# Effect of Temperature on the Sodium 1-Hexyl Sulfate-Water System

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Electrical conductivity measurements for aqueous solutions of sodium 1-hexyl sulfate (SHS) have been carried out from (293.15 to 313.15) K. From the molar conductivity at infinite dilution values the transport numbers of SHS anions have been obtained for each temperature. Densities of the binary system water sodium 1-hexyl sulfate were measured at 298.15 K and 308.15 K. Excess volumes have been evaluated at concentrations above and below the critical micellar concentration.

#### Introduction

The self-association of sodium n-hexyl sulfate (SHS) in aqueous solution has been investigated as a function of the temperature. Several authors have reported systematic studies on the micellar behavior of the sodium 1-alkyl sulfate series with 8, 10, 12, 14, and 16 carbon atoms in the alkyl chain (Van Os, 1993). Preliminary evidence suggesting the possibility of self-association of this surfactant was from the apparent solubilization of the water-insoluble dye Sudan IV by concentrated aqueous solutions of SHS. A value of 0.517 mol  $L^{-1}$  for the critical micelle concentration (cmc) of SHS has been reported (Suarez, 1999).

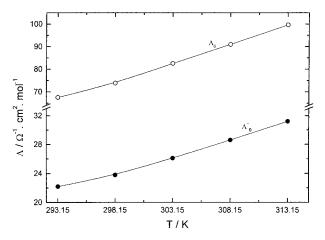
It has been generally recognized that studies of thermodynamic and transport properties of surfactants are important for understanding their behavior in solutions (Kresheck, 1975). In this article we report results on electrical conductivity, the apparent and partial molal volumes, and excess volumes of sodium 1-hexyl sulfate in aqueous solution at various temperatures.

## **Materials and Methods**

Sodium 1-hexyl sulfate (SHS) (purity  $\geq 99\%$ ) from Lancaster (No. 6245) was used without further purification. All concentrations were determined by mass using distilled and degassed water.

The conductance was measured by using a conductivity meter (Kyoto Electronic type C-117), the cell of which was calibrated with KCl solutions in the appropriate concentration range. SHS solutions of known concentration were progressively added to water using an automatic pump (Dosimat 665 Metrohm). The measuring cell was immersed in a thermostat bath, maintaining the temperature control within  $\pm 0.01$  K. The automatic pump and the temperature control were achieved using a Hewlett-Packard Vectra computer.

The densities of all solutions were measured with an Anton Paar DMA 60/602 density meter with an accuracy of  $\pm 1.5\times 10^{-6}$  g cm $^{-3}$ . The temperature was kept constant within  $\pm 0.01$  K by a proportional temperature controller HETO and checked with a digital precision thermometer



**Figure 1.** Variation of the molar conductivity at infinite dilution of sodium 1-hexyl sulfate,  $\Lambda_0$ , and 1-hexyl sulfate anion,  $\Lambda_0^-$ , with the temperature.

Anton Paar DT 100-30. The densimeter was calibrated at each temperature with air at known pressure and water, where the density of air-saturated water was assumed to be 0.997 043 g cm $^{-3}$  and 0.994 030 g cm $^{-3}$  at 298.15 K and 308.15 K, respectively.

### **Results and Discussion**

Table 1 shows the specific conductivity of SHS as a function of concentration. The molar conductivity of SHS at infinite dilution,  $\Lambda_0$ , is plotted vs temperature in Figure 1. By subtracting from the values of  $\Lambda_0$  the corresponding conventional value for the sodium cation,  $\Lambda_0^{\mathrm{Na}^+}=45.4$ , 50.1,56.5,62.4, and  $68.5~\Omega^{-1}~\mathrm{cm}^2~\mathrm{mol}^{-1}$  at  $293.15~\mathrm{K},298.15~\mathrm{K},303.15~\mathrm{K},308.15~\mathrm{K}$ , and  $313.15~\mathrm{K}$ , respectively, the values of  $\Lambda_0^-$  for surfactant anions were obtained. As expected, the values slightly increase with the increase in temperature. From  $\Lambda_0$  and  $\Lambda_0^-$  values the transport numbers of sodium 1-hexyl sulfate anions,  $t_0^-=\Lambda_0^-/\Lambda_0$ , can be calculated. The obtained results are summarized in Table 2. These values compare with the literature (Vanýsek, 1996): 0.367, 0.342, and 0.324 for the anions octyl sulfate, decyl sulfate, and dodecyl sulfate, respectively.

From the density data, apparent molal volumes,  $V_{\phi}$ , of the surfactant in water were calculated using the equation

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Table 1. Specific Conductivity, K, for the System 1-Hexyl **Sulfate Water at Different Temperatures** 

Sulfate Water at Different Temperatures						
c/mol	κ/mS	c/mol	κ/mS	c/mol	κ/mS	
$dm^{-3}$	$cm^{-1}$	dm <sup>-3</sup>	$cm^{-1}$	$dm^{-3}$	$cm^{-1}$	
uiii	CIII	um	CIII	uiii	CIII	
		T = 29	93.15			
0.1066	6.0	0.2908	14.1	0.5645	23.4	
0.1200	6.6	0.3199	15.2	0.5998	24.5	
0.1371	7.5	0.3309	15.7	0.6398	25.7	
0.1600	8.5	0.3428	16.1	0.6855	27.0	
0.1745	9.2	0.3555	16.6	0.7383	28.6	
0.1919	10.0	0.3691	17.1	0.7998	30.2	
0.2133	10.6	0.4799	20.8	0.8725	32.2	
0.2399	12.0	0.5051	21.6	0.9597	34.5	
0.2666	13.1	0.5332	22.5	1.0664	37.1	
		T = 298	8.15 K			
0.0999	5.7	0.3107	16.5	0.4753	22.9	
0.1010	6.3	0.3232	17.1	0.5050	24.0	
0.1346	8.2	0.3366	17.1	0.5386	25.1	
0.1616	10.1	0.3513	18.2	0.5771	26.5	
0.2020	11.5	0.3672	18.8	0.6215	27.9	
0.2308	12.9	0.3847	19.5	0.6733	29.5	
0.2525	13.9	0.4040	20.3	0.7245	31.3	
0.2693	14.7	0.4252	21.1	0.8079	33.4	
0.2885	15.5	0.4489	22.0	0.8977	35.9	
		T = 303	2 15 K			
0.0070	0.1		10.4	0.2006	99.0	
0.0273	2.1	0.1577		0.3906	22.0	
0.0328	2.5	0.1745	11.3	0.4100	22.9	
0.0410	3.1	0.1953	12.5	0.4317	23.8	
0.0513	3.8	0.2158	13.5	0.4557	24.8	
0.0586	4.3	0.2412	14.9	0.4825	25.9	
0.0683	4.9	0.2563	15.6	0.5126	27.0	
0.0745	5.3	0.2734	16.4	0.5468	28.4	
0.0820	5.8	0.2929	17.5	0.5858	29.8	
0.0911	6.4	0.3155	18.6	0.6309	31.4	
0.0965	6.7	0.3281	19.2	0.6835	33.2	
0.1093	7.5	0.3417	19.9	0.7456	35.3	
0.1262	8.5	0.3566	20.6	0.8202	37.7	
0.1414	9.4	0.3728	21.2	0.9113	40.7	
0.1111	0.1			0.0110	10.7	
		T = 308				
0.0140	1.2	0.1747	12.5	0.3882	24.2	
0.0349	2.7	0.1888	13.3	0.4110	25.2	
0.0582	4.7	0.2117	14.8	0.4367	26.4	
0.0699	5.5	0.2329	15.9	0.4358	27.8	
0.0822	6.4	0.2588	17.4	0.4991	29.2	
0.0932	7.2	0.2795	18.5	0.5375	30.9	
0.1075	8.2	0.3038	19.9	0.5823	32.7	
0.1270	9.5	0.3327	21.5	0.6352	34.8	
0.1397	10.3	0.3494	22.3	0.6987	37.7	
0.1553	11.3	0.3678	23.1	0.7764	40.2	
0.1333	11.3	0.3076	23.1	0.7704	40.2	
T = 313.15  K						
0.0886	7.5	0.2214	16.6	0.4429	29.5	
0.0996	8.4	0.2416	17.8	0.4689	30.8	
0.1063	8.9	0.2657	19.4	0.4982	32.1	
0.1134	9.5	0.2847	20.5	0.5314	33.7	
0.1226	10.1	0.3066	21.9	0.5694	35.6	
0.1329	10.1	0.3322	23.6	0.6132	37.4	
0.1329	11.7	0.3623	25.2	0.6643	39.6	
0.1594	12.7	0.3796	16.1	0.7247	42.0	
0.1733	13.6	0.3986	27.0	0.7972	45.2	
0.1993	15.2	0.4196	28.3	0.8858	48.4	

Table 2. Transport Numbers of 1-Hexyl Sulfate Anion,  $t_0^-$ , and Transport Numbers of Sodium Cation,  $t_0^+$ 

_			-			
	T/K	$t_0^-$	$t_0^+$	<i>T</i> /K	$t_0^-$	$t_0^+$
	293.15 K	0.328	0.672	308.15 K	0.314	0.686
	298.15 K	0.321	0.679	313.15 K	0.313	0.687
	303.15 K	0.316	0.684			

(Harned and Owen, 1958):

$$V_{\phi} = \frac{M}{\rho} - \frac{10^{3}(\rho - \rho_{0})}{m\rho\rho_{0}}$$
 (1)

where m is the molality of the solution, M is the molecular

Table 3. Densities,  $\rho$ , Apparent Molal Volumes,  $V_{\phi}$ , Excess Volumes,  $V_{\phi}^{\rm EX}$ , and Partial Molal Volumes,  $\bar{V}_2$ , for the System 1-Hexyl Sulfate Water at two Different **Temperatures** 

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				EV	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\rho$ /	$V_{\phi}$ /	$V_{\phi}^{\rm E.X}$	$V_2$ /
$\begin{array}{c} 0.2556 \\ 0.2904 \\ 0.1013 92 \\ 0.2904 \\ 1.013 92 \\ 143.92 \\ -0.30 \\ 144.7 \\ 0.3380 \\ 1.016 53 \\ 144.07 \\ -0.24 \\ 145.0 \\ 0.4095 \\ 1.020 34 \\ 144.24 \\ -0.18 \\ 145.2 \\ 0.4437 \\ 1.022 13 \\ 144.33 \\ -0.14 \\ 145.4 \\ 0.4865 \\ 1.024 34 \\ 144.43 \\ -0.10 \\ 146.4 \\ 0.5607 \\ 1.027 99 \\ 144.81 \\ 0.19 \\ 0.19 \\ 148.6 \\ 0.6663 \\ 1.032 81 \\ 145.61 \\ 0.86 \\ 150.3 \\ 0.7197 \\ 1.035 15 \\ 145.99 \\ 1.18 \\ 150.7 \\ 0.8159 \\ 1.039 29 \\ 146.53 \\ 1.62 \\ 150.6 \\ 0.8843 \\ 1.042 17 \\ 146.84 \\ 1.87 \\ 151.0 \\ 0.9436 \\ 1.044 58 \\ 147.13 \\ 2.09 \\ 151.5 \\ 1.0476 \\ 1.048 71 \\ 147.57 \\ 2.43 \\ 151.3 \\ 1.1849 \\ 1.054 05 \\ 105 405 \\ 147.96 \\ 2.71 \\ 152.1 \\ 1.2578 \\ 1.060 87 \\ 148.62 \\ 3.21 \\ 152.3 \\ 1.4589 \\ 1.063 80 \\ 148.83 \\ 3.35 \\ 152.4 \\ 1.6301 \\ 1.069 60 \\ 149.19 \\ 3.58 \\ 152.9 \\ 1.8302 \\ 1.076 00 \\ 1.081 20 \\ 149.85 \\ 3.99 \\ 152.8 \\ 2.1868 \\ 1.086 68 \\ 150.10 \\ 4.11 \\ 152.9 \\ 2.4316 \\ 1.093 46 \\ 150.40 \\ 4.26 \\ 153.0 \\ 2.6564 \\ 1.099 40 \\ 150.60 \\ 4.33 \\ 152.7 \\ 2.0000 \\ 1.081 20 \\ 149.85 \\ 3.99 \\ 152.8 \\ 2.1868 \\ 1.086 68 \\ 150.10 \\ 4.11 \\ 152.9 \\ 2.4316 \\ 1.093 46 \\ 150.88 \\ 4.46 \\ 153.2 \\ 3.2556 \\ 1.113 75 \\ 151.08 \\ 4.48 \\ 152.9 \\ 3.6013 \\ 1.121 40 \\ 151.22 \\ 0.48 \\ 152.9 \\ 147.5 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.19 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5729 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5729 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5925 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 10.24 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 10.24 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5729 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 152.5 \\ 0.7792 \\ 1.033 49 \\ 148.31 \\ 1.21 \\ 152.9 \\ 0.8946 \\ 1.038 15 \\ 144.92 \\ 1.70 \\ 153.0 \\ 1.52.5 \\ 153.7 \\ 1.2330 \\ 1.056 66 \\ 151.10 \\ 3.18 \\ 153.7 \\ 1.2330 \\ 1.056 66 \\ 151.10 \\ 3.18 \\ 153.7 \\ 1.4422 \\ 1.058 23 \\ 150.66 \\ 151.10 \\ 3.18 \\ 153.7 \\ 1.244 1 \\ 153.7 \\ 1.2577 \\ 1.083 21 \\ 151.85 \\ 3.53 \\ 154.4 \\ 153.7 \\ 154.4 \\ 153.7 \\ 1.54.4 \\ 153.7 \\ 1.54.4 \\ 1$	$ m kg^{-1}$	$(g cm^{-3})$	$(cm^3 mol^{-1})$	$(cm^3 mol^{-1})$	$(\mathrm{cm}^3\mathrm{mol}^{-1})$
$\begin{array}{c} 0.2556 \\ 0.2904 \\ 0.1013 92 \\ 0.2904 \\ 1.013 92 \\ 143.92 \\ -0.30 \\ 144.7 \\ 0.3380 \\ 1.016 53 \\ 144.07 \\ -0.24 \\ 145.0 \\ 0.4095 \\ 1.020 34 \\ 144.24 \\ -0.18 \\ 145.2 \\ 0.4437 \\ 1.022 13 \\ 144.33 \\ -0.14 \\ 145.4 \\ 0.4865 \\ 1.024 34 \\ 144.43 \\ -0.10 \\ 146.4 \\ 0.5607 \\ 1.027 99 \\ 144.81 \\ 0.19 \\ 0.19 \\ 148.6 \\ 0.6663 \\ 1.032 81 \\ 145.61 \\ 0.86 \\ 150.3 \\ 0.7197 \\ 1.035 15 \\ 145.99 \\ 1.18 \\ 150.7 \\ 0.8159 \\ 1.039 29 \\ 146.53 \\ 1.62 \\ 150.6 \\ 0.8843 \\ 1.042 17 \\ 146.84 \\ 1.87 \\ 151.0 \\ 0.9436 \\ 1.044 58 \\ 147.13 \\ 2.09 \\ 151.5 \\ 1.0476 \\ 1.048 71 \\ 147.57 \\ 2.43 \\ 151.3 \\ 1.1849 \\ 1.054 05 \\ 105 405 \\ 147.96 \\ 2.71 \\ 152.1 \\ 1.2578 \\ 1.060 87 \\ 148.62 \\ 3.21 \\ 152.3 \\ 1.4589 \\ 1.063 80 \\ 148.83 \\ 3.35 \\ 152.4 \\ 1.6301 \\ 1.069 60 \\ 149.19 \\ 3.58 \\ 152.9 \\ 1.8302 \\ 1.076 00 \\ 1.081 20 \\ 149.85 \\ 3.99 \\ 152.8 \\ 2.1868 \\ 1.086 68 \\ 150.10 \\ 4.11 \\ 152.9 \\ 2.4316 \\ 1.093 46 \\ 150.40 \\ 4.26 \\ 153.0 \\ 2.6564 \\ 1.099 40 \\ 150.60 \\ 4.33 \\ 152.7 \\ 2.0000 \\ 1.081 20 \\ 149.85 \\ 3.99 \\ 152.8 \\ 2.1868 \\ 1.086 68 \\ 150.10 \\ 4.11 \\ 152.9 \\ 2.4316 \\ 1.093 46 \\ 150.88 \\ 4.46 \\ 153.2 \\ 3.2556 \\ 1.113 75 \\ 151.08 \\ 4.48 \\ 152.9 \\ 3.6013 \\ 1.121 40 \\ 151.22 \\ 0.48 \\ 152.9 \\ 147.5 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.19 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5729 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5729 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5925 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 10.24 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 10.24 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 147.7 \\ 0.5479 \\ 1.023 50 \\ 146.67 \\ -0.15 \\ 149.0 \\ 0.5729 \\ 1.024 66 \\ 146.82 \\ -0.03 \\ 150.9 \\ 152.5 \\ 0.7792 \\ 1.033 49 \\ 148.31 \\ 1.21 \\ 152.9 \\ 0.8946 \\ 1.038 15 \\ 144.92 \\ 1.70 \\ 153.0 \\ 1.52.5 \\ 153.7 \\ 1.2330 \\ 1.056 66 \\ 151.10 \\ 3.18 \\ 153.7 \\ 1.2330 \\ 1.056 66 \\ 151.10 \\ 3.18 \\ 153.7 \\ 1.4422 \\ 1.058 23 \\ 150.66 \\ 151.10 \\ 3.18 \\ 153.7 \\ 1.244 1 \\ 153.7 \\ 1.2577 \\ 1.083 21 \\ 151.85 \\ 3.53 \\ 154.4 \\ 153.7 \\ 154.4 \\ 153.7 \\ 1.54.4 \\ 153.7 \\ 1.54.4 \\ 1$			T = 298.1	5 K	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.2556	1 011 99			144 3
0.3380         1.016 53         144.07         -0.24         145.0           0.4095         1.020 34         144.24         -0.18         145.2           0.4437         1.022 13         144.33         -0.14         145.4           0.4865         1.024 34         144.43         -0.10         146.4           0.5607         1.027 99         144.81         0.19         148.6           0.6663         1.032 81         145.61         0.86         150.3           0.7197         1.035 15         145.99         1.18         150.7           0.8159         1.039 29         146.53         1.62         150.6           0.8843         1.042 17         146.84         1.87         151.0           0.9436         1.044 58         147.13         2.09         151.5           1.0476         1.048 71         147.96         2.71         152.1           1.2578         1.056 68         148.26         2.95         152.8           1.3751         1.060 87         148.62         3.21         152.3           1.4589         1.063 80         148.83         3.35         152.4           1.6301         1.069 60         149.19         3.58					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
T = 308.15  K $0.1305  1.002  61  145.68  -0.40  146.2$ $0.2441  1.007  94  145.93  -0.41  146.6$ $0.3197  1.010  73  146.17  -0.31  146.9$ $0.3954  1.016  55  146.31  -0.29  147.2$ $0.4481  1.018  56  146.44  -0.24  147.5$ $0.5065  1.021  47  146.57  -0.19  147.7$ $0.5479  1.023  50  146.67  -0.15  149.0$ $0.5729  1.024  66  146.82  -0.03  150.9$ $0.6031  1.026  00  147.06  0.17  151.9$ $0.6596  1.028  47  147.49  0.53  152.5$ $0.7792  1.033  49  148.31  1.21  152.9$ $0.8946  1.038  15  148.92  1.70  153.0$ $1.0445  1.044  13  149.50  2.13  153.5$ $1.1370  1.047  62  149.87  2.41  153.7$ $1.2330  1.051  08  150.13  2.58  153.5$ $1.4422  1.058  23  150.67  2.95  153.7$ $1.6932  1.066  66  151.10  3.18  153.7$ $1.9818  1.075  38  151.50  3.37  154.1$ $2.2577  1.083  21  151.85  3.53  154.4$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.0015	1.121 40			102.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
0.6031     1.026 00     147.06     0.17     151.9       0.6596     1.028 47     147.49     0.53     152.5       0.7792     1.033 49     148.31     1.21     152.9       0.8946     1.038 15     148.92     1.70     153.0       1.0445     1.044 13     149.50     2.13     153.5       1.1370     1.047 62     149.87     2.41     153.7       1.2330     1.051 08     150.13     2.58     153.5       1.4422     1.058 23     150.67     2.95     153.7       1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
0.7792     1.033     49     148.31     1.21     152.9       0.8946     1.038     15     148.92     1.70     153.0       1.0445     1.044     13     149.50     2.13     153.5       1.1370     1.047     62     149.87     2.41     153.7       1.2330     1.051     08     150.13     2.58     153.5       1.4422     1.058     23     150.67     2.95     153.7       1.6932     1.066     66     151.10     3.18     153.7       1.9818     1.075     38     151.50     3.37     154.1       2.2577     1.083     21     151.85     3.53     154.4					
0.8946     1.038 15     148.92     1.70     153.0       1.0445     1.044 13     149.50     2.13     153.5       1.1370     1.047 62     149.87     2.41     153.7       1.2330     1.051 08     150.13     2.58     153.5       1.4422     1.058 23     150.67     2.95     153.7       1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
1.0445     1.044 13     149.50     2.13     153.5       1.1370     1.047 62     149.87     2.41     153.7       1.2330     1.051 08     150.13     2.58     153.5       1.4422     1.058 23     150.67     2.95     153.7       1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
1.1370     1.047 62     149.87     2.41     153.7       1.2330     1.051 08     150.13     2.58     153.5       1.4422     1.058 23     150.67     2.95     153.7       1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
1.2330     1.051 08     150.13     2.58     153.5       1.4422     1.058 23     150.67     2.95     153.7       1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
1.4422     1.058 23     150.67     2.95     153.7       1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
1.6932     1.066 66     151.10     3.18     153.7       1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
1.9818     1.075 38     151.50     3.37     154.1       2.2577     1.083 21     151.85     3.53     154.4					
2.2577 1.083 21 151.85 3.53 154.4					
2.5324 1.090 52 152.12 3.63 154.4					
	2.5324	1.090 52	152.12	3.63	154.4

weight of the solute (204.22 g mol<sup>-1</sup>), and  $\rho$  and  $\rho_0$  represent the densities for the solution and solvent (water), respectively. The apparent molal volumes of SHS in water at 298.15 K and 308.15 K together with the experimental values of density are summarized in Table 3.

The partial molal volumes,  $\bar{V}_2$ , of the surfactant have been computed from  $V_{\phi}$  by the equation

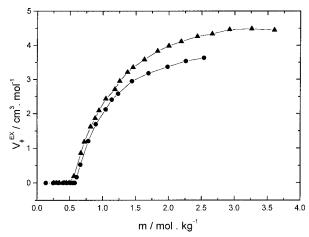
$$\bar{V}_2 = V_\phi + m \left( \frac{\partial V_\phi}{\partial m} \right)_{T,P} \tag{2}$$

The values of  $\bar{V}_2$  so obtained are tabulated at various molalities, m, and at 298.15 K and 308.15 K, in Table 3. The concentration and temperature dependence of  $\bar{V}_2$  is similar to that of other surfactants (Desnoyers et al., 1979).

The excess volumes,  $V_{\phi}^{\rm EX}$ , calculated by the expression

$$V_{\phi}^{\rm EX} = V_{\phi} - A_{\nu} m^{1/2} - V_{\phi}^{0} \tag{3}$$

where  $V_\phi^0$  is the standard (infinite dilution) apparent



**Figure 2.** Variation of the excess volume of SHS with molality:  $(\bullet)$  298.15 K;  $(\blacktriangle)$  308.15 K.

molal volume and  $A_{\nu}$  (1.865 cm³ kg¹¹² mol⁻³¹² for 1:1 electrolyte at 298.15 K) is the Debye−Hückel limiting law coefficient, are plotted in Figure 2 for each temperature (Musbally et al., 1974; Desnoyers et al., 1987). Table 3 includes too the  $V_{\phi}^{\rm EX}$  values obtained by eq 3. The concentration dependence of  $V_{\phi}^{\rm EX}$  is similar to that of other surfactants (De Lisi et al., 1979; Desnoyers et al., 1979). The increase of  $V_{\phi}^{\rm EX}$  with temperature is typical of hydrophobic solutes in water (De Lisi et al., 1980).

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