of CO₂ (166 mbar), N₂ (679 mbar), and H₂O (20 mbar) at 40 °C. Orange diamonds represent the amount of CO₂ and N₂ predicted to be adsorbed by IAST from a mixture of CO₂ (166 mbar) and N₂ (679 mbar). (b) Pure H₂O adsorption isotherm (red circles) for AX-21 at 40 °C. The purple dashed line represents the partial pressure of H₂O in the multicomponent experiment.

CO₂ adsorbed from a mixture of CO₂, N₂, and H₂O is then plotted using a square symbol at the appropriate partial pressure of CO₂, and this value can be easily compared to the pure CO₂ isotherm to gauge the effect of N₂ and H₂O on CO₂ adsorption. The partial pressure of H₂O is indicated by the color of the square data points, with the partial pressure of H₂O increasing from blue to purple to red. For nearly all multicomponent experiments reported here, the equilibrium partial pressure of N₂ is very close to 700 mbar. All error bars shown correspond to ± 1.96 standard deviations (95% confidence interval).

Note that these two-dimensional plots do not include any information about the amount of N₂ or H₂O adsorbed at equilibrium, but these values are included in the Supporting Information. For carbon capture applications, the amount of N₂ adsorbed is needed to determine the purity of captured CO₂, while the amount of H₂O adsorbed is important for evaluating the energy required to regenerate the adsorbent and to compress the CO₂. Except for a few cases discussed below, the multicomponent N₂ adsorption capacities at equilibrium are within error of zero. Before considering N₂ and H₂O adsorption, however, an adsorbent must at least maintain some capacity for CO₂ in the presence of N₂ and H₂O in order to have any use in CO₂ capture. In the following sections, the multicomponent instrument is used to directly measure the amount of CO₂ adsorbed at flue gas-like conditions for

adsorbents with surface chemistries and binding sites representative of the most studied materials for CO₂ capture, including those featuring nonpolar surfaces, exposed metal cations, exposed anions, and alkylamines.

Nonpolar Surfaces. Many high surface area metal–organic frameworks and activated carbons have relatively nonpolar pore surfaces that lack any strong CO₂ binding sites, resulting in materials with little affinity for CO₂ at low pressures. For instance, Zn₄O(bdc)₃ (bdc²⁻ = 1,4-benzenedicarboxylate; MOF-5)³⁶ and the activated carbon AX-21 (Maxsorb)³⁷ have Langmuir surface areas of 3995 and 4880 m²/g but adsorb only 0.1 mmol/g (0.4 wt %) and 0.3 mmol/g (1.3 wt %) of CO₂ at 0.15 bar and 40 °C, respectively. Although many adsorbents have significantly higher 0.15 bar CO₂ capacities, most materials with nonpolar surfaces are relatively hydrophobic, and as a result, they have attracted some interest for post-combustion carbon capture.^{11a,38,39}

As is the case for many activated carbons, AX-21 has a classical type V H₂O isotherm at 40 °C; there is negligible H₂O adsorption on its hydrophobic pore surface until pressures above 45 mbar, at which point clustering of H₂O molecules on the surface leads to a sharp increase in the amount of H₂O adsorbed (Figure 6b).^{40,41} As long as the partial pressure of H₂O is kept below 45 mbar ($p/p_0 = 0.61$), H₂O adsorption should be negligible and would not be expected to interfere with CO₂ adsorption. To confirm this, a multicomponent

Table 2. Physical Properties of CO₂, N₂, and H₂O^{17a}

	CO ₂	N ₂	H ₂ O
kinetic diameter (Å)	3.3–3.9	3.64–3.80	2.64
polarizability ($\times 10^{-25}$ cm ³)	26.5	17.6	14.5
dipole moment ($\times 10^{18}$ esu·cm)	0	0	1.87
quadrupole moment ($\times 10^{-26}$ esu·cm ²)	4.30	1.52	—

adsorption experiment was performed for a mixture of CO₂, N₂, and H₂O in AX-21 at 40 °C and equilibrium partial pressures of 166, 679, and 20 mbar, respectively (Figure 6a). As expected, no H₂O is adsorbed under these conditions, and the amount of CO₂ adsorbed is 0.3(1) mmol/g, within error of the amount adsorbed from pure CO₂ at the same pressure. Moreover, the experimental amounts of CO₂ and N₂ adsorbed in the presence of H₂O match IAST predictions for a binary mixture of just CO₂ and N₂.

While AX-21 has some capacity for CO₂ and negligible H₂O adsorption under these conditions, it has very poor CO₂/N₂ selectivity with nearly the same amount of N₂ adsorbed as CO₂. It is also important to note that the partial pressure of H₂O in 40 °C flue gas is nearly 70 mbar, so the flue gas would likely need to be dried to below 45 mbar for H₂O adsorption to remain negligible. There may, however, be other adsorbents with type V H₂O isotherms at 40 °C that have a step closer to 70 mbar. Regardless, materials with higher selectivities for CO₂ over N₂ and higher CO₂ capacities at 0.15 bar will require stronger adsorption sites than are likely to be found in adsorbents with entirely nonpolar surfaces. Since minimizing H₂O adsorption is important to lowering the regeneration energy in a carbon capture process, designing adsorbents that have both hydrophobic surfaces and strong CO₂ binding sites is a key challenge in developing a next generation of carbon capture materials.

Exposed Metal Cations. Owing to its larger quadrupole moment and greater polarizability (Table 2), CO₂ will have a stronger electrostatic interaction than N₂ with an exposed partial charge. By incorporating metal cations with open coordination sites into metal–organic frameworks and zeolites, exposed positive charges can be created that act as strong CO₂ adsorption sites,^{42,43} leading to materials with some of the highest reported 0.15-bar capacities for CO₂ and selectivities for CO₂ over N₂. In many zeolites, exposed positive charges result from extra-framework cations that are present in the pores to balance the negative charge generated from replacing a fraction of the Si⁴⁺ cations in pure silica zeolites with Al³⁺. Zeolite 13X (NaAlSi_{1.18}O_{4.36}; FAU, Na-X) and zeolite 5A (Na_{0.28}Ca_{0.36}AlSiO₄; LTA, Ca-A), for instance, feature extra-framework Na⁺ and/or Ca²⁺ cations that strongly adsorb CO₂.⁴⁴ For certain metal–organic frameworks, exposed metal cations can be generated directly on the framework by postsynthetically removing metal-bound solvent molecules. Exposed Mg²⁺, Ni²⁺, Cu²⁺, and Fe³⁺ cations of this type are present in Mg₂(dobdc) (dobdc⁴⁻ = 2,5-dioxido-1,4-benzenediacarboxylate; Mg-MOF-74, CPO-27-Mg),^{43,45} Ni₂(dobdc) (Ni-MOF-74, CPO-27-Ni),⁴⁶ Cu₃(btc)₂ (btc³⁻ = 1,3,5-benzene-tricarboxylate; HKUST-1),⁴⁷ and Fe₃OX(btc)₂ (X = OH, F; Fe-MIL-100),⁴⁸ respectively.

Zeolites 5A, 13X, and M₂(dobdc). Zeolite 5A adopts the LTA (Linde Type A) structure type, wherein sodalite cages are connected via square faces to form a three-dimensional cubic framework of 4.2 Å diameter pores. Extra-framework Na⁺ and Ca²⁺ cations are located at the six-ring windows (Si_nAl_{6-n}O₆) of

the sodalite cages.⁴⁹ Zeolite 13X adopts the FAU (faujasite) structure type, wherein sodalite cages are connected via hexagonal faces to form a three-dimensional cubic framework of 7.4 Å diameter pores. Extra-framework Na⁺ cations are located primarily above the plane of the four-ring and six-ring windows of the sodalite cages.⁵⁰ In contrast to zeolites 5A and 13X, the exposed metal cations in the metal–organic frameworks Mg₂(dobdc) and Ni₂(dobdc) are part of the framework structure, in which helical chains of square pyramidal Mg²⁺ or Ni²⁺ cations, respectively, are bridged by dobdc⁴⁻ ligands to form 12 Å hexagonal channels (Figure 1).

Because of their high density of exposed metal cations, Mg₂(dobdc), Ni₂(dobdc), zeolite 13X, and zeolite 5A each adsorb over 3.1 mmol/g (12 wt %) of CO₂ at 0.15 bar and 40 °C and have been extensively studied for carbon capture applications (Figure 7).^{12a,b,16a,c–e,43,44,51} In fact, the 5.3

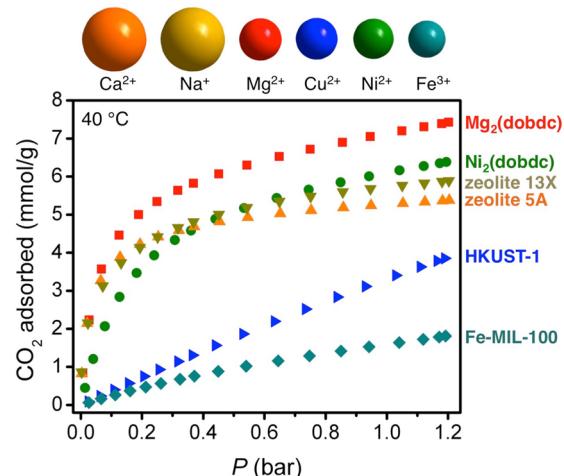


Figure 7. Pure CO₂ adsorption isotherms at 40 °C for metal–organic frameworks and zeolites that feature exposed Ca²⁺, Na⁺, Mg²⁺, Cu²⁺, Ni²⁺, or Fe³⁺ cations.

mmol/g (18.9 wt %) of CO₂ adsorbed by Mg₂(dobdc) at 0.15 bar and 40 °C is the highest uptake reported for any solid adsorbent under these conditions.^{11d} While the majority of studies on the carbon capture potential of metal–organic frameworks and zeolites with exposed metal cations have relied exclusively on single-component CO₂ and N₂ adsorption isotherms, there has been some work toward understanding the effect of H₂O on CO₂ capacity and selectivity.

Not surprisingly, DFT calculations have shown that H₂O, with its strong dipole moment, is expected to have a much greater affinity than CO₂ for exposed metal cation adsorption sites.⁵² Several experimental studies have used binary adsorption measurements for mixtures of CO₂ and H₂O in zeolites 13X and 5A to show that CO₂ adsorption is indeed significantly reduced at low partial pressures of H₂O.⁵³ While initial breakthrough studies suggested that H₂O did not adversely affect the adsorption properties of Mg₂(dobdc),^{51a}

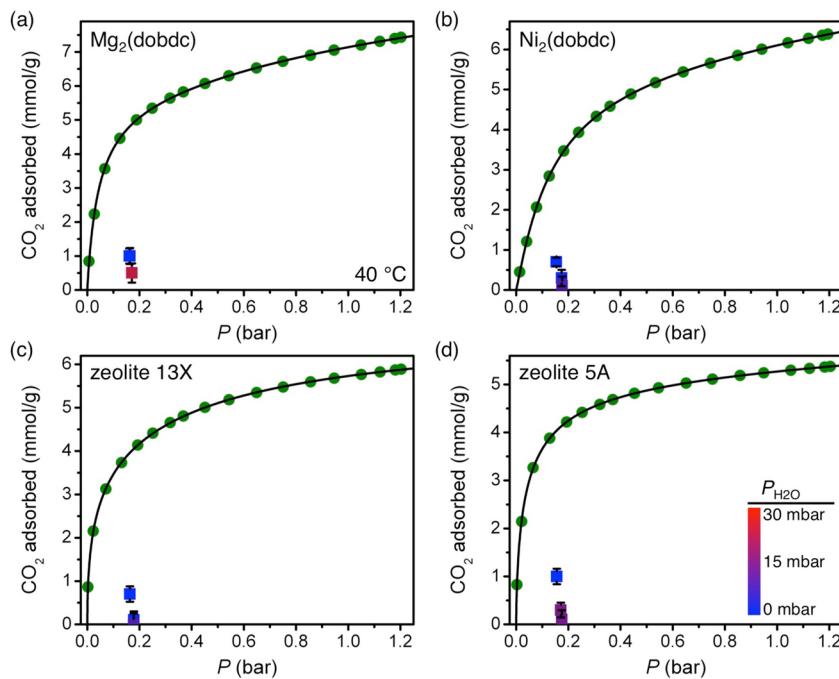


Figure 8. A summary of multicomponent equilibrium measurements at 40 °C for (a) Mg₂(dobdc), (b) Ni₂(dobdc), (c) zeolite 13X, and (d) zeolite 5A. Green circles represent pure CO₂ adsorption isotherms for each compound, and black lines are the corresponding single- or dual-site Langmuir fits. Square data points represent the amount of CO₂ adsorbed from a mixture of CO₂, N₂, and H₂O, and the color of the square indicates the equilibrium partial pressure of H₂O, with the partial pressure of H₂O increasing from blue to purple to red. The exact values of $P_{\text{H}_2\text{O}}$ can be found in Table S3. For all multicomponent data points, the partial pressure of N₂ is 680–700 mbar.

this was eventually challenged by two experimental studies that showed a significant decrease in the pure CO₂ adsorption of Mg₂(dobdc) and Ni₂(dobdc) after exposure to mixtures containing CO₂ and H₂O.^{16d,e} Additionally, the amount of CO₂ adsorbed at 25 °C was measured for Ni₂(dobdc) at different H₂O loadings, revealing a continuous decrease in CO₂ adsorption with increasing H₂O loading.^{16c}

Under dynamic breakthrough conditions, a recent study found that Ni₂(dobdc) retained a CO₂ capacity of 2.2 mmol/g (8.8 wt %) in the presence of a 15:85 mixture of CO₂:N₂ with 3% RH (0.95 mbar H₂O) at 25 °C and a total pressure of 1 bar.⁵⁴ Based on these results, it was suggested that Ni₂(dobdc) could be used for CO₂ capture from flue gas, provided a desiccant was used to pre-dry the gas to around 1 mbar of H₂O. We note, however, that this measurement was not performed under equilibrium conditions, and that the average partial pressure of H₂O in the bed at the time of CO₂ breakthrough was likely significantly below 1 mbar. Since the column was only cycled three times, these experiments may not adequately capture the expected buildup of bound H₂O over time, particularly if the H₂O adsorption front remained close to the column inlet in each experiment.²⁵ Moreover, the CO₂ breakthrough capacity will be highly dependent on the exact set of dynamic conditions used, and the results may not necessarily translate to larger scales. As an alternative, multicomponent experiments can be used to directly evaluate the effects of different partial pressures of H₂O on CO₂ capacity at equilibrium conditions similar to those expected in an actual CO₂ capture process.

In this work, three-component adsorption measurements were performed with mixtures of CO₂, N₂, and H₂O at 40 °C for Mg₂(dobdc), Ni₂(dobdc), zeolite 13X, and zeolite 5A, and all results clearly show a significant decrease in the amount of

CO₂ adsorbed in the presence of N₂ and H₂O (Figure 8). In fact, the amount of CO₂ adsorbed in all four materials decreases to <25% of the pure-component value at H₂O partial pressures of <2 mbar. The multicomponent results for zeolites 13X and 5A are in excellent agreement with previously reported binary adsorption equilibria for mixtures of CO₂ and H₂O at similar conditions.^{53b} The multicomponent result for Ni₂(dobdc), however, differs significantly from the amount of CO₂ adsorbed in the previously reported breakthrough experiment, where a substantial CO₂ capacity was still observed at a low partial pressure of H₂O.⁵⁴ These conflicting results can be attributed to the fact that the breakthrough experiment was performed under dynamic conditions with the adsorbent exposed to a range of H₂O partial pressures below 1 mbar, while the multicomponent experiment was at equilibrium.

At even higher H₂O partial pressures of 10–25 mbar, which are still well short of the >70 mbar expected in a flue gas, all four of these materials have high H₂O adsorption and a negligible CO₂ capacity, directly confirming that H₂O fully outcompetes CO₂ for the exposed metal cations under equilibrium carbon capture conditions (Figure 8). In order for any of these materials to be used in a carbon capture process, the flue gas would need to be dried significantly. While part of the adsorbent bed could be sacrificed to dry the incoming flue gas rather than capture CO₂,²⁴ this would almost certainly be more expensive than processes based on materials that can selectively capture CO₂ in the presence of high partial pressures of H₂O.

On a more fundamental level, it is worth mentioning that previous *in situ* diffraction studies of CO₂ adsorption in zeolite 5A found that, in addition to exposed Na⁺ and Ca²⁺ cations, CO₂ is also strongly adsorbed at the center of eight-ring windows ($\text{Si}_n\text{Al}_{8-n}\text{O}_8$) because of several close interactions

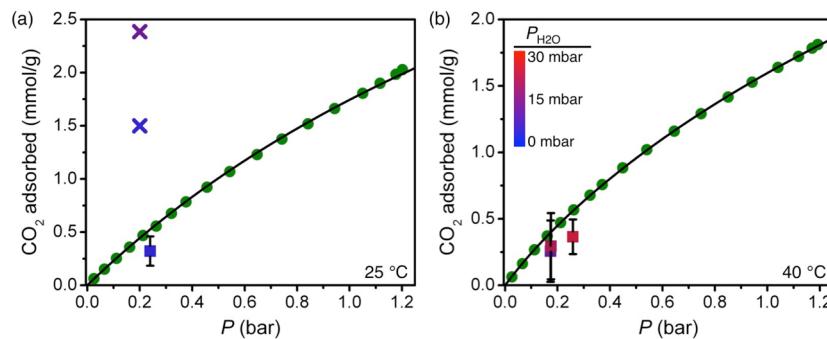


Figure 9. A summary of CO_2 , N_2 , H_2O multicomponent equilibrium measurements for Fe-MIL-100 at (a) 25°C and (b) 40°C . Green circles represent pure CO_2 adsorption isotherms at each temperature, and black lines are the corresponding dual-site Langmuir fits. Square data points represent the amount of CO_2 adsorbed from a mixture of CO_2 , N_2 , and H_2O , and the color of the square indicates the equilibrium partial pressure of H_2O . The exact values of $P_{\text{H}_2\text{O}}$ can be found in Table S3. Crosses represent the amount of CO_2 adsorbed at 25°C and 6.3 mbar of H_2O (blue) or 12.7 mbar of H_2O (purple), as determined from previous breakthrough experiments.⁵⁸

between CO_2 and zeolite O atoms.^{44c} It had been suggested that these eight-ring sites, which were also shown to strongly adsorb CO_2 in the Chabazite-type zeolite Cu-SSZ-13, may still be able to bind CO_2 in the presence of H_2O ,⁵⁵ but the multicomponent results do not support this. Additional diffraction studies are needed to probe whether the lack of CO_2 adsorption in the presence of H_2O is due to H_2O binding directly to the eight-ring sites preferentially over CO_2 or due to H_2O adsorption at the exposed metal cations blocking access of CO_2 to the eight-ring sites.

HKUST-1. The metal–organic framework HKUST-1 is composed of Cu_2 -paddlewheel units bridged by 1,3,5-benzenetricarboxylate to form a cubic structure with three types of microporous cages (Figure 1).⁴⁷ Although the exposed Cu^{2+} cations in HKUST-1 have a weaker interaction with CO_2 than the exposed Na^+ and Ca^{2+} cations of zeolites 13X and 5A or the exposed Mg^{2+} and Ni^{2+} cations of $\text{M}_2(\text{dobdc})$,⁵⁶ with just 0.6 mmol/g (2.6 wt %) of CO_2 adsorbed at 0.15 bar and 40°C , previous experimental and theoretical studies found an increase in the amount of CO_2 adsorbed at low loadings of H_2O .^{16b} More specifically, the amount of CO_2 adsorbed at 25°C was shown to increase by roughly 160%, from 2.2 mmol/g (8.8 wt %) at 0.29 bar to 3.6 mmol/g (13.7 wt %) at 0.24 bar when 2.3 mmol/g of H_2O was pre-adsorbed (0.46 H_2O molecules per Cu^{2+} site). This increase was attributed to a stronger electrostatic interaction between Cu-bound H_2O and CO_2 than between exposed Cu^{2+} cations and CO_2 .^{16b} A later study on a pelletized sample of HKUST-1 also found an increase in CO_2 adsorption at low H_2O loadings, albeit to a much smaller extent.^{16c}

In this work, multicomponent measurements were used to measure the CO_2 capacity of HKUST-1 at conditions more representative of a post-combustion flue gas (Figure S8). Interestingly, we do not observe a significant change in the amount of CO_2 adsorbed by HKUST-1 at 40°C with 1.9(3) mmol/g of H_2O adsorbed (0.38 H_2O per Cu^{2+} ; $P_{\text{H}_2\text{O}} = 0.001$ bar) and CO_2 and N_2 partial pressures of 0.161 and 0.686 bar, respectively. Because of the error in the multicomponent CO_2 adsorption uptake, it is not possible to distinguish between a moderate increase in CO_2 adsorption of up to 0.3 mmol/g and a slight decrease of up to 0.1 mmol/g from the pure-component capacity of 0.6 mmol/g based on this single measurement. Somewhat unexpectedly, we still observe the same amount of CO_2 adsorbed at an even higher equilibrium

H_2O loading of 7.7 mmol/g (1.54 H_2O per Cu^{2+} ; $P_{\text{H}_2\text{O}} = 0.004$ bar), which is well past the point at which all Cu^{2+} sites should be saturated with H_2O . This could be explained by the fact that two strong CO_2 adsorption sites exist in HKUST-1: at the exposed Cu^{2+} cations (5.0 mmol/g) and at the center of the windows of the small octahedral cages (3.3 mmol/g).^{51c} It is possible that CO_2 has a strong interaction with Cu-bound H_2O as was previously suggested; however, it seems more likely that, provided the CO_2 binding energy at each site is similar, the constant CO_2 capacity at H_2O loadings below 8 mmol/g is due to CO_2 adsorption still occurring at the window sites even as H_2O begins to block the exposed Cu^{2+} cations. Regardless, at higher H_2O partial pressures closer to the 0.075 bar expected in flue gas, all strong CO_2 binding sites are likely occupied or blocked by adsorbed H_2O molecules, and HKUST-1 has a negligible CO_2 capacity. This result is in agreement with previous binary measurements performed at 25°C .^{16c,25}

Fe-MIL-100. The metal–organic framework Fe-MIL-100 is composed of μ_3 -O-centered trinuclear iron(III) clusters that are bridged by 1,3,5-benzenetricarboxylate to form a three-dimensional network of supertetrahedra, wherein microporous windows provide entrances to mesoporous cages (Figure 1).⁴⁸ While one-third of the Fe^{3+} cations are ligated by a charge-balancing OH^- or F^- anion, bound solvent can be removed from the remaining Fe^{3+} centers during activation to give five-coordinate exposed metal cations.⁵⁷ Intriguingly, it was reported that the amount of CO_2 adsorbed at 25°C from a mixture of CO_2 , N_2 , and H_2O at 20% RH (6.3 mbar H_2O) or 40% RH (12.7 mbar H_2O) increased 3-fold or 5-fold, respectively, from the pure CO_2 capacity.⁵⁸ This dramatic increase in CO_2 uptake was determined from a breakthrough-type experiment after pre-equilibrating Fe-MIL-100 with H_2O vapor and was tentatively attributed to the formation of microporous pockets created by partial H_2O filling of the mesoporous cages. Even more surprisingly, the CO_2 adsorption enthalpy at 40% RH was determined using microcalorimetry to be just -1 kJ/mol, which was believed to be the result of endothermic H_2O desorption offsetting exothermic CO_2 adsorption.

Because of the significance of these results, we attempted to reproduce this increase in CO_2 adsorption under equilibrium conditions. After synthesizing Fe-MIL-100 and confirming that the surface area and 25°C CO_2 adsorption isotherm matched those previously reported (Figures S7, S9), multicomponent measurements were performed at both 25 and 40°C and at

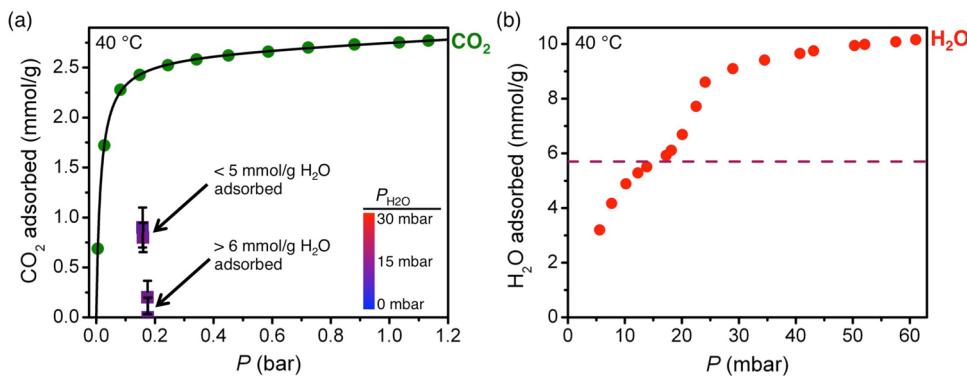


Figure 10. (a) A summary of CO_2 , N_2 , H_2O multicomponent equilibrium measurements for $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ at 40°C . Green circles represent a pure CO_2 adsorption isotherm, and the black line is the corresponding dual-site Langmuir fit. Square data points represent the amount of CO_2 adsorbed from a mixture of CO_2 , N_2 , and H_2O , and the color of the square indicates the equilibrium partial pressure of H_2O . The exact values of $P_{\text{H}_2\text{O}}$ can be found in Table S3. (b) Pure H_2O adsorption isotherm (red circles) for $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ at 40°C .

different partial pressures of H_2O . Regardless of whether the measurement was at 25 or 40°C , we consistently observe a slight decrease in the amount of CO_2 adsorbed in the presence of N_2 and H_2O , even at equilibrium partial pressures that are nearly identical to the previously reported breakthrough conditions (Figure 9). Note that the crosses in the 25°C multicomponent plot of Figure 9 represent the previously reported CO_2 breakthrough capacities.⁵⁸ Further work is necessary to determine the origin of these conflicting results and to establish why a 5-fold increase in CO_2 adsorption might be observed under dynamic conditions, but not at equilibrium.

Exposed Anions. Exposed negative charges are much less common in metal–organic frameworks than exposed positive charges, but just as a positive charge can attract the electronegative O atoms of CO_2 , a negative charge can attract its electropositive C atom.⁵⁹ The compound $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ provides an important example of a three-dimensional framework with exposed anions. Its structure is composed of square grids of Zn^{2+} and pyrazine pillared by hexafluorosilicate (SiF_6^{2-}) anions to form one-dimensional channels that have a 3.8 \AA diagonal dimension (Figure 1).⁶⁰ Although the octahedral Zn cations are coordinatively saturated, the combination of small pores and exposed F^- anions that protrude from the corners of each channel leads to strong CO_2 adsorption at low pressures, with a low-coverage heat of adsorption of -45 kJ/mol and a capacity of 2.4 mmol/g (9.6 wt %) at 40°C and 0.15 bar . Even more significantly, breakthrough experiments performed for a mixture of 10% CO_2 in N_2 at 74% RH ($23.5\text{ mbar H}_2\text{O}$) at 25°C suggested that H_2O has a negligible effect on the ability of the material to adsorb CO_2 selectively at high capacity.^{59a}

In this work, multicomponent experiments were used to compare the equilibrium capacity and selectivity of $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ for CO_2 in the presence of N_2 and H_2O to the earlier breakthrough results. Toward this end, a sample of $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ was synthesized, and the resulting CO_2 adsorption isotherms were found to be in close agreement to those previously reported (Figure S11). While previously reported variable temperature powder X-ray diffraction experiments indicated that $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ was stable to 250°C under vacuum,^{59a} our thermogravimetric analysis results show rapid thermal decomposition occurring above 115°C (Figure S12), which is in agreement with the initial report on the thermal stability of $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$.⁶⁰ The reasons for these

differences are not clear, but this low thermal stability could be problematic for designing a temperature swing adsorption process with a reasonable CO_2 working capacity.^{12b} Regardless, the multicomponent measurements performed here show that at 40°C and an H_2O equilibrium partial pressure of 13 mbar , the amount of CO_2 adsorbed at a partial pressure of 0.16 bar decreased by 60% to $0.9(2)\text{ mmol/g}$, and the amount of N_2 adsorbed at a partial pressure of 0.7 bar was within error of 0 mmol/g (Figure 10a). Under these equilibrium conditions, it thus appears that $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ retains at least some capacity for CO_2 and a high selectivity over N_2 , but H_2O is clearly affecting the CO_2 capture properties in contrast to the previously reported dynamic breakthrough results.

Surprisingly, when repeating this multicomponent measurement on a fresh sample, we found that the amount of CO_2 adsorbed at nearly identical equilibrium partial pressures had dropped to within error of 0 mmol/g (Figure 10a). While the partial pressure of H_2O was 13 mbar in both measurements, the amount of H_2O adsorbed had increased from $3.8(3)$ to $6.4(4)\text{ mmol/g}$. Such significant changes in the amount of CO_2 and H_2O adsorbed at nearly constant partial pressures are indicative of a phase transition, something that was previously suggested to occur based on X-ray powder diffraction experiments at increasing partial pressures of H_2O .^{59a} To investigate this further, a pure-component H_2O isotherm was measured at 40°C and found to have an inflection at an H_2O loading of nearly 6 mmol/g (Figure 10b). The multicomponent results and pure-component H_2O isotherm are thus consistent with a phase change occurring at H_2O loadings above 6 mmol/g and leading to an unknown material with no capacity or selectivity for CO_2 adsorption in the presence of H_2O . Since this phase change would occur at the over 70 mbar of H_2O that is present in flue gas, it seems unlikely that $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ could be used in a post-combustion carbon capture process without significant drying of the flue gas, even if the phase change is fully reversible.

Still, it is interesting that $\text{Zn}(\text{pyz})_2(\text{SiF}_6)$ has a reasonable capacity for CO_2 and a high selectivity over N_2 before the phase change occurs, and it would be useful to determine exactly where CO_2 and H_2O adsorb in the framework under these conditions. Moreover, it would be informative to measure a similar compound with exposed anions that does not exhibit a phase change to determine the amount of CO_2 adsorbed, if any, at higher partial pressures of H_2O . Additionally, the reasons for

the very different CO₂ capacities observed for Zn(pyz)₂(SiF₆) under dynamic breakthrough and equilibrium conditions are not clear and need to be understood. We note, however, that the CO₂ breakthrough capacity appears to have been determined simply by multiplying the CO₂ breakthrough time by the CO₂ flow rate at the inlet of the column, and it is unclear how much H₂O was in the column at the breakthrough time and whether or not any extra-column effects were taken into account.^{59a}

Alkylamines. Owing to their ability to capture high-purity CO₂ in the presence of N₂ and H₂O, aqueous amine solutions have been the most studied carbon capture technology to date.¹⁰ However, amine solutions suffer from several drawbacks that have prevented major reductions in the cost of captured CO₂, despite nearly 40 years of research and optimization.⁵ Most importantly, the concentration of amines in water is limited to 30–40 wt % to minimize corrosion and degradation issues,⁶¹ which in turn limits the CO₂ capacity of the solutions and leads to high regeneration energies, as a significant amount of heat is wasted boiling water rather than desorbing CO₂. Incorporating amines into solid adsorbents represents a promising strategy for increasing CO₂ capacity and reducing regeneration energy while maintaining a high selectivity for CO₂ over other flue gas components.^{11a}

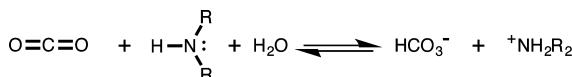
In designing amine-based adsorbents, it is important to consider that isolated amine groups do not have a particularly strong affinity for CO₂. Rather, strong CO₂ binding only occurs when the amine binding CO₂ can transfer a proton to another Lewis base. Typically, this proton transfer occurs to another amine to form an ammonium carbamate, resulting in an overall amine:CO₂ stoichiometry of 2:1 (Scheme 1).⁶² In humid gas

Scheme 1. Under Dry Conditions, Reaction of CO₂ with 2 equiv of a 1° or 2° Alkylamine Amine Typically Forms Ammonium Carbamate



mixtures, H₂O can participate in the reaction of CO₂ with an amine, often leading to the formation of ammonium bicarbonate and an overall amine:CO₂ stoichiometry of 1:1 (Scheme 2).⁶³

Scheme 2. Under Humid Conditions, Reaction of CO₂ with 1 equiv of a 1° or 2° Alkylamine Typically Forms Ammonium Bicarbonate



Amine-Functionalized Mesoporous Silicas. Early efforts to incorporate amines into porous materials focused primarily on mesoporous silicas. With BET surface areas ranging from 500 to 1500 m²/g, a high density of amines can be impregnated inside or grafted directly onto the pore surface of a mesoporous silica.⁶⁴ While there has been some controversy as to the exact nature of adsorbed CO₂ inside these materials, it is now generally accepted that CO₂ reacts to form an ammonium carbamate under dry conditions (0.5 CO₂ per amine) and ammonium bicarbonate (1 CO₂ per amine) under humid conditions, provided that the silica has a high density of 1° or

2° amines.^{62b,65} It is important to note that although these are the thermodynamically favored products under each set of conditions, ammonium carbamate formation occurs at a much faster rate than bicarbonate formation.⁶⁶ As a result, it can take a very long time to reach a full equilibrium capacity of 1 CO₂ per amine in the presence of H₂O, as there is often a mixture of ammonium carbamate and bicarbonate present before equilibrium is reached. This perhaps explains the wide range of CO₂ to amine ratios that have been reported for different amine-appended or -impregnated silicas in the presence of H₂O.^{11a} Additionally, the majority of reports on the equilibrium CO₂ capacity of mesoporous silicas in the presence of H₂O involve flowing CO₂ over a sample that has been pre-equilibrated with H₂O and measuring the increase in weight. To calculate the CO₂ uptake, it is assumed that the amount of H₂O adsorbed is unaffected by CO₂ adsorption. Recent binary adsorption measurements, however, have shown that this assumption often leads to incorrect conclusions about the amount of CO₂ adsorbed in the presence of H₂O.⁶⁷

Many of the amine-functionalized silicas investigated for CO₂ capture have been based on MCM-41 (Mobil composition of matter no. 41), which consists of cylindrical mesopores that are arranged in a hexagonal lattice.⁶⁸ In this work, three amine-functionalized derivatives of MCM-41 were synthesized according to previous reports: 3-aminopropyl grafted MCM-41 (1°-MCM-41), 3-methylaminopropyl grafted MCM-41 (2°-MCM-41), and polyethylenimine impregnated MCM-41 (PEI-MCM-41).^{69,70b} Based on elemental analysis, 4.2 mmol of 1° amine per g silica and 3.7 mmol of 2° amine per g silica were grafted in 1°-MCM-41 and 2°-MCM-41, respectively, which is comparable to the average loading for all reported monoamine-appended silicas of just over 3 mmol/g.^{11a} At 40 °C and 1 bar, both 1°-MCM-41 and 2°-MCM-41 adsorb nearly 0.5 molecules of CO₂ per amine, as expected for ammonium carbamate formation under dry conditions (Figure 11).

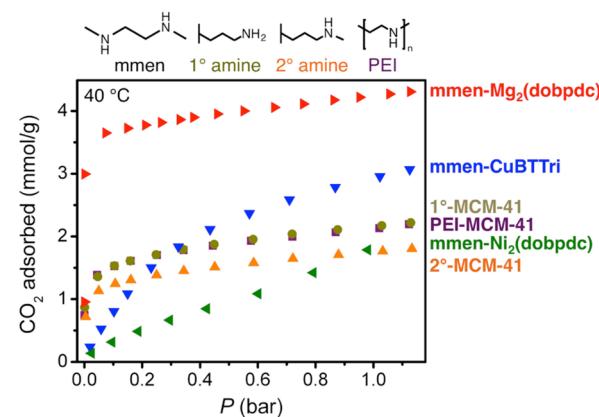


Figure 11. Pure CO₂ adsorption isotherms at 40 °C for metal–organic frameworks and mesoporous silicas that feature alkylamine groups.

With 33% of N by mass and a roughly 1:1:1 mixture 1°, 2°, and 3° amines, branched PEI has a high density of amine groups and has been shown to have improved CO₂ capture performance when it is impregnated inside a solid support rather than neat.⁷⁰ The PEI-MCM-41 sample synthesized in this work contained 32 wt % of PEI (7.4 mmol N per g silica). At 40 °C and 1 bar, PEI-MCM-41 adsorbs 0.28 molecules of CO₂ per amine (2.1 mmol/g), which is consistent with the

amine efficiencies of previously reported amine-impregnated silicas (Figure 11).¹¹

Here, multicomponent experiments were used to measure directly the amount of CO₂ adsorbed from a mixture of CO₂, N₂, and H₂O at 40 °C and a CO₂ partial pressure near 0.15 bar. Note that since primary amines are prone to deactivate by forming urea linkages under dry conditions,⁶⁹ the pure CO₂ and multicomponent isotherms reported here were measured on separate samples. At an equilibrium H₂O partial pressure of 19 mbar (26% RH), the amount of CO₂ adsorbed by 1°-MCM-41 decreased by 25%. This result appears to be in conflict with an earlier report that used a thermogravimetric analyzer coupled to a mass spectrometer to show a 76% increase in CO₂ adsorption for 1°-MCM-41 at 24 mbar of H₂O and 25 °C.⁶⁷ The two 1°-MCM-41 samples have nearly identical amine loadings, but the bare MCM-41 silica used in this work has an average pore size of 2.4 nm, while the previously reported material used a pore-enlarged variant of MCM-41 with an average pore size of nearly 11 nm.⁷¹ The different pore sizes of the resulting amine-grafted materials could be responsible for the different CO₂ capacities observed under humid conditions.

The amount of CO₂ adsorbed by 2°-MCM-41 at 17 mbar of H₂O was within error of the dry CO₂ uptake, suggesting that no bicarbonate was formed. Although the sample was equilibrated for over 24 h, it is likely that bicarbonate formation is exceedingly slow in this secondary amine material and equilibrium was not reached over the course of the multicomponent measurement.⁶⁶ During the multicomponent measurement, the total pressure of the system was still decreasing at a very slow rate even after 24 h of forced equilibration, which suggests that some CO₂ adsorption was still occurring with very slow kinetics. There are several literature reports of constant CO₂ uptake for amine-appended silicas under both dry and humid conditions, but whether or not kinetics are a factor in these experiments is uncertain.^{11a}

In contrast to 1°-MCM-41 and 2°-MCM-41, the amount of CO₂ adsorbed in PEI-MCM-41 increased significantly from 1.5 mmol/g (0.20 CO₂ per N) to 2.5(1) mmol/g (0.34 CO₂ per N) at 17 mbar of H₂O. This 67(7)% increase is slightly higher than the 40% increase observed for 50 wt % PEI-MCM-41 in a dynamic breakthrough experiment at 75 °C.^{70c} Although the observed CO₂ capacity is <1 CO₂ per amine, it is possible that either bicarbonate is still forming but the CO₂ partial pressure is not high enough to reach a full capacity of 1 CO₂ per amine or that not all of the amine sites of the PEI are accessible to CO₂.

Amine-Appended Metal–Organic Frameworks. While initial efforts to functionalize solid adsorbents with amines involved mostly mesoporous silicas, several amine-appended metal–organic frameworks have recently shown promising CO₂ capture properties.⁷² For instance, the amine-appended metal–organic framework H₃[Cu₄Cl₃(BTTri)₈(mmen)₁₂] (mmen-CuBTTri; H₃BTTri = 1,3,5-tri(1H-1,2,3-triazol-4-yl)-benzene) features diamines that are coordinated to the exposed Cu²⁺ cations of its sodalite-type cages (Figure 1), resulting in a nearly 250% increase in the amount of CO₂ adsorbed at 0.15 bar and 25 °C as compared to the bare framework.^{72c} Similar to 1°-MCM-41, mmen-CuBTTri shows a very slight decrease in CO₂ uptake in the presence of N₂ and H₂O, but still adsorbs 0.9(2) mmol/g of CO₂ (Table S3). This demonstrates that appending amines to exposed metal cation sites in metal–organic frameworks is a viable strategy for adsorbing CO₂ under humid conditions.

In contrast to mesoporous silicas, highly crystalline metal–organic frameworks offer the advantage of well-defined and ordered sites for attaching amines, a feature that was recently shown to lead to unprecedented cooperative CO₂ binding and low CO₂ capture regeneration energies in the diamine-appended metal–organic framework mmen-Mg₂(dobpdc).⁷³ In this material, which features an expanded version of Mg₂(dobdc), one end of each diamine is attached to an exposed Mg²⁺ cation, while the other end is exposed on the surface (Figure 1). With all diamines spaced exactly 6.8 Å apart along each hexagonal channel, the density of amine groups in mmen-Mg₂(dobpdc) is 7.3 mmol/mL, exceeding that of a 30 wt % monoethanolamine solution (4.9 mmol/mL).

At 40 °C and pressures below 0.5 mbar, the mechanism for CO₂ adsorption in mmen-Mg₂(dobpdc) is thought to be similar to that of classical amine-appended silicas: two free amine groups react with a CO₂ molecule to form ammonium carbamate (Figure 12). At higher pressures, however, there is

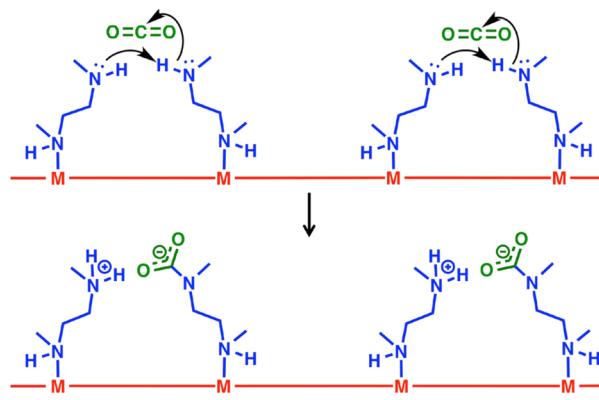


Figure 12. Proposed mechanism for CO₂ adsorption in mmen-Ni₂(dobpdc) and pre-step CO₂ adsorption in mmen-Mg₂(dobpdc) is shown at four neighboring M-mmen sites within an infinite one-dimensional chain of such sites running along the crystallographic *c* axis of the compound. Simultaneous proton transfer and nucleophilic attack of an uncoordinated amine on a CO₂ molecule forms an ammonium carbamate species.

a sharp step in the CO₂ adsorption isotherm of mmen-Mg₂(dobpdc), and both ends of the diamine begin to participate in CO₂ binding. Specifically, a proton is transferred from a metal-bound amine to a neighboring free amine as CO₂ simultaneously inserts into the Mg–N bond, resulting in the formation of one-dimensional chains of ammonium carbamate that run parallel to each chain of Mg²⁺ cations.⁷³ This insertion-based CO₂ adsorption mechanism leads to strong, cooperative CO₂ binding, and at 0.15 bar and 40 °C, one CO₂ molecule is adsorbed per mmen to give a total capacity of 3.73 mmol/g (14.1 wt %).

Since CO₂, but not N₂ or H₂O, induces a phase transition in mmen-Mg₂(dobpdc), changing both the structure and composition of the adsorbent, it is impossible to use pure-component adsorption isotherms to predict CO₂ selectivity and capacity for a mixture of CO₂, N₂, and H₂O. Instead, the direct measurement of multicomponent adsorption is the only way to investigate the effects of H₂O and N₂ on CO₂ binding in mmen-Mg₂(dobpdc) at equilibrium. Of particular interest is to determine whether the insertion-based CO₂ adsorption mechanism is affected by H₂O and if ammonium carbamate is still the only form of adsorbed CO₂ under humid conditions.

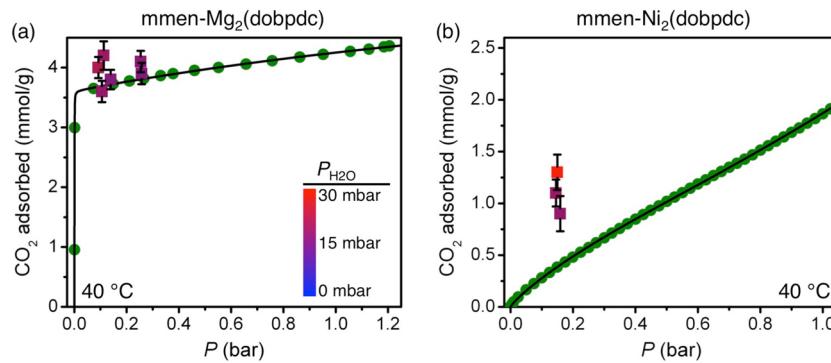


Figure 13. A summary of CO₂, N₂, H₂O multicomponent equilibrium measurements at 40 °C for (a) mmn-Mg₂(dobpdc) and (b) mmn-Ni₂(dobpdc). Green circles represent pure CO₂ adsorption isotherms for each compound, and black lines are the corresponding dual-site Langmuir fits. Square data points represent the amount of CO₂ adsorbed from a mixture of CO₂, N₂, and H₂O, and the color of the square indicates the equilibrium partial pressure of H₂O. The exact values of $P_{\text{H}_2\text{O}}$ can be found in Table S3.

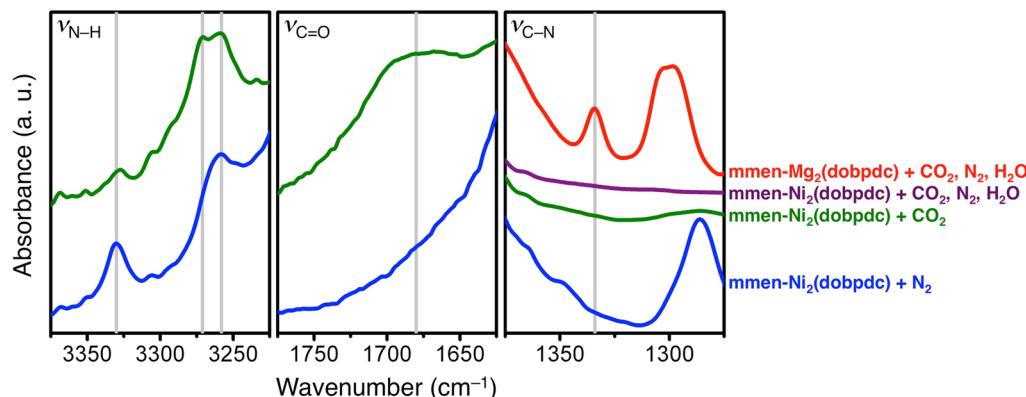


Figure 14. Infrared spectra upon dosing activated mmn-Ni₂(dobpdc) with N₂ (blue), CO₂ (green), and a mixture of CO₂, N₂, and H₂O (purple), and dosing activated mmn-Mg₂(dobpdc) with a mixture of CO₂, N₂, and H₂O (red) at 25 °C. The three different regions show bands corresponding to N–H, C=O, and C–N stretching vibrations, from left to right, respectively.

Significantly, multicomponent measurements with H₂O partial pressures as high as 19 mbar, CO₂ partial pressures between 100 and 300 mbar, and N₂ partial pressures between 500 and 700 mbar, clearly show that the amount of CO₂ adsorbed from a mixture of CO₂, N₂, and H₂O is the same as, or slightly higher than, from pure CO₂. Thus, H₂O and N₂ do not have a significant effect on CO₂ adsorption in mmn-Mg₂(dobpdc) (Figure 13a). To the best of our knowledge, the multicomponent CO₂ uptake of 4.2(2) mmol/g (15.6 wt %) for mmn-Mg₂(dobpdc) represents the highest value ever reported for any metal–organic framework or silica under similar humid conditions. While no N₂ adsorption is observed in mmn-Mg₂(dobpdc) during the multicomponent experiments, between 4.9 and 9.5 mmol/g of H₂O is adsorbed, depending on the exact equilibrium conditions. Since CO₂ and H₂O do not compete for the same binding sites, it should be possible to reduce this H₂O adsorption without affecting the amount of CO₂ adsorbed by, for instance, tuning the alkylamine or bridging organic ligand to increase the hydrophobicity of the pore surface. Note that one of the multicomponent measurements was repeated four further times on the same sample with identical results after regenerating at 100 °C under vacuum for 2 h, demonstrating that CO₂ and H₂O adsorption is fully reversible (Figure 5). Longer cycling studies with mixtures of CO₂, N₂, and H₂O and regeneration using a pure temperature swing are currently in progress.

To confirm that CO₂ insertion into the Mg–N bond is still occurring in the presence of H₂O, infrared spectroscopy measurements were performed after equilibrating a sample of mmn-Mg₂(dobpdc) with a mixture of CO₂, N₂, and H₂O (Figure 14). Previously, a sharp band was observed at 1334 cm⁻¹ in the infrared spectrum of mmn-Mg₂(dobpdc) dosed with pure CO₂. This band was assigned to the C–N stretch of a carbamate and is only present after insertion of CO₂ into the M–N bond generates an O-bound carbamate species with more double-bond character in the C–N bond.⁷³ Significantly, there is also a sharp band observed at 1334 cm⁻¹ for mmn-Mg₂(dobpdc) in the presence of CO₂, N₂, and H₂O, confirming that CO₂ insertion into the M–N bond is still occurring and that H₂O does not change the mechanism for CO₂ adsorption (Figure 14). Although the multicomponent measurements indicate a very slight increase in the amount of CO₂ adsorbed in the presence of H₂O, there is no evidence of any carbonate or bicarbonate species in the infrared spectrum.

In the isostructural nickel analogue of this framework, mmn-Ni₂(dobpdc), the increased strength of the Ni–N bond makes the insertion of CO₂ thermodynamically unfavorable, and the CO₂ adsorption isotherms do not contain a step, resulting in just 0.4 mmol/g (1.7 wt %) of CO₂ adsorbed at 40 °C and 0.15 bar.⁷³ Note that while the pure CO₂ isotherm of mmn-Ni₂(dobpdc) is not nearly as steep as expected for an adsorbent with strong CO₂ binding sites, the isosteric heat of adsorption at low coverage is still –40 to –60 kJ/mol. The isotherm is not

as steep as that of most metal–organic frameworks with CO₂ binding energies in this range, such as Mg₂(dobpd), because the entropy of CO₂ adsorption is much more positive in mmnen-Ni₂(dobpd) than in more classical materials.⁷³ This strong CO₂ binding and large entropy of adsorption can likely be explained by a similar mechanism as for the pre-step adsorption in mmnen-Mg₂(dobpd): a proton is transferred between the free ends of two neighboring diamines and CO₂ is bound via the formation of ammonium carbamate, resulting in one CO₂ bound per every two mmnen (Figure 12). In order for this proton transfer to occur, the diamines likely lose some rotational degrees of freedom as ammonium carbamate pairs are formed, which leads to the large entropy penalty associated with CO₂ binding.

To support the proposed mechanism for dry CO₂ adsorption in mmnen-Ni₂(dobpd), infrared spectroscopy measurements were performed on mmnen-Ni₂(dobpd) in the presence of pure N₂ and pure CO₂ (Figure 14). Under a pure N₂ atmosphere, two distinct N–H vibrations are observed at 3330 and 3258 cm⁻¹ and can be assigned to the free and Ni-bound ends of the diamines, respectively. The metal-bound N–H stretch is identical to that observed for mmnen-Mg₂(dobpd), while the free N–H stretch is red-shifted by 4 cm⁻¹.⁷³ Upon exposure to 1 bar of pure CO₂, the free N–H resonance at 3330 cm⁻¹ disappears, and a new vibration is observed at 3271 cm⁻¹. The disappearance of the free N–H vibration is consistent with the formation of ammonium. If only the free ends of each diamine participate in the reaction with CO₂, then half of all diamines would be expected to have an ammonium on the free end, while the other half of diamines would have a carbamate (Figure 12). Indeed, there are two N–H resonances of roughly equal intensity observed at 3271 and 3258 cm⁻¹ in the presence of CO₂ that can be assigned to the N–H on Ni-bound ends of diamines that have either an ammonium or a carbamate on the free end. A broad feature also grows in at roughly 1680 cm⁻¹ after CO₂ dosing, which is consistent with the C=O vibration of carbamate. Finally, no new bands are observed between 1275 and 1375 cm⁻¹ after CO₂ adsorption, which is consistent with the ammonium carbamate reaction occurring at the free ends of the diamines, with no insertion of CO₂ into the M–Ni bond.

Somewhat unexpectedly, the amount of CO₂ adsorbed in mmnen-Ni₂(dobpd) increases nearly 3-fold to 1.3(2) mmol/g (5.4 wt %) in the presence of 29 mbar of H₂O and 691 mbar of N₂ (Figure 13b). This substantial increase in CO₂ adsorption is greater than typically observed for amine-appended silicas and suggests that H₂O has a strong effect on the CO₂ binding mechanism. Despite the large increase in CO₂ uptake, only 0.37(7) mmol of CO₂ is adsorbed per mmol of free amine under the multicomponent conditions.

To gain further insight into these multicomponent results, infrared spectroscopy measurements were also performed for mmnen-Ni₂(dobpd) under an atmosphere of N₂, CO₂, and H₂O (Figure 14). Unfortunately, a very broad and high intensity band above 3000 cm⁻¹, resulting from the large amount of H₂O in the gas-phase, overwhelms any N–H resonances (Figures S18, S19). Still, no new bands are observed between 1275 and 1375 cm⁻¹, demonstrating that CO₂ insertion into the M–Ni bond does not occur in mmnen-Ni₂(dobpd) even in the presence of H₂O. Although CO₂ insertion is ruled out, the infrared spectrum of mmnen-Ni₂(dobpd) does not provide any conclusive evidence that can explain the increased CO₂ uptake in the presence of H₂O. It is possible that bicarbonate is formed, but its infrared bands

are masked by H₂O or the organic bridging ligand. Alternatively, H₂O may facilitate the formation of more ammonium carbamate at lower CO₂ partial pressures by, for instance, breaking up hydrogen-bonding between neighboring diamines to expose more CO₂ binding sites than are present under dry conditions.^{68g}

CONCLUSIONS

The multicomponent results reported in this work for adsorption of CO₂, N₂, and H₂O in 15 different materials, including metal–organic frameworks, zeolites, mesoporous silicas, and an activated carbon, are summarized in Figure 15.

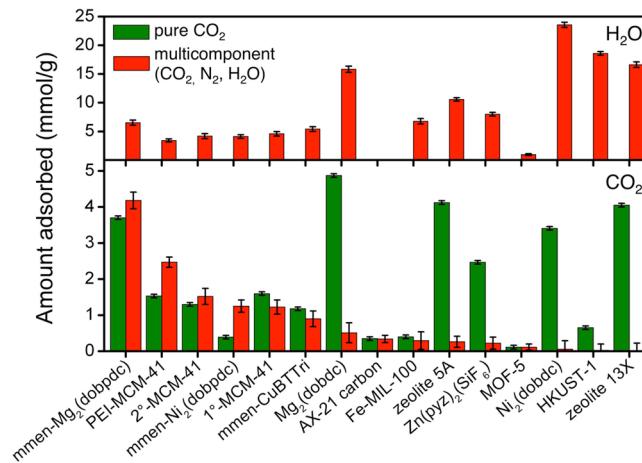


Figure 15. A summary of the multicomponent adsorption measurements performed in this work for mixtures of CO₂, N₂, and H₂O at 40 °C and equilibrium conditions representative of a coal-fired power plant flue gas. The green bars represent the amount of CO₂ adsorbed in a single-component isotherm at the same CO₂ partial pressure as the multicomponent experiment. The red bars in the bottom pane represent the amount of CO₂ adsorbed in the multicomponent experiment. The red bars in the upper pane represent the amount of H₂O adsorbed in the multicomponent experiment. For the multicomponent experiments, all partial pressures of N₂ are between 679 and 698 mbar, of CO₂ are between 113 and 178 mbar, and of H₂O are between 10 and 29 mbar. Total pressures are between 821 and 890 mbar. See Table S3 for exact equilibrium partial pressures and amounts adsorbed. Error bars are shown at a 95% confidence interval.

Here, a multicomponent data point is plotted for each material at the equilibrium conditions most representative of the composition of a coal-fired power plant flue gas. In the bottom pane of the bar graph, the amount of CO₂ adsorbed from the multicomponent mixture of CO₂, N₂, and H₂O (red) is compared to the amount of CO₂ adsorbed at the same partial pressure in the absence of N₂ and H₂O (green). In the top pane, the amount of H₂O adsorbed in the multicomponent experiment is shown. As has been discussed in detail, all of the adsorbents with exposed metal cations or anions take up a significant amount of H₂O and negligible amount of CO₂ under these simulated flue gas equilibrium conditions, while MOF-5 and the AX-21 activated carbon have mostly nonpolar surfaces that lead not only to very little H₂O adsorption but also to very little CO₂ uptake at these low pressures. Adsorbents functionalized with alkylamines, however, maintain a significant CO₂ capacity at the multicomponent equilibrium conditions, with mmnen-Mg₂(dobpd) adsorbing a record amount of CO₂ in the presence of H₂O.

In addition to maximizing CO₂ adsorption, minimizing H₂O adsorption is critical to achieving low regeneration energies in any CO₂ capture process that involves a temperature swing since some of the heat supplied to desorb CO₂ will also go toward desorbing H₂O. The direct measurement of equilibrium H₂O adsorption in the presence of N₂ and CO₂ is thus important for identifying adsorbents with the best CO₂ capture performance. This is particularly true for adsorbents that change upon binding CO₂, where H₂O adsorption may be very different before and after CO₂ adsorption. It is worth noting that measuring the amount of H₂O adsorbed in a breakthrough experiment with CO₂ is extremely challenging, if not impossible, when the column is pre-equilibrated with H₂O, as is often necessary when running small-scale breakthrough experiments.

Although the multicomponent results presented in this work targeted equilibrium conditions representative of adsorption from a post-combustion flue gas, evaluating multicomponent equilibria at desorption conditions is also important. Since a pure temperature swing or vacuum-assisted temperature swing process will likely be most effective for CO₂ capture,^{8,12c} evaluating the amount of CO₂ and H₂O adsorbed from mixtures as a function of regeneration temperature and pressure is necessary to determine CO₂ and H₂O working capacities and to calculate regeneration energies. Recently, it was shown that the cooperative CO₂ binding in mmen-Mg₂(dobpdc) allows a CO₂ working capacity of nearly 14 wt % (3.7 mmol/g) to be achieved with an unprecedented temperature swing of just 50 °C.⁷³ The effects of H₂O on this working capacity are currently being investigated under both dynamic and equilibrium conditions. Because of their structural and chemical tunability, metal–organic frameworks functionalized with alkylamines are a particularly promising class of solid adsorbents for achieving high CO₂ working capacities, minimal H₂O adsorption, and low regeneration energies at post-combustion CO₂ capture conditions.

In addition to CO₂, N₂, and H₂O, multicomponent measurements and long-term cycling studies that include other flue gas components, such as O₂, NO_x, and SO_x, will be valuable in assessing adsorbents for CO₂ capture applications. Measuring multicomponent equilibrium kinetics and heats of adsorption, which are particularly challenging experiments, is also important but rarely reported in the literature for gas mixtures.^{17b} While no real CO₂ capture process will operate under true equilibrium conditions, equilibrium data are essential for comparing different materials and for simulating the dynamic processes of a large-scale separation.

■ ASSOCIATED CONTENT

Supporting Information

Experimental details, surface area measurements, additional adsorption isotherms, descriptions of isotherm fitting, multicomponent calculations, multicomponent error analysis, and complete multicomponent data set. This material is available free of charge via the Internet at <http://pubs.acs.org>.

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Notes

The authors declare no competing financial interest.

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